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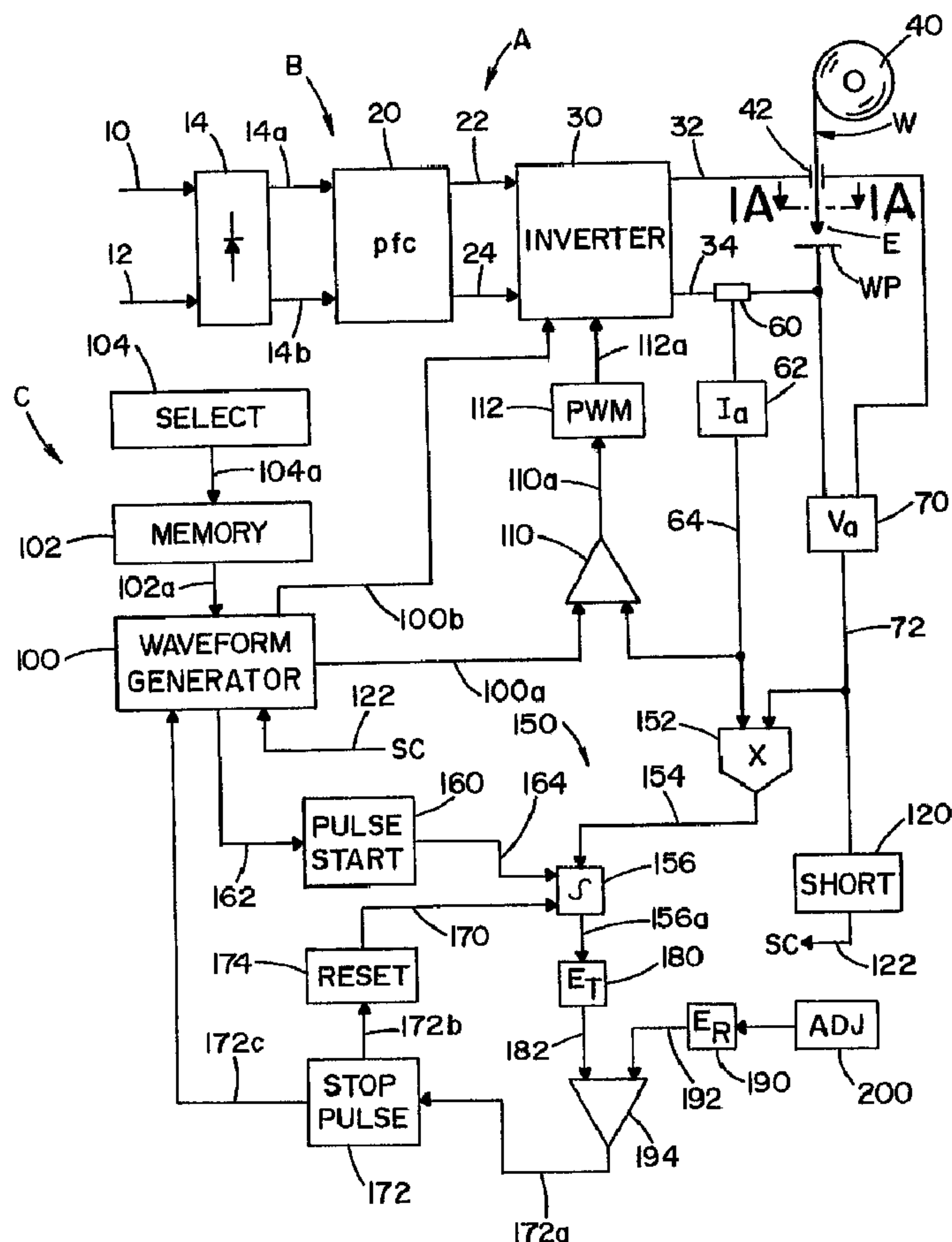
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(54) Titre : DISPOSITIF DE SOUDAGE SYNERGIQUE

(54) Title: SYNERGISTIC WELDING SYSTEM



(57) Abrégé/Abstract:

A welding system is disclosed for performing a short arc welding process between an advancing wire electrode and a workpiece. The system comprises a power source with a controller for creating a current pulse introducing energy into the electrode to melt the

(57) **Abrégé(suite)/Abstract(continued):**

end of the electrode and a low current quiescent metal transfer section following the end of the melting pulse during which the melted electrode short circuits against the workpiece; a timer to measure the actual time between the end of the pulse and the short circuit; a device for setting a desired time from the pulse to the short circuit; a circuit to create a corrective signal based upon the difference between the actual time and the desired time; and, a circuit responsive to the corrective signal to control a given parameter of the current pulse. Also disclosed is a strategy for arc welding utilizing a cored electrode that produces welds with low levels of contaminants and which are strong, tough, and durable. The arc welding process generally utilizes an AC waveform. The cored electrode can be a self-shielded flux cored electrode (FCAW-S). Various electrode compositions are described that are particularly beneficial when used in conjunction with an AC waveform.

Abstract

A welding system is disclosed for performing a short arc welding process between an advancing wire electrode and a workpiece. The system comprises a power source with a controller for creating a current pulse introducing energy into the electrode to melt the end of the electrode and a low current quiescent metal transfer section following the end of the melting pulse during which the melted electrode short circuits against the workpiece; a timer to measure the actual time between the end of the pulse and the short circuit; a device for setting a desired time from the pulse to the short circuit; a circuit to create a corrective signal based upon the difference between the actual time and the desired time; and, a circuit responsive to the corrective signal to control a given parameter of the current pulse. Also disclosed is a strategy for arc welding utilizing a cored electrode that produces welds with low levels of contaminants and which are strong, tough, and durable. The arc welding process generally utilizes an AC waveform. The cored electrode can be a self-shielded flux cored electrode (FCAW-S). Various electrode compositions are described that are particularly beneficial when used in conjunction with an AC waveform.

SYNERGISTIC WELDING SYSTEM

The present invention relates to the art of electric arc welding and more particularly to an improved short arc welding system, methods of welding with self-shielded flux cored arc welding (FCAW-S) electrodes, and the composition of the
5 electrodes.

This invention involves a novel short arc welding process employing a novel cored electrode. There is a synergistic relationship when combining the novel
10 welding process and the novel flux cored electrode. As an attribute of the overall invention, there are independent advantages of the novel process combined with the flux cored electrode.

(Short Arc Welding)

Short-circuit arc welding systems, techniques, and associated concepts, as
15 well as pipe welding methods and apparatuses are generally set forth in the following United States patents.

Parks 4,717,807; Parks 4,954,691; Parker 5,676,857; Stava 5,742,029; Stava 5,961,863; Parker 5,981,906; Nicholson 6,093,906; Stava 6,160,241; Stava 6,172,333; Nicholson 6,204,478; Stava
20 6,215,100; Houston 6,472,634; and Stava 6,501,049.

(Power Source)

The electric arc welding field uses a variety of welding processes between the end of a consumable advancing electrode and a workpiece, which workpiece may

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include two or more components to be welded together. This invention relates to the short arc process wherein the advancing electrode is melted by the heat of the arc during a current pulse and then, after the molten metal forms into a ball by surface tension action, the molten metal ball is transferred to the workpiece by a short circuit
5 action. The short circuit occurs when the advancing wire moves the ball into contact with the molten metal puddle on the workpiece, which short is sensed by a plunge in the welding voltage. Thereafter, the short circuit is broken and the short arc welding process is repeated. The invention is an improvement in short arc welding and is preferably performed by using a power source wherein the profile of the welding
10 waveform is controlled by a waveform generator operating a pulse width modulator of a high switching speed inverter, as disclosed in several patents by assignee, such as shown in Parks 4,866,247; Blankenship 5,278,390; and, Houston 6,472,634.

These three patents illustrate the type of high switching speed power source employed for practicing the preferred
15 embodiment of the present invention.

The waveform of the waveform generator is stored in memory as a state table, which table is selected and outputted to the waveform generator in accordance with standard technology pioneered by The Lincoln Electric Company of Cleveland, Ohio. Such selection of a table for creating the waveform profile in the
20 waveform generator is disclosed in several prior art patents, such as the previously mentioned Blankenship 5,278,390. Consequently, a power source used in practicing the present invention is now commonly known and constitutes background technology used in the present invention. An aspect of the novel short arc welding

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system of the present invention employs a circuit to determine the total energy of the melting pulse forming the molten metal ball of the advancing electrode, such as described in Parks 4,866,247. The total energy of the melting pulse is sensed by a watt meter having an integrated output over the time of the melting pulse.

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After a short has been created in a short arc welding system, the short is cleared by a subsequent increase in the welding current. Such procedure is well known in short arc welding systems and is described generally in Ihde 6,617,549 and in Parks 4,866,247.

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The preferred embodiment of the invention is a modification of a standard AC pulse welding system well known in the welding industry. A prior pending application of assignee describes standard pulse welding, both DC and AC, with an energy measurement circuit or program for a high frequency switching power source of the type used in practicing the AC short circuit preferred implementation of the present invention. Although not necessary for understanding the present invention or practicing the present invention, the background art is disclosed in U.S. Publication No. 2006/00226131 published October 12, 2006, and U.S. Publication No. 2006/0070983 published April 6, 2006.

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The present invention relates to a cored electrode and a short arc welding system for controlling the melting pulse of the system for depositing a special cored electrode so no shielding gas is needed. The system maintains a desired time

between the pulse and the actual short circuit. This time is controlled by a feedback loop involving a desired timing of the short circuit and the pulse, so that the size of the ball of the pulse is varied to maintain a consistent short circuit timing. This process is a substantial improvement of other short arc control arrangements, such as disclosed in Pijls 4,020,320 using two power sources. A first source maintains a constant size melting pulse and there is a fixed time between the short circuit and the subsequent clearing pulse. There is no feedback between the pulsed timing and a parameter of the melting pulse, as employed in the present invention. A desired time is maintained between the end of the melting pulse and the short circuit event. By fixing the desired time using a feedback loop concept, arc stability is improved. This invention is applicable to a DC process, as shown in Pijls 4,020,320, but is primarily advantageous when using an AC short arc welding system.

Pijls 4,020,320

shows a control circuit for a DC short arc system wherein two unrelated timings are maintained constant without a closed loop control of the melting pulse.

(Cored Electrode)

The invention involves a novel welding method employing a novel flux cored electrode or welding wire. Details of arc welding electrodes or wires and specifically, cored electrodes for welding are provided in U.S. Patents 5,369,244; 5,365,036; 5,233,160; 5,225,661; 5,132,514; 5,120,931; 5,091,628; 5,055,655; 5,015,823; 5,003,155; 4,833,296; 4,723,061; 4,717,536; 4,551,610; and 4,186,293.

U.S. Publication No. 2005/0051524 published March 10, 2005, U.S. Publication No. 2005/0242076 published November 3, 2005 and U.S. Publication No. 2007/0095807 published May 3, 2007 provide background, non-prior art technology.

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THE INVENTION

In accordance with a first aspect of the invention as it relates to the method, the melting pulse of the short arc waveform is controlled interactively by a feedback loop and not by fixing constant values of the melting pulse. The time between the
10 end of the melting pulse and the short circuit is maintained by reactively changing parameters of the melting pulse in a short arc welding system. The system is preferably an AC system, but can be used in a DC system of the type generally described in Pijls 4,020,320. Novel manipulation of the short arc waveform is facilitated by using a single power source having the waveform controlled by a
15 waveform generator operating the pulse width modulator of a high switching speed inverter, such as disclosed in Houston 6,472,634. The advance realized by implementation of the present invention is an improvement over short arc welding using two separate power sources, as shown in the prior art.

In accordance with the preferred embodiment of the first aspect of the present
20 invention, the short arc welding system is an AC system wherein the melting pulse has a negative polarity. To maintain a constant molten metal bead, there is a joule threshold switch to shift the power supply to a low level positive current so the molten metal on the end of the advancing electrode forms into a ball and then short

circuits against the workpiece weld puddle. This AC waveform is preferably controlled by a waveform generator controlling the profile of the individual current segments of the waveform and determining the polarity of the waveform segments. In the prior art, a joule threshold switch was used to provide a constant energy to the melting pulse. In accordance with the present invention, there is a timer to measure the time for the electrode to short after the melting pulse. A feedback loop is employed to maintain a consistent time between the melting pulse and the short circuit event. This control of time stabilizes the arc and the shorting cycle. Ideally the time between the melting pulse and the short is about 1.0 ms. Depending upon the electrode size and deposition rate, the time between the melting pulse and the short circuit event is adjusted to a fixed value in the general range of 0.5 ms to 2.0 ms. Control of the timing is primarily applicable to AC short arc welding; however, the same concept is applicable to straight DC positive polarity. In both instances, the advancing wire with molten metal formed by the melting pulse is held at a low quiescent positive current facilitating the formation of a ball preparatory to the short circuit event. In either implementation of the invention, the joules or other parameter of the melting pulse is controlled by a feedback loop conditioned to maintain a preset time to the short circuit event.

The AC implementation of the first aspect of the present invention is primarily useful for tubular electrodes of the flux cored type and especially a novel implimentation of a flux core electrode with alloy ingredients in the core. Control of the melting cycle of a flux cored electrode based upon feedback from the short circuit time is a very precise procedure to maintain stability of the AC short circuit

welding process. The invention is also especially applicable to pipe welding with a cored electrode (especially the novel version of a flux cored electrode). The welding current for such electrode, when using the novel method, is below the threshold current for spray welding. Thus, the metal transfer to the pipe joint must involve
5 some type of short circuit, normally a globular short circuit transfer of the type to which the present invention is directed. Improving the weld stability by using AC short arc welding still resulted in instability of the arc. This instability has been overcome by implementing the present invention. Thus, the present invention is particularly applicable to AC short arc welding of a pipe joint using a cored electrode.

10 In accordance with the first aspect of the present invention there is provided a welding system for performing a short arc welding process between an advancing wire electrode and a workpiece, where the system comprises a power source with a controller for creating a current pulse introducing energy into the electrode to melt the end of the electrode and a low current quiescent metal transfer section allowing
15 the melted metal on the end of the electrode to be deposited into the weld puddle of the workpiece. During the low current metal transfer section, the molten metal short circuits against the molten metal puddle. A timer measures the actual time between the end of the melting pulse and the short circuit event. A device is used to set a desired time between the pulse and short circuit event and a circuit is used to create
20 a corrective signal based upon the difference between the actual time and the desired time. This corrective signal is used to control a given parameter of the melting pulse, such as the total energy introduced into the wire during the melting pulse.

In accordance with the preferred implementation of the first aspect of the present invention, the short arc welding process is an AC process wherein the melting pulse is performed with a negative current and the quiescent low current metal transfer section of the waveform is at a positive polarity. The AC version of the present invention is particularly applicable for welding with a flux cored electrode in several environments, such as the root pass of a pipe welding joint.

In accordance with another aspect of the novel power source, the controller of the short arc welding system includes a circuit to create a short circuit clearing pulse after the short circuit. In the preferred power source a waveform generator determines the polarity and profile of the welding waveform at any given time. The welding system of the present invention is used to maintain the time between the melting pulse and the short at a fixed value, which fixed value is in the general range 0.5-2.0 ms and is preferably approximately 1.0 ms.

In accordance with another aspect of the power source or method performed by the power source, the short arc system is performed DC positive with both the melting pulse and the quiescent section being positive and followed by a short circuit positive clearing pulse. This implementation of the present invention does not involve a polarity change from the waveform generator during the processing of the waveform to practice the short arc welding process. The short arc welding system is AC and there is a circuit to control the current pulse for causing the actual time between the melting pulse and short circuit so it is the same as the desired time. Indeed, this implementation of the invention maintains a constant time, as does the preferred embodiment of the invention.

The principal implementation of the present invention controls the energy of the melting pulse to control the time between the melting pulse and the ultimate short circuit event.

Yet another aspect of the first aspect of the invention is the provision of a method for controlling the melting pulse of a short arc welding process so that the process has a selected time between the melting pulse and the short circuit event. The parameter controlled by this method is preferably the total energy of the melting pulse. The invention is particularly applicable for use in the root pass of a circular open root pipe joint using a flux cored electrode.

The present second aspect of the invention relates at least in part, to a discovery that by utilizing a relatively short arc length during AC welding as obtained by this novel short arc method, contamination of the weld from the atmosphere can be significantly reduced. The invention also relates at least in part, to a discovery of a particular flux alloy system, which when used in an electrode according to the second aspect. The flux/alloy system of the cored electrode enables and promotes a short arc length. Combining these aspects in accordance with the present invention, provides a synergistic phenomenon , i.e. the novel method and novel flux cored electrode that produces a sound and tough weld metal with strength of over 60 to 70 ksi. These alloys allow use of thinner pipes and there is no need for shielding gas in the pipe welding area.

Waveform technology as pioneered by The Lincoln Electric Company of Cleveland, Ohio has been modified for use in AC welding with flux cored electrodes. Cored electrodes allow the welding operation to be more precisely controlled with

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the alloy of the weld bead being tailored to the desired mechanical characteristics for the bead and with the position of the welding operation being less limited. However, to provide arc stability and appropriate melting temperatures and rates, the actual control of the waveform for the AC process is quite complicated. Contamination of the weld metal during arc welding is still a problem using AC welding for cored electrodes. Contaminants, in the weld metal after the welding operation can cause porosity, cracking and other types of defects in the weld metal. Consequently, a major challenge confronting designers of arc welding processes has been to develop techniques for excluding elements, such as contaminants from the atmosphere, from the arc environment or for neutralizing the potentially harmful effects of such impurities. The potential source of contamination, includes the materials that comprise the welding electrode, impurities in the workpiece itself and ambient atmosphere. Cored electrodes may contain "killing" agents, such as aluminum, magnesium, zirconium and titanium which agents combine chemically with potential contaminants to prevent them from forming porosity and harmful inclusion in the weld metal. The present invention involves the use of a unique, novel electrode composition that reduces the tendency of a cored electrode to allow inclusion of contaminants in the weld metal. The method also reduces the amount of material required as a "killing" agent.

Specifically, the present invention provides a self-shielded flux cored arc welding (FCAW-S) electrode particularly adapted for forming welds having reduced levels of contaminants using an AC waveform. The electrode has an alloy/flux system comprising from about 35 to about 55% barium fluoride, from about 2 to

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about 12% lithium fluoride, from about 0 to about 15% lithium oxide, from about 0 to about 15% barium oxide, from about 5 to about 20% iron oxide, and up to about 25% of a deoxidation and denitrifying agent. This agent can be selected from aluminum, magnesium, titanium, zirconium, and combinations thereof.

5 The present invention provides a method of arc welding using a flux cored electrode that utilizes a particular alloy/flux system. The method comprises applying a first negative voltage between an electrode and a substrate to cause at least partial melting of the electrode proximate the substrate. The method also comprises applying a positive voltage between the electrode and the substrate to promote
10 formation of a flowable mass of material from the electrode. The method further comprises monitoring for occurrence of an electrical short between the electrode and the substrate through the flowable mass. The method further comprises upon detecting an electrical short, applying a second negative voltage between the electrode and the substrate. And, the method comprises increasing the magnitude
15 of the second negative voltage, to thereby clear the electrical short and form a weld on the substrate from the flowable mass. The flux cored electrode can comprise from about 35 to about 55% barium fluoride, from about 2 to about 12% lithium fluoride, from about 2 to about 15% lithium oxide, from about 5 to about 20% iron oxide, and up to about 25% of a deoxidation and denitrifying agent selected from the
20 group consisting of aluminum, magnesium, titanium, zirconium, and combinations thereof.

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An object of the present invention is the provision of a short arc welding system, which system controls the spacing of the short circuit events during the process, especially when the process is performed in the AC mode.

Another object of the present invention is the provision of a method for short
5 arc welding, which method controls the melting pulse based upon the time between the melting pulse and short so this time remains fixed at a desired value.

Yet another object of the present invention is the provision of an improved electrode composition, and particularly an electrode fill composition which is particularly adapted for use in combination with the novel short arc welding system
10 and method.

A further object of the present invention is to provide a synergistic system comprising a short arc process and flux cored electrode to stabilize the arc at the shortest possible arc length. Thus, the contamination from the atmosphere is minimized. The combination of an alloy system and a weld process allows the arc to
15 be stable at such short arc lengths and result in a sound and tough weld metal.

These and other objects and advantages will become apparent from the following description taken together with the accompanying drawings.

BRIEF DESCRIPTION OF DRAWINGS

20 FIGURE 1 is a block diagram of a short arc welding system used in the preferred embodiment of the present invention;

FIGURE 1A is an enlarged cross-sectional view taken generally along line 1A-1A of FIGURE 1;

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FIGURE 2 is a series of side elevational views showing the stages I-IV in a short arc welding process;

FIGURE 3 is a combined current and voltage waveform graph showing the waveform implementing the preferred embodiment of the present invention as disclosed in FIGURE 4 for the various stages as shown in FIGURE 2;

FIGURE 4 is a flow chart block diagram illustrating a modification of the system in FIGURE 1 to perform the preferred embodiment of the present invention;

FIGURES 5 and 6 are flow chart block diagrams of a portion of the welding system shown in FIGURE 1 for implementing two further embodiments of the present invention;

FIGURES 7 and 8 are partial flow chart block diagrams of the welding system as shown in FIGURE 1 combining the preferred embodiment of the present invention shown in FIGURE 4 with a combined waveform control from the embodiments of the invention shown in FIGURES 5 and 6, respectively;

FIGURE 9 is a current waveform for the DC positive implementation of the present invention;

FIGURE 10 is a schematic elevational view showing the invention used in the root pass or tacking pass of a pipe welding joint;

FIGURE 11 is a side elevational view with a block diagram illustrating the use of a representative welding system and an electrode;

FIGURE 12 is an enlarged cross-sectioned pictorial view taken generally along line 12-12 of FIGURE 11, depicting the electrode in greater detail;

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FIGURE 13 is an enlarged, schematic view representing a cored electrode where the sheath and core are melted at different rates;

FIGURE 14 is a view similar to FIGURE 13 illustrating the disadvantage of a failure to employ a tailored waveform for welding with cored electrodes;

5 FIGURE 15 is a view similar to FIGURES 13 and 14; and

FIGURE 16 is a partial, side elevational view illustrating a cored electrode in accordance with the present invention and showing the arc length, which length is minimized by use of the present invention.

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PREFERRED EMBODIMENTS OF THE INVENTION

(Novel Power Source/Method)

In the electric arc welding industry, short arc welding is a common practice and involves the four stages I, II, III and IV as schematically disclosed in FIGURE 2. The power source for performing short arc welding can be a transformer based
15 power source; however, in accordance with the preferred embodiment of the present invention, system A, shown in FIGURE 1, utilizes a high switching speed inverter based power source B having an AC supply across lines 10, 12, or a three phase supply, directed to inverter 14 creating a first DC signal across lines 14a, 14b. In accordance with standard architecture, boost or buck converter 20 is used in power
20 source B for correcting the input power factor by creating a controlled second DC signal across output lines 22, 24. High switching speed inverter 30 converts the second DC signal across lines 22, 24 to a waveform created by a large number of current pulses across output leads 32, 34. In accordance with the preferred

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embodiment of the present invention, the waveform across leads 32, 34 is either DC positive or AC; therefore, inverter 30 has an output stage, not shown, that dictates the polarity of the profiled waveform across leads 32, 34. These leads are connected to electrode E and workpiece WP, respectively. In accordance with

5 standard short arc technology, electrode E is an advancing end of wire W supplied through contact tip 42 from supply spool or drum 40. Thus, wire W is driven toward workpiece WP at a given WFS as a controlled waveform having the desired polarity is created across the gap between electrode E and workpiece WP. Wire W is preferably a flux cored wire schematically illustrated in FIGURE 1A and shown to

10 include an outer low carbon steel sheath 50 surrounding an internal flux core 52 having a fluxing agent and normally including alloying particles. Shunt 60 drives feedback current device 62 so the voltage signal on line 64 is representative of the instantaneous arc current of the welding process. In a like manner, device 70 creates a signal on output line 72 representative of the instantaneous voltage of the

15 welding process. Controller C of inverter 30 is a digital device, such as a DSP or microprocessor, that performs functions schematically illustrated in generally analog architecture. As a central component of controller C a waveform generator 100 processes a specific waveform from a state table stored in memory unit 102 and selected according to the desired welding process by device or circuit 104. Upon

20 selecting the desired short arc welding process a select signal 104a is directed to memory unit 102 so that the state table defining the attributes and parameters of the desired short arc welding waveform is loaded into waveform generator 100 as indicated by line 102a. Generator 100 outputs the profile of the waveform at any

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given time on output line 100a with the desired polarity indicated by the logic on line 100b. Illustrated power source B controlled by digital controller C is of the current control feedback type wherein the current representative voltage on line 64 is combined with the waveform profile signal on line 100a by error amplifier 110 having
5 an output signal on line 110a to control pulse width modulator 112 in accordance with standard waveform control technology. The output signal on line 112a controls the shape of the waveform across lines 32, 34 and the polarity of the particular waveform profile being implemented is set by the logic on line 100b. In this manner, waveform generator 100 controls pulse width modulator 112 to have pulses in line
10 112a controlling the high frequency operation of inverter 30. This inverter switching frequency is generally greater than 18 kHz and preferably greater than about 40 kHz. As so far described, power source B with controller C operates in accordance with standard technology pioneered by The Lincoln Electric Company of Cleveland, Ohio. Controller C is digital, but illustrated in analog format. To implement a short
15 arc welding process, it is necessary for controller C to receive feedback information regarding a short circuit condition between electrode E and workpiece WP. This feature of controller C is schematically illustrated as a short circuit detector 120 that creates a logic on line 122 to announce the existence of a short circuit event SC to waveform generator 100. Thus, the generator is informed when there is a short
20 circuit and implements a waveform in accordance with processing a short circuit as accomplished in any short arc welding process. As so far described, controller C is standard technology, with the exception of controlling a polarity switch at the output of inverter 30 by the logic on line 100b.

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To practice the invention, controller C is provided with a circuit 150 for controlling the melting pulse preparatory to the short circuit. Circuit 150 is digital, but schematically illustrated in analog architecture. The functions are implemented by the digital processor of controller C to control the energy of the melting pulse. Such
5 energy control circuitry is described in U.S. Publication No. 2006/0226131.

This prior application is incorporated by reference herein not as prior art, but as related technology. As shown in the prior application, the energy of the melting pulse of a pulsed welding waveform can be controlled by circuit 150 including multiplier 152 for
10 multiplying the instantaneous signal on lines 64, 72 to provide a signal on line 154 representing the instantaneous watts of the welding process. The wattage signal on line 154 is accumulated by a standard integrator 156 as described in Parks 4,866,247. Integration of the watt signal on line 154 is controlled by waveform generator 100 that creates a pulse start command shown as block 160 to
15 correspond to the start of the melting pulse indicated by logic on line 162. The starting point is the time t_1 when the melting pulse is started by waveform generator 100. Output signal on line 164 starts integration of the watt signal on line 154 by integrator 156. The integration process is stopped by a logic on line 170 produced by activation of stop pulse device or circuit 172 upon receipt of logic on input line
20 172a. Logic on line 172a toggles device 172 to change the logic in output lines 172b and 172c. The logic on line 172c informs the waveform generator that the melting pulse is to stop to change the profile on output line 100a. At the same time, the signal on line 172b toggles reset device or circuit 174 to change the logic on line 170

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to stop integration of the instantaneous watt signal. The digital number on output line 156a is loaded into digital register 180 having an output 182 representing the total energy of a given melting pulse in the short arc welding process. This total energy signal is compared with a desired energy level stored in register 190 to
5 provide a digital number or signal on line 192. Comparator 194 compares the actual energy for a given pulse represented by a number on line 182 with a desired energy level indicated by the number on line 192. The relationship between the actual energy and the desired energy controls the logic on line 172a. When the signal from line 182 equals the signal on line 192, comparator 194 changes the logic on line
10 172a to stop the pulse as indicated by device or circuit 172. This stops integration and stops the melting pulse being created by waveform generator 100. Circuit 150 is employed for performing the preferred embodiment of the present invention which changes the reference or desired energy for the melting pulse by changing the number on line 192 through adjustment of circuit 200. The pulse is stopped when
15 the adjusted energy or energy threshold is reached as determined by the number signal on line 182 as compared to the signal on line 192. The preferred embodiment of the novel power source and method used in the combined invention adjusts circuit 200 to change the reference energy for performing a novel short arc welding process by changing the melting pulse.

20 Short arc welding system A using power source B with digital controller C is operated by adjusting circuit 200 to perform the waveform shown in FIGURE 3. AC current waveform 210 has a negative melting pulse 212 represented by stage I in FIGURE 2 where the melting pulse produces molten metal 220 on the end of

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electrode E. The level of current in pulse 212 is below current needed for spray arc so there is a transfer by a short. The time t_1 starts the Joule measurement as explained later. The pulse has a start position 212a at time t_1 and a stop position 212b at time t_2 . Following the melting pulse, in accordance with standard practice,

5 there is a positive low current quiescent transfer section 214, as represented by stage II of FIGURE 2. In this stage, the molten metal 220 on the end of advancing electrode E is formed into a ball by surface tension action awaiting a short circuit which occurs at time t_3 and is shown as stage III. Consequently, the time between t_2 and t_3 is the time between the end of the melting pulse and the short circuit event,

10 which time is indicated by the logic on line 122 as shown in FIGURE 1. After stage II, a current pinch action shown as neck 222 separates the molten metal 220 from puddle 224. This electrical pinching action shown in stage IV is accelerated in accordance with standard practice by a negative short circuit pulse 216 having a first current section 216a with a steep slope and followed by a second current section

15 216b with a more gradual slope. Ultimately, the shorted metal separates and the SC logic on line 122 shifts to start the next current pulse at time t_1 indicated by a transition section 218. Waveform 210 is an AC waveform having a negative melting pulse 212, a low current quiescent section 214 ending at point 214a and a clearance pulse 216 transitioning into the next negative pulse 212 at time t_1 . The

20 corresponding voltage has a waveform 230 with negative section 232, a low level positive section 234 that plunges at short 236 and is followed by a negative voltage section 238 that transitions at section 240 into the next melting pulse voltage 232. The total cycle

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time is from t_1 to the next t_1 and the positive transfer 214 has a time less than 20% of the total cycle time. This prevents stubbing.

The present invention involves a novel power source and method for controlling waveform 210 by waveform generator 100 of controller C so the time
5 between the end of melting pulse 212 at t_2 and the time of the actual short event t_3 is constant based upon adjustment of circuit 200. This time delay adjustment, in the preferred embodiment, is accomplished by the circuit 250 shown in FIGURE 4. In this circuit, the time between the melting pulse and at time t_2 and the short circuit at time t_3 is set to a desired level between 0.5 to 2.0 ms. Preferably, the set desired
10 time delay is 1.0 ms, which is the level of the signal on line 254. Thus, the numerical number on line 254 is the desired time t_2 to t_3 . The actual time between t_2 and t_3 is determined by timer 260 which is started at time t_2 and stopped at time t_3 . The timer is reset for the next measurement by an appropriate time indicated as t_5 which can be adjusted to be located at various positions after t_3 , which position is illustrated to
15 be during the melting pulse in FIGURE 3. The number on line 262 is the actual time between t_2 and t_3 . This actual time is stored in register 270 which is reset at any appropriate time such as time t_2 . Thus, the digital data on line 272 is the actual measured time between t_2 and t_3 . This time is compared to the desired time on line 254. Any error amplifier can be used to digitally process the relationship of actual
20 time to the set time. The process is schematically illustrated as a summing junction 280 and digital filter 282 having an output 284 for adjusting circuit 200. The difference between the desired time and the actual time is an error signal in line 284 which increases or decreases the desired total energy of circuit 200. The desired

total energy is periodically updated at an appropriate time indicated as t_4 by an update circuit 290. Thus, at all times the signal in line 192 of FIGURE 1 is the desired total energy for pulse 212 of the short arc process. This total energy is adjusted by any difference between time t_2 and time t_3 so the energy of pulse 212
5 maintains a constant or desired time delay for the upcoming short circuit. This time control stabilizes the short arc welding process of system A.

In FIGURE 4, the preferred embodiment of the novel power source is implemented by changing the energy threshold for the melting pulse to change the timing between the pulse and the short event. This time can also be changed by
10 voltage or power of the melting pulse as schematically illustrated in FIGURES 5 and 6. In both of these embodiments, the time of the melting pulse t_1 to t_2 is maintained fixed as indicated by block 300. During this constant time melting pulse, the voltage or power is changed to control the time between the pulse and the short circuit event. In FIGURE 5, the number on output line 284 from filter 282 controls feedback
15 loop 310 to adjust the voltage of the melting pulse, as indicated by the numerical data on line 312. To adjust the power for controlling the delay time of the short circuit event, the number on output line 284 is used to adjust feedback loop 320, which is compared to the instantaneous power on line 154 by waveform generator
100. The change in power is a numerical value on line 322 which is compared to the
20 digital number on line 154 for controlling the power of the melting pulse. Thus, in the first three embodiments of the present invention, the total energy of the waveform, the voltage of the waveform or the power of the waveform is adjusted to maintain a

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constant time between t_2 to t_3 to stabilize the arc and control the short circuit events of system A shown in FIGURE 1.

In accordance with another embodiment of the novel power source, the energy adjustment of melting pulse 212 is combined with the two modifications of the present invention illustrated in FIGURES 5 and 6. Such combination controls are shown in FIGURES 7 and 8 wherein prior summing junction 280 and digital filter 282 are illustrated as combined in analog error amplifier 330. The component or program has output 332 with a logic for stopping the melting pulse when the threshold energy has been reached, as indicated by the logic on line 182. Thus, the total energy of the pulse is controlled together with the pulse voltage control circuit 310 in FIGURE 7 and the pulse power control 320 as shown in FIGURE 8. Output 312 is combined with output 172c for controlling the waveform profile in line 100a of generator 100. In a like manner, the energy level is controlled by logic on line 172c in combination with the digital information on output line 322 of power pulse control circuit 320. Other combinations of parameters can be used to control melting pulse 212 to assure an accurate control of the time between the melting pulse and the short circuit event. Such other parameters are within the skill of the art in controlling a waveform generator by closed feedback loops.

The invention is preferably an AC process, as shown in FIGURE 4; however, DC positive waveform 400 can be used as shown in FIGURE 9. Melting pulse 402 has a high positive current 402a until the pulse is terminated at time t_2 . The current, in the DC positive mode, is limited to a level below that needed for spray arc so the metal is not detached without shorting. This concept defines the short arc welding

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process. Then the waveform transitions into a low level positive current section 404 awaiting the short at time t_4 . This low level positive current is used in the preferred embodiment of the present invention and terminates at time t_3 . Thereafter, short clearing pulse 410 is created by the waveform generator. Pulse 410 has high ramp area 412 and a stepped area 414 to bring the current back up to the high current level 402a. Various illustrated embodiments of the present invention can be used in implementing the positive current waveform 400; however, the logic on line 100b for controlling the polarity of the output waveform on lines 32, 34 is not necessary.

(Novel Flux Cored Electrode)

10 The preferred implementation of the inventive power source is in pipe welding operation using a novel flux cored electrode as schematically represented in FIGURE 1A. Such pipe welding operation is schematically illustrated in FIGURE 10 wherein pipe sections 420, 422 define an open root 424. The present invention as shown in FIGURE 4 controls the waveform on wire W as it moves through contact tip 15 42 to open root 424 of the pipe joint. FIGURE 10 shows a particular embodiment using the present invention for welding the root pass of a pipe joint to tack the pipe sections together for subsequent joining with standard welding techniques.

In certain embodiments, the power sources and/or welding operations according to the present invention exhibit one or more of the following aspects. The 20 current density is generally less than that required for spray welding since the primary mode of metal transfer is short circuit welding. As in many short circuit processes, a pinch current is established depending upon the wire diameter, for example for a 5/64 inch flux cored wire, a current of 625 amps can be used.

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Generally, the positive current tends to set the arc length. If the positive current is allowed to reach the same level as the negative current arc length, even for half a millisecond, the positive current arc will reach a non-desirable length. Generally, positive side control current is in the range of from about 50 amps to about 125
5 amps, and preferably about 75 amps. The negative portion of the wave shape can either be a constant power or voltage with a slope of from about 5 to 15 percent current. Typically, welding can be performed at about 60 hertz, 10 percent positive. Since the positive current is set at a relatively low level, the portion that the wave shape is positive is typically less than 20 percent.

10 FIGURES 11 and 12 schematically illustrate a waveform technology welder and/or welding system 510, and a cored electrode 530. The welding system comprises a welder 510 having a torch 520 for directing an electrode 530 toward workpiece W. The welding system 510 includes a three phase input power supply L1, L2, and L3, which is rectified through rectifier 550, 560, and a power source 540.
15 The power source 540 provides an output, and specifically, an AC waveform as described in U.S. Publication 2007/0095807.

An arc AC is created between the end of electrode 530 and workpiece W. The electrode is a cored electrode with a sheath 600 and an internal filled core 610. The core includes flux ingredients, such
20 as represented by particles 610a. The purpose of these ingredients 610a is to (a) shield the molten weld metal from atmospheric contamination by covering the molten metal with slag, (b) combine chemically with any atmospheric contaminants such that their negative impact on the weld quality is minimized and/or (c) generate arc

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shielding gases. In accordance with standard practice, core 610 also includes alloying ingredients, referred to as particles 610b, together with other miscellaneous particles 610c that are combined to provide the fill of core 610. To optimize the welding operation, it has been necessary to use solid wire with an external shielding
5 gas. However, in order to produce a weld with specific mechanical and metallurgical properties, specific alloys are required, which can be difficult to obtain in the form of a solid wire. Gas shielding is not always a feasible alternative due to access to gas or difficulty to achieve adequate shielding due to windy conditions, accessibility to clean gas mixtures and difficult terrains. It would be advantageous to therefore use a
10 self shielding cored electrode, so that the environment does not affect the welding.

A common problem caused when using cored electrodes without control of the welding waveform profile is illustrated in FIGURE 13. The welding process melts sheath 600 to provide a portion of molten metal 630 melted upwardly around the electrode, as indicated by melted upper end 640. Thus, the sheath of the electrode
15 is melted more rapidly than the core. This causes a molten metal material to exist at the output end of electrode 530 without protective gas or chemical reaction created by melting of the internal constituents of core 610. Thus, arc AC melts the metal of electrode 610 in an unprotected atmosphere. The necessary shielding for the molten metal is formed when the sheath and core are melted at the same rate.
20 The problem of melting the molten metal more rapidly than the core is further indicated by the pictorial representation of FIGURE 14. Molten metal 650 from sheath 600 has already joined workpiece W before the core 610 has had an opportunity to be melted. Thus, the core 610 can not provide the necessary shielding

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for the welding process. FIGURES 13 and 14 show the reason why AC welding using cored electrodes has not been used for off-shore pipeline welding and other pipeline welding. However, an AC waveform can be utilized to control the heat input when using a cored electrode.

5 By controlling the precise profile for the AC waveform used in the welding process, sheath 600 and core 610 can be made to melt at approximately the same rate. The failure to adequately coordinate the melting of the sheath with the melting of the core is one reason why a shielding gas SG, as shown in FIGURE 15 may be used. The advantage of controlling the profile of the AC waveform is that external
10 shielding gas SG, may be avoided.

Although control of the AC waveform can lead to significant advantages, as previously noted, in order to provide arc stability and appropriate melting temperatures and rates, the actual control of the AC waveform, is quite complicated. And, even with the use of sophisticated AC waveforms, contamination of the weld is
15 possible. Contamination of welds formed by using sophisticated AC waveforms, is still possible, even if shielding gas is used. Accordingly, in a preferred aspect of the present invention, certain electrode compositions are provided that, when used in conjunction with AC waveforms, can form strong, tough, and durable welds, without significant contamination problems, and without the degree of control otherwise
20 required for the AC waveforms.

(Novel Electrodes)

When welding by the novel method or power source with a cored electrode, it is desired to have the sheath and core melt at the same rate. This operation

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promotes homogeneous mixing of certain core materials with the outer sheath, such that the mixture of molten materials chemically resists the effects of atmospheric contamination. Alloying elements required to produce desired weld metal mechanical and metallurgical characteristics are uniformly distributed in the weld metal. In addition, the protective benefits derived from slag and/or gas-forming constituents are optimized. As previously noted, this situation is illustrated in FIGURE 15. In contrast, FIGURE 14 illustrates a situation where the sheath has melted more rapidly than the core. In this deleterious situation, molten metal 650 from sheath 500 has already joined workpiece W before core 610 has had an opportunity to be melted. Metal 650 has not been protected from the effects of atmospheric contamination to the degree that it would have been if the unmelted core constituents had actually been melted. Additionally, alloying elements needed to achieve desired mechanical and metallurgical characteristics may be missing from molten metal 650.

As previously indicated, an electric welder of the type using waveform technology can be used for AC welding using a cored electrode, such as electrode 700 shown in FIGURE 16. Such electrode includes an outer steel sheath 710 surrounding core 720 formed of particulate material, including alloying metals and slag or flux materials. By having internal flux or slag materials, there is no need for external shielding gas during the welding operation. By including alloying material in core 720, the puddle of weld metal 740 on workpiece 730 can be modified to have exact alloy constituents. This is a substantial advantage and reason for using cored electrodes, instead of solid welding wire where alloying must be accomplished by

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the actual constituent of the welding wire. Adjustment of alloying for the weld metal is quite difficult when using solid welding wire. Therefore, it is extremely advantageous in high quality welding to employ a cored electrode. Arc AR melts sheath 710 and melts constituents or fill in core 720 at a rate which can be controlled to be essentially the same. Contamination in weld metal 740, such as hydrogen, nitrogen and oxygen can cause porosity problems, cracking and other types of physical defects in the weld metal. Thus, it is a challenge to design the welding process to exclude contaminants from the molten weld metal. It is common to use "killing" agents, typically silicon, aluminum, titanium and/or zirconium which will combine chemically with potential contaminants to prevent them from forming porosity or harmful inclusions in the weld metal. Furthermore, "scavengers" may also be added to react with hydrogen containing a species in order to remove hydrogen from the weld. In order to deposit consistently sound weld metal 740, it has often been necessary to add such killing agents in quantities that are themselves detrimental to properties of the weld metal, such as ductility and low temperature toughness. Thus, it is desirable to reduce the exposure of the molten metal in arc AR to prevent contamination of the metal passing from electrode 700 to workpiece 730 so the killing agents can be minimized.

The novel electrode compositions when used in AC welding, produce desirable welds that are durable, tough, and which are not susceptible to problems otherwise associated with the use of conventional electrode compositions. The electrode compositions of the present invention are preferably used in conjunction with AC waveforms where the positive and negative shapes of the AC waveform are

modified to reduce the overall arc length LA. In this manner, there is less exposure to the atmosphere and less time during which the metal is molten. A detailed description of the AC waveforms and related welding processes, for which the present invention electrode compositions are designed, is set forth in U.S.

5 Publication No. 2007/0095807.

Indeed, by reducing the arc length, the temperature of the molten metal can be reduced as it travels from the electrode 700 to weld metal puddle 740. Only by using a welder that can perform an AC welding process with different shapes for the negative and positive sections, can AC welding
10 with cored electrodes be used effectively in the field. Parameters of the positive and negative portions of the alternating waveform can be independently adjusted to compensate for and optimize the melting of both sheath 710 and cored 720 for selected electrode 700.

More specifically, the overall invention involves the combination of a novel
15 electrode and an AC welding wherein the positive and negative sections of the waveform are individually adjusted to accomplish the objective of a low arc length and reduce contamination. Using this strategy, the inventive electrode composition, particularly because it is self-shielding, can provide significant advantages. The electrodes are used without shielding gas and depending upon the particular
20 application, can rely on deoxidizing and denitrifying agents in the core for additional protection from atmospheric contamination.

The invention provides a synergistic system of a novel welding method with a unique set of alloying and flux components in the core of a FCAW-S electrode. As

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noted, a cored electrode is a continuously fed tubular metal sheath with a core of powdered flux and/or alloying ingredients. These may include fluxing elements, deoxidizing and denitrifying agents, and alloying materials, as well as elements that increase toughness and strength, improve corrosion resistance, and stabilize the arc. Typical core materials may include aluminum, calcium, carbon, chromium, iron, manganese, and other elements and materials. While flux cored electrodes are more widely used, metal-cored products are useful for adjusting the filler metal composition when welding alloy steels. The powders in metal-cored electrodes generally are metal and alloy powders, rather than compounds, producing only small islands of slag on the face of the weld. By contrast, flux cored electrodes produce an extensive slag cover during welding, which supports and shapes the bead.

The alloy/flux system of the present invention comprises particular amounts of a barium source, particular amounts of a lithium source, lithium oxide, iron oxide, and optional amounts of calcium oxide, silicon oxide, and manganese oxide. One or more fluoride, oxide and/or carbonate salts of barium can be used for the barium source. And, one or more fluoride and/or carbonate salts of lithium can be used for the lithium source. The alloy/flux system is included in the electrode fill. The electrode fill generally constitutes from about 18 to about 24% of the electrode. A preferred alloy/flux system comprises:

from about 35 to about 55% barium fluoride as the barium source,
from about 2 to about 12% lithium fluoride as the lithium source,
from about 0 to about 8% barium carbonate as a secondary barium source,

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from about 0 to about 8% lithium carbonate as the secondary lithium source,

from about 0 to about 15% of lithium oxide,

from about 0 to about 15% of barium oxide,

5 from about 5 to about 20% of iron oxide,

from about 0 to about 5% of calcium oxide,

from about 0 to about 5% of silicon oxide,

from about 0 to about 5% of manganese oxide, and

up to about 25% of aluminum, magnesium, titanium, zirconium, or
10 combinations thereof, for deoxidation and denitrifying and the remaining metallics optionally including iron, nickel, manganese, silicon, or combinations thereof. All percentages expressed herein are percentages by weight unless noted otherwise. Preferably, the electrode fill composition comprises from about 35 to about 55% barium fluoride, from about 2 to about 12% lithium fluoride, from about 0 to about
15 15% lithium oxide, from about 0 to about 15% barium oxide, from about 5 to about 20% iron oxide, and up to about 25% of a deoxidizing and denitrifying agent as previously noted. In other embodiments, the previously noted preferred electrode fill composition can also include from about 0 to about 8% barium carbonate. In yet another embodiment, the preferred electrode fill composition may additionally
20 include from about 0 to about 8% lithium carbonate. In yet another embodiment, the preferred fill composition can include from about 0 to about 5% calcium oxide. In yet a further embodiment, the electrode fill composition can include from about 0 to about 5% silicon oxide. And, in another embodiment, the preferred electrode fill

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composition can comprise from about 0 to about 5% manganese oxide. Other embodiments include the use of one or more of these agents, i.e. the barium carbonate, lithium carbonate, calcium oxide, silicon oxide, manganese oxide, and combinations thereof.

5 The preferred embodiment of the novel method comprises applying a first negative voltage between an electrode and a substrate to cause at least partial melting of the electrode near the substrate. The method also comprises applying a positive voltage between the electrode and the substrate to promote formation of a flowable mass of material from the electrode. The method further comprises
10 monitoring for occurrence of an electrical short between the electrode and the substrate through the flowable mass. The method further comprises upon detecting an electrical short, applying a second negative voltage between the electrode and the substrate. And, the method comprises increasing the magnitude of the second negative voltage, to thereby clear the electrical short and form a weld on the
15 substrate from the flowable mass. The preferred composition of the electrode fill in a flux cored electrode comprises from about 35 to about 55% barium fluoride, from about 2 to about 12% lithium fluoride, from about 0 to about 15% lithium oxide, from about 0 to about 15% barium oxide, from about 5 to about 20% iron oxide, and up to about 25% of a deoxidation and denitrifying agent selected from the group consisting
20 of aluminum, magnesium, titanium, zirconium, and combinations thereof. In other embodiments, additional agents can be incorporated in the preferred electrode fill. For instance, from about 0 to about 8% barium carbonate can be included. Another embodiment of the electrode fill composition includes from about 0 to about 8%

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lithium carbonate. Yet another embodiment includes from about 0 to about 5% calcium oxide. Another embodiment includes from about 0 to about 5% silicon oxide. And, yet another embodiment includes from about 0 to about 5% manganese oxide. In yet a further embodiment, one or more of these agents can be added or
5 otherwise included in the electrode fill composition. For example, the preferred electrode fill can also comprise, in addition to the previously noted proportions of barium fluoride, lithium fluoride, lithium oxide, barium oxide, iron oxide, and one or more particular deoxidation and denitrifying agents from about 0 to about 8% barium carbonate, from about 0 to about 8% lithium carbonate, from about 0 to about 5%
10 calcium oxide, from about 0 to about 5% silicon oxide, and from about 0 to about 5% manganese oxide.

The novel flux/alloy system is modified from traditional flux/alloy systems used for FCAW-S electrodes to achieve the short arc length and to weld at low heat inputs that result from the unique waveforms used in this process. The short arc
15 length and the stable arc is a result of the combination of the alloy and flux system and the unique characteristics of the waveform. In essence, both the welding consumable and the process are optimized in tandem to achieve the final weld product requirements.

In certain embodiments, the present invention provides methods of forming
20 weld metals having attractive properties. Generally, these methods involve providing a welding wire or electrode having a core with the previously described composition. Preferably, the welding wire or electrode is used free of shielding gas, or rather agents that form such a gas. The methods also include an operation in

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which the wire or electrode is moved toward the region of interest, such as a joint formed between two sections of pipe. Preferably such movement is made at a controlled feed speed. The method also includes creating a welding current to melt the wire or electrode by an arc between the wire and the pipe sections to thereby
5 form a molten metal bead in the joint. The method also includes transferring the melted wire to the molten metal bead by a succession of short circuit events. The method is particularly well suited for application to welding of a joint between two sections of pipe formed from a metal having a yield strength of at least about 70 ksi and a thickness less than about 0.75 inches. However, it will be appreciated that the
10 present invention can be used in applications on pipes having thicknesses greater than or less than 0.75 inches. The resulting bead that is formed generally has a tensile strength greater than 70 ksi and in certain applications, greater than about 90 ksi. In particular aspects, the melting current can be negative. If the melting current is negative, the metal transferring operation can be performed by a positive current.
15 The metal transferring can however, be performed by a positive current independent of the melting current. When performing the previously described method, it is generally preferred that the average arc length is less than 0.30 inches, preferably less than 0.20 inches, and most preferably less than 0.10 inches. In the previously described method, the rate of the short circuit events is preferably automatically
20 controlled. The rate of short circuit events is generally from about 40 to about 100 cycles per second.

In other embodiments, the previously described concepts, i.e. using the power sources and control techniques in combination with the novel electrode

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compositions noted herein, can be utilized to produce a weld metal having a minimum Charpy V-Notch toughness of 60J at -20°C. Similarly, the methods can be used to produce a weld metal having a minimum Charpy V-Notch toughness of 40J at -40°C. And, the methods can be used to produce a weld metal having a tensile
5 strength exceeding 90 ksi. Thus, thin pipe of less than about 0.75 inches can be used with the resultant savings. No shielding gas is needed, so the cost of on site gas is eliminated.

The present application can be utilized in a wide array of applications. The system, process, and/or compositions described herein are particularly adapted for
10 use in welding X80 pipe (the designation X80 being in accordance with the API 5L:2000 industry specification) with self-shielded flux core wire. However, the present invention can be utilized in conjunction with other pipe grades. The present invention can also be utilized in "root pass" or tack welding operations performed on pipes. The present invention can be utilized to melt greater amounts of welding wire
15 with less arc force as compared to currently known practices of using a buried short arc for the initial welding pass. Yet another application for the present invention is in robotic welding applications for high speed welding of thin gauge metals.

The present invention has been described with certain embodiments and applications. These can be combined and interchanged without departing from the
20 scope of the invention as defined in the appended claims. The systems, methods, electrodes and combinations thereof as defined in these appended claims are incorporated by reference herein as if part of the description of the novel features of the synergistic invention.

Claims:

1. A welding system for performing a short arc welding process between an advancing wire electrode and a workpiece wherein said electrode has an end facing said workpiece, said system comprising a power source, a timer, a timing device, a corrective circuit, a pulse circuit, and said wire electrode;

said power source including a controller that creates a current pulse that introduces energy into said end of said electrode to melt said end and a low current quiescent metal transfer section following an end of said current pulse during which said melted electrode short circuits against said workpiece; said timer measuring an actual time between the end of said current pulse and a beginning of said short circuit; said timing device setting a desired time from said current pulse to said short circuit; said corrective circuit creating a corrective signal based upon a difference between said actual time and said desired time; said pulse circuit responsive to said corrective signal to control a given parameter of said current pulse; and said wire electrode including an alloy/flux system, said alloy/flux system including barium fluoride, lithium fluoride and iron oxide.

2. The welding system as defined in claim 1, wherein said metal transfer section has a current of a positive polarity.

3. The welding system as defined in claim 1 or 2, wherein said controller includes a circuit operatively coupled to said power source to create a short circuit clearing pulse after said short circuit.

4. The welding system as defined in claim 3, wherein said clearing pulse has a first current followed by a higher second current.

5. The welding system as defined in claim 4, wherein at least one of said first and second currents is a ramped up current.

6. The welding system as defined in any one of claims 1 to 5, wherein said controller includes a circuit operatively coupled to said power source to create a short circuit clearing pulse after said short circuit.

7. The welding system as defined in any one of claims 1 to 6, wherein said given parameter includes total energy of said current pulse.
8. The welding system as defined in any one of claims 1 to 7, wherein said given parameter includes an instantaneous power of said current pulse.
9. The welding system as defined in any one of claims 1 to 8, wherein said given parameter includes an instantaneous voltage of said current pulse.
10. The welding system as defined in any one of claims 1 to 9, wherein said desired time is 0.5-2.0 ms.
11. The welding system as defined in claim 10, wherein said desired time is 1.0 ms.
12. The welding system as defined in any one of claims 1 to 11, wherein said current pulse has a negative polarity.
13. The welding system as defined in any one of claims 1 to 12, wherein said welding process has a cycle time equal to a time of said positive metal transfer section and said current pulse, and said transfer section time is less than 20% of said cycle time.
14. The welding system as defined in any one of claims 1 to 13, wherein said welding process having a current density that is less than required for spray welding of the wire electrode.
15. The welding system as defined in any one of claims 1 to 14, wherein said pulse circuit is operatively coupled to said power source and responsive to control the given parameter of said current pulse to provide a substantially constant time between said current pulse and said short circuit.
16. The welding system as defined in any one of claims 1 to 15, wherein said pulse circuit is operatively coupled to said power source and responsive to said corrective signal to control the energy of said current pulse to provide constant rate of shorting.

17. The welding system as defined in any one of claims 1 to 16, wherein said current pulse to introduce energy into said end of said electrode is a negative current pulse and said metal transfer section has a current of a positive polarity.

18. The welding system as defined in any one of claims 1 to 17, wherein said welding process is performed in a root pass of a circuit open root pipe joint by an alternating current waveform between said advancing wire and a pipe joint; and the pipe joint as said workpiece.

19. The welding system as defined in any one of claims 1 to 18, wherein said wire electrode is a flux cored electrode.

20. The welding system as defined in claim 19, wherein a profile of said welding current is controlled by the controller to cause a sheath of said flux cored electrode and said core of flux cored electrode to melt at a same rate.

21. The welding system as defined in any one of claims 1 to 20, wherein said wire electrode is a self-shielded flux cored electrode, said alloy/flux system positioned in a core of said welding wire, said alloy/flux system comprising:

- 35-55% barium fluoride;
- 2-12% lithium fluoride;
- 0-15% lithium oxide;
- 0-15% of barium oxide; and
- 5-20% iron oxide.

22. The welding system as defined in any one of claims 1 to 21, wherein said alloy/flux system includes up to 25 weight percent of at least one deoxidation and denitrating agent selected from the group consisting of aluminum, magnesium, titanium, zirconium, and combinations thereof.

23. The welding system as defined in any one of claims 1 to 22, wherein said alloy/flux system includes barium carbonate, said barium carbonate constituting up to 8 weight percent of said alloy/flux system.

24. The welding system as defined in any one of claims 1 to 23, wherein said alloy/flux system includes lithium carbonate, said lithium carbonate constituting up to 8 weight percent of said alloy/flux system.
25. The welding system as defined in any one of claims 1 to 24, wherein said alloy/flux system includes calcium oxide, said calcium oxide constituting up to 5 weight percent of said alloy/flux system.
26. The welding system as defined in any one of claims 1 to 25, wherein said alloy/flux system includes silicon oxide, said silicon oxide constituting up to 5 weight percent of said alloy/flux system.
27. The welding system as defined in any one of claims 1 to 26, wherein said alloy/flux system includes manganese oxide, said manganese oxide constituting up to 5 weight percent of said alloy/flux system.
28. The welding system as defined in any one of claims 19 to 27, wherein said alloy/flux system constitutes from 18-24 weight percent of said wire electrode.
29. The welding system as defined in any one of claims 1 to 28, wherein a weld bead formed by said welding process having a strength of over 60 ksi.
30. A method of controlling a melting pulse of a short arc welding process where the melting pulse for a wire electrode is followed by a low current transfer cycle, said method comprising:
- (a) measuring the actual time for a duration between an end of said melting pulse and a beginning of a short circuit during said transfer cycle of molten metal from said wire electrode to a workpiece, said wire electrode including an alloy/flux system, said alloy/flux system including barium fluoride, lithium fluoride and iron oxide;
 - (b) setting a desired time for said duration;
 - (c) creating a corrective signal by comparing said actual time and said desired time;
- and,
- (d) adjusting at least one parameter of said melting pulse based upon said corrective signal so as to regulate said desired time between said melting pulse and said short circuit.

31. The method as defined in claim 30, wherein said parameter is total energy.
32. The method as defined in claim 30 or 31, wherein said parameter is instantaneous voltage.
33. The method as defined in any one of claims 30 to 32, wherein said parameter is instantaneous power.
34. The method as defined in any one of claims 30 to 33, wherein said parameter is a combination of total energy and instantaneous voltage or total energy and instantaneous power.
35. The method as defined in any one of claims 30 to 34, wherein said current of said transfer cycle is positive.
36. The method as defined in any one of claims 30 to 35, including the step of creating a short circuit clearing pulse after said short circuit.
37. The method as defined in claim 36, wherein said clearing pulse has a first current followed by a higher second current.
38. The method as defined in claim 37, wherein at least one of said first and second currents is a ramped up current.
39. The method as defined in any one of claims 30 to 38, wherein said desired time is in the range of 0.5-2.0 ms.
40. The method as defined in claim 39, wherein said desired time is about 1.0 ms.
41. The method as defined in any one of claims 30 to 40, wherein said melting pulse has a positive polarity.
42. The method as defined in any one of claims 30 to 41, wherein said melting pulse has a negative polarity.
43. The method as defined in any one of claims 30 to 42, wherein said current of said transfer cycle is positive.

44. The method as defined in any one of claims 30 to 43, wherein said wire electrode is a flux cored electrode.

45. The method as defined in any one of claims 30 to 44, wherein said wire electrode is a self-shielded flux cored electrode, said alloy/flux system positioned in a core of said welding wire, said alloy/flux system comprising:

- 35-55% barium fluoride;
- 2-12% lithium fluoride;
- 0-15% lithium oxide;
- 0-15% of barium oxide; and
- 5-20% iron oxide.

46. The method as defined in any one of claims 30 to 45, wherein said alloy/flux system includes up to 25 weight percent of at least one deoxidation and denitrating agent selected from the group consisting of aluminum, magnesium, titanium, zirconium, and combinations thereof.

47. The method as defined in any one of claims 30 to 46, wherein said alloy/flux system includes barium carbonate, said barium carbonate constituting up to 8 weight percent of said alloy/flux system.

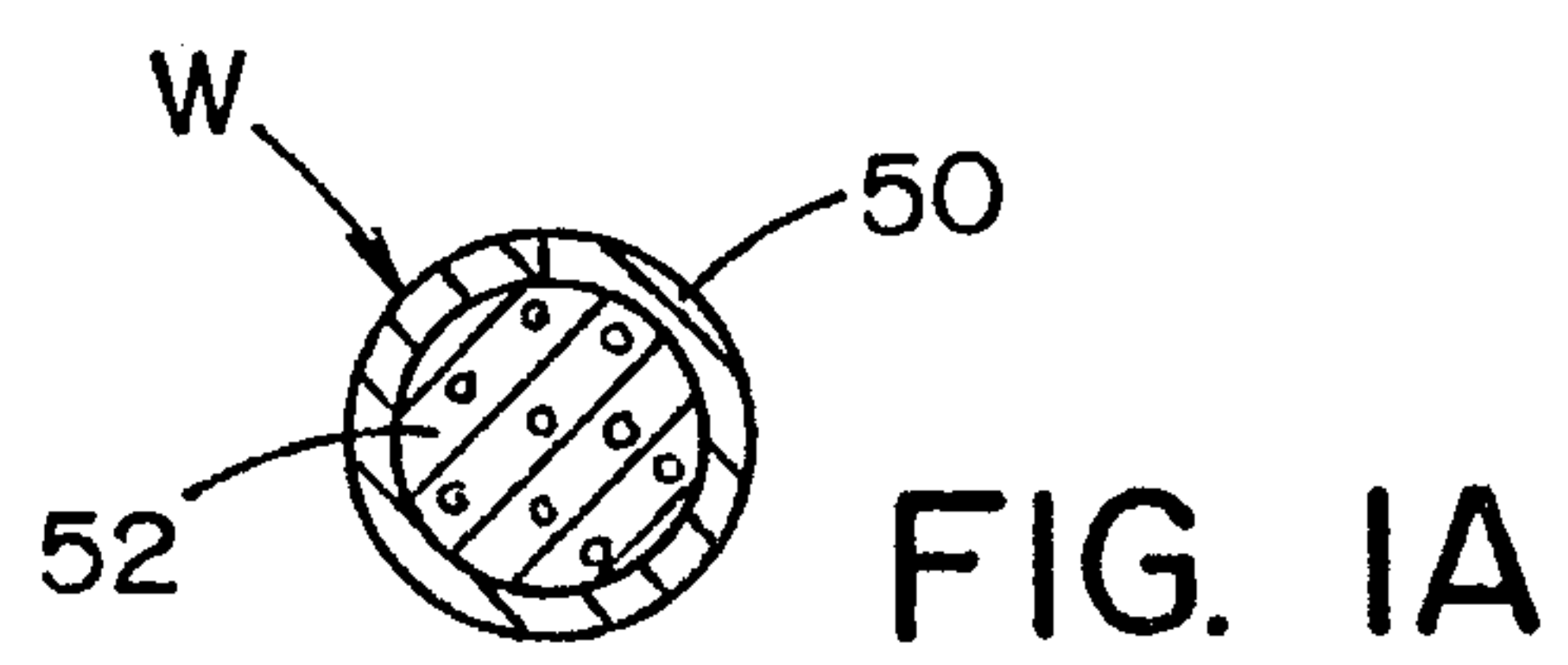
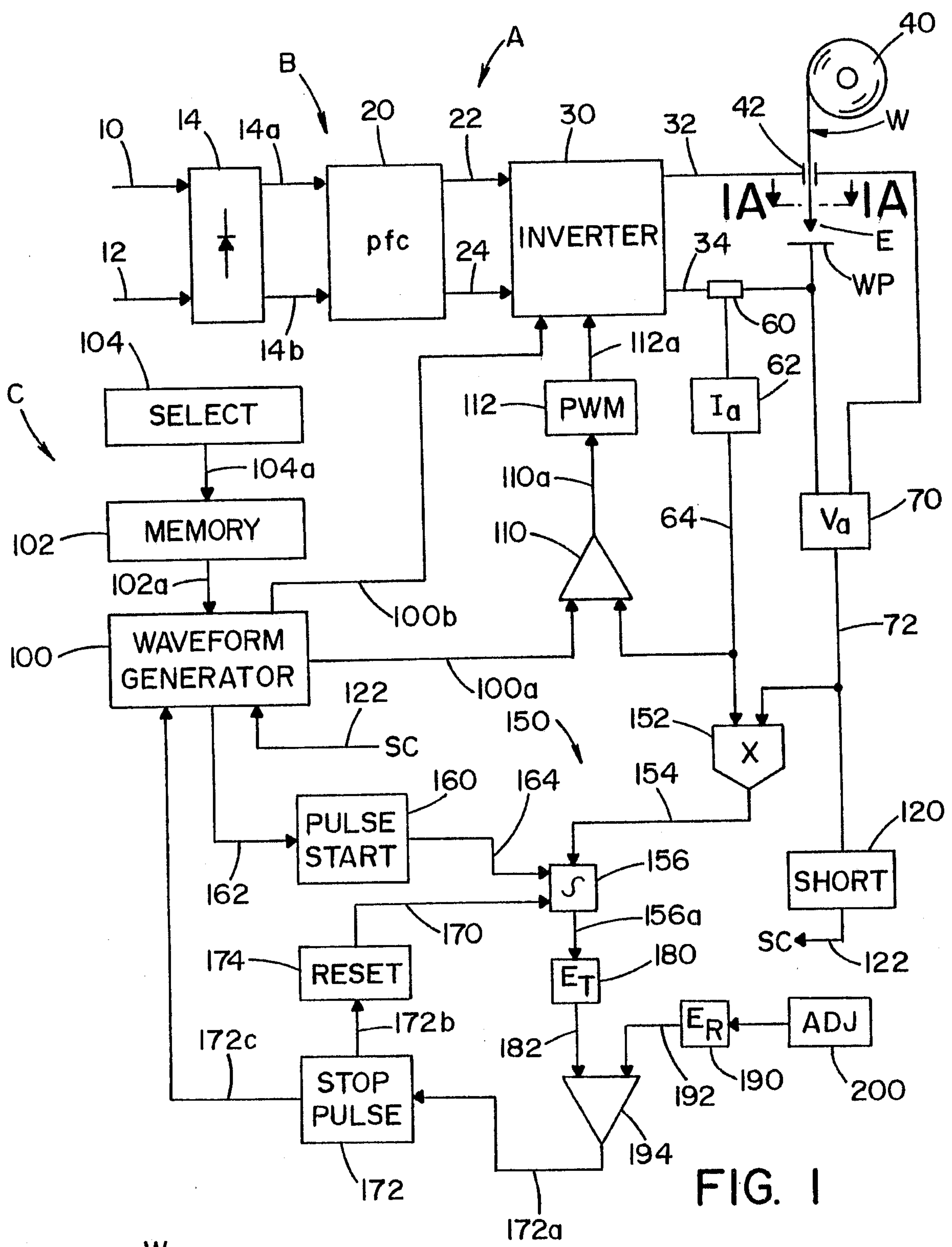
48. The method as defined in any one of claims 30 to 47, wherein said alloy/flux system includes lithium carbonate, said lithium carbonate constituting up to 8 weight percent of said alloy/flux system.

49. The method as defined in any one of claims 30 to 48, wherein said alloy/flux system includes calcium oxide, said calcium oxide constituting up to 5 weight percent of said alloy/flux system.

50. The method as defined in any one of claims 30 to 49, wherein said alloy/flux system includes silicon oxide, said silicon oxide constituting up to 5 weight percent of said alloy/flux system.

51. The method as defined in any one of claims 30 to 50, wherein said alloy/flux system includes manganese oxide, said manganese oxide constituting up to 5 weight percent of said alloy/flux system.

52. The method as defined in any one of claims 30 to 51, wherein said alloy/flux system constitutes from 18-24 weight percent of said wire electrode.



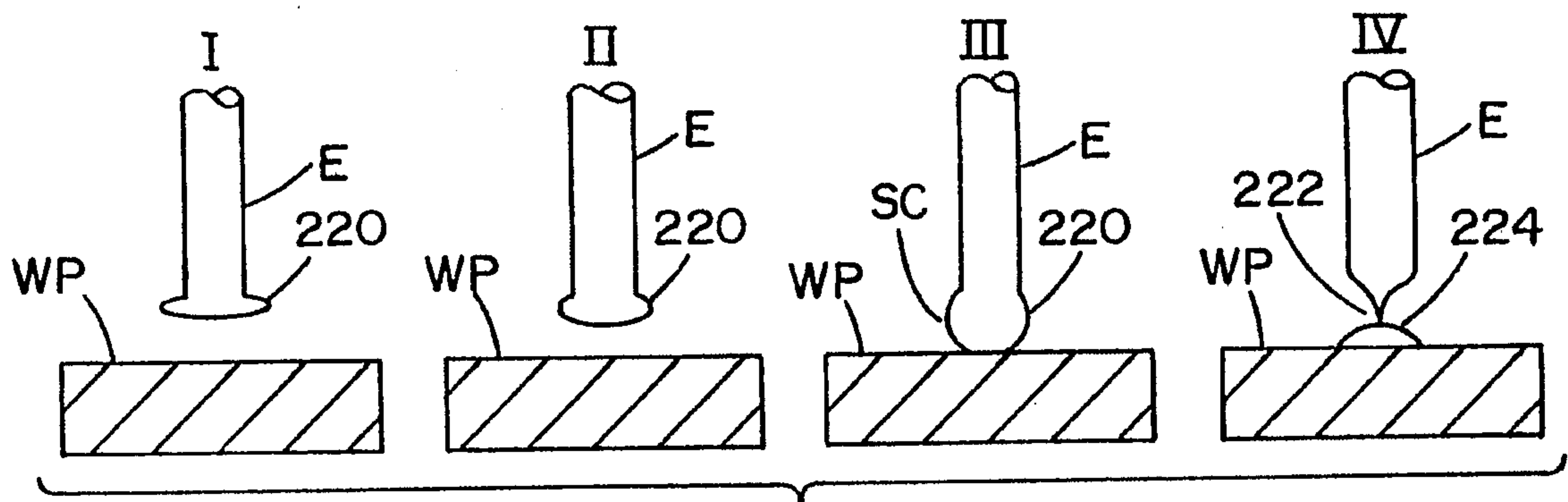


FIG. 2

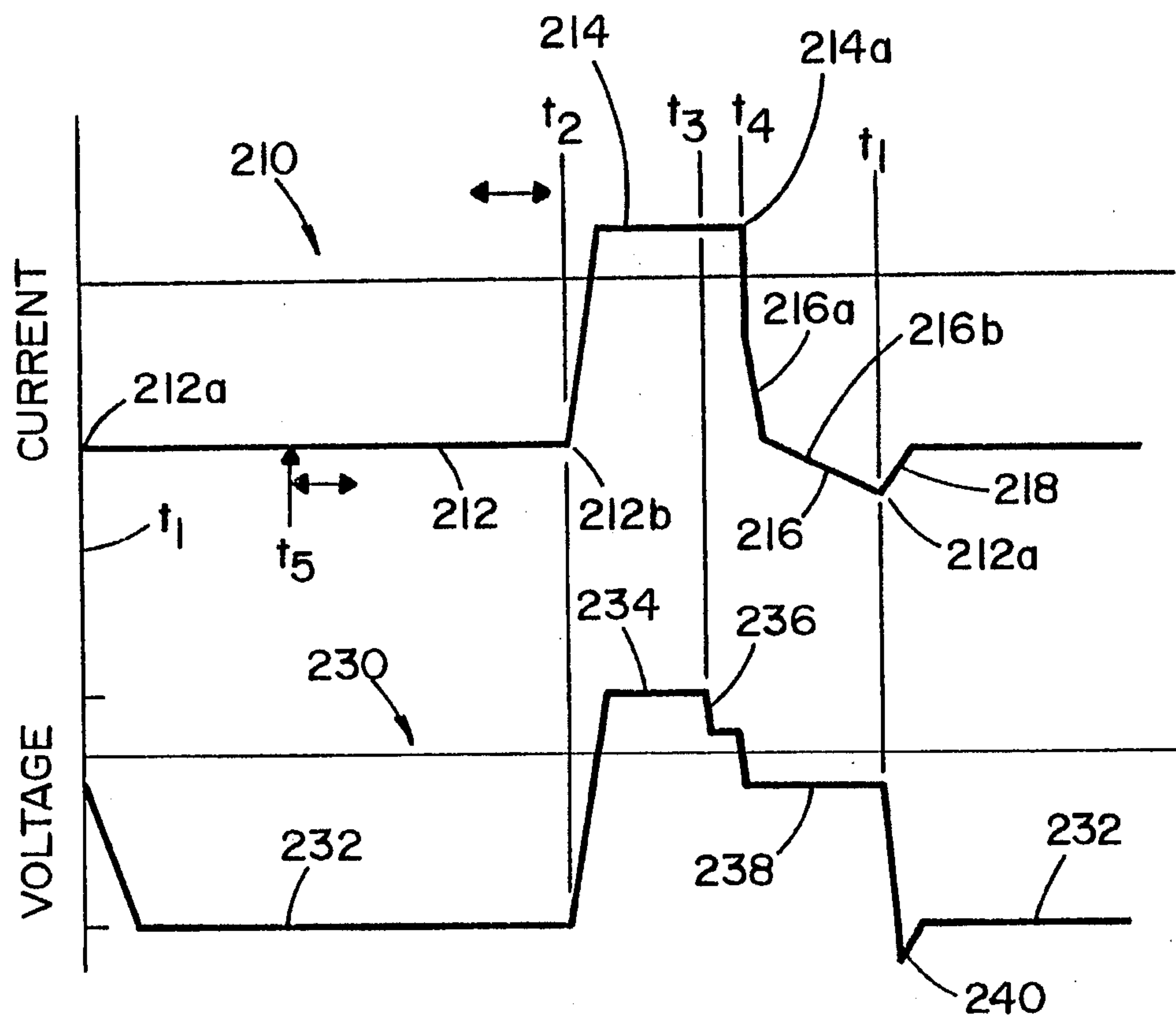


FIG. 3

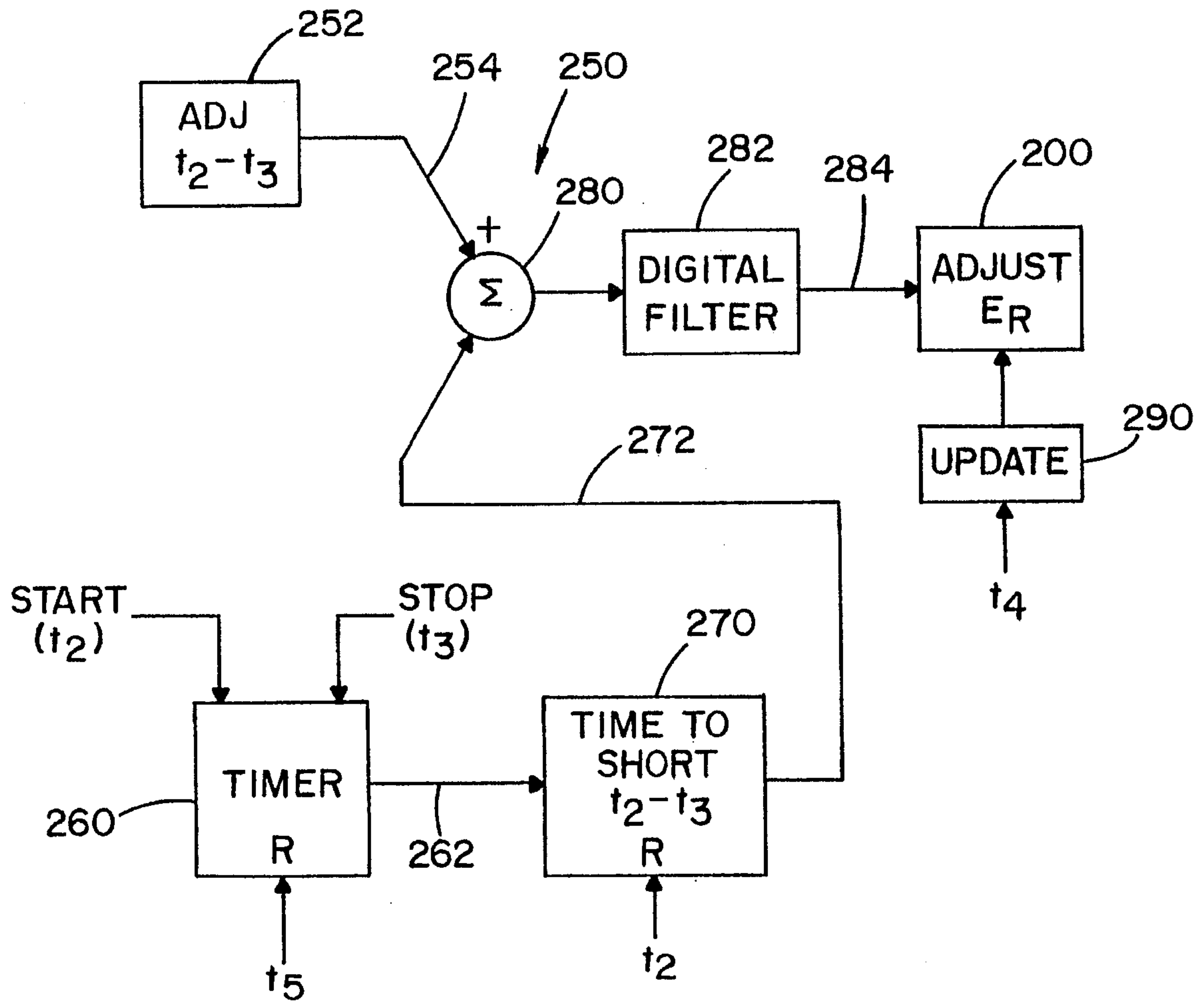


FIG. 4

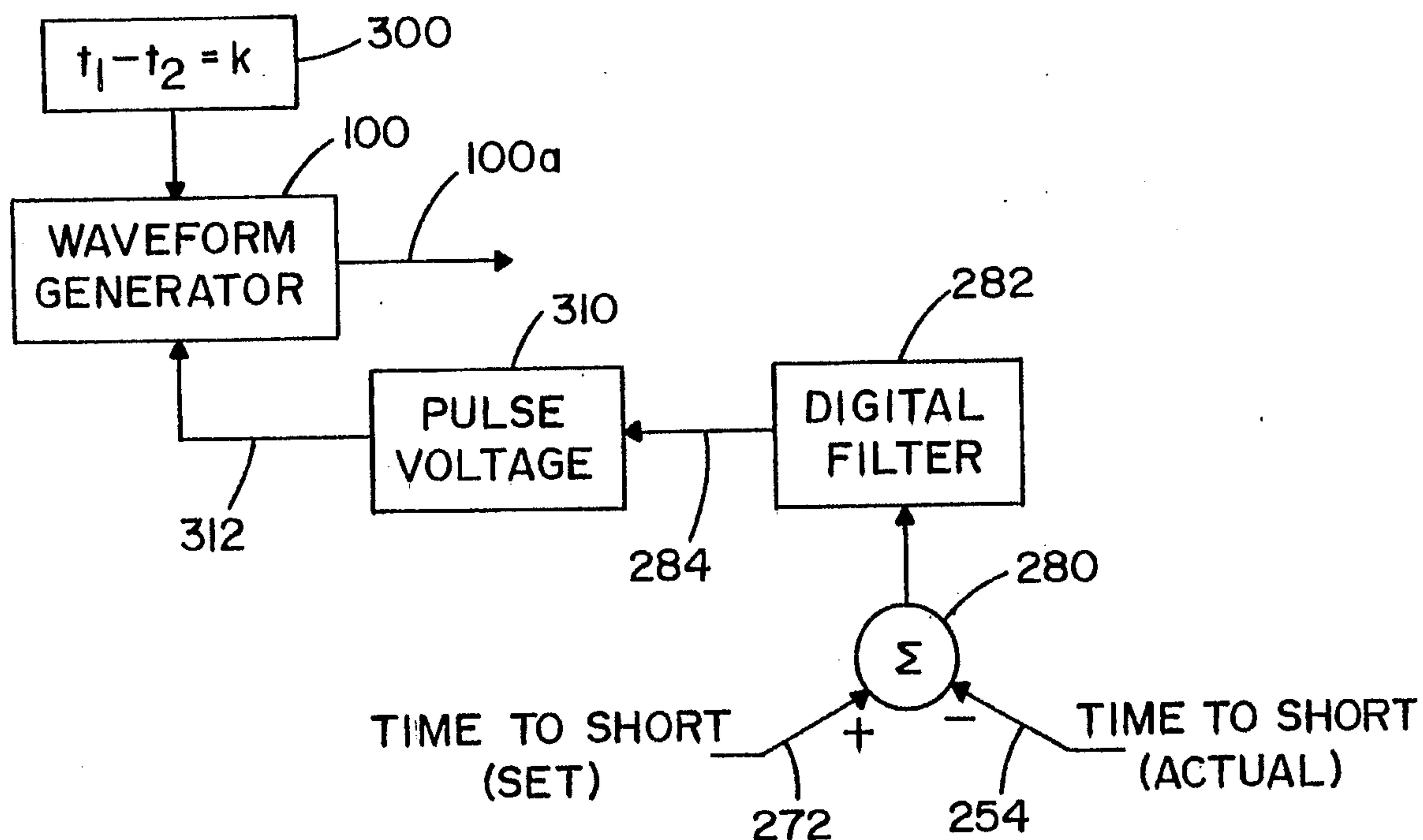


FIG. 5

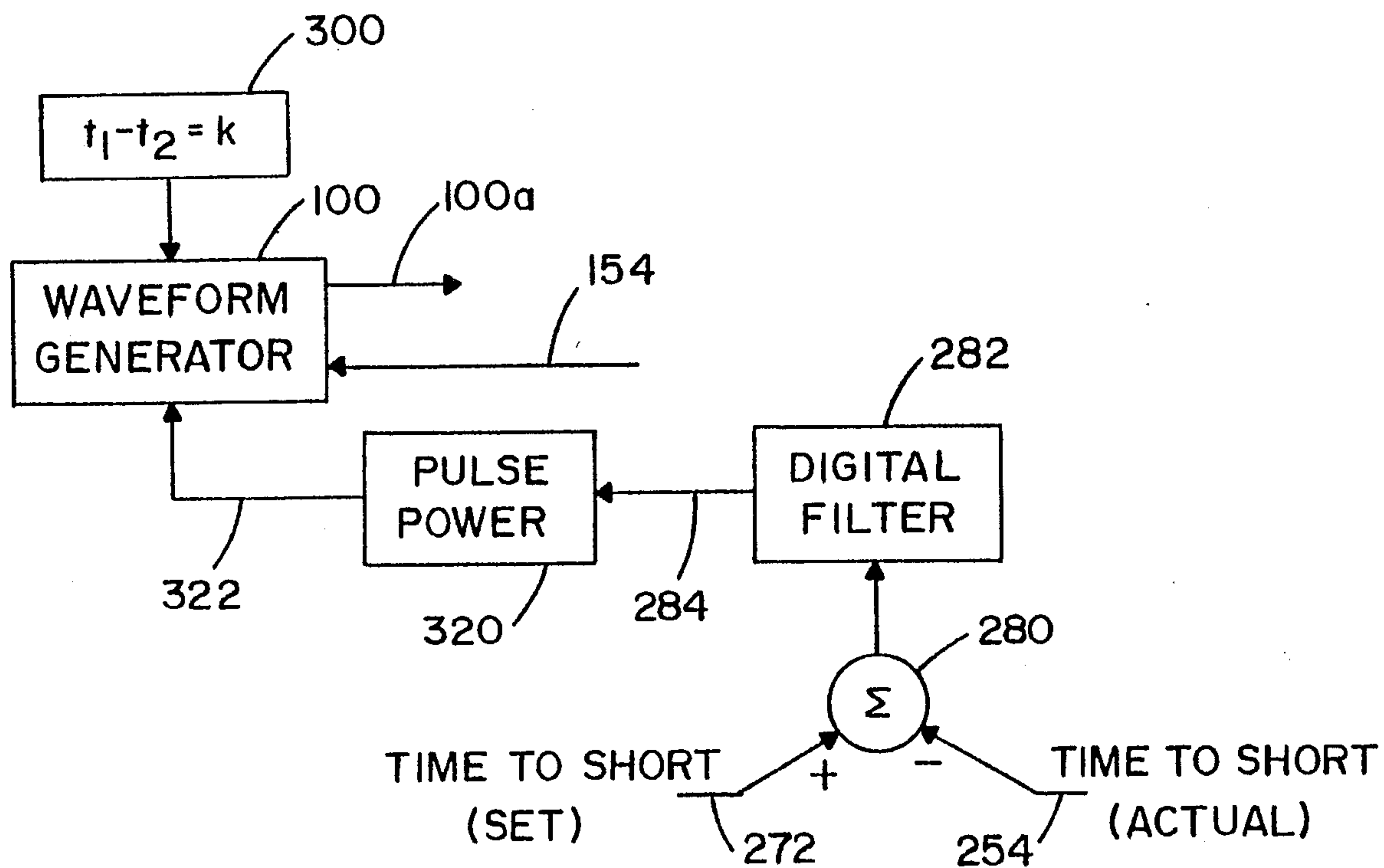


FIG. 6

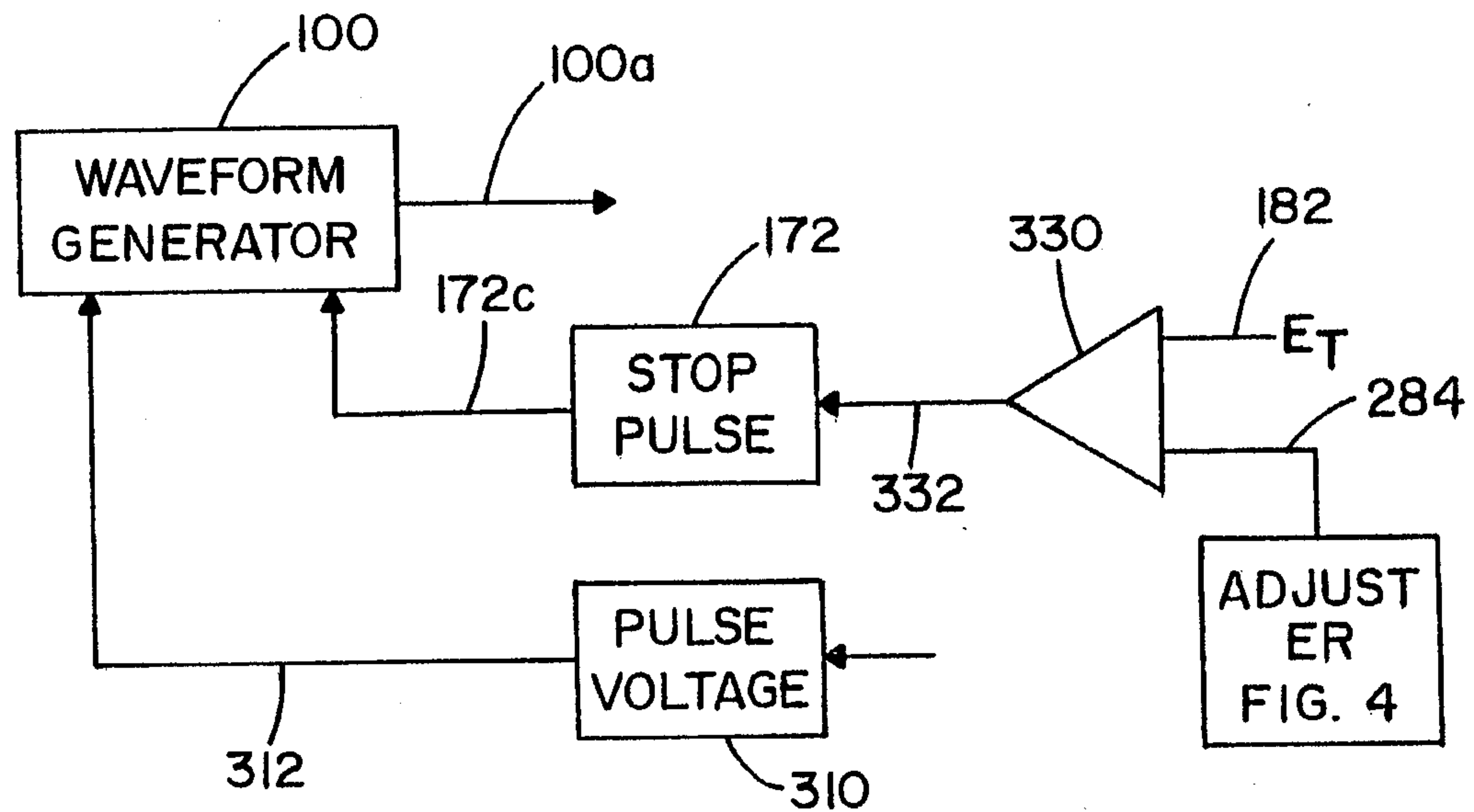


FIG. 7

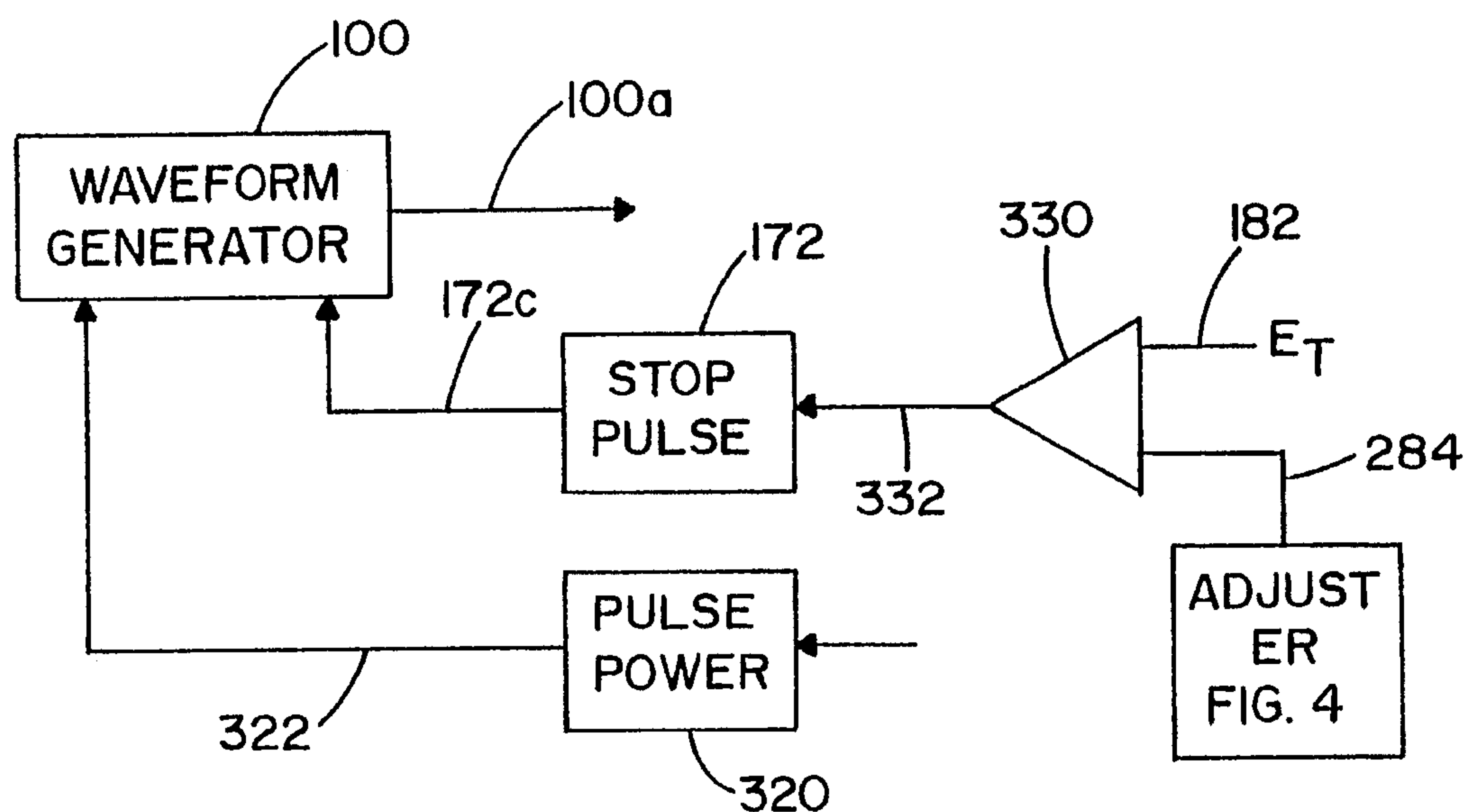


FIG. 8

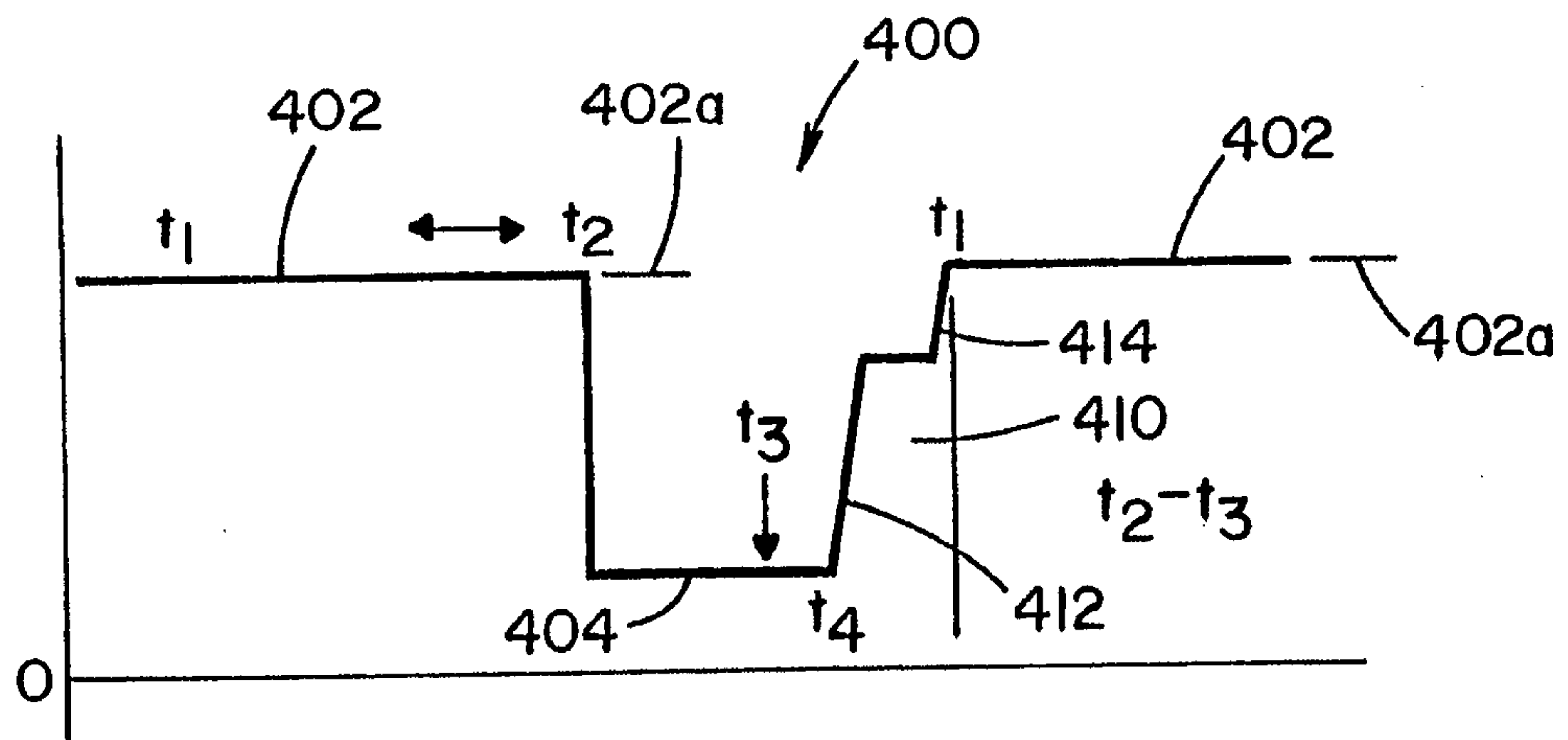


FIG. 9

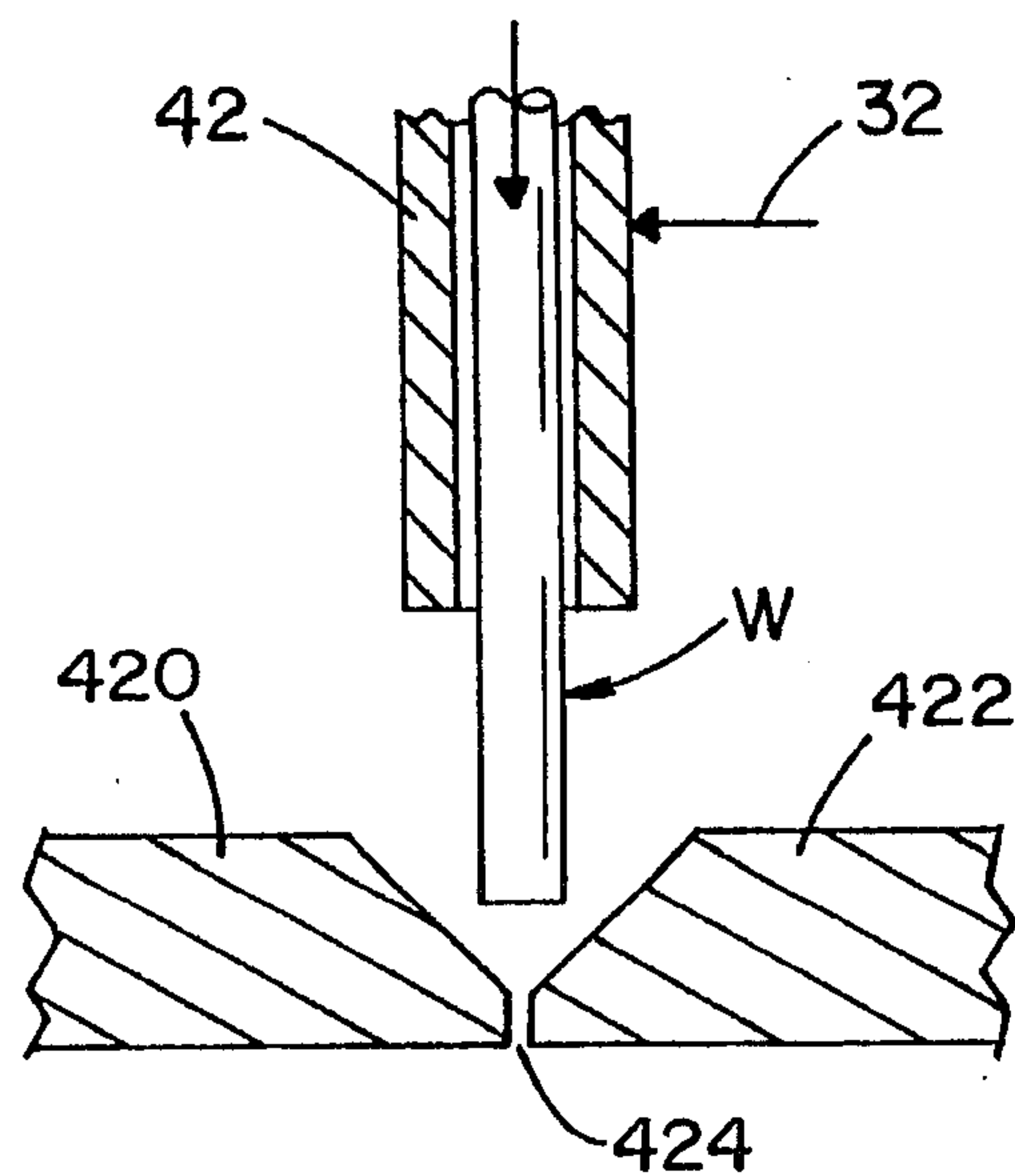


FIG. 10

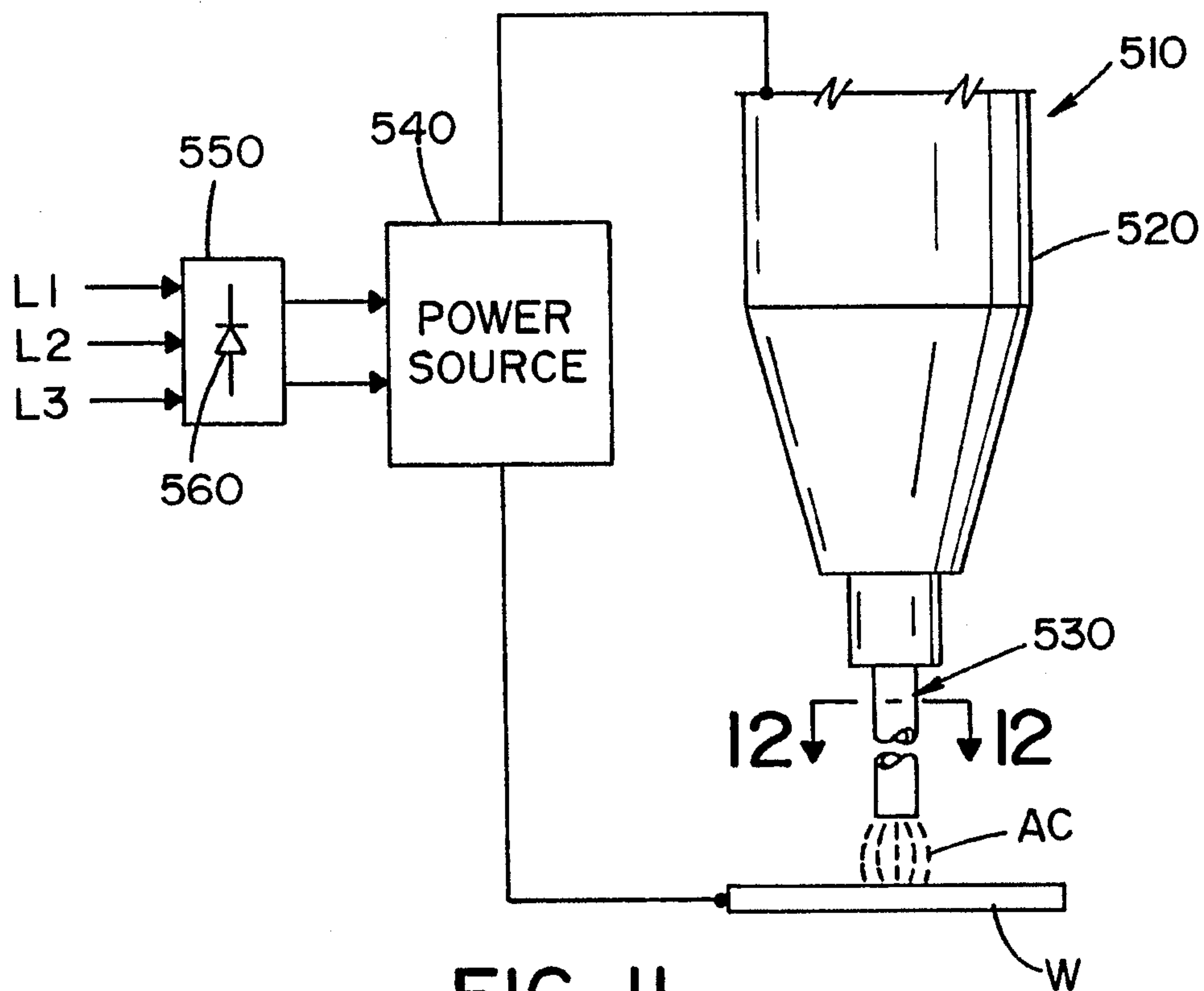


FIG. 11

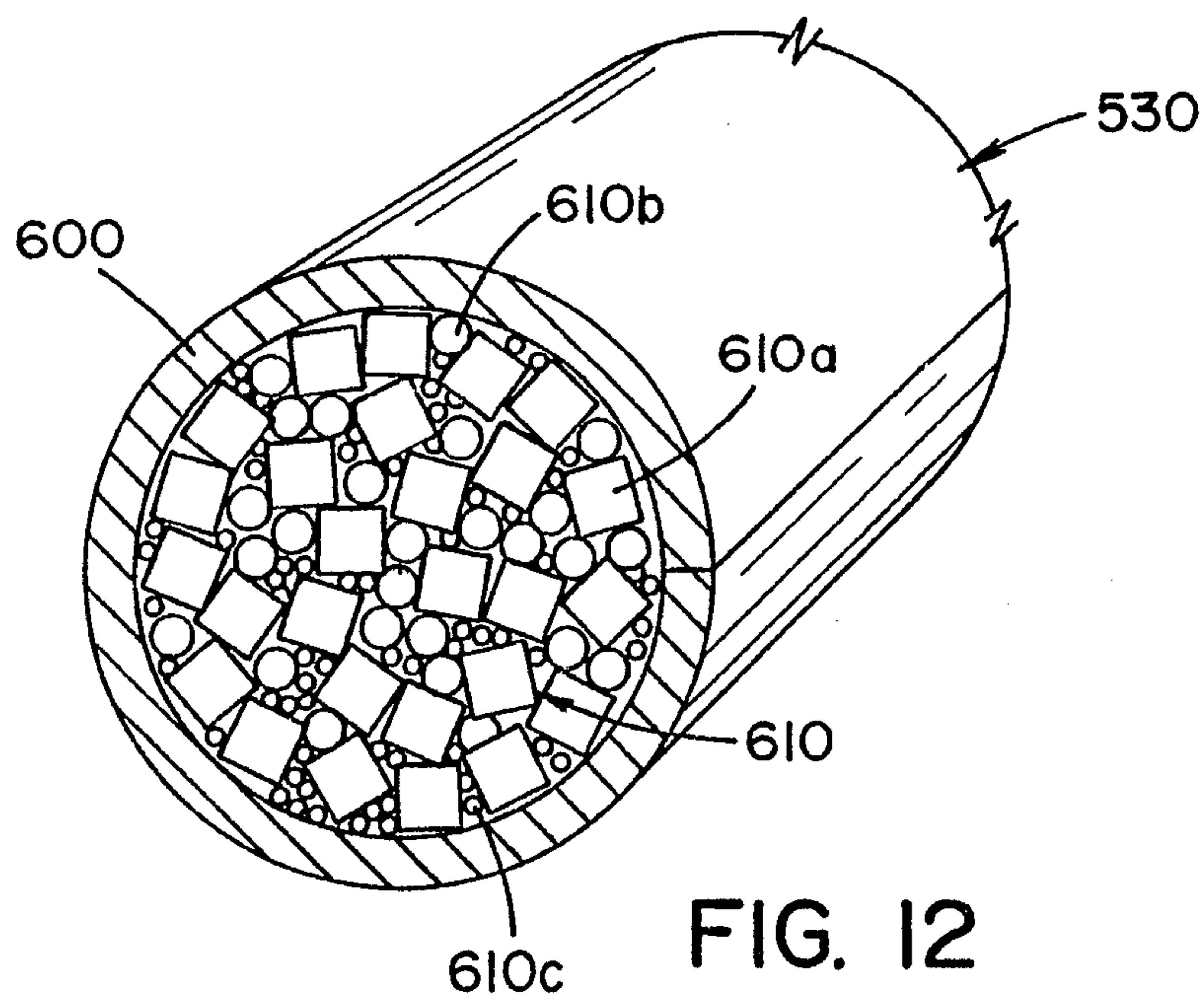


FIG. 12

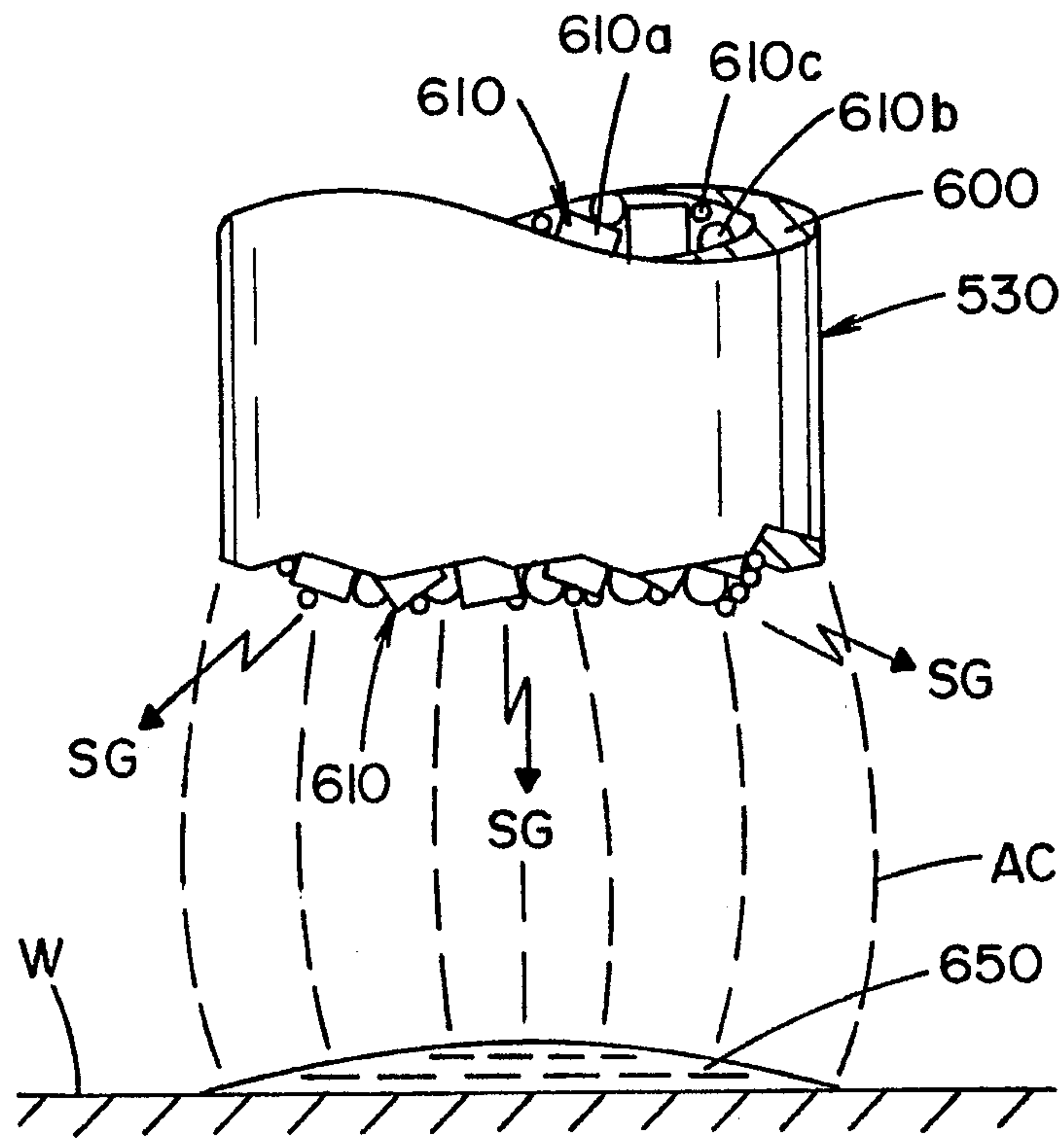


FIG. 15

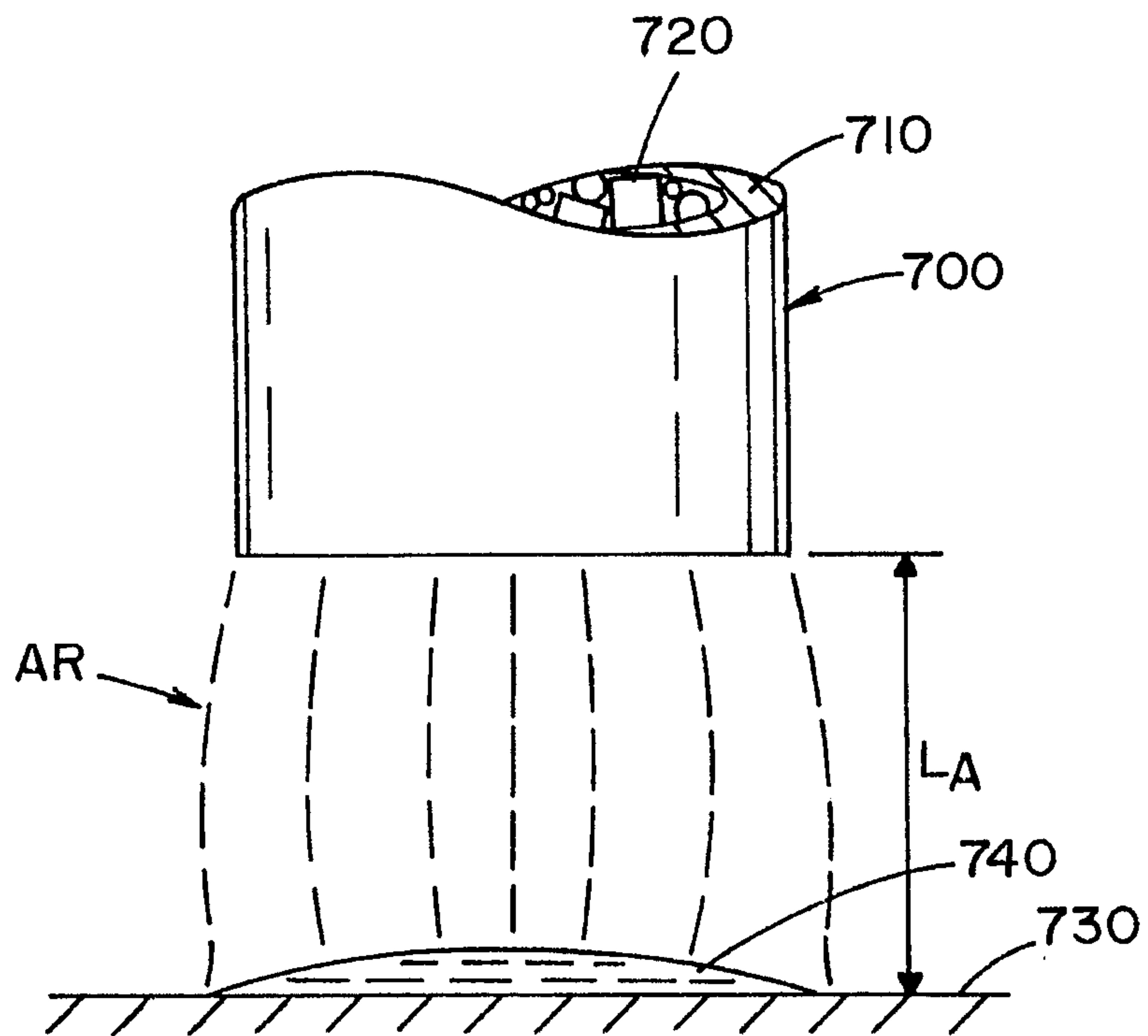


FIG. 16

