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(54) Title: THERMOCOUPLE APPARATUS AND METHOD

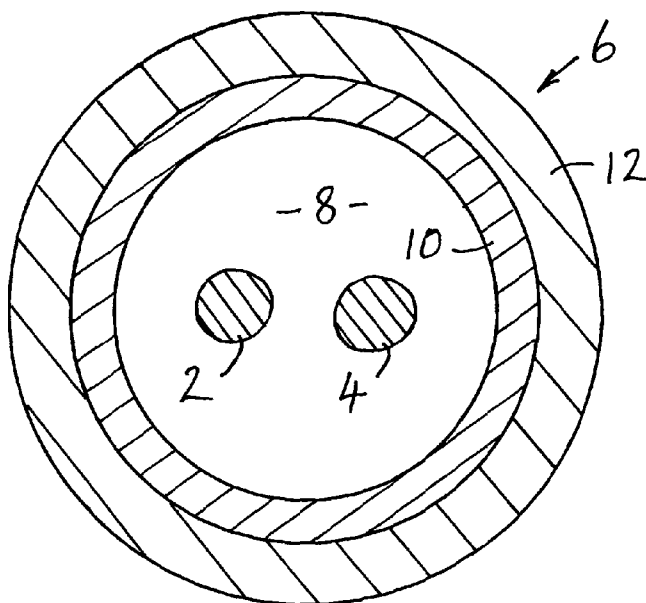


FIGURE 1

(57) Abstract: In a thermocouple, a pair of thermoelements (2, 4) extend within a protective sheath (6). The thermoelements are spaced from the sheath by an insulator (8). The sheath comprises an outer sheath (12) formed from a metal alloy adapted to provide mechanical support and corrosion resistance during use of the thermocouple, typically at elevated temperature. The sheath further comprises an inner sheath (10) positioned between the outer sheath and the thermoelements and formed from a nickel-based alloy containing less than 10wt% Cr, to prevent diffusion of Cr and/or Mn from the outer sheath to the thermoelements.

Thermocouple Apparatus and Method

The invention relates to a thermocouple apparatus and method, and in particular to a Mineral Insulated Metal Sheathed (MIMS) thermocouple.

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MIMS thermocouples are widely used in industry and certain types have become popular as industry standards. For high-temperature applications, these include Type K and Type N thermocouples. However, at elevated temperatures above about 1000C, conventional MIMS thermocouples suffer from two problems, namely oxidation (when used in oxidising atmospheres) and drift, i.e. a change of the measured voltage with time during exposure of the thermocouple to high temperatures, which limits the reliability of temperature measurement. For conventional nickel-based MIMS thermocouples, drift typically worsens above about 1000C. Temperature measurement at temperatures above about 1000C then disadvantageously requires the use of much more expensive thermocouples made of noble metals such as platinum.

In a MIMS thermocouple, positive and negative thermoelements are contained within a tubular metal sheath, and insulated from each other and from the sheath by a compacted ceramic or mineral material (except at the thermocouple tip where the thermoelements are joined together and may, in some thermocouple designs, be in electrical contact with the sheath). The sheath is designed to provide oxidation resistance, i.e. to prevent oxidation of the thermoelements, but it can affect the drift behaviour of the thermocouple. In particular, alloys which optimise the oxidation resistance of the sheath commonly contain manganese, and it is known that migration of manganese from the sheath to the thermoelements due to diffusion at elevated temperature can change the Seebeck coefficient of the thermoelements and so cause drift. This problem is described, for example, in US patent number 5,043,023. This is a particular problem with nickel-based thermocouples, and undesirably limits the high-temperature performance of these thermocouples.

The invention provides a thermocouple and a method as defined in the appended independent claims, to which reference should now be made.

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Preferred or advantageous features of the invention are set out in dependent sub-claims.

In a first aspect, the invention may thus provide a thermocouple in which a thermoelement extends within a metal outer sheath, and a nickel-based inner sheath containing less than 10wt% of chromium is positioned between the thermoelement and the metal outer sheath.

The term nickel-based means that the inner sheath comprises a nickel alloy, which contains nickel as the largest wt% component of the alloy, and is preferably more than 50wt% Ni.

Advantageously, the metal outer sheath may serve to protect the thermoelement, and other components of the thermocouple within the outer sheath, from the environment during operation of the thermocouple. For example, if the thermocouple is for use in an oxidising environment, then the outer sheath may advantageously protect the thermoelement from oxidation. This is a common requirement, for example for thermocouples operating in air at elevated temperatures. For thermocouples operating in other environments, the outer sheath may advantageously be designed to protect the thermoelement from those environments during operation.

It is known, as described above, that manganese contained in the outer sheath of a conventional thermocouple may contaminate thermoelements and cause drift. In addition, the inventor has now appreciated that chromium contained in the outer sheath of a conventional thermocouple may also contaminate thermoelements and cause drift. Many conventional sheaths for MIMS thermocouples are based on nickel-chromium alloys and therefore the inventor has identified a significant problem. In practice, nickel-chromium alloys have properties which are highly desirable for thermocouple sheaths (for example, they show high-oxidation resistance and are mechanically tough), but the inventor has appreciated that use of these materials may limit the high-temperature performance of thermocouples by causing drift, even though they may provide satisfactory oxidation protection. In practice, it may not be

possible to exclude chromium from a thermocouple sheath alloy if adequate oxidation resistance is to be achieved.

In order to increase the maximum operating temperature of a conventional
5 MIMS thermocouple from, say, 1000C to 1200C or more, it is necessary both
to ensure that the thermocouple is adequately protected from the environment
(usually from oxidation) and that drift is prevented. A good environmental
(oxidation) resistance may be achieved by using a conventional oxidation-
resistant alloy for the sheath, but in prior art thermocouples, contamination of
10 the thermoelements by alloying elements in such alloys has then limited the
maximum operating temperature by causing unacceptable drift. The diffusion
barrier provided by the inner sheath of the present invention may
advantageously enable the maximum operating temperature of a MIMS
thermocouple to be increased by preventing or reducing drift. Advantageously,
15 embodiments of the invention may allow operation of a MIMS thermocouple at
1100C or more, or 1200C or more. This may advantageously give operating
temperature ranges from 1100C or 1150C or 1200C up to 1250C or 1300C or
1350C for example.

20 In various aspects of the invention, a number of materials are proposed for the
inner sheath. These include a pure nickel sheath, of greater than 99wt% nickel
or preferably greater than 99.5wt% nickel. An example would be Nickel 270
(UNS N02270/W. Nr. 2.4050). Alternatively, a nickel-based sheath may be
used which does not contain chromium, or contains chromium at less than
25 10wt%, or less than 9wt%, preferably less than 5wt% and particularly
preferably less than 3wt%.

A further preferred alternative is a nickel-based sheath which does not contain
manganese or has a manganese concentration lower than 0.2wt% or 0.1wt%,
30 and also does not contain chromium or has a chromium concentration less
than 10wt%, less than 9wt%, less than 5wt% or less than 3wt%.

A further aspect of the invention may advantageously provide a thermocouple
comprising a nickel-based inner sheath which does not contain manganese or
35 has a manganese concentration lower than 0.2wt%, or preferably lower than

0.1wt%. In this aspect of the invention the inner sheath may comprise 10wt% Cr or more. This inner sheath may be used where contamination of the thermoelement(s) with Mn is to be avoided but where a higher concentration of Cr in the inner sheath, and therefore the possibility of Cr contamination of the thermoelements, may be acceptable.

Each of the inner sheaths described above is formed using a nickel-based alloy comprising a limited concentration of Cr and/or Mn. As described above, the term nickel-based may mean that the alloy contains a higher content (in wt%) of Ni than of any other element. In view of this, the skilled person would be able to fabricate inner sheaths embodying the invention, taking into account the thermal and mechanical properties required for the inner sheath of a thermocouple designed for operation at 1100C or above, or between 1100C and 1200C or even 1300C or 1350C.

In a first preferred embodiment, nickel may form the whole of the balance of the alloy composition except for the Cr and/or Mn content described above, or Ni may form at least 80%, 90%, 95% or 98% of the balance of the alloy composition. Alternatively, the nickel content of the alloy may be greater than 50 wt%, 60 wt%, 70wt%, 80wt%, 85wt% or 90wt%.

Where Ni and Cr and/or Mn do not constitute the only components of the alloy, the balance may comprise one or more of the following:

Fe and/or Co, each up to 49wt%, or preferably up to 40wt%, 30wt%, 20wt% or 10wt%;
Mo up to 25wt%, or preferably up to 15wt%, 10wt% or 5wt%;
W up to 15wt%, or preferably up to 10wt% or 5wt%;
Nb, Ta, V, Ti, Al, Si, Mg, Cu and/or Hf each up to 5wt%, or preferably up to 3wt%, 2wt% or 1wt, up to a cumulative maximum for these elements of 15wt%, or preferably up to 10wt% or 5wt%.

In all cases, as the skilled person would appreciate, the alloy may comprise other trace elements or contaminants at acceptably low concentrations in known manner without affecting the performance of the alloy.

In an embodiment of the invention, a thermocouple may comprise a pair of thermoelements extending within an inner sheath, with the outer sheath encircling the inner sheath. The inner sheath and the outer sheath may be in the form of a pair of concentric or coaxial tubes, which may be in contact with each other. In a preferred embodiment, the inner sheath and the outer sheath may take the form of a double-walled sheath structure, the inner and outer sheaths optionally being formed simultaneously by coextrusion or swaging.

In alternative embodiments, the inner sheath and the outer sheath may be spaced from one another, and optionally insulated from one another.

A thermocouple comprises two or more thermoelements and in aspects of the invention one, two or more thermoelements may extend within the same inner sheath.

In another embodiment, two thermoelements may each extend within one of two separate inner sheaths. In this structure, each inner sheath may advantageously provide a diffusion barrier for its respective thermoelement, not only preventing diffusion of elements from the outer sheath, but also preventing contamination of one thermoelement by diffusion of elements from the other thermoelement.

In embodiments of the invention the thermocouple is preferably a nickel based thermocouple. In such a thermocouple the thermoelements are nickel-based thermoelements, or are formed of Ni alloys, that is alloys which contain Ni as the largest wt% component. Often such alloys may comprise more than 50wt% Ni.

In each case, the provision of the inner sheath as a diffusion barrier between the outer sheath and one or more thermoelements may advantageously enable the design of the outer sheath to be optimised for environmental protection of the thermocouple, without the constraint of avoiding the use of manganese and/or chromium in the outer sheath, which cause thermoelement contamination and drift at elevated temperatures due to the effect of these contaminants in changing the Seebeck coefficient of the thermoelements.

A conventional MIMS thermocouple such as a Type K or Type N thermocouple may be usable to measure temperatures up to about 1000C, but if conventional thermocouple sheaths are used, these thermocouples typically suffer from increasing amounts of drift at higher temperatures, such as 1100C, 1200C, or 1300C. It may be possible to fabricate sheaths for MIMS thermocouples using conventional alloys (such as Inconel 600) to provide oxidation resistance at these higher temperatures but these alloys contain elements which then lead to contamination of the thermoelements at temperatures above about 1000C, causing drift. Inconel 600 is a commonly-used material for conventional thermocouple sheaths, which contains up to 1wt% Mn and usually contains between 0.3wt% and 0.5wt% Mn. Provision of a diffusion barrier in the form of an inner sheath, according to the aspects of the invention described, may advantageously overcome the problem of thermocouple drift when high-temperature-resistant alloys (such as Inconel 600) are used for an outer sheath and enable operation of thermocouples such as Type K or Type N thermocouples, or other thermocouples, including in particular nickel-based thermocouples, at or above higher temperatures, such as 1100C, 1200C or 1300C.

The thickness of the inner sheath needs to be sufficient for the sheath to function as a diffusion barrier or contamination barrier. For example, the sheath thickness may be about 300 micrometres.

The or each thermoelement in each embodiment of the invention is electrically insulated from the or each inner sheath and each other thermoelement, at least along the length of the thermocouple, as required for functionality of the thermocouple. For example, an insulating material may space and insulate the or each thermoelement from the or each inner sheath. For the avoidance of doubt, this reference and other references in this document to the thermoelement(s) being spaced and/or insulated from the inner sheath refer to the length of the thermocouple, or thermocouple wire, excluding the thermocouple tip. At the thermocouple tip, thermoelements of the thermocouple are joined together, in electrical contact, and in some thermocouple designs the thermoelements may be electrically connected to

the outer and/or the inner sheath(s) at the thermocouple tip. For example, in a thermocouple having an ungrounded configuration, the thermoelements may be connected to each other but not to the inner or outer sheath at the thermocouple tip, while in a grounded configuration the thermoelements are electrically connected to the outer and/or the inner sheaths at the thermocouple tip, and the respective inner and/or outer sheaths may be electrically connected to ground or earth.

In implementations of the invention, the outer sheath may be fabricated from any suitable material, without needing to avoid elements which may contaminate the thermoelements. The outer sheath may be nickel-based, or may be based on some other material. In conventional MIMS thermocouples, the sheaths are fabricated by conventional methods for tube fabrication, such as extrusion and/or drawing. In embodiments of the present invention, the inner and outer sheaths may similarly be fabricated by conventional methods for tube fabrication. In a similar way to a conventional MIMS thermocouple, an assembly of the inner and outer sheaths, the thermoelements and the insulating material (such as a ceramic or mineral material) can then be extruded or swaged down to a required size, or diameter, to form a MIMS cable. During this process, the thermoelements and insulation may be fabricated in the same way as for a conventional thermocouple, as the skilled person would appreciate.

To form a thermocouple, currently the end of a length of MIMS cable is usually crimped and welded (TIG welded usually) so that a sealed end is produced. This straightforward method applied to a double sheath thermocouple embodying the invention may result locally at the tip in an alloy whose concentration is lower in chromium (and for this reason less oxidation resistant) because of mixing between the low Cr content inner sheath and higher Cr content outer sheath. Three possible sealing strategies to solve this problem are as follows:

- Removal of the inner sheath at the end to be sealed by drilling and sealing of the outer sheath with standard prior art technology. Once the MIMS cable has been cut, at its open end a drill or cutting tool of diameter equal to the external diameter of the inner sheath can be used

to remove a predetermined length of the inner sheath, leaving only the outer sheath at the end of the cable. An annular drill or cutting tool may be used to prevent damage to the ends of the thermoelements within the sheath. The end portion of the outer sheath can then be, for example, crimped and welded without affecting its alloy composition.

- Using a filler metal with higher Cr content than the outer sheath: a small volume of the filler metal is located, or inserted, in the gap at the open end of the MIMS cable and then the end of the MIMS cable is welded. The composition and mass of the filler metal are chosen to compensate for the mixing between the lower Cr content inner sheath and the higher Cr content outer sheath.
- Crimping of the inner sheath and welding of the inner sheath followed by sealing of the outer sheath. This may involve crimping of the outer sheath and welding with lower power to achieve welding of the outer sheath but not remelting of the inner sheath. Alternatively, a filler metal may be provided before welding of the outer sheath with lower power to achieve welding of the outer sheath and filler metal but not remelting of the inner sheath.

In the embodiments of the invention described above, in which an assembly of inner and outer sheaths is formed into a MIMS cable by extrusion and/or drawing and/or swaging, the inner and outer sheaths may typically extend along the entire length of a thermocouple. In many cases this is satisfactory and provides an effective way to fabricate thermocouples, but to achieve the benefit of the inner sheath in preventing contamination of the thermoelements by diffusion of material from the outer sheath, in an alternative embodiment it may only be necessary for the inner sheath to extend along the portion of the thermocouple which is to be exposed to high temperatures during use.

It may be noted that in some of the techniques described above for sealing an end of a thermocouple cable, a small portion of the thermoelements may not be shielded by the inner sheath from the outer sheath at the end of the thermocouple. For example if an end portion of the inner sheath is removed and the end of the outer sheath is crimped and welded, or if a filler metal (such as a high Cr-content filler metal) is provided and the inner and outer sheaths

are crimped and welded at the same time, then the inner sheath may not be continuous or may have an open end. In that case the portions of the thermoelements at or near to the end of the thermocouple may be disadvantageously not entirely shielded by the inner sheath. In practice, this is unlikely to have a significant effect on the efficacy of the inner sheath as all of the length of the thermoelements extending within the portion of the thermocouple exposed to high temperature during use is shielded by the inner sheath except for a small portion at the thermocouple tip.

As the operating temperature of a MIMS thermocouple is increased above about 1000C, the oxidation resistance provided by the sheath may no longer be adequate. A further aspect of the invention therefore provides that at least a portion of the outer surface of the sheath may be coated with an intermetallic or coated using chromizing. Advantageously, the intermetallic may be a nickel-aluminide or platinum-doped nickel-aluminide. The coating may preferably only be applied to the portion of the thermocouple sheath which will be exposed to high temperatures.

For example, in a preferred embodiment of the invention a thermocouple comprising an outer sheath and an inner sheath (functioning as a contamination barrier as described above) may be allowed to operate at a still higher temperature if at least a portion of the outer surface of the outer sheath is coated with an intermetallic or coated using chromizing as described above.

Although applying a temperature-resistant coating to the outer sheath of a thermocouple comprising an outer sheath and an inner sheath may thus be particularly advantageous, this aspect of the invention may also be used to enhance the performance of a sheath of a thermocouple which does not comprise an inner sheath, but which only comprises a single sheath. For example, if an intermetallic coating or a coating obtained by chromizing is to be used, then an alloy for a sheath may be selected which does not contain elements that contaminate the thermoelements at a proposed operating temperature, but which does not provide adequate environmental protection at that proposed operating temperature. For example, any of the alloys described above for fabricating the inner sheath of the thermocouple according to the

previous aspects of the invention could be used. The environmental protection (e.g. oxidation resistance) provided by the sheath may then be enhanced by coating at least a portion of the outer surface of the sheath (preferably the portion of the outer surface which will be exposed to high temperatures during use of the thermocouple) with an intermetallic or using chromizing, such that the coated sheath does provide adequate environmental protection at the proposed operating temperature. In this way, a thermocouple capable of operating at elevated temperatures may be provided, such as a temperature at or above 1100C, 1200C, 1300C or even 1350C.

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Embodiments of the invention may be used in any industrial temperature measurement application suitable for thermocouples, such as gas turbine, high-temperature process control, furnace temperature control and so on. Advantageously, however, aspects of the invention may enable conventional types of thermocouple, such as Type K and Type N thermocouples, to operate at higher temperatures than previously.

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Specific Embodiments and Best Mode of the Invention

Specific embodiments of the invention will now be described by way of example, with reference to the accompanying drawings, in which:

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Figure 1 is a schematic transverse section of a thermocouple according to a first embodiment of the invention;

Figure 2 is a schematic transverse section of a thermocouple according to a second embodiment of the invention; and

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Figure 3 is a schematic transverse section of a thermocouple according to a third embodiment of the invention.

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Figure 1 is a transverse section of a thermocouple comprising two thermoelements 2, 4 extending within a composite sheath 6. The thermoelements are as in a conventional thermocouple, such as a Type K or Type N thermocouple. Along the length of the thermocouple, the thermoelements are insulated from each other and from the inner surface of

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the sheath by an insulating ceramic material 8, in the same way as in a conventional thermocouple.

The sheath is tubular and comprises an inner sheath 10 and an outer
5 sheath 12. The outer sheath is of a conventional oxidation-resistant alloy such as Inconel 600, but may be of any conventional environment-resisting alloy. The inner sheath is of nickel-based alloy 270 (Nickel 270), but may be of any of the nickel-based compositions described above. The thermocouple is intended for operation at elevated temperature, such as above 1000C. In this
10 temperature range, in a conventional thermocouple the manganese and chromium content in the Inconel 600 would cause contamination of the thermoelements and consequently cause drift. In the embodiment, the inner sheath provides a diffusion barrier and prevents contamination of the thermoelements by either the manganese or chromium in the outer sheath.

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The outer sheath is of similar dimensions to a conventional thermocouple sheath, both in terms of diameter and thickness. The inner sheath is between 300 and 500 micrometres thick.

20 Figure 2 is a transverse section of a thermocouple comprising two thermoelements 52, 54 extending within an outer sheath 56. Each thermoelement is contained within a respective inner sheath 58, 60. Along the length of the thermocouple, each thermoelement is insulated from its respective inner sheath, and each inner sheath is insulated from the other
25 inner sheath and from the outer sheath, by an insulating ceramic material 62. The materials of the thermoelements, the inner and outer sheaths and the insulating material may be the same as in the first embodiment.

As in the first embodiment, the inner sheaths provide a contamination barrier to
30 prevent contamination of the thermoelements by elements such as manganese and chromium in the outer sheath. In addition, each thermoelement is separated from the other thermoelement by the inner sheaths, and so any contamination of one thermoelement by diffusion of elements from the other is prevented.

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Figure 3 is a transverse section of a thermocouple having a similar structure to the thermocouple of figure 1. Reference numerals corresponding to those in figure 1 will therefore be used. The thermocouple of figure 3 comprises two thermoelements 2, 4 extending within a composite sheath 6 comprising an inner sheath 10 and an outer sheath 12. Along the length of the thermocouple, the thermoelements are insulated from the inner sheath and from each other by an insulating ceramic material 8. The outer surface of the outer sheath is coated with a layer of a nickel-aluminide or a platinum-doped nickel-aluminide 14 of thickness approximately 100 to 200 micrometres.

Alternatively, the outer surface of the outer sheath can be coated by chromizing. The coating enhances the oxidation resistance of the outer sheath.

The nickel-aluminide or platinum-doped nickel-aluminide coating, or the coating produced by chromizing, is particularly effective in combination with the outer sheath, in providing an oxidation-resistant and protective sheath for the thermocouple. The outer sheath is typically made of a nickel-chromium alloy or nickel-chromium-aluminium alloy and the coating bonds well to these alloys. The coating is typically more expensive than a nickel-chromium alloy sheath material and therefore is advantageously selectively used to coat only the portion of the thermocouple which will be exposed to elevated temperatures during use, i.e. the portion of the thermocouple sheath close to the junction between the thermoelements.

Claims

1. A thermocouple, in which a thermoelement extends within a metal outer sheath, comprising a nickel-based inner sheath containing less than 10wt% of chromium, positioned between the thermoelement and the metal outer sheath.
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2. A thermocouple according to claim 1, in which the inner sheath comprises nickel of purity equal to or greater than 99wt% or preferably equal to or greater than 99.95wt%.
- 10 3. A thermocouple according to claim 1, in which the inner sheath comprises Nickel 270.
4. A thermocouple according to claim 1, in which the inner sheath contains chromium at a concentration less than 5wt%, preferably less than 3wt%, and particularly preferably less than 1wt%.
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5. A thermocouple according to claim 1, in which the inner sheath contains less than 0.1wt% chromium.
- 20 6. A thermocouple according to any preceding claim, in which the inner sheath has a manganese concentration less than 0.2wt% or preferably less than 0.1wt%.
- 25 7. A thermocouple according to any preceding claim, in which the inner sheath contains less than 0.01wt% manganese.
8. A thermocouple according to any preceding claim, in which the outer sheath and the inner sheath are in the form of coaxial tubes.
- 30 9. A thermocouple according to any preceding claim, in which the outer sheath is in contact with the inner sheath.

10. A thermocouple according to any of the claims 1 to 9, comprising two thermoelements and two inner sheaths, each thermoelement extending within a respective inner sheath.
- 5 11. A thermocouple according to any preceding claim, in which the thermoelements are formed from Ni alloys, in which Ni is the largest component by weight.
12. A thermocouple according to any preceding claim, in which at least a
10 portion of an outer surface of the outer sheath is coated with an intermetallic or is coated using chromizing.
13. A thermocouple according claim 12, in which the intermetallic is a nickel-aluminide or platinum-doped nickel-aluminide.
- 15 14. A method for fabricating a thermocouple according to any preceding claim, in which the outer sheath and the inner sheath are formed simultaneously by coextrusion or swaging.
- 20 15. A thermocouple comprising a thermoelement extending within a sheath, in which at least a portion of the sheath is coated with an intermetallic or is coated using chromizing.
16. A thermocouple according to claim 15, in which the intermetallic is
25 nickel-aluminide or platinum-doped nickel-aluminide.
17. A thermocouple according to claim 15 or 16, in which the sheath has a composition as for the inner sheath of any of claims 1 to 7.
- 30 18. A thermocouple, in which a thermoelement extends within an outer sheath, comprising an inner sheath positioned between the thermoelement and the outer sheath, in which the inner sheath is adapted to prevent diffusion of contaminants which if absorbed by the thermoelement would change its Seebeck coefficient, from the outer sheath to the thermoelement during
35 exposure of the thermocouple to elevated temperatures.

19. A thermocouple according to claim 18, in which the inner sheath is a nickel-based inner sheath containing less than 10wt% of chromium.
- 5 20. A thermocouple substantially described herein, with reference to the drawings.

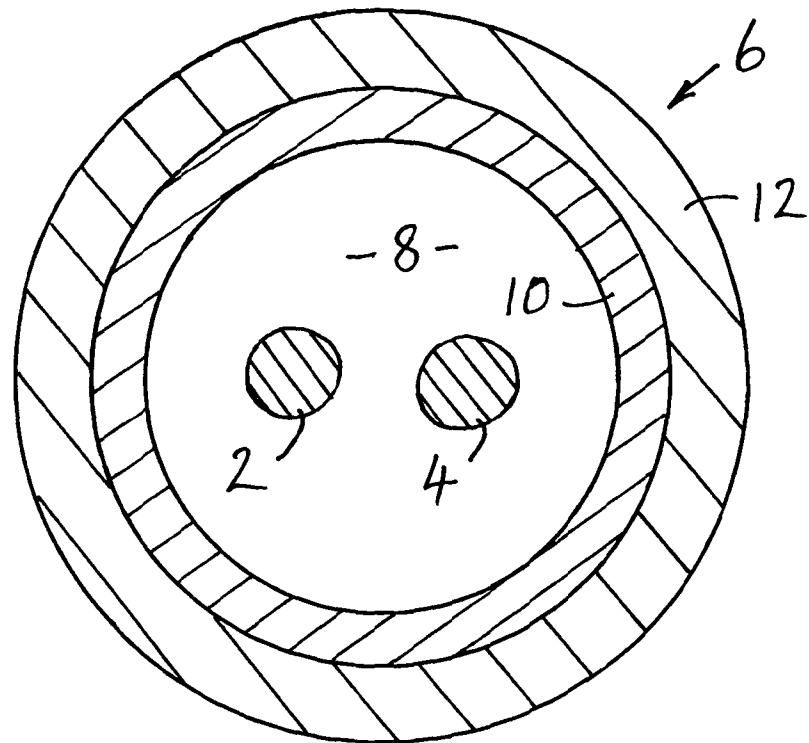


FIGURE 1

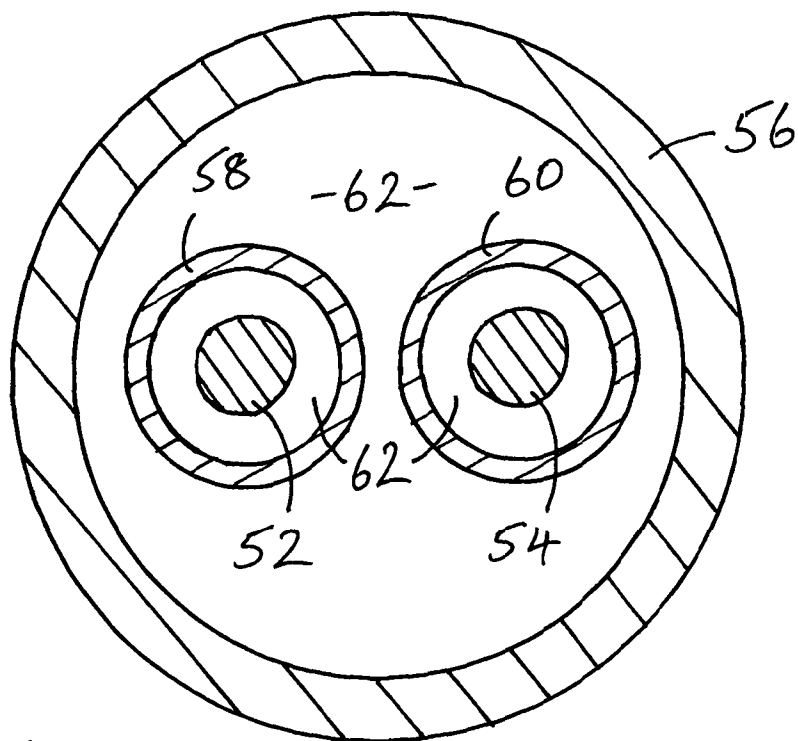


FIGURE 2

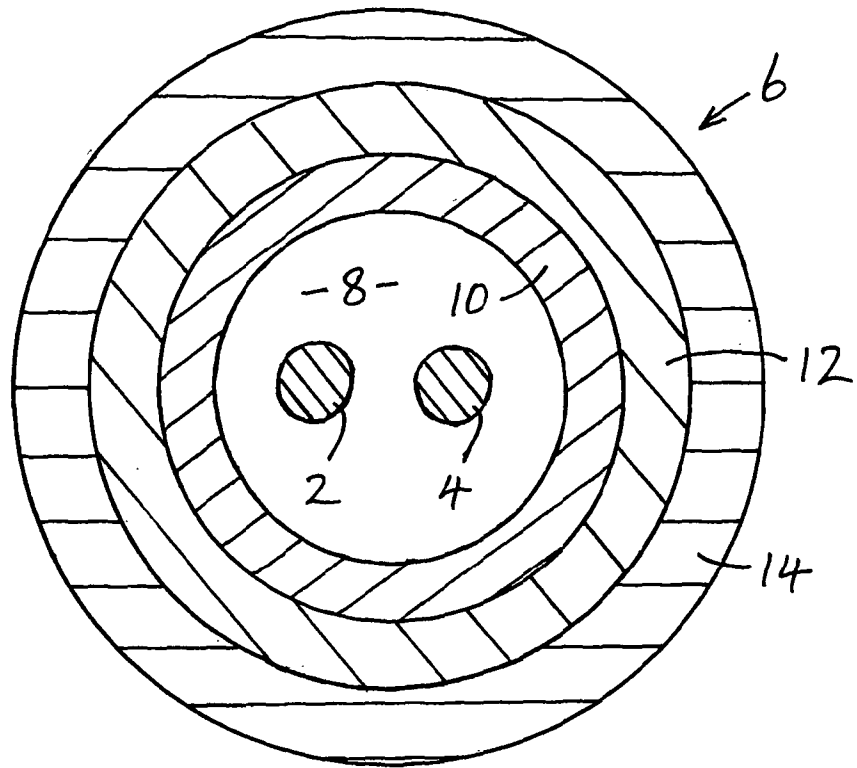


FIGURE 3

INTERNATIONAL SEARCH REPORT

International application No

PCT/GB2011/000506

A. CLASSIFICATION OF SUBJECT MATTER

INV. H01L35/20

ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

H01L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	DE 36 36 468 C1 (HERAEUS GMBH W C) 17 September 1987 (1987-09-17)	15
A	column 4, lines 43-61 abstract; figure 1	1,8,9,18
A	----- US 5 747 727 A (SAWADA KAZUO [JP] ET AL) 5 May 1998 (1998-05-05) abstract; figures 2,3 column 3, lines 4-22	1,8,9,18
A	----- US 5 043 023 A (BENTLEY ROBIN E [AU]) 27 August 1991 (1991-08-27) cited in the application abstract; figure 1 column 1, lines 58-66 -----	1,18



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents :

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Information on patent family members

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