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CASTOR OIL LUBRICATING COMPOSITION

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This invention consists in improvements in the treatment of castor oil and related materials particularly to inhibit oxidation and/or "drying," gumming or hardening of such materials.

It is well known that castor oil, while possessing excellent lubricating properties, possesses the serious disadvantages of being prone to fairly rapid oxidation by atmospheric oxygen, leading to what is known as "drying," namely the hardening of the oil to form a solid resinous product or a sticky gum.

The rate of oxidation of fatty oils depends on the types of fatty acids present and particularly on their degree of unsaturation. The principal constituents of castor oil are the glycerides of ricinoleic acid, a hydroxy-substituted unsaturated fatty acid containing one ethylenic linkage. The oxidation which takes place is almost certainly accompanied by a polymerisation process in which the unsaturated molecules take part. The rate of oxidation and gum formation will, of course, depend on the temperature to which the oil is subjected and the presence of oxidation catalysts.

The invention relates not only to castor oil but to related materials such as the esters of ricinoleic acid, e. g., the simple esters of monohydric alcohols and the polyhydric alcohol esters, to lubricants consisting of mixtures of castor oil and mineral oil (comprising a major proportion of castor oil) and to the so-called castorbase greases containing a major proportion of castor oil.

It is one particular object of this invention to provide lubricating compositions suitable for use in internal combustion engines and for the lubrication of bearings, gears, etc. in which castor oil is the major ingredient. It is known to employ easter oil or mixtures of castor oil with minor amounts of mineral oil as lubricants in a variety of applications and especially in the lubrication of motor car and motor cycle engines where high speeds and severe operating conditions obtain. The excellent lubricating properties and high load-carrying capacity of 45

such lubricants are well known, but they suffer from the serious disadvantage of gum formation due to oxidation and polymerisation. Furthermore the free acid normally present to some extent in castor oil and the acidic products produced on oxidation are liable to cause corrosion of composite metal (e. g. copper-lead) bearings under operating conditions.

It is accordingly an object of this invention to provide lubricants consisting of castor oil or mixtures of castor oil and mineral oil in which the castor oil is present in a major proportion, which lubricants have substantially increased resistance to oxidation and gum-formation under operating conditions and which are also relatively non-corrosive to composite metal bearings.

Other practical uses of this invention will be obvious to those who are familiar with the industrial uses of castor oil. Thus castor oil and blends of castor and mineral oil are used extensively for the lubrication of automotive and industrial gears. In such instances the question of corrosion does not arise, but resistance to gum formation is of great importance.

It is already known to inhibit the oxidation of fatty oils by the addition of various organic compounds of which the phenols (especially the polyhydric phenols) and the aromatic amines are examples.

Such compounds, however, suffer from the disadvantage that their effect is only of comparatively short duration.

We have found that very much more effective resistance to oxidation and gum-formation can be obtained in the case of castor oil by the addition of a mixture of (a) an organic compound of tin or antimony and (b) an aromatic or heterocyclic secondary mono- or poly-amine containing at least three cyclic nuclei, at least two of which nuclei are aromatic nuclei attached directly to the nitrogen atom.

gines where high speeds and severe operating conditions obtain. The excellent lubricating properties and high load-carrying capacity of 45 This invention in its broadest aspect therefore consists of a method of treating an oil of the kind described to inhibit oxidation and gumming which method consists in adding to the oil

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(a) a very small proportion of an organic compound of tin or antimony and (b) a very small proportion of an aromatic or heterocyclic secondary mono- or poly-amine containing at least three cyclic nuclei at least two of which nuclei are aromatic nuclei attached directly to the nitrogen atom.

Typical formulae representative of the types of amines suitable for use in accordance with the present invention are:

Xylyl- $\beta$ -naphthylamine

 $\begin{array}{c} R_1-NH-R_2 \\ R_1-NH-R_3-NH-R_4 \end{array}$ 

 $Di(\beta$ -naphthyl)-p-phenylene diamine

where R<sub>1</sub>, R<sub>3</sub> and R<sub>4</sub> are the same or different and are aromatic radicals, and R<sub>2</sub> is a condensed 25 aromatic nucleus having at least ten carbon atoms. Any or all of these radicals may be further substituted by alkyl, aryl, hydroxyl or amine groups, although the preferred substituents are hydrocarbon radicals only.

Specific examples of amines which may be employed are:

Phenyl-\$-naphthylamine

Phenothiazine

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Phenyl-α-naphthylamine

Thio-phenyl-β-naphthylamine (benzonaphthothiazine)

ββ-Dinaphthylamine

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We have found surprisingly that only amines of the type described are effective for the purpose of the present invention, such closely refool lated amines as  $\alpha$ - and  $\beta$ -naphthylamine and diphenylamine being virtually without antioxidant effect.

The organic compounds of tin or antimony to be employed in conjunction with the amines 65 already described are derivatives of divalent (stannous) tin or of antimony and may be the tin or antimony salts or soaps of organic carboxylic acids, organic sulphonic acids, organic dithiophosphoric acids, or the tin or antimony 70 derivatives of phenols, phenol thioethers, or mercaptans. In the present specification and claims all of such compounds including the derivatives of phenols, phenol thioethers and mercaptans are considered to be salts of organic acidic compounds capable of salt formation.

Tin laurate

Tin oleate

Tin naphthenate

Tin petroleum sulphonate

Tin derivative of p-tertiary amyl phenol thioether

Tin derivative of o-stearyl phenol thioether

Tin salt of ethylene glycol mononaphthenate cresyl dithiophosphate

where R.COOH=naphthenic acid.

It will be understood that the compounds selected must be soluble in the particular oil in the proportion in which they are to be employed.

We have found that whereas the tin compounds do not themselves possess any appreciable anticoxidant or gum-inhibiting properties, they cooperate with the aromatic amines of the type described to give inhibition of oxidation over a period of time considerably longer than could be obtained by the use of the amines themselves in 65 comparable proportions. In this respect the petroleum sulphonates of tin and antimony are particularly effective.

The aromatic amines used in this invention may be employed in amounts ranging from about 70 0.1 to about 5.0 per cent and preferably between 0.5 and 2.0 per cent depending on the particular material to be inhibited, and the conditions under which it is to be employed while the tin or antimony compounds may be employed in amounts 75

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varying between about 0.05 and 2.0 per cent and preferably between 0.1 and 1.0 per cent. In general the best results are obtained when the amount of tin or antimony compound present does not exceed the amount of amine by weight and preferably the amount of amine employed is at least double the amount of tin or antimony compound.

In certain applications, notably the lubrica-10 tion of internal combustion engines fitted with composite metal (e.g. copper-lead) bearings, the inhibition of the corrosion of said bearings at elevated temperatures becomes of importance.

We have found that whereas the combinations 15 of additives already described possess excellent anti-oxidant properties they are not effective in retarding bearing corrosion appreciably.

By the addition of a third additive (c), however, not in itself effective to any great extent in reducing such corrision produced by fatty acids and acidic oxidation products of castor oil, we have found surprisingly that a very substantial reduction in corrosion can be effected.

The additives falling within class (c) which 25 may be employed where necessary in conjunction with the additives of classes (a) and (b) comprise the neutral organic phosphite esters of hydroxy-substituted aromatic thioethers and disulphides.

30 Specific examples of such phosphite esters are di-(3-carbomethoxy-4-hydroxy phenyl) thioether cresyl phosphite, and the phosphite ester of t-butyl cresol thioether. These materials may be employed in amounts ranging from about 0.2 to about 5.0 per cent and preferably from 0.5 to 2.0 percent.

If desired, further additives may be present in the compositions of this invention. Thus it may be desirable in certain instances to add viscosity index improvers, foam inhibitors, detergents, or ferrous metal corrosion inhibitors.

In particular we have found that certain additional benefits may accrue from the use in conjunction with the three types of additives already described of the reaction products of aldehydes or ketones with basic water-soluble primary or secondary amines.

We have found, for example that the addition of di-morpholinyl phenyl methane to a castor oil-mineral blend containing additives of types (a), (b) and (c) improved both its resistance to oxidation and its anti-corrosive properties. Advantage may accrue from the employment in certain instances of an antioxidant additive effective at high temperatures, along with the additives of the present invention. Such an antioxidant might be, for example, the metal salt of an organic dithiophosphoric acid or the metal derivative of an alkylated phenol thioether.

Lubricating oil compositions typical of those falling within the scope of the present invention are:

(1) Firsts castor oil

+0.5% phenyl- $\beta$ -naphthylamine

+0.2% tin petroleum sulphonate

(2) 90% acidless castor oil

10% mineral lubricating oil of viscosity 500'' Redwood at 140° F.

+1.0% phenyl- $\beta$ -naphthylamine +0.2% tin petroleum sulphonate

+ 1.0% phenyl-β-naphthylamine
0.2% tin petroleum sulphonate
2.0% di (3-carbomethoxy - 4 - hydroxyphenyl) thioether cresyl
phosphite

0.2% dimorpholinyl phenyl methane

By "tin petroleum sulphonate" is meant the tin salt of the oil-soluble petroleum sulphonic acids commonly known as "mahogany acids."

The following series of tests were carried out 1 to determine the effectiveness of the compounds of the present invention:

# A. GUMMING TESTS AT 120° C.

One drop of the oil was placed in the centre of a watch-glass and heated at 120° C. in an oven for a prolonged period. At intervals the watch glasses were withdrawn, allowed to cool and the liquid examined for signs of tackiness or gum formation.

The majority of the test results quoted were the mean of two or more such tests.

Table 1.—Tests in this table serve to illustrate the surprising advantage of the use of the combination of two additives of the present invention over that of either additive used separately. A blend of:

90% acidless castor oil 10% mineral lubricating oil of viscosity 500'' Redwood at 140° F. (Oil A)

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was used as a basis for experimentation.

Table 2.—Tests in this table illustrate the range of tin and antimony compounds which may be employed in conjunction with a typical amine.

A blend of (90% acidless castor oil and 10% mineral lubricating oil of viscosity 500" Redwood at 140° F.—Oil A)+phenyl-β-naphthylamine (PBN) was employed throughout.

Table 2

10	1 6000 2						
				Approximate time (hours) to—			
15 Test of P		Amount of PBN present, percent	Metal compound added	Inci- dence of tacki- ness	Gum forma- tion		
				100	125		
20	1	1.0	None	320	440		
	2	1.0	Tin petroleum surphonate (0.276)	170	185		
	3	1.0	Tin naphthenate (0.2%)	125	145		
	4	1.0	Tin oleate (0.2%)	165	180		
	5	1.0	Tin derivative of p-tertiary amyl phenol thioether (0.2%).	200			
				80	90		
	6	0.5	None Tin petroleum sulphonate (0.2%)	157	190		
0.5	7	0.5	Tin perforeum surphonate (0.2707)	120	130		
25	8	0.5	Tin laurate (0.2%) Tin derivative of o-stearyl	130	155		
	9	0.5	Tin derivative of o-stearyl phenol thioether (0.2%).		1		
	10	0.5	Tin salt of ethylene glycol mononaphthenate cresyl di-	115	125		
	11	0.5	thiophosphate (0.2%). Antimony petroleum sulpho-	160	180		
30	12	0.5	nate (0.2%). Antimony naphthenate (0.2%)	120	135		
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While, therefore, benefit accrued from the use of a wide variety of tin and antimony compounds, the petroleum sulphonates were outstandingly effective.

Table 3.—Tests in this table illustrate the types of amines which may be employed in carrying out the present invention, in addition to those already cited in Table 1. The same blend was used as before.

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Table 3

Table 1						
	Ad	Approx time (b	iours)	50	Test No.	
Test No.	Amine	Tin or antimony compound	Incl- dence of tacki- ness	Gum forma- tion	55	1 2 3
1	Nonedo	None	18 18	33 23		5
3	Phenyl-\$-naph-	phonate (0.2%).	110	125	60	
V	thylamine (1%). Phenyl- $\beta$ -naph-thylamine	dò	80	90		8 9
5	(0.5%). Phenyl-β-naph-	Tin petroleum sul-	320	440		
	thylamine (1%). Phenyl- $\beta$ -naph-thylamine	phonate (0.2%). Tin petroleum sul- phonate (0.2%).	157	190	65 <sup>-</sup>	
7	(0.5%). Phenyl- $\beta$ -naph- thylamine	Tin petroleum sul- phonate (1.0%).	156	200		r tive
8	(1.0%). Phenyl-8-naph- thylamine (0.5%).	Antimony petroleum sulphonate (0.2%).	160	180	70	nes
9	(0.5%). Phenyl-α-naph- thylamine	None	115	135	10	of
10	(1.0%).	Tin petroleum sul- phonate (0.2%).	160	185	i	hib of
	(1.070).	]	1	1		

Approximate time (hours) to— Tin petro-leum sulpho-Amine nate Incidence of forma-tion tackiness 200 180\_\_\_\_\_ ββ-Dinaphthylamine 0.2 (0.5%). Xylyl-8-naphthylamine (0.5%). 160 0.2(0.5%).
Phenothiazine (0.5%)—
Benzonaphthothiazine
Diphenylbenzidine (saturated solution, less than 0.5%).
Di β-naphthyl-p-phenylene diamine (0.5%).
β-Naphthyl mine (0.5%).
Diphenylamine (0.5%).
Triphenylamine (1.0%)— 220 225 Over 320\_\_\_\_ 0.2 320 . . . . . . . 345 Less than 60.

The last three results are quoted for comparative purposes to illustrate the relative ineffectiveness of certain amines closely related to those of the present invention.

Table 4.—Tests in this table illustrate the range of ricinoleic acid derivatives which may be inhibited against gum formation by the additives of the present invention, and also the use of supplementary additives

75 plementary additives.

#### Table 4

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Test No.	Material inhibited	Inhibitors added	Approxi (hou	mate time
			Incidence of tacki- ness	Gum forma- tion
1	Firsts castor oil	None		
2	do	[1% Phenyl-6-naphthylamine	21	2
3	\$90% acidless castor oil	10.2% Discarbomethoxy-4-hydroxy-phenyl)thioether cresyl phosphite	400	44
4	10% mineral oil A 90% acidless castor oil. 10% mineral oil A	None [1% phenyl-\$-naphthylamine] [0.2% tin petroleum sulphonate]	18	3
5	(90% acidless castor oil	12% d1(3-carbomethoxy-4-hydroxyphenyl) cresyl phographic	230	25
3	10% mineral oil A  Butyl ricinoleate	None	250	275
3	Glyceryl diricinoleate	1% phenyl-\$\textit{\mathcal{B}}-naphthylamine_ As No. 7 with the addition of 0.2% tin petroleum sulphonate None	54 235 255	285
.0	do	[1% phenyl-g-nanhthylamine	205	40
		0.2% tin petroleum sulphonate	120	175

#### B. CORROSION TESTS

The following test was employed for obtaining information as to the tendency for corrosion of composite metal bearings, particularly copperlead bearings, to occur in use of lubricating compositions provided by the present invention.

400 ml. of lubricant was weighed into 1500 ml. tall lipless glass beakers, eight of which were heated in a circular electrically heated oil bath thermostatically controlled to maintain the lubriequipped with closely fitted aluminium covers having central slides which were normally closed but capable of being opened for the insertion of a test specimen. The slides when closed allowed sufficient clearance for centrally placed steel stir- 40 ring rods to revolve freely. The latter were electrically driven from a common driving shaft at  $400\pm40$  R. P. M. and carried at their lower end

Tests were conducted for 12 hours in two periods of six hours, the copper and lead specimens being removed every two hours and replaced by fresh clean ones. Copper catalysts were cleaned with carborundum powder and washed in petroleum ether. Lead specimens were flattened, scraped with a special scraper and finally polished by brushing in one direction with file carding before washing in benzene and weighing. After a 2 hour period a further washing in bencant temperature at 140° C. The beakers were 35 zene, brushing with a camel hair brush and reweighing was effected. The total corrosion was calculated by adding together the weight losses of the lead specimens after each two-hour period.

The following test results illustrate the effectiveness of the hydroxyaryl thioether phosphites in conjunction with the other additives of the present invention, in inhibiting corrosion of lead at elevated temperatures.

Table 5

Test No.	Oil	Additives		Lead specimen weight loss (cumulative) after—			
			2 hours	4 hours	6 hours	12 hours	
1	\$\frac{90\%}{10\%}\$ acidless castor oil \$\frac{10\%}{90\%}\$ acidless castor oil	None	58	153			
2	(10% mineral oil A	0.5% phenyl-\$-naphthylamine 0.3% tin petroleum sulphonate 1.0% phenyl-\$-naphthylamine	264	371			
3	10% mineral oil A	0.2% tin petroleum sulphonate 2.0% di(3-carbomethoxy-4-hydroxy-phenyl) thioether cresyl phosphite. 0.2% dimorpholinyl phenyl methane	4	37	81	20	
	\$90% acidless castor oil 10% mineral oil A	(1.0% phenyl-\$-naphthylamine 0.2% tin petroleum sulphonate 2.0% tertiary butyl cresyl thioether phosphite (1.0% phenyl-\$-naphthylamine	6	102	263		
	\$90% acidless castor oil 10% mineral oil A	0.2% tin petroleum sulphonate 1.0% di(3-carbomethoxy-4-hydroxy-phenyl)thioether cresyl phosphite. 1.0% zinc di(\alpha-methyl isoamyl) dithiophosphate	13	25	42	13	

slotted holders to which lead test pieces were 65 attached by means of screws. For the test-pieces rectangular plates of pure lead 134" by 1" were mounted vertically just below the surface of the lubricant with the longer axis horizontal. Copper strips, as catalysts,  $\frac{1}{2}$ " wide and bent into a semi- 70 circle 334" in diameter were placed wholly below the surface of the lubricant and attached by means of vertical copper wires to corks fitted in the beaker covers. Each beaker was also fitted with a thermometer.

### C. ENGINE TESTS

Tests were carried out in a standard H-2 type Lauson engine under the following conditions:

Jacket temperature Oil sump temperature Test duration	
Test duration	60 hours.

The following test results illustrate the effectiveness of certain of the compositions contem-75 plated in the present invention as lubricants for

internal combustion engines operating under severe conditions:

Table 6

		Piston		Used oil	5	
Test No.	Lubricant	rating (C. R. C. vis- ual rating)	Bearing weight loss, mgs.	Percent vise. inc.	Acidity (mgs. KOH per gm.)	10
1	87.5% acidless castor oil   12.5% mineral oil B   12.5% phenyl-β-naph-	8.7	513	285	5. 2	
2	thylamine). 0.2% tin petroleum sulphonate). 2% di(3-carbomethoxy-4-hydroxyphenyl) thioether cresyl phosphite. 0.2% dimorpholinyl	8. 2 (I	68 Mean figt	156 1res—2 te	5.0. (sts)	15
3 4	(phenyl methane. 187.5% firsts castor oil	8.5 8.3	103	1	6. 5	~

In tests 1 and 3 there was a very heavy buildup of soft black gum on the neck of the inlet valve. In tests 2 and 4 the amount of deposit on the inlet valve was extremely light.

Oil B was a mineral lubricating oil of viscosity.

44'' Redwood at 140° F. The method of rating piston cleanliness was 30 that adopted by the Co-ordinating Research Council (C. R. C.) in which a perfectly clean piston is given a rating of 10 and a perfectly black piston a rating of zero.

We claim:

- 1. A lubricating composition comprising a major proportion of castor oil in which is incorporated a proportion of from 0.05% to 2.0% of a metallic organic compound soluble in castor oil and selected from the group consisting of tin and  $_{40}$ antimony salts of aliphatic monocarboxylic acids having 12 to 18 carbon atoms, organic sulphonic acids, naphthenic acids, and phenol thioethers and a proportion of from 0.1% to 5.0% of an aromatic secondary amine containing at least three cyclic nuclei, at least two of which nuclei are aromatic nuclei attached directly to the nitrogen atom.
- 2. A lubricating composition as claimed in claim 1 in which the amine is selected from the group consisting of a compound represented by the general formula

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where R1, R3 and R4 are aromatic radicals and R<sub>2</sub> is a condensed aromatic nucleus having at 60 least ten carbon atoms.

3. A lubricating composition as claimed in claim 1 in which is incorporated a proportion of from 0.2% to 5.0% of a neutral organic phosphite ester of a hydroxy-substituted aromatic thio- 65 ether.

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- 4. A lubricating composition as claimed in claim 1 in which is incorporated a proportion of from 0.2% to 5.0% of a neutral organic phosphite ester of a hydroxy-substituted aromatic disulfide.
- 5. A lubricating composition as claimed in claim 1 comprising also a minor proportion of a further lubricant additive selected from the group consisting of the reaction product of an aldehyde with a basic water-soluble amine and the reaction product of a ketone with a basic watersoluble amine.
- 6. A lubricating composition as claimed in claim 1, comprising also a proportion of up to  $12\frac{1}{2}\%$  of a mineral oil.
- 7. A lubricating composition comprising a major proportion of castor oil in which is incorporated a proportion of from 0.05% to 2.0% of a castor oil soluble tin salt of an organic sulphonic acid and a proportion of from 0.1% to 5.0% of 0 an aromatic secondary amine containing at least three cyclic nuclei, at least two of which nuclei are aromatic nuclei attached directly to the nitrogen atom.
- 8. A lubricating composition comprising a ma-25 jor proportion of castor oil in which is incorporated a proportion of from 0.05% to 2.0% of a castor oil soluble antimony salt of an organic sulphonic acid and a proportion of from 0.1% to 5.0% of an aromatic secondary amine containing at least three cyclic nuclei, at least two of which nuclei are aromatic nuclei attached directly to the nitrogen atom.
  - 9. A lubricating composition comprising a major proportion of castor oil in which is incorporated a proportion of from 0.05% to 2.0% of tin petroleum sulphonate and a proportion of from 0.1% to 5.0% of an aromatic secondary amine containing at least three cyclic nuclei, at least two of which nuclei are aromatic nuclei attached directly to the nitrogen atom.
  - 10. A lubricating composition comprising a major proportion of castor oil in which is incorporated a proportion of from 0.05% to 2.0% of antimony petroleum sulphonate and a proportion of from 0.1% to 5.0% of an aromatic secondary amine containing at least three cyclic nuclei, at least two of which nuclei are aromatic nuclei attached directly to the nitrogen atom.

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