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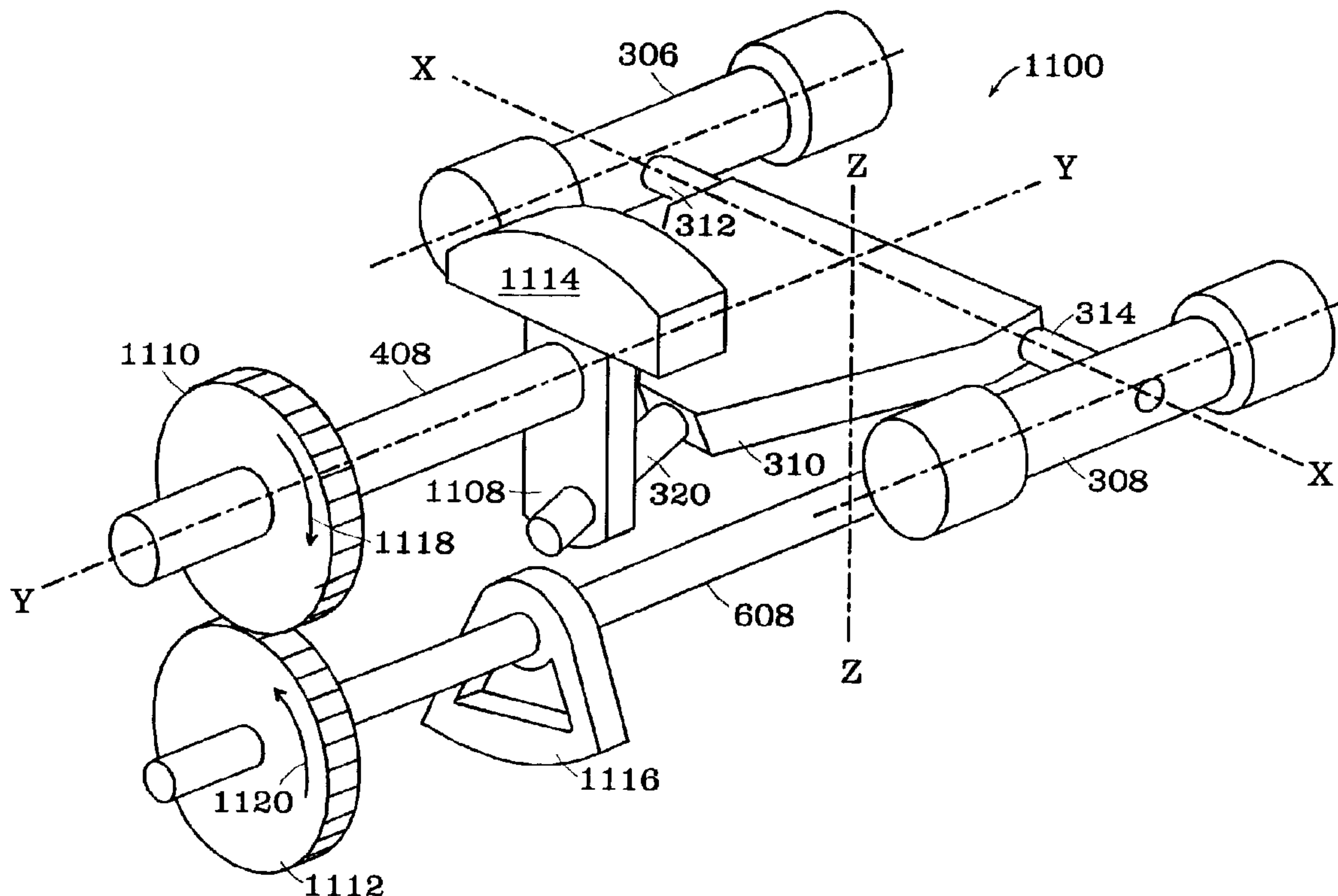
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(54) Title: PISTON ENGINE BALANCING



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A piston assembly includes first and second pistons, a transition arm coupled to each of the pistons, and a rotating member rotating in a first direction about a first axis. The transition arm includes a drive member coupled to the rotating member off-axis of the rotating member. A first counterbalance is mounted to rotate in the first direction, and a second counterbalance is mounted to rotate in a second direction opposite the first direction. The second counterbalance rotates about a second axis offset and parallel to the first axis. Alternatively, the second counterbalance rotates about the first axis. A method of counterbalancing a piston assembly includes mounting a first counterbalance to the piston assembly to rotate in the first direction, and mounting a second counterbalance to the piston assembly to rotate in the second direction.

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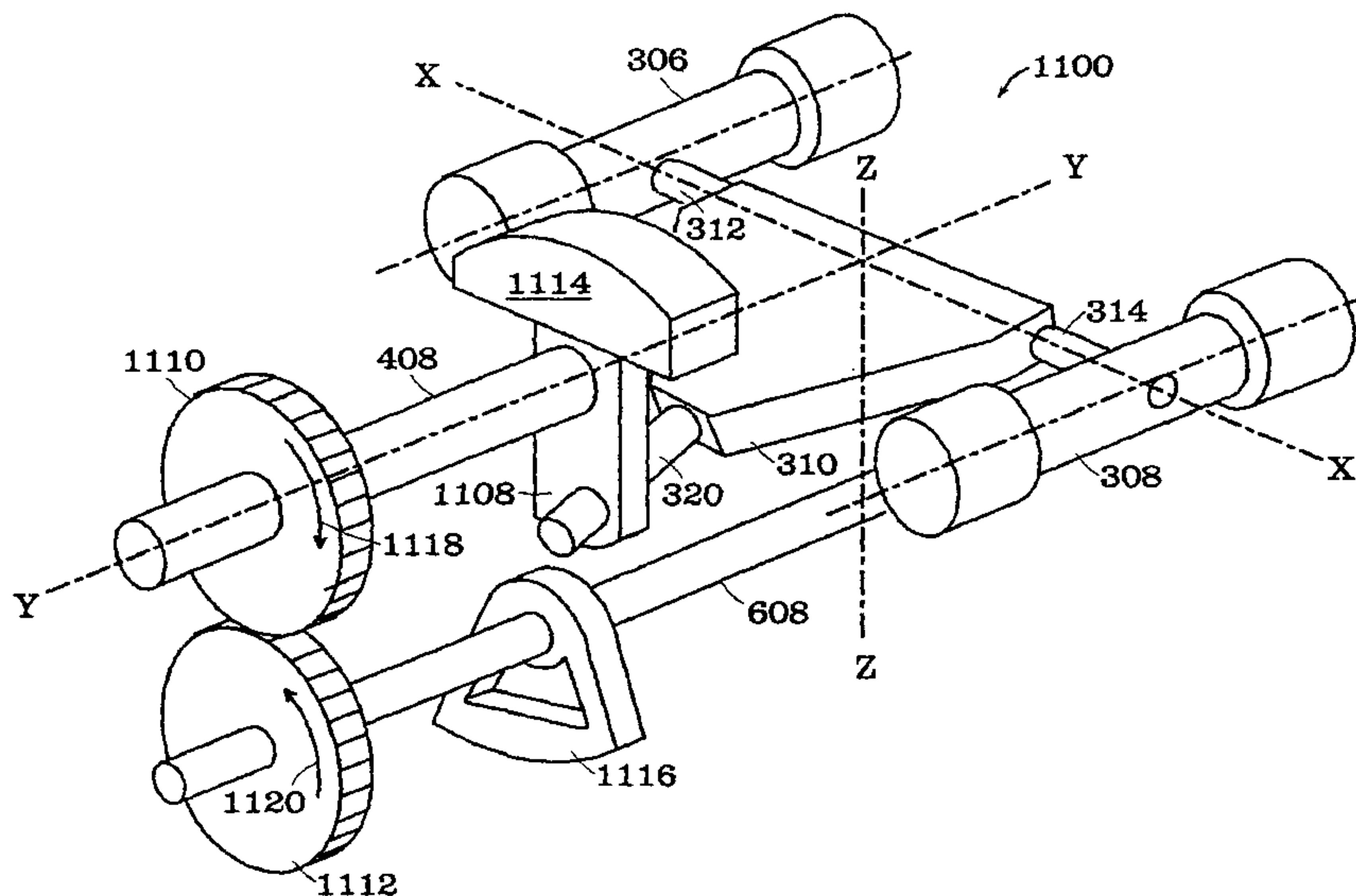
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(54) Title: PISTON ENGINE BALANCING



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(57) Abstract: A piston assembly includes first and second pistons, a transition arm coupled to each of the pistons, and a rotating member rotating in a first direction about a first axis. The transition arm includes a drive member coupled to the rotating member off-axis of the rotating member. A first counterbalance is mounted to rotate in the first direction, and a second counterbalance is mounted to rotate in a second direction opposite the first direction. The second counterbalance rotates about a second axis offset and parallel to the first axis. Alternatively, the second counterbalance rotates about the first axis. A method of counterbalancing a piston assembly includes mounting a first counterbalance to the piston assembly to rotate in the first direction, and mounting a second counterbalance to the piston assembly to rotate in the second direction.

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PISTON ENGINE BALANCING

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Background of the Invention

The invention relates to piston engine balancing.

Most piston driven engines have pistons that are attached to offset portions of a crankshaft such that as the pistons are moved in a reciprocal direction transverse to the axis of the crankshaft, the crankshaft will rotate.

10 U.S. Patent 5,535,709, defines an engine with a double ended piston that is attached to a crankshaft with an off set portion. A lever attached between the piston and the crankshaft is restrained in a fulcrum regulator to provide the rotating motion to the crankshaft.

15 U.S. Patent 4,011,842, defines a four cylinder piston engine that utilizes two double ended pistons connected to a T-shaped connecting member that causes a crankshaft to rotate. The T-shaped connecting member is attached at each of the T-cross arm to a double ended piston. A centrally located point on the T-cross arm is rotatably attached to a fixed point, and the bottom of the T is rotatably attached to a crank pin which is connected to the crankshaft by a crankthrow which includes a 20 counter weight.

In each of the above examples, double ended pistons are used that drive a crankshaft that has an axis transverse to the axis of the pistons.

Summary of the Invention

According to the invention, a piston assembly includes first and second 25 pistons, e.g., double-ended pistons or single-ended pistons with guide rods, a transition arm coupled to each of the pistons, and a rotating member rotating in a first direction. The transition arm includes a drive member coupled to the rotating member off-axis of the rotating member. A first counterbalance is mounted to rotate in the first direction, and a second counterbalance is mounted to rotate in a second direction 30 opposite the first direction.

Embodiments of this aspect of the invention may include one or more of the following features.

The first and second double ended pistons are arranged for reciprocating motion in a common plane. The first counterbalance is coupled to the rotating member opposite the drive member coupling. The rotating member rotates about a first axis, and the second counterbalance rotates about a second axis offset and parallel to the first axis.

A first gear is mounted to rotate in the first direction about the first axis, and a second gear is driven by the first gear to rotate about the second axis in the second direction.

In certain illustrated embodiments, the rotating member, the first counterbalance, and the second counterbalance rotate about a first axis. A first gear is mounted to rotate in the first direction about the first axis, and a second gear is driven by the first gear to rotate in the second direction about a second axis offset and parallel to the first axis.

A first pulley is driven to rotate by the second gear in the second direction, and a second pulley is coupled to the first pulley and driven by the first pulley to rotate in the second direction about the first axis. The second counterbalance is driven by the second pulley.

A third counterbalance is coupled to the rotating member opposite the drive member coupling.

In further illustrated embodiments, a third counterbalance is mounted to rotate in the first direction, and a fourth counterbalance is mounted to rotate in the second direction. The rotating member and the first, second, third and fourth counterbalances rotate about a first axis. The first and third counterbalances are oriented 180 degrees apart relative to the first axis, and the second and fourth counterbalances are oriented 180 degrees apart relative to the first axis. The first and fourth counterbalances are both oriented in a first direction relative to the first axis, and the second and third counterbalances are both oriented in a second direction relative to the first axis, the second direction being 180 degrees from the first direction.

A first gear is mounted to rotate in the first direction about the first axis, and a second gear is driven by the first gear to rotate in the second direction about a second axis offset and parallel to the first axis. A first pulley is driven to rotate by the second gear in the second direction, and a second pulley is coupled to the first pulley 5 and driven by the first pulley to rotate in the second direction about the first axis. The second and fourth counterbalances are driven by the second pulley.

A fifth counterbalance is coupled to the rotating member opposite the drive member coupling, and the second counterbalance is integrated with the fifth counterbalance.

10 According to another aspect of the invention, a piston assembly includes at least three equally spaced members. Two of the members are pistons. A transition arm is coupled to each of the members. The transition arm includes a drive member coupled to a rotating member off-axis of the rotating member. The rotating member rotates in a first direction. A first counterbalance is mounted to rotate in the first 15 direction, and a second counterbalance is mounted to rotate in the first direction.

Embodiments of this aspect of the invention may include one or more of the following features.

A fourth member is coupled to the transition arm. The four members are 20 equally spaced about the transition arm with a first of the two piston being positioned opposite a second of the two pistons. A third counterbalance is coupled to the rotating member opposite the drive member coupling. The pistons are double-ended pistons or single ended pistons with guide rods.

According to another aspect of the invention, a piston assembly includes at 25 least three equally spaced members. Two of the members are pistons. A transition arm is coupled to each of the pistons. The transition arm includes a drive member coupled to a rotating member off-axis of the rotating member. The rotating member rotates in a first direction. A counterbalance is mounted to rotate in the first direction. The counterbalance is positioned axially aligned with and spaced from the rotating member.

30 Embodiments of this aspect of the invention may include one or more of the following features.

A fourth member is coupled to the transition arm. The four members are equally spaced about the transition arm with a first of the two piston being positioned opposite a second of the two pistons. The pistons are double-ended pistons or single ended pistons with guide rods.

5 According to another aspect of the invention, a method of counterbalancing a piston assembly including first and second double-ended pistons, a transition arm coupled to each of the pistons, and a rotating member rotating in a first direction, the transition arm including a drive member coupled to the rotating member off-axis of the rotating member, includes mounting a first counterbalance to the piston 10 assembly to rotate in the first direction, and mounting a second counterbalance to the piston assembly to rotate in a second direction opposite the first direction.

According to another aspect of the invention, a piston assembly includes at least two pistons and a transition arm coupled to each of the pistons. The transition arm including a drive member with a spherical portion. The spherical portion couples 15 the drive member to a rotating member off-axis of the rotating member.

Embodiments of this aspect of the invention may include one or more of the following features.

The rotating member includes a counterbalance. The drive member includes a cylindrical end portion. The rotating member includes a flywheel, and the 20 counterbalance is mounted to the flywheel. The flywheel defines a cylindrical opening for receiving the cylindrical end portion of the drive member, and the counterbalance defines a spherical opening for receiving the spherical end portion of the drive member.

Advantages of the invention include limiting vibration of the piston 25 assembly. The invention greatly reduces vibration of the engine, due to internal canceling of vibrating forces and couples. A balanced machine has greatly reduced forces on its bearings and mounting hardware. The bearing life may be extended many times, and lighter parts and mounts can be used, if the vibrational forces and couples have been reduced by balancing. Another advantage achieved by balancing is 30 the ability to run smoothly at higher speeds. Since this balancing method nearly completely compensates for rotating and inertial imbalance, the engine can be run at

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higher speeds. Imbalance forces that are not compensated increase as the square of the speed and quickly become a limiting factor as speeds increase. In many engine applications, the trend is toward higher speeds, placing 5 more importance on the better balancing methods available with the invention.

In one broad aspect, there is provided a piston assembly comprising: at least one piston coupled to a transition arm; the transition arm having a drive arm 10 eccentrically coupled to a rotatable member about a rotation axis such that there is an angle between the drive arm and the rotation axis; the axis of movement of said piston being spaced from the rotation axis, whereby the transition arm translated between rotational movement of the rotatable 15 member and reciprocal linear movement of said piston, wherein a counterbalance spaced from the rotatable member is mounted for rotation about the rotation axis, and wherein a counterbalancing member simulating a piston is mounted on the transition arm.

20 In another broad aspect, there is provided a method of counterbalancing a piston assembly; comprising at least one piston coupled to a transition arm, the transition arm having a drive arm eccentrically coupled to a rotatable member about a rotation axis such that there is an angle 25 between the drive arm and the rotation axis, and the axis of movement of said piston being spaced from the rotation axis, whereby the transition arm translated between rotational movement of the rotatable member and reciprocal linear movement of said piston, in which method a counterbalance spaced from the rotatable member is mounted for rotation 30 about the rotation axis, and a counterbalancing member simulating a piston is mounted on the transition arm.

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Other features and advantages of the invention will be apparent from the following description and from the claims.

Brief Description of the Drawings

5 FIGS. 1 and 2 are side view of a simplified illustration of a four cylinder engine of the present invention;

10 FIGS. 3, 4, 5 and 6 are a top views of the engine of FIG. 1 showing the pistons and flywheel in four different positions;

FIG. 7 is a top view, partially in cross-section of an eight cylinder engine of the present invention;

FIG. 8 is a side view in cross-section of the engine of FIG. 7;

15 FIG. 9 is a right end view of FIG. 7;

FIG. 10 is a side view of FIG. 7;

FIG. 11 is a left end view of FIG. 7;

20 FIG. 12 is a partial top view of the engine of FIG. 7 showing the pistons, drive member and flywheel in a high compression position;

FIG. 13 is a partial top view of the engine in FIG. 7 showing the pistons, drive member and flywheel in a low compression position;

FIG. 14 is a top view of a piston;

25 FIG. 15 is a side view of a piston showing the drive member in two positions;

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FIG. 16 shows the bearing interface of the drive member and the piston;

FIG. 17 is an air driven engine/pump embodiment;

FIG. 18 illustrates the air valve in a first 5 position;

FIGS. 18a, 18b and 18c are cross-sectional view of three cross-sections of the air valve shown in FIG. 18;

FIG. 19 illustrates the air valve in a second position;

FIGS. 19a, 19b and 19c are cross-sectional view of three cross-sections for the air valve shown in FIG. 19;

FIG. 20 shows an embodiment with slanted cylinders;

FIG. 21 shows an embodiment with single ended pistons;

5 FIG. 22 is a top view of a two cylinder, double ended piston assembly;

FIG. 23 is a top view of one of the double ended pistons of the assembly of FIG. 22;

FIG. 23a is a side view of the double ended piston of FIG. 23, taken along lines 23A, 23A;

10 FIG. 24 is a top view of a transition arm and universal joint of the piston assembly of FIG. 22;

FIG. 24a is a side view of the transition arm and universal joint of FIG. 24, taken along lines 24a, 24a;

15 FIG. 25 is a perspective view of a drive arm connected to the transition arm of the piston assembly of FIG. 22;

FIG. 25a is an end view of a rotatable member of the piston assembly of FIG. 22, taken along lines 25a, 25a of FIG. 22, and showing the connection of the drive arm to the rotatable member;

20 FIG. 25b is a side view of the rotatable member, taken along lines 25b, 25b of FIG. 25a;

FIG. 26 is a cross-sectional, top view of the piston assembly of FIG. 22;

FIG. 27 is an end view of the transition arm, taken along lines 27, 27 of FIG. 24;

25 FIG. 27a is a cross-sectional view of a drive pin of the piston assembly of FIG. 22;

FIGS. 28-28b are top, rear, and side views, respectively, of the piston assembly of FIG. 22;

FIG. 28c is a top view of an auxiliary shaft of the piston assembly of FIG. 22;

30 FIG. 29 is a cross-sectional side view of a zero-stroke coupling;

FIG. 29a is an exploded view of the zero-stroke coupling of FIG. 29;

FIG. 30 is a graph showing the figure 8 motion of a non-flat piston assembly;

FIG. 31 shows a reinforced drive pin;

5 FIG. 32 is a top view of a four cylinder engine for directly applying combustion pressures to pump pistons;

FIG. 32a is an end view of the four cylinder engine, taken along lines 32a, 32a of FIG. 32;

FIG. 33 is a cross-sectional top view of an alternative embodiment of a variable stroke assembly shown in a maximum stroke position;

10 FIG. 34 is a cross-sectional top view of the embodiment of FIG. 33 shown in a minimum stroke position;

FIG. 35 is a partial, cross-sectional top view of an alternative embodiment of a double-ended piston joint;

15 FIG. 35A is an end view and FIG. 35B is a side view of the double-ended piston joint, taken along lines 35A, 35A and 35B, 35B, respectively, of FIG. 35;

FIG. 36 is a partial, cross-sectional top view of the double-ended piston joint of FIG. 35 shown in a rotated position;

FIG. 37 is a side view of an alternative embodiment of the joint of FIG. 35;

20 FIG. 38 is a top view of an engine/compressor assembly;

FIG. 38A is an end view and FIG. 38B is a side view of the engine/compressor assembly, taken along lines 38A, 38A and 38B, 38B, respectively, of FIG. 38;

25 FIG. 39 is a perspective view of a piston engine assembly including counterbalancing;

FIG. 40 is a perspective view of the piston engine assembly of FIG. 39 in a second position;

FIG. 41 is a perspective view of an alternative embodiment of a piston engine assembly including counterbalancing;

30 FIG. 42 is a perspective view of the piston engine assembly of FIG. 41 in a second position.

FIG. 43 is a perspective view of an additional alternative embodiment of a piston engine assembly including counterbalancing;

FIG. 44 is a perspective view of the piston engine assembly of FIG. 43 in a second position;

5 FIG. 45 is a perspective view of an additional alternative embodiment of a piston engine assembly including counterbalancing;

FIG. 46 is a perspective view of the piston engine assembly of FIG. 43 in a second position;

10 FIG. 47 is a side view showing the coupling of a transition arm to a flywheel;

FIG. 48 is a side view of an alternative coupling of the transition arm to the flywheel; and

FIG. 49 is a side view of an additional alternative coupling of the transition arm to the flywheel.

15 Description of the Preferred Embodiments

FIG. 1 is a pictorial representation of a four piston engine 10 of the present invention. Engine 10 has two cylinders 11 (FIG. 3) and 12. Each cylinder 11 and 12 house a double ended piston. Each double ended piston is connected to transition arm 13 which is connected to flywheel 15 by shaft 14. Transition arm 13 is connected to 20 support 19 by a universal joint mechanism, including shaft 18, which allows transition arm 13 to move up and down and shaft 17 which allows transition arm 13 to move side to side. FIG. 1 shows flywheel 15 in a position shaft 14 at the top of wheel 15.

FIG. 2 shows engine 10 with flywheel 15 rotated so that shaft 14 is at the bottom of flywheel 15. Transition arm 13 has pivoted downward on shaft 18.

25 FIGS. 3-6 show a top view of the pictorial representation, showing the transition arm 13 in four positions and shaft moving flywheel 15 in 90° increments. FIG. 3 shows flywheel 15 with shaft 14 in the position as illustrated in FIG. 3a. When piston 1 fires and moves toward the middle of cylinder 11, transition arm 13 will pivot on universal joint 16 rotating flywheel 15 to the position shown in FIG. 2. Shaft 14 30 will be in the position shown in FIG. 4a. When piston 4 is fired, transition arm 13 will move to the position shown in FIG. 5. Flywheel 15 and shaft 14 will be in the

position shown in FIG 5a. Next piston 2 will fire and transition arm 13 will be moved to the position shown in FIG. 6. Flywheel 15 and shaft 14 will be in the position shown in FIG. 6a. When piston 3 is fired, transition arm 13 and flywheel 15 will return to the original position that shown in FIGS. 3 and 3a.

5 When the pistons fire, transition arm will be moved back and forth with the movement of the pistons. Since transition arm 13 is connected to universal joint 16 and to flywheel 15 through shaft 14, flywheel 15 rotates translating the linear motion of the pistons to a rotational motion.

FIG. 7 shows (in partial cross-section) a top view of an embodiment of a 10 four double piston, eight cylinder engine 30 according to the present invention. There are actually only four cylinders, but with a double piston in each cylinder, the engine is equivalent to a eight cylinder engine. Two cylinders 31 and 46 are shown. Cylinder 31 has double ended piston 32, 33 with piston rings 32a and 33a, respectively. Pistons 32, 33 are connected to a transition arm 60 (FIG. 8) by piston 15 arm 54a extending into opening 55a in piston 32, 33 and sleeve bearing 55. Similarly piston 47, 49, in cylinder 46 is connected by piston arm 54b to transition arm 60.

Each end of cylinder 31 has inlet and outlet valves controlled by a rocker arms and a spark plug. Piston end 32 has rocker arms 35a and 35b and spark plug 44, and piston end 33 has rocker arms 34a and 34b, and spark plug 41. Each piston has 20 associated with it a set of valves, rocker arms and a spark plug. Timing for firing the spark plugs and opening and closing the inlet and exhaust values is controlled by a timing belt 51 which is connected to pulley 50a. Pulley 50a is attached to a gear 64 by shaft 63 (FIG. 8) turned by output shaft 53 powered by flywheel 69. Belt 50a also turns pulley 50b and gear 39 connected to distributor 38. Gear 39 also turns gear 40. 25 Gears 39 and 40 are attached to cam shaft 75 (FIG. 8) which in turn activate push rods that are attached to the rocker arms 34, 35 and other rocker arms not illustrated.

Exhaust manifolds 48 and 56 as shown attached to cylinders 46 and 31 respectively. Each exhaust manifold is attached to four exhaust ports.

FIG. 8 is a side view of engine 30, with one side removed, and taken 30 through section 8-8 of FIG. 7. Transitions arm 60 is mounted on support 70 by pin 72 which allows transition arm to move up and down (as viewed in FIG. 8) and pin 71

which allows transition arm 60 to move from side to side. Since transition arm 60 can move up and down while moving side to side, then shaft 61 can drive flywheel 69 in a circular path. The four connecting piston arms (piston arms 54b and 54d shown in FIG. 8) are driven by the four double end pistons in an oscillator motion around pin 5 71. The end of shaft 61 in flywheel 69 causes transition arm to move up and down as the connection arms move back and forth. Flywheel 69 has gear teeth 69a around one side which may be used for turning the flywheel with a starter motor 100 (FIG. 11) to start the engine.

The rotation of flywheel 69 and drive shaft 68 connected thereto, turns 10 gear 65 which in turn turns gears 64 and 66. Gear 64 is attached to shaft 63 which turns pulley 50a. Pulley 50a is attached to belt 51. Belt 51 turns pulley 50b and gears 39 and 40 (FIG. 7). Cam shaft 75 has cams 88-91 on one end and cams 84-87 on the other end. Cams 88 and 90 actuate push rods 76 and 77, respectively. Cams 89 and 91 actuate push rods 93 and 94, respectively. Cams 84 and 86 actuate push rods 95 15 and 96, respectively, and cams 85 and 87 actuate push rods 78 and 79, respectively. Push rods 77, 76, 93, 94, 95, 96 and 78, 79 are for opening and closing the intake and exhaust valves of the cylinders above the pistons. The left side of the engine, which has been cutaway, contains an identical, but opposite valve drive mechanism.

Gear 66 turned by gear 65 on drive shaft 68 turns pump 67, which may be, 20 for example, a water pump used in the engine cooling system (not illustrated), or an oil pump.

FIG. 9 is a rear view of engine 30 showing the relative positions of the cylinders and double ended pistons. Piston 32, 33 is shown in dashed lines with 25 valves 35c and 35d located under lifter arms 35a and 35b, respectively. Belt 51 and pulley 50b are shown under distributor 38. Transition arm 60 and two, 54c and 54d, of the four piston arms 54a, 54b, 54c and 54d are shown in the pistons 32-33, 32a-33a, 47-49 and 47a-49a.

FIG. 10 is a side view of engine 30 showing the exhaust manifold 56, 30 intake manifold 56a and carburetor 56c. Pulleys 50a and 50b with timing belt 51 are also shown.

FIG. 11 is a front end view of engine 30 showing the relative positions of the cylinders and double ended pistons 32-33, 32a-33a, 47-49 and 47a-49a with the four piston arms 54a, 54b, 54c and 54d positioned in the pistons. Pump 67 is shown below shaft 53, and pulley 50a and timing belt 51 are shown at the top of engine 30.

5 Starter 100 is shown with gear 101 engaging the gear teeth 69a on flywheel 69.

A feature of the invention is that the compression ratio for the engine can be changed while the engine is running. The end of arm 61 mounted in flywheel 69 travels in a circle at the point where arm 61 enters flywheel 69. Referring to FIG. 13, the end of arm 61 is in a sleeve bearing ball bushing assembly 81. The stroke of the 10 pistons is controlled by arm 61. Arm 61 forms an angle, for example about 15°, with shaft 53. By moving flywheel 69 on shaft 53 to the right or left, as viewed in FIG. 13, the angle of arm 61 can be changed, changing the stroke of the pistons, changing the compression ratio. The position of flywheel 69 is changed by turning nut 104 on threads 105. Nut 104 is keyed to shaft 53 by thrust bearing 106a held in place by ring 15 106b. In the position shown in FIG. 12, flywheel 69 has been moved to the right, extending the stroke of the pistons.

FIG. 12 shows flywheel moved to the right increasing the stroke of the pistons, providing a higher compression ratio. Nut 105 has been screwed to the right, moving shaft 53 and flywheel 69 to the right. Arm 61 extends further into bushing 20 assembly 80 and out the back of flywheel 69.

FIG. 13 shows flywheel moved to the left reducing the stroke of the pistons, providing a lower compression ratio. Nut 105 has been screwed to the left, moving shaft 53 and flywheel 69 to the left. Arm 61 extends less into bushing assembly 80.

25 The piston arms on the transition arm are inserted into sleeve bearings in a bushing in piston. FIG. 14 shows a double piston 110 having piston rings 111 on one end of the double piston and piston rings 112 on the other end of the double piston. A slot 113 is in the side of the piston. The location the sleeve bearing is shown at 114.

FIG. 15 shows a piston arm 116 extending into piston 110 through slot 116 30 into sleeve bearing 117 in bushing 115. Piston arm 116 is shown in a second position

at 116a. The two pistons arms 116 and 116a show the movement limits of piston arm 116 during operation of the engine.

FIG. 16 shows piston arm 116 in sleeve bearing 117. Sleeve bearing 117 is in pivot pin 115. Piston arm 116 can freely rotate in sleeve bearing 117 and the 5 assembly of piston arm 116, Sleeve bearing 117 and pivot pin 115 and sleeve bearings 118a and 118b rotate in piston 110, and piston arm 116 can moved axially with the axis of sleeve bearing 117 to allow for the linear motion of double ended piston 110, and the motion of a transition arm to which piston arm 116 is attached.

FIG. 17 shows how the four cylinder engine 10 in FIG. 1 may be 10 configured as an air motor using a four way rotary valve 123 on the output shaft 122. Each of cylinders 1, 2, 3 and 4 are connected by hoses 131, 132, 133, and 144, respectively, to rotary valve 123. Air inlet port 124 is used to supply air to run engine 120. Air is sequentially supplied to each of the pistons 1a, 2a, 3a and 4a, to move the pistons back and forth in the cylinders. Air is exhausted from the cylinders out 15 exhaust port 136. Transition arm 126, attached to the pistons by connecting pins 127 and 128 are moved as described with references to FIGS. 1-6 to turn flywheel 129 and output shaft 22.

FIG. 18 is a cross-sectional view of rotary valve 123 in the position when 20 pressurized air or gas is being applied to cylinder 1 through inlet port 124, annular channel 125, channel 126, channel 130, and air hose 131. Rotary valve 123 is made up of a plurality of channels in housing 123 and output shaft 122. The pressurized air entering cylinder 1 causes piston 1a, 3a to move to the right (as viewed in FIG. 18). Exhaust air is forced out of cylinder 3 through line 133 into chamber 134, through passageway 135 and out exhaust outlet 136.

FIGS. 18a, 18b and 18c are cross-sectional view of valve 23 showing the 25 air passages of the valves at three positions along valve 23 when positioned as shown in FIG. 18.

FIG. 19 shows rotary valve 123 rotated 180° when pressurized air is applied to cylinder 3, reversing the direction of piston 1a, 3a. Pressurized air is 30 applied to inlet port 124, through annular chamber 125, passage way 126, chamber 134 and air line 133 to cylinder 3. This in turn causes air in cylinder 1 to be

exhausted through line 131, chamber 130, line 135, annular chamber 137 and out exhaust port 136. Shaft 122 will have rotated 360° turning counter clockwise when piston 1a, 3a complete its stroke to the left.

Only piston 1a, 3a have been illustrated to show the operation of the air engine and valve 123 relative to the piston motion. The operation of piston 2a, 4a is identical in function except that its 360° cycle starts at 90° shaft rotation and reverses at 270° and completes its cycle back at 90°. A power stroke occurs at every 90° of rotation.

FIGS. 19a, 19b and 19c are cross-sectional views of valve 123 showing the air passages of the valves at three positions along valve 123 when positioned as shown in FIG. 19.

The principle of operation which operates the air engine of FIG. 17 can be reversed, and engine 120 of FIG. 17 can be used as an air or gas compressor or pump. By rotating engine 10 clockwise by applying rotary power to shaft 122, exhaust port 136 will draw in air into the cylinders and port 124 will supply air which may be used to drive, for example air tool, or be stored in an air tank.

In the above embodiments, the cylinders have been illustrated as being parallel to each other. However, the cylinders need not be parallel. FIG. 20 shows an embodiment similar to the embodiment of FIG. 1-6, with cylinders 150 and 151 not parallel to each other. Universal joint 160 permits the piston arms 152 and 153 to be at an angle other than 90° to the drive arm 154. Even with the cylinders not parallel to each other the engines are functionally the same.

Still another modification may be made to the engine 10 of FIGS. 1-6. This embodiment, pictorially shown in FIG. 21, may have single ended pistons. Piston 1a and 2a are connected to universal joint 170 by drive arms 171 and 172, and to flywheel 173 by drive arm 174. The basic difference is the number of strokes of pistons 1a and 2a to rotate flywheel 173 360°.

Referring to FIG. 22, a two cylinder piston assembly 300 includes cylinders 302, 304, each housing a variable stroke, double ended piston 306, 308, respectively. Piston assembly 300 provides the same number of power strokes per revolution as a conventional four cylinder engine. Each double ended piston 306, 308

is connected to a transition arm 310 by a drive pin 312, 314, respectively. Transition arm 310 is mounted to a support 316 by, e.g., a universal joint 318 (U-joint), constant velocity joint, or spherical bearing. A drive arm 320 extending from transition arm 310 is connected to a rotatable member, e.g., flywheel 322.

5 Transition arm 310 transmits linear motion of pistons 306, 308 to rotary motion of flywheel 322. The axis, A, of flywheel 322 is parallel to the axes, B and C, of pistons 306, 308 (though axis, A, could be off-axis as shown in FIG. 20) to form an axial or barrel type engine, pump, or compressor. U-joint 318 is centered on axis, A. As shown in FIG. 28a, pistons 306, 308 are 180° apart with axes A, B and C lying
10 along a common plane, D, to form a flat piston assembly.

Referring to FIGS. 22 and 23, cylinders 302, 304 each include left and right cylinder halves 301a, 301b mounted to the assembly case structure 303. Double ended pistons 306, 308 each include two pistons 330 and 332, 330a and 332a, respectively, joined by a central joint 334, 334a, respectively. The pistons are shown
15 having equal length, though other lengths are contemplated. For example, joint 334 can be off-center such that piston 330 is longer than piston 332. As the pistons are fired in sequence 330a, 332, 330, 332a, from the position shown in FIG. 22, flywheel 322 is rotated in a clockwise direction, as viewed in the direction of arrow 333. Piston assembly 300 is a four stroke cycle engine, i.e., each piston fires once in two
20 revolutions of flywheel 322.

As the pistons move back and forth, drive pins 312, 314 must be free to rotate about their common axis, E, (arrow 305), slide along axis, E, (arrow 307) as the radial distance to the center line, B, of the piston changes with the angle of swing, α , of transition arm 310 (approximately $\pm 15^\circ$ swing), and pivot about centers, F, (arrow
25 309). Joint 334 is constructed to provide this freedom of motion.

Joint 334 defines a slot 340 (FIG. 23a) for receiving drive pin 312, and a hole 336 perpendicular to slot 340 housing a sleeve bearing 338. A cylinder 341 is positioned within sleeve bearing 338 for rotation within the sleeve bearing. Sleeve bearing 338 defines a side slot 342 shaped like slot 340 and aligned with slot 340.
30 Cylinder 341 defines a through hole 344. Drive pin 312 is received within slot 342 and hole 344. An additional sleeve bearing 346 is located in through hole 344 of

cylinder 341. The combination of slots 340 and 342 and sleeve bearing 338 permit drive pin 312 to move along arrow 309. Sleeve bearing 346 permits drive pin 312 to rotate about its axis, E, and slide along its axis, E.

If the two cylinders of the piston assembly are configured other than 180° apart, or more than two cylinders are employed, movement of cylinder 341 in sleeve bearing 338 along the direction of arrow 350 allows for the additional freedom of motion required to prevent binding of the pistons as they undergo a figure 8 motion, discussed below. Slot 340 must also be sized to provide enough clearance to allow the figure 8 motion of the pin.

Referring to FIGS. 35-35B, an alternative embodiment of a central joint 934 for joining pistons 330 and 332 is configured to produce zero side load on pistons 330 and 332. Joint 934 permits the four degrees of freedom necessary to prevent binding of drive pin 312 as the pistons move back and forth, i.e., rotation about axis, E, (arrow 905), pivoting about center, F, (arrow 909), and sliding movement along orthogonal axes, M (up and down in the plane of the paper in FIG. 35) and N (in and out of the plane of the paper in FIG. 35), while the load transmitted between joint 934 and pistons 330, 332 only produces a force vector which is parallel to piston axis, B (which is orthogonal to axes M and N).

Sliding movement along axis, M, accommodates the change in the radial distance of transition arm 310 to the center line, B, of the piston with the angle of swing, α , of transition arm 310. Sliding movement along axis, N, allows for the additional freedom of motion required to prevent binding of the pistons as they undergo the figure eight motion, discussed below. Joint 934 defines two opposed flat faces 937, 937a which slide in the directions of axes M and N relative to pistons 330, 332. Faces 937, 937a define parallel planes which remain perpendicular to piston axis, B, during the back and forth movement of the pistons.

Joint 934 includes an outer slider member 935 which defines faces 937, 937a for receiving the driving force from pistons 330, 332. Slider member 935 defines a slot 940 in a third face 945 of the slider for receiving drive pin 312, and a slot 940a in a fourth face 945a. Slider member 935 has an inner wall 936 defining a hole 939 perpendicular to slot 940 and housing a slider sleeve bearing 938. A cross

shaft 941 is positioned within sleeve bearing 938 for rotation within the sleeve bearing in the direction of arrow 909. Sleeve bearing 938 defines a side slot 942 shaped like slot 940 and aligned with slot 940. Cross shaft 941 defines a through hole 944. Drive pin 312 is received within slot 942 and hole 944. A sleeve bearing 946 is 5 located in through hole 944 of cross shaft 941.

The combination of slots 940 and 942 and sleeve bearing 938 permit drive pin 312 to move in the direction of arrow 909. Positioned within slot 940a is a cap screw 947 and washer 949 which attach to drive pin 312 retaining drive pin 312 against a step 951 defined by cross shaft 941 while permitting drive pin 312 to rotate 10 about its axis, E, and preventing drive pin 312 from sliding along axis, E. As discussed above, the two addition freedoms of motion are provided by sliding of slider faces 937, 937a relative to pistons 330, 332 along axis, M and N. A plate 960 is placed between each of face 937 and piston 330 and face 937a and piston 332. Each plate 960 is formed of a low friction bearing material with a bearing surface 962 in 15 contact with faces 937, 937a, respectively. Faces 937, 937a are polished.

As shown in FIG. 36, the load, P_L , applied to joint 934 by piston 330 in the direction of piston axis, B, is resolved into two perpendicular loads acting on pin 312: axial load, A_L , along the axis, E, of drive pin 312, and normal load, N_L , perpendicular to drive pin axis, E. The axial load is applied to thrust bearings 950, 952, and the 20 normal load is applied to sleeve bearing 946. The net direction of the forces transmitted between pistons 330, 332 and joint 934 remains along piston axis, B, preventing side loads being applied to pistons 330, 332. This is advantageous because side loads on pistons 330, 332 can cause the pistons to contact the cylinder wall creating frictional losses proportional to the side load values.

25 Pistons 330, 332 are mounted to joint 934 by a center piece connector 970. Center piece 970 includes threaded ends 972, 974 for receiving threaded ends 330a and 332a of the pistons, respectively. Center piece 970 defines a cavity 975 for receiving joint 934. A gap 976 is provided between joint 934 and center piece 970 to permit motion along axis, N.

30 For an engine capable of producing, e.g., about 100 horsepower, joint 934 has a width, W, of, e.g., about 3 5/16 inches, a length, L_1 , of, e.g., 3 5/16 inches, and a

height, H, of, e.g., about 3 1/2 inches. The joint and piston ends together have an overall length, L_2 , of, e.g., about 9 5/16 inches, and a diameter, D_1 , of, e.g., about 4 inches. Plates 960 have a diameter, D_2 , of, e.g., about 3 1/4 inch, and a thickness, T, of, e.g., about 1/8 inch. Plates 960 are press fit into the pistons. Plates 960 are 5 preferably bronze, and slider 935 is preferably steel or aluminum with a steel surface defining faces 937, 937a.

Joint 934 need not be used to join two pistons. One of pistons 330, 332 can be replaced by a rod guided in a bushing.

Where figure eight motion is not required or is allowed by motion of drive 10 pin 312 within cross shaft 941, joint 934 need not slide in the direction of axis, N. Referring to Fig. 37, slider member 935a and plates 960a have curved surfaces permitting slider member 935a to slide in the direction of axis, M, (in and out of the paper in Fig. 37) while preventing slider member 935a to move along axis, N.

Referring to FIGS. 24 and 24a, U-joint 318 defines a central pivot 352 15 (drive pin axis, E, passes through center 352), and includes a vertical pin 354 and a horizontal pin 356. Transition arm 310 is capable of pivoting about pin 354 along arrow 358, and about pin 356 along arrow 360.

Referring to FIGS. 25, 25a and 25b, as an alternative to a spherical bearing, to couple transition arm 310 to flywheel 322, drive arm 320 is received 20 within a cylindrical pivot pin 370 mounted to the flywheel offset radially from the center 372 of the flywheel by an amount, e.g., 2.125 inches, required to produce the desired swing angle, α (FIG. 22), in the transition arm.

Pivot pin 370 has a through hole 374 for receiving drive arm 320. There is a sleeve bearing 376 in hole 374 to provide a bearing surface for drive arm 320. Pivot 25 pin 370 has cylindrical extensions 378, 380 positioned within sleeve bearings 382, 384, respectively. As the flywheel is moved axially along drive arm 320 to vary the swing angle, α , and thus the compression ratio of the assembly, as described further below, pivot pin 370 rotates within sleeve bearings 382, 384 to remain aligned with drive arm 320. Torsional forces are transmitted through thrust bearings 388, 390, 30 with one or the other of the thrust bearings carrying the load depending on the direction of the rotation of the flywheel along arrow 386.

Referring to FIG. 26, to vary the compression and displacement of piston assembly 300, the axial position of flywheel 322 along axis, A, is varied by rotating a shaft 400. A sprocket 410 is mounted to shaft 400 to rotate with shaft 400. A second sprocket 412 is connected to sprocket 410 by a roller chain 413. Sprocket 412 is 5 mounted to a threaded rotating barrel 414. Threads 416 of barrel 414 contact threads 418 of a stationary outer barrel 420.

Rotation of shaft 400, arrow 401, and thus sprockets 410 and 412, causes rotation of barrel 414. Because outer barrel 420 is fixed, the rotation of barrel 414 causes barrel 414 to move linearly along axis, A, arrow 403. Barrel 414 is positioned 10 between a collar 422 and a gear 424, both fixed to a main drive shaft 408. Drive shaft 408 is in turn fixed to flywheel 322. Thus, movement of barrel 414 along axis, A, is translated to linear movement of flywheel 322 along axis, A. This results in flywheel 322 sliding along axis, H, of drive arm 320 of transition arm 310, changing angle, β , and thus the stroke of the pistons. Thrust bearings 430 are located at both ends of 15 barrel 414, and a sleeve bearing 432 is located between barrel 414 and shaft 408.

To maintain the alignment of sprockets 410 and 412, shaft 400 is threaded at region 402 and is received within a threaded hole 404 of a cross bar 406 of assembly case structure 303. The ratio of the number of teeth of sprocket 412 to sprocket 410 is, e.g., 4:1. Therefore, shaft 400 must turn four revolutions for a single 20 revolution of barrel 414. To maintain alignment, threaded region 402 must have four times the threads per inch of barrel threads 416, e.g., threaded region 402 has thirty-two threads per inch, and barrel threads 416 have eight threads per inch.

As the flywheel moves to the right, as viewed in FIG. 26, the stroke of the pistons, and thus the compression ratio, is increased. Moving the flywheel to the left 25 decreases the stroke and the compression ratio. A further benefit of the change in stroke is a change in the displacement of each piston and therefore the displacement of the engine. The horsepower of an internal combustion engine closely relates to the displacement of the engine. For example, in the two cylinder, flat engine, the displacement increases by about 20% when the compression ratio is raised from 6:1 to 30 12:1. This produces approximately 20% more horsepower due alone to the increase in displacement. The increase in compression ratio also increases the horsepower at

the rate of about 5% per point or approximately 25% in horsepower. If the horsepower were maintained constant and the compression ratio increased from 6:1 to 12:1, there would be a reduction in fuel consumption of approximately 25%.

5 The flywheel has sufficient strength to withstand the large centrifugal forces seen when assembly 300 is functioning as an engine. The flywheel position, and thus the compression ratio of the piston assembly, can be varied while the piston assembly is running.

Piston assembly 300 includes a pressure lubrication system. The pressure is provided by an engine driven positive displacement pump (not shown) having a 10 pressure relief valve to prevent overpressures. Bearings 430 and 432 of drive shaft 408 and the interface of drive arm 320 with flywheel 322 are lubricated via ports 433 (Fig. 26).

Referring to FIG. 27, to lubricate U-joint 318, piston pin joints 306, 308, and the cylinder walls, oil under pressure from the oil pump is ported through the 15 fixed U-joint bracket to the top and bottom ends of the vertical pivot pin 354. Oil ports 450, 452 lead from the vertical pin to openings 454, 456, respectively, in the transition arm. As shown in FIG. 27A, pins 312, 314 each define a through bore 458. Each through bore 458 is in fluid communication with a respective one of openings 454, 456. As shown in FIG. 23, holes 460, 462 in each pin connect through slots 461 20 and ports 463 through sleeve bearing 338 to a chamber 465 in each piston. Several oil lines 464 feed out from these chambers and are connected to the skirt 466 of each piston to provide lubrication to the cylinders walls and the piston rings 467. Also leading from chamber 465 is an orifice to squirt oil directly onto the inside of the top of each piston for cooling.

25 Referring to FIGS. 28-28c, in which assembly 300 is shown configured for use as an aircraft engine 300a, the engine ignition includes two magnetos 600 to fire the piston spark plugs (not shown). Magnetos 600 and a starter 602 are driven by drive gears 604 and 606 (FIG. 28c), respectively, located on a lower shaft 608 mounted parallel and below the main drive shaft 408. Shaft 608 extends the full 30 length of the engine and is driven by gear 424 (Fig. 26) of drive shaft 408 and is geared with a one to one ratio to drive shaft 408. The gearing for the magnetos

reduces their speed to half the speed of shaft 608. Starter 602 is geared to provide sufficient torque to start the engine.

Camshafts 610 operate piston push rods 612 through lifters 613. Camshafts 610 are geared down 2 to 1 through bevel gears 614, 616 also driven from shaft 608. Center 617 of gears 614, 616 is preferably aligned with U-joint center 352 such that the camshafts are centered in the piston cylinders, though other configurations are contemplated. A single carburetor 620 is located under the center of the engine with four induction pipes 622 routed to each of the four cylinder intake valves (not shown). The cylinder exhaust valves (not shown) exhaust into two manifolds 624.

Engine 300a has a length, L, e.g., of about forty inches, a width, W, e.g., of about twenty-one inches, and a height, H, e.g., of about twenty inches, (excluding support 303).

Referring to FIGS. 29 and 29a, a variable compression compressor or pump having zero stroke capability is illustrated. Here, flywheel 322 is replaced by a rotating assembly 500. Assembly 500 includes a hollow shaft 502 and a pivot arm 504 pivotally connected by a pin 506 to a hub 508 of shaft 502. Hub 508 defines a hole 510 and pivot arm 504 defines a hole 512 for receiving pin 506. A control rod 514 is located within shaft 502. Control rod 514 includes a link 516 pivotally connected to the remainder of rod 514 by a pin 518. Rod 514 defines a hole 511 and link 516 defines a hole 513 for receiving pin 518. Control rod 514 is supported for movement along its axis, Z, by two sleeve bearings 520. Link 516 and pivot arm 514 are connected by a pin 522. Link 516 defines a hole 523 and pivot arm 514 defines a hole 524 for receiving pin 522.

Cylindrical pivot pin 370 of FIG. 25 which receives drive arm 320 is positioned within pivot arm 504. Pivot arm 504 defines holes 526 for receiving cylindrical extensions 378, 380. Shaft 502 is supported for rotation by bearings 530, e.g., ball, sleeve, or roller bearings. A drive, e.g., pulley 532 or gears, mounted to shaft 502 drives the compressor or pump.

In operation, to set the desired stroke of the pistons, control rod 514 is moved along its axis, M, in the direction of arrow 515, causing pivot arm 504 to pivot

about pin 506, along arrow 517, such that pivot pin 370 axis, N, is moved out of alignment with axis, M, (as shown in dashed lines) as pivot arm 504 slides along the axis, H, (FIG. 26) of the transition arm drive arm 320. When zero stroke of the pistons is desired, axes M and N are aligned such that rotation of shaft 514 does not 5 cause movement of the pistons. This configuration works for both double ended and single sided pistons.

The ability to vary the piston stroke permits shaft 514 to be run at a single speed by drive 532 while the output of the pump or compressor can be continually varied as needed. When no output is needed, pivot arm 504 simply spins around drive 10 arm 320 of transition arm 310 with zero swing of the drive arm. When output is needed, shaft 514 is already running at full speed so that when pivot arm 504 is pulled off-axis by control rod 514, an immediate stroke is produced with no lag coming up to speed. There are therefore much lower stress loads on the drive system as there are no start/stop actions. The ability to quickly reduce the stroke to zero provides 15 protection from damage especially in liquid pumping when a downstream blockage occurs.

An alternative method of varying the compression and displacement of the pistons is shown in FIG. 33. The mechanism provides for varying of the position of a counterweight attached to the flywheel to maintain system balance as the stroke of the 20 pistons is varied.

A flywheel 722 is pivotally mounted to an extension 706 of a main drive shaft 708 by a pin 712. By pivoting flywheel 722 in the direction of arrow, Z, flywheel 722 slides along axis, H, of a drive arm 720 of transition arm 710, changing angle, β (Fig. 26), and thus the stroke of the pistons. Pivoting flywheel 722 also 25 causes a counterweight 714 to move closer to or further from axis, A, thus maintaining near rotational balance.

To pivot flywheel 722, an axially and rotationally movable pressure plate 820 is provided. Pressure plate 820 is in contact with a roller 822 rotationally mounted to counterweight 714 through a pin 824 and bearing 826. From the position 30 shown in FIG. 33, a servo motor or hand knob 830 turns a screw 832 which advances to move pressure plate 820 in the direction of arrow, Y. This motion of pressure plate

820 causes flywheel 722 to pivot in the direction of arrow, Z, as shown in the FIG. 34, to decrease the stroke of the pistons. Moving pressure plate 820 by 0.75" decreases the compression ratio from about 12:1 to about 6:1.

Pressure plate 820 is supported by three or more screws 832. Each screw 5 has a gear head 840 which interfaces with a gear 842 on pressure plate 820 such that rotation of screw 832 causes rotation of pressure plate 820 and thus rotation of the remaining screws to insure that the pressure plate is adequately supported. To ensure contact between roller 822 and pressure plate 820, a piston 850 is provided which biases flywheel 722 in the direction opposite to arrow, Z.

10 Referring to FIG. 30, if two cylinders not spaced 180° apart (as viewed from the end) or more than two cylinders are employed in piston assembly 300, the ends of pins 312, 314 coupled to joints 306, 308 will undergo a figure 8 motion. FIG. 30 shows the figure 8 motion of a piston assembly having four double ended pistons. Two of the pistons are arranged flat as shown in FIG. 22 (and do not undergo the 15 figure 8 motion), and the other two pistons are arranged equally spaced between the flat pistons (and are thus positioned to undergo the largest figure 8 deviation possible). The amount that the pins connected to the second set of pistons deviate from a straight line (y axis of FIG. 30) is determined by the swing angle (mast angle) of the drive arm and the distance the pin is from the central pivot point 352 (x axis of 20 FIG. 30).

In a four cylinder version where the pins through the piston pivot assembly of each of the four double ended pistons are set at 45° from the axis of the central pivot, the figure eight motion is equal at each piston pin. Movement in the piston pivot bushing is provided where the figure eight motion occurs to prevent binding.

25 When piston assembly 300 is configured for use, e.g., as a diesel engines, extra support can be provided at the attachment of pins 312, 314 to transition arm 310 to account for the higher compression of diesel engines as compared to spark ignition engines. Referring to FIG. 31, support 550 is bolted to transition arm 310 with bolts 551 and includes an opening 552 for receiving end 554 of the pin.

30 Engines according to the invention can be used to directly apply combustion pressures to pump pistons. Referring to FIGS. 32 and 32a, a four

cylinder, two stroke cycle engine 600 (each of the four pistons 602 fires once in one revolution) applies combustion pressure to each of four pump pistons 604. Each pump piston 604 is attached to the output side 606 of a corresponding piston cylinder 608. Pump pistons 604 extend into a pump head 610.

5 A transition arm 620 is connected to each cylinder 608 and to a flywheel 622, as described above. An auxiliary output shaft 624 is connected to flywheel 622 to rotate with the flywheel, also as described above.

The engine is a two stroke cycle engine because every stroke of a piston 602 (as piston 602 travels to the right as viewed in FIG. 32) must be a power stroke.

10 The number of engine cylinders is selected as required by the pump. The pump can be a fluid or gas pump. In use as a multi-stage air compressor, each pump piston 606 can be a different diameter. No bearing loads are generated by the pumping function (for single acting pump compressor cylinders), and therefore, no friction is introduced other than that generated by the pump pistons themselves.

15 Referring to FIGS. 38-38B, an engine 1010 having vibration canceling characteristics and being particularly suited for use in gas compression includes two assemblies 1012, 1014 mounted back-to-back and 180° out of phase. Engine 1010 includes a central engine section 1016 and outer compressor sections 1018, 1020. Engine section 1016 includes, e.g., six double acting cylinders 1022, each housing a 20 pair of piston 1024, 1026. A power stroke occurs when a center section 1028 of cylinder 1022 is fired, moving pistons 1024, 1026 away from each other. The opposed movement of the pistons results in vibration canceling.

Outer compression section 1018 includes two compressor cylinders 1030 and outer compression section 1020 includes two compressor cylinders 1032, though 25 there could be up to six compressor cylinders in each compression section.

Compression cylinders 1030 each house a compression piston 1034 mounted to one of pistons 1024 by a rod 1036, and compression cylinders 1032 each house a compression piston 1038 mounted to one of pistons 1026 by a rod 1040. Compression cylinders 1030, 1032 are mounted to opposite piston pairs such that the 30 forces cancel minimizing vibration forces which would otherwise be transmitted into mounting 1041.

Pistons 1024 are coupled by a transition arm 1042, and pistons 1026 are coupled by a transition arm 1044, as described above. Transition arm 1042 includes a drive arm 1046 extending into a flywheel 1048, and transition arm 1044 includes a drive arm 1050 extending into a flywheel 1052, as described above. Flywheel 1048 is 5 joined to flywheel 1052 by a coupling arm 1054 to rotate in synchronization therewith. Flywheels 1048, 1052 are mounted on bearings 1056. Flywheel 1048 includes a bevel gear 1058 which drives a shaft 1060 for the engine starter, oil pump and distributor for ignition, not shown.

10 Engine 1010 is, e.g., a two stroke natural gas engine having ports (not shown) in central section 1028 of cylinders 1022 and a turbocharger (not shown) which provides intake air under pressure for purging cylinders 1022. Alternatively, engine 1010 is gasoline or diesel powered.

15 The stroke of pistons 1024, 1026 can be varied by moving both flywheels 1048, 1052 such that the stroke of the engine pistons and the compressor pistons are adjusted equally reducing or increasing the engine power as the pumping power requirement reduces or increases, respectively.

The vibration canceling characteristics of the back-to-back relationship of assemblies 1012, 1014 can be advantageously employed in a compressor only system and an engine only system.

20 Counterweights can be employed to limit vibration of the piston assembly. Referring to FIG. 39, an engine 1100 includes counterweights 1114 and 1116. Counterweight 1114 is mounted to rotate with a rotatable member 1108, e.g., a flywheel, connected to drive arm 320 extending from transition arm 310. Counterweight 1116 is mounted to lower shaft 608 to rotate with shaft 608.

25 Movement of the double ended pistons 306, 308 is translated by transition arm 310 into rotary motion of member 1108 and counterweight 1114. The rotation of member 1108 causes main drive shaft 408 to rotate. Mounted to shaft 408 is a first gear 1110 which rotates with shaft 408. Mounted to lower shaft 608 is a second gear 1112 driven by gear 1110 to rotate at the same speed as gear 1110 and in the opposite 30 direction to the direction of rotation of gear 1110. The rotation of gear 1112 causes rotation of shaft 608 and thus rotation of counterweight 1116.

As viewed from the left in FIG. 39, counterweight 1114 rotates clockwise (arrow 1118) and counterweight 1116 rotates counterclockwise (arrow 1120). Counterweights 1114 and 1116 are mounted 180 degrees out of phase such that when counterweight 1114 is above shaft 408, counterweight 1116 is below shaft 608. A 5 quarter turn results in both counterweights 1114, 1116 being to the right of their respective shafts (see FIG. 40). After another quarter turn, counterweight 1114 is below shaft 408 and counterweight 1116 is above shaft 608. Another quarter turn and both counterweights are to the left of their respective shafts.

Referring to FIG. 40, movement of pistons 306, 308 along the Y axis, in 10 the plane of the XY axes, creates a moment about the Z axis, M_{zy} . When counterweights 1114, 1116 are positioned as shown in FIG. 40, the centrifugal forces due to their rotation creates forces, F_{x1} and F_{x2} , respectively, parallel to the X axis. These forces act together to create a moment about the Z axis, M_{zx} . The weight of counterweights 1114, 1116 is selected such that M_{zx} substantially cancels M_{zy} .

15 When pistons 306, 308 are centered on the X axis (FIG. 39) there are no forces acting on pistons 306, 308, and thus no moment about the Z axis. In this position, counterweights 1114, 1116 are in opposite positions as shown in FIG. 39 and the moments created about the X axis by the centrifugal forces on the counterweights cancel. The same is true after 180 degrees of rotation of shafts 408 and 608, when the 20 pistons are again centered on the X axis and the counterweight 1114 is below shaft 408 and counterweight 1116 is above shaft 608.

Between the quarter positions, the moments about the X axis due to rotation of counterweights 1114 and 1116 cancel, and the moments about the Z axis due to rotation of counterweights 1114 and 1116 add.

25 Counterweight 1114 also accounts for moments produced by drive arm 320.

In other piston configurations, for example where pistons 306, 308 do not lie on a common plane or where there are more than two pistons, counterweight 1116 is not necessary because at no time is there no moment about the Z axis requiring the 30 moment created by counterweight 1114 to be cancelled.

One moment not accounted for in the counterbalancing technique of FIGS. 39 and 40 a moment about axis Y, M_{yx} , produced by rotation of counterweight 1116. Another embodiment of a counterbalancing technique which accounts for all moments is shown in FIG. 41. Here, a counterweight 1114a mounted to rotating member 1108 5 is sized to only balance transition arm 310. Counterweights 1130, 1132 are provided to counterbalance the inertial forces of double-ended pistons 306, 308.

Counterweight 1130 is mounted to gear 1110 to rotate clockwise with gear 1110. Counterweight 1132 is driven through a pulley system 1134 to rotate 10 counterclockwise. Pulley system 1134 includes a pulley 1136 mounted to rotate with shaft 608, and a chain or timing belt 1138. Counterweight 1132 is mounted to shaft 408 by a pulley 1140 and bearing 1142. Counterclockwise rotation of pulley 1136 causes counterclockwise rotation of chain or belt 1138 and counterclockwise rotation of counterweight 1132.

Referring to FIG. 42, as discussed above, movement of pistons 306, 308 15 along the Y axis, in the plane of the XY axes, creates a moment about the Z axis, M_{zy} . When counterweights 1130, 1132 are positioned as shown in FIG. 42, the centrifugal forces due to their rotation creates forces, F_{x3} and F_{x4} , respectively, in the same direction along the X axis. These forces act together to create a moment about the Z axis, M_{zx} . The weight of counterweights 1130, 1132 is selected such that M_{zx} 20 substantially cancels M_{zy} .

When pistons 306, 308 are centered on the X axis (FIG. 41) there are no forces acting on pistons 306, 308, and thus no moment about the Z axis. In this position, counterweights 1130, 1132 are in opposite positions as shown in FIG. 41 and the moments created about the X axis by the centrifugal forces on the counterweights 25 cancel. The same is true after 180 degrees of rotation of shafts 408 and 608, when the pistons are again centered on the X axis and the counterweight 1130 is below shaft 408 and counterweight 1132 is above shaft 408.

Between the quarter positions, the moments about the X axis due to 30 rotation of counterweights 1130 and 1132 cancel, and the moments about the Z axis due to rotation of counterweights 1130 and 1132 add. Since counterweights 1130 and 1132 both rotate about the Y axis, there is no moment M_{yx} created about axis Y.

Counterweights 1130, 1132 are positioned close together along the Y axis to provide near equal moments about the Z axis. The weights of counterweights 1130, 1132 can be slightly different to account for their varying location along the Y axis so that each counterweight generates the same moment about the center of gravity of the engine.

Counterweights 1130, 1132, in addition to providing the desired moments about the Z axis, create undesirable lateral forces directed perpendicular to the Y-axis (in the direction of the X axis), which act on the U-joint or other mount supporting transition arm 310. When counterweights 1130, 1132 are positioned as shown in FIG. 10 41, this does not occur because the upward force, F_u , and the downward force, F_d , cancel. But, when counterweights 1130, 1132 are positioned other than as shown in FIG. 41 or 180° from that position, this force is applied to the mount. For example, as shown in FIG. 42, forces F_{x3} and F_{x4} create a side force, F_s , along the X axis. One technique of incorporating counterbalances which provide the desired moments about 15 the Z axis without creating the undesirable forces on the mount is shown in FIG. 43.

Referring to FIG. 43, a second pair of counterweights 1150, 1152 are provided. Counterweights 1130 and 1152 are mounted to shaft 408 to rotate clockwise with shaft 408. Counterweights 1132 and 1150 are mounted to a cylinder 1154 surrounding shaft 408 which is driven through pulley system 1134 to rotate 20 counterclockwise. Counterweights 1130, 1152 extend from opposite sides of shaft 408 (counterweight 1130 being directed downward in Fig. 43, and counterweight 1152 being directed upward), and counterweights 1132, 1150 extend from opposite sides of cylinder 1154 (counterweight 1132 being directed upward, and counterweight 1150 being directed downward). Counterweights 1130, 1150 are aligned on the same 25 side of shaft 408, and counterweights 1132, 1152 are aligned on the opposite side of shaft 408.

Referring to FIG. 44, with counterweights 1130, 1132, 1150, 1152 positioned as shown, the centrifugal forces due to the rotation of counterweights 1130, 1132 creates forces, F_{x3} and F_{x4} , respectively, in the same direction in the X axis, and 30 the centrifugal forces due to the rotation of counterweights 1150, 1152 creates forces, F_{x5} and F_{x6} , respectively, in the opposite direction in the X axis. Since F_{x3} and F_{x4}

are equal and opposite to F_{x5} and F_{x6} , these forces cancel such that no undesirable lateral forces are applied to the transition arm mount.

In addition, as discussed above, movement of pistons 306, 308 in the direction of the Y axis, in the plane of the XY axes, creates a moment about the Z axis, M_{zy} . Since counterweights 1130, 1132, 1150, 1152 are substantially the same weight, and counterweights 1150, 1152 are located further from the Z axis than counterweights 1130, 1132, the moment created by counterweights 1150, 1152 is larger than the moment created by counterweights 1130, 1132 such that these forces act together to create a moment about the Z axis, M_{zx} , which acts in the opposite direction to M_{zy} . The weight of counterweights 1130, 1132, 1150, 1152 is selected such that M_{zx} substantially cancels M_{zy} .

When pistons 306, 308 are centered on the X axis (FIG. 43), there is no moment about the Z axis. In this position, counterweights 1130, 1132 are oppositely directed and counterweights 1150, 1152 are oppositely directed such that the moments created about the X axis by the centrifugal forces on the counterweights cancel.

Likewise, the forces created perpendicular to the Y axis, F_u and F_d , cancel. The same is true after 180 degrees of rotation of shafts 408 and 608, when the pistons are again centered on the X axis.

Counterweight 1130 can be incorporated into flywheel 1108, thus
20 eliminating one of the counterweights.

Referring to FIG. 45, another configuration for balancing a piston engine having two double ended pistons 306, 308 180° apart around the Y axis includes two members 1160, 1162, which each simulate a double ended piston, and two counterweights 1164, 1166. Members 1160, 1162 are 180° apart and equally spaced
25 between pistons 306, 308. Counterweights 1164, 1166 extend from opposite sides of shaft 408, with counterweight 1166 being spaced further from the Z axis than counterweight 1164. Here again, counterweight 1114a mounted to rotating member 1108 is sized to only balance transition arm 310.

Movement of members 1160, 1162 along the Y axis, in the plane of the
30 YZ axis, creates a moment about the X axis, M_{xy} . When counterweights 1164, 1166 are positioned as shown in FIG. 45, the centrifugal forces due to the rotation of

counterweights 1164, 1166 creates forces, F_u and F_d , respectively, in opposite directions along the Z axis. Since counterweight 1166 is located further from the Z axis than counterweight 1164, the moment created by counterweight 1166 is larger than the moment created by counterweight 1164 such that these forces act together to 5 create a moment about the X axis, M_{xz} , which acts in the opposite direction to M_{xy} . The weight of counterweights 1164, 1166 is selected such that M_{xz} substantially cancels M_{xy} .

In addition, since the forces, F_u and F_d , are oppositely directed, these forces cancel such that no undesirable lateral forces are applied to the transition arm 10 mount.

Referring to FIG. 46, movement of pistons 306, 308 along the Y axis, in the plane of the XY axes, creates a moment about the Z axis, M_{zy} . When counterweights 1164, 1166 are positioned as shown in FIG. 45, the centrifugal forces due to the rotation of counterweights 1164, 1166 creates forces, F_{x7} and F_{x8} , 15 respectively, in opposite directions along the X axis. These forces act together to create a moment about the Z axis, M_{zx} , which acts in the opposite direction to M_{zy} . The weight of counterweights 1164, 1166 is selected such that M_{zx} substantially cancels M_{zy} .

. In addition, since the forces perpendicular to Y axis, F_{x7} and F_{x8} , are 20 oppositely directed, these forces cancel such that no undesirable lateral forces are applied to the transition arm mount.

Counterweight 1164 can be incorporated into flywheel 1108 thus eliminating one of the counterweights.

The piston engine can include any number of pistons and simulated piston 25 counterweights to provide the desired balancing, e.g., a three piston engine can be formed by replacing one of the simulated piston counterweights in FIG. 43 with a piston, and a two piston engine can be formed with two pistons and one simulated piston counterweight equally spaced about the transition arm.

If the compression ratio of the pistons is changed, the position of the 30 counterweights along shaft 408 is adjusted to compensate for the resulting change in moments.

Another undesirable force that can be advantageously reduced or eliminated is a thrust load applied by transition arm 310 to flywheel 1108 that is generated by the circular travel of transition arm 310. Referring to FIG. 47, the circular travel of transition arm 310 generates a centrifugal force, C_1 , which is 5 transmitted through nose pin 320 and sleeve bearing 376 to flywheel 1108. Although counterweight 1114 produces a centrifugal force in the direction of arrow 2010 which balances force C_1 , at the 15° angle of nose pin 320, a lateral thrust, T , of 26% of the centrifugal force, C_1 , is also produced. The thrust can be controlled by placing thrust bearings or tapered roller bearings 2040 on shaft 408.

10 To reduce the load on bearings 2040, and thus increase the life of the bearings, as shown in FIG. 48, nose pin 320a is spherically shaped with flywheel 1108a defining a spherical opening 2012 for receiving the spherical nose pin 320a. Because of the spherical shapes, no lateral thrust is produced by the centrifugal force, C_1 .

15 FIG. 49 shows another method of preventing the application of a thrust load to the transition arm. Here, a counterbalance element 2014, rather than being an integral component of the flywheel 1108b, is attached to the flywheel by bolts 2016. The nose pin 320b includes a spherical portion 2018 and a cylindrical portion 2020. Counterbalance element 2014 defines a spherical opening 2022 for receiving spherical 20 portion 2018 of nose pin 320b. Cylindrical portion 2020 of nose pin 320b is received within a sleeve bearing 2024 in a cylindrical opening 2026 defined by flywheel 1108b. Because of the spherical shapes, no lateral thrust is produced by the centrifugal force, C_1 .

Counterbalance element 2014 is not rigidly held to flywheel 1108b so that 25 there is no restraint to the full force of the counterweight being applied to the spherical joint to cancel the centrifugal force created by the circular travel of transition arm 310. For example, a clearance space 2030 is provided in the screw holes 2032 defined in counterbalance element 2014 for receiving bolts 2016.

One advantage of this embodiment over that of FIG. 48 is that the life 30 expectancy of a cylindrical joint with a sleeve bearing coupling the transition arm to

the flywheel is longer than that of the spherical joint of FIG. 48 coupling the transition arm to the flywheel.

Other embodiments are within the scope of the following claims.

For example, the double-ended pistons of the forgoing embodiments can
5 be replaced with single-ended pistons having a piston at one end of the cylinder and a guide rod at the opposite end of the cylinder, such as the single-ended pistons shown in FIG. 32 where element 604, rather than being a pump piston acts as a guide rod.

10 The various counterbalance techniques, variable-compression embodiments, and piston to transition arm couplings can be integrated in a single engine.

What is claimed is:

60412-3619

CLAIMS:

1. A piston assembly comprising:

at least one piston coupled to a transition arm;

the transition arm having a drive arm

5 eccentrically coupled to a rotatable member about a rotation axis such that there is an angle between the drive arm and the rotation axis;

the axis of movement of said piston being spaced from the rotation axis,

10 whereby the transition arm translates between rotational movement of the rotatable member and reciprocal linear movement of said piston,

wherein a counterbalance spaced from the rotatable member is mounted for rotation about the rotation axis, and

15 wherein a counterbalancing member simulating a piston is mounted on the transition arm.

2. The piston assembly of claim 1 wherein the piston simulating counterbalancing member is mounted to the transition arm such that the movement of the transition arm 20 simulates a moment that would be created by at least one piston mounted to the transition arm.

3. The piston assembly of claim 1 or claim 2 including a second counterbalance mounted to rotate in the same direction as the first counterbalance.

25 4. The piston assembly of claim 3 wherein the second counterbalance is incorporated into the rotating member.

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5. The piston assembly of claim 3 wherein the second counterbalance is spaced from the rotating member.

6. The piston assembly of claim 3 or claim 5 including a drive shaft extending from and coupled to the 5 rotating member to rotate in the first direction, the first and second counterbalances being mounted to the drive shaft for rotation therewith.

7. The piston assembly of any one of claims 3 to 6 including a third counterbalance incorporated into the 10 rotating member.

8. The piston assembly of any one of claims 1 to 7 including at least one additional counterbalancing member coupled to the transition arm.

9. The piston assembly of claim 8 wherein the 15 counterweight, said at least one additional member and the piston are equally spaced about the transition arm.

10. The piston assembly of claim 8 or claim 9 wherein said at least one additional member comprises a piston.

11. The piston assembly of claim 8 or claim 9 wherein 20 said at least one additional member is an additional counterbalance that simulates a piston.

12. The piston assembly of any one of claims 1 to 11 wherein the piston is a double-ended piston.

13. The piston assembly of any one of claims 1 to 11 25 wherein the piston comprises a single-ended piston with a guide rod.

14. The piston assembly of any one of claims 1 to 13 including a plurality of said pistons.

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15. A method of counterbalancing a piston assembly; comprising at least one piston coupled to a transition arm, the transition arm having a drive arm eccentrically coupled to a rotatable member about a rotation axis such that there
5 is an angle between the drive arm and the rotation axis, and the axis of movement of said piston being spaced from the rotation axis, whereby the transition arm translates between rotational movement of the rotatable member and reciprocal linear movement of said piston, in which method a
10 counterbalance spaced from the rotatable member is mounted for rotation about the rotation axis, and a counterbalancing member simulating a piston is mounted on the transition arm.

16. A method according to claim 15 wherein the assembly includes a plurality of said pistons.

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OTTAWA, CANADA

PATENT AGENTS

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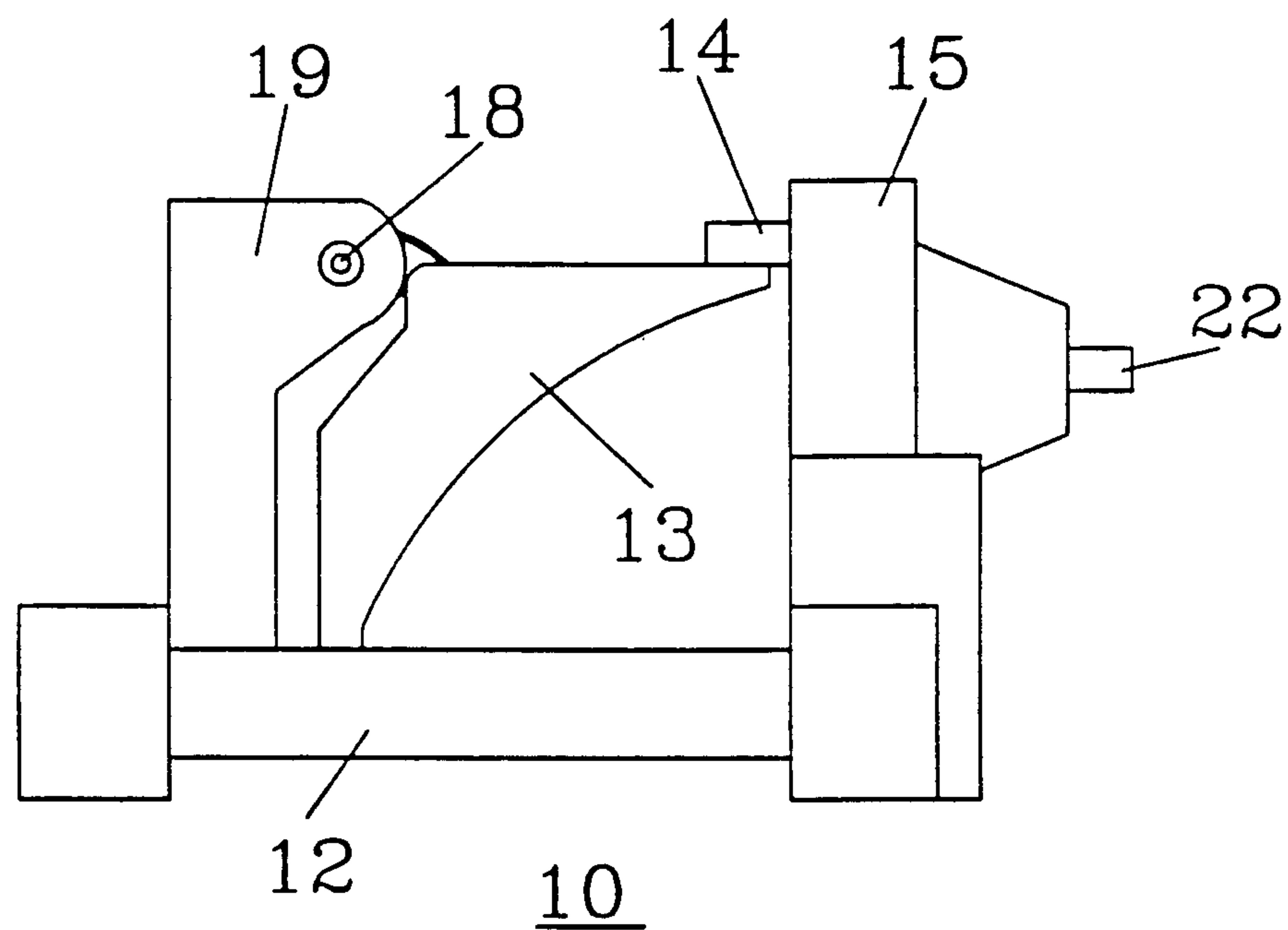


FIG. 1

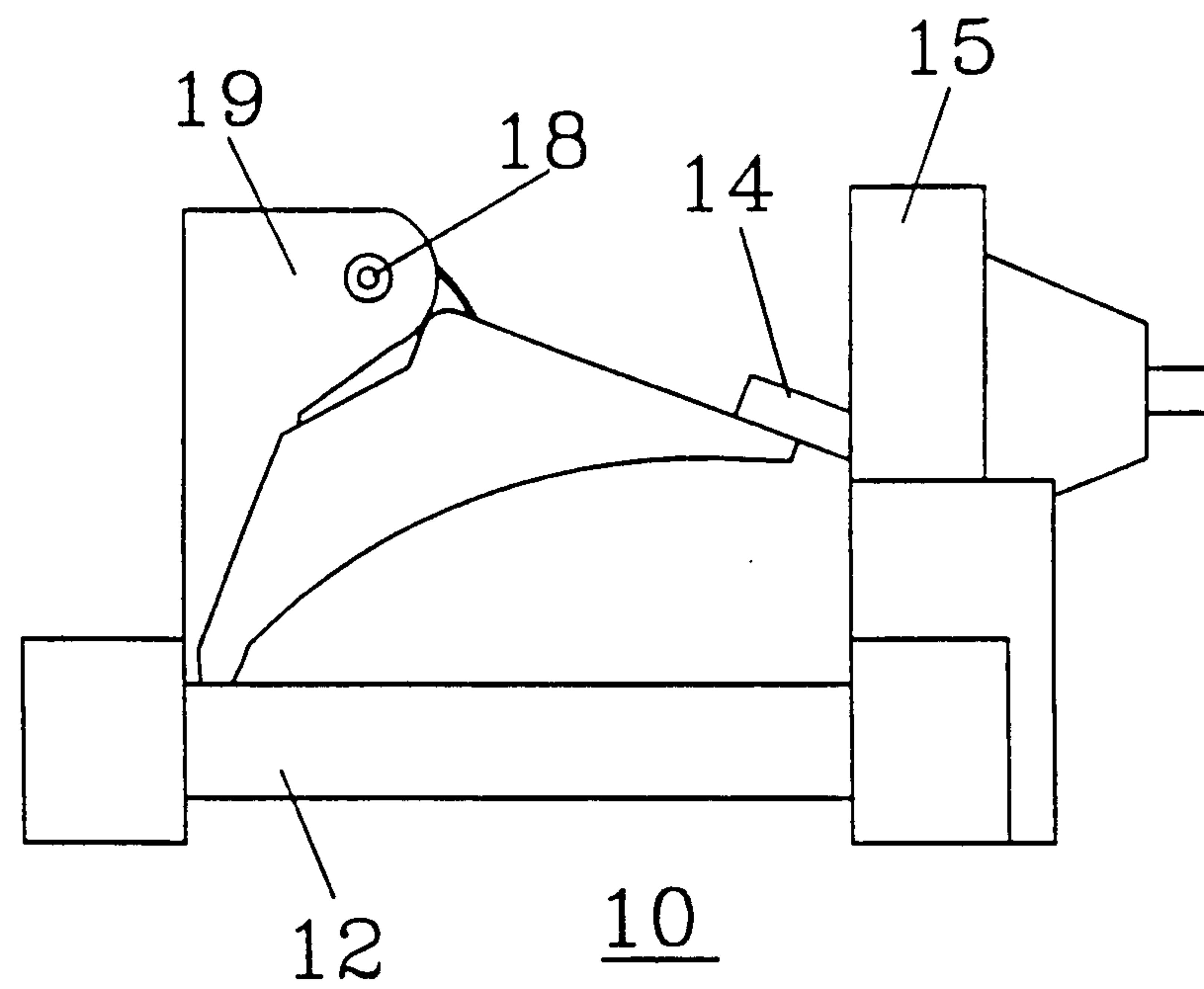


FIG. 2

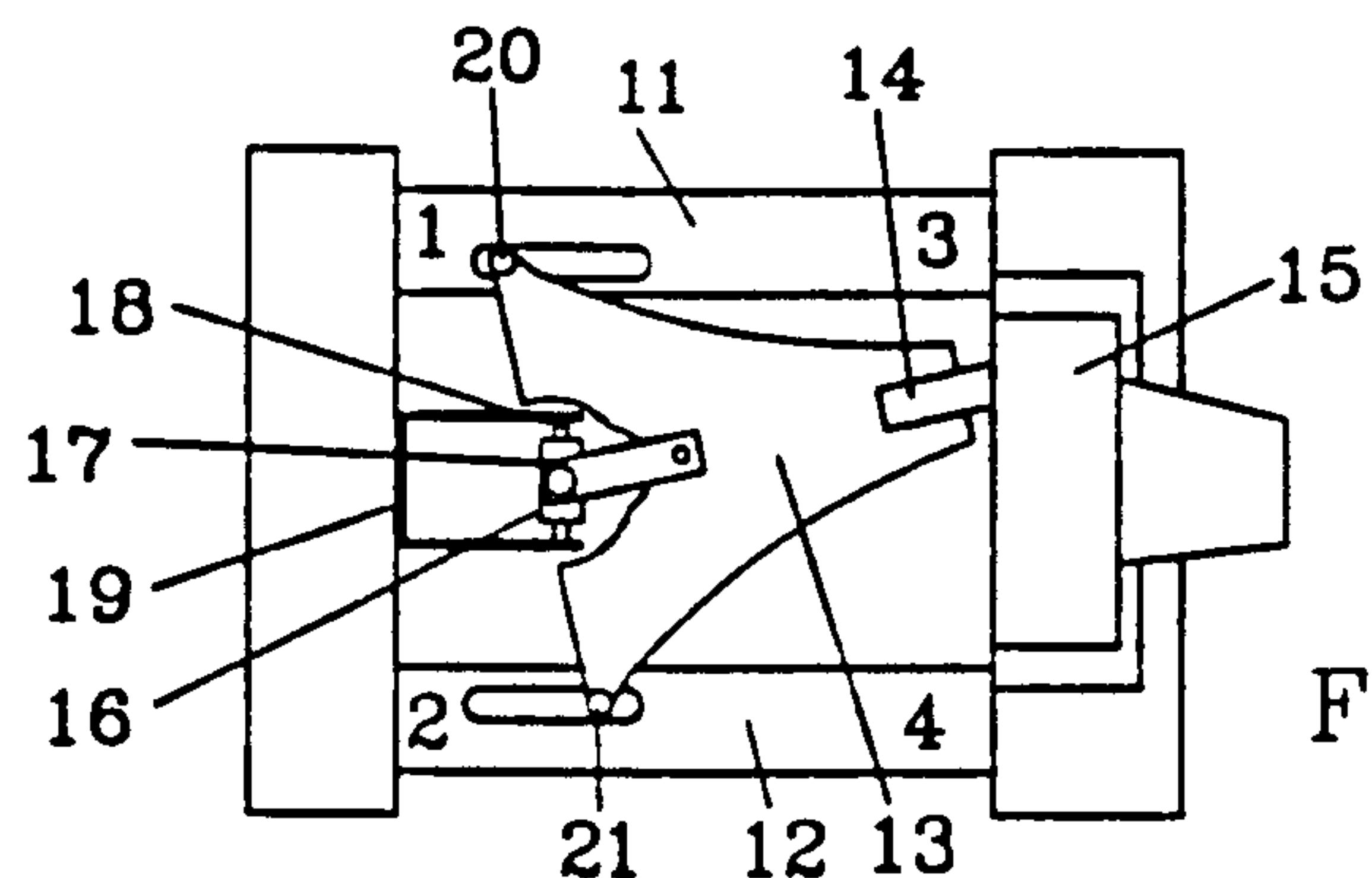


FIG. 3

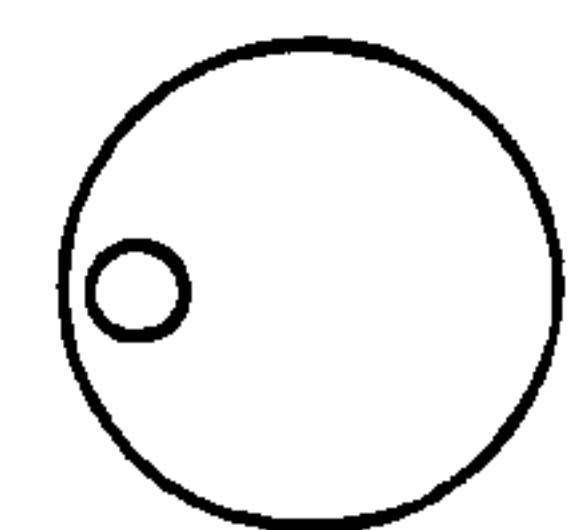


FIG. 3a

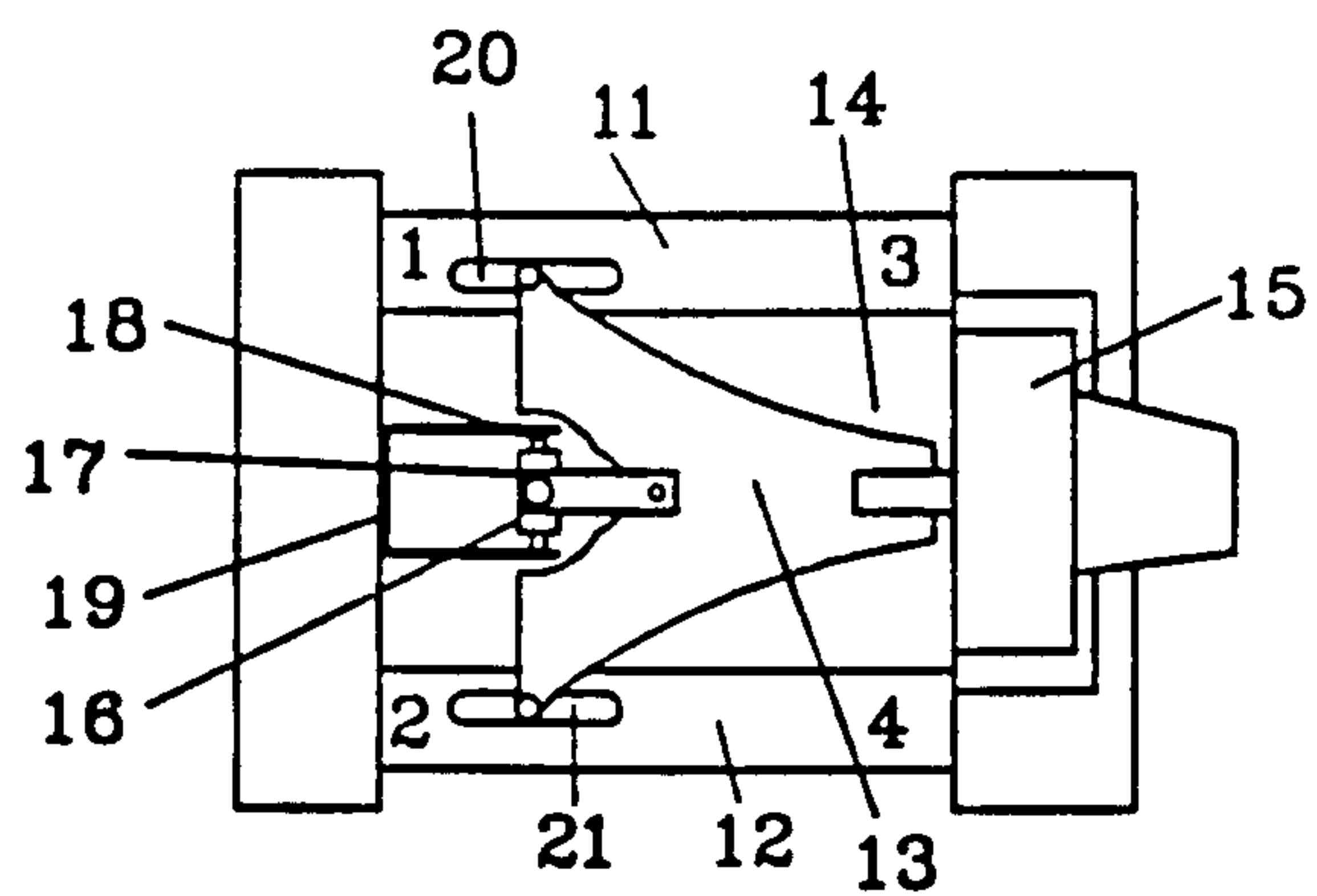


FIG. 4

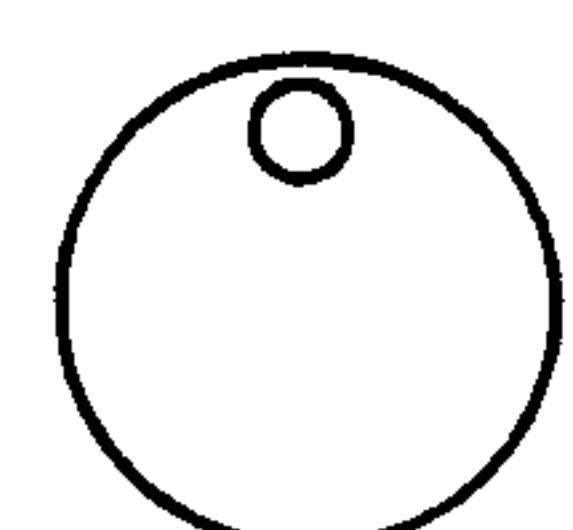


FIG. 4a

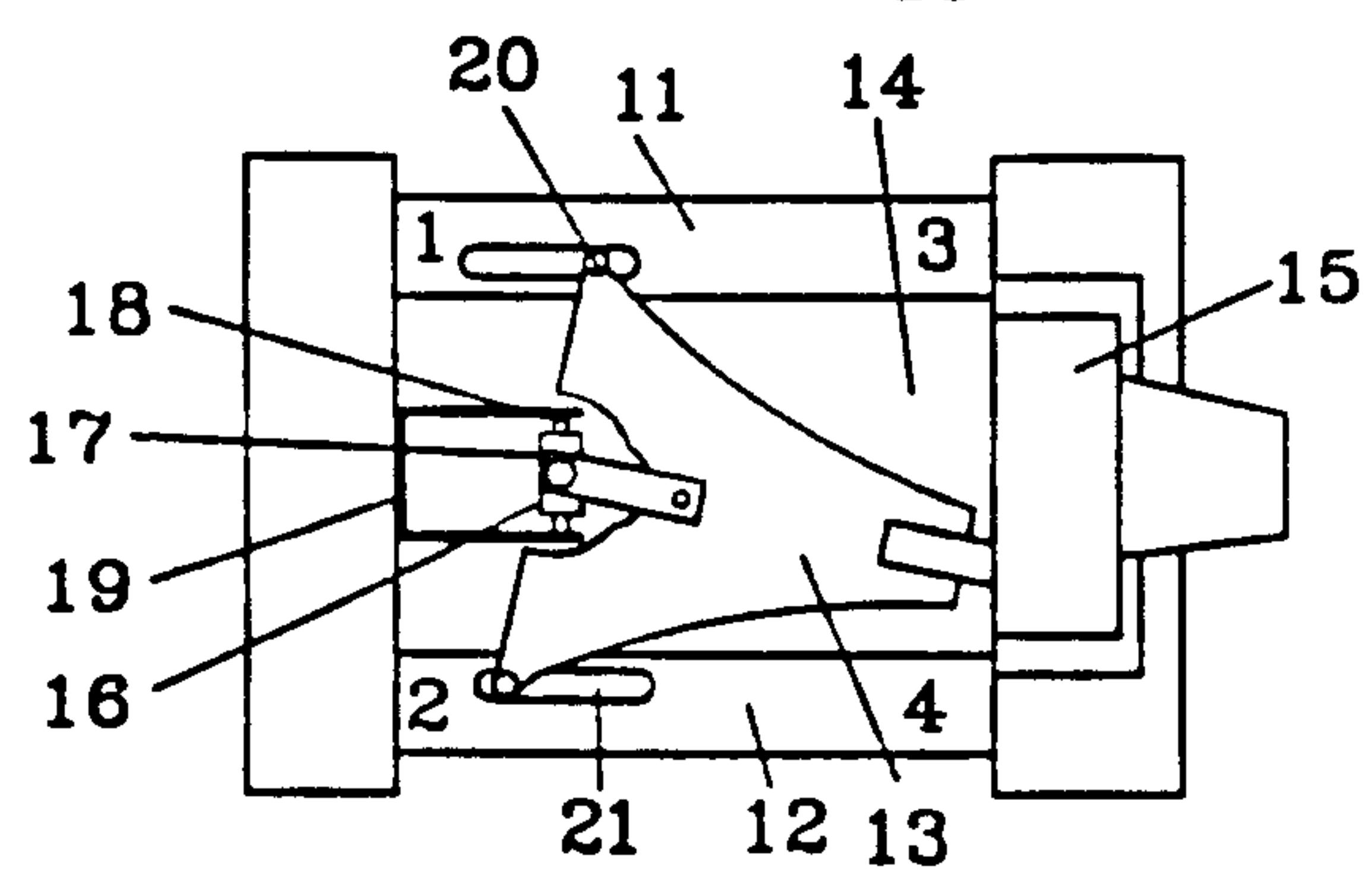


FIG. 5

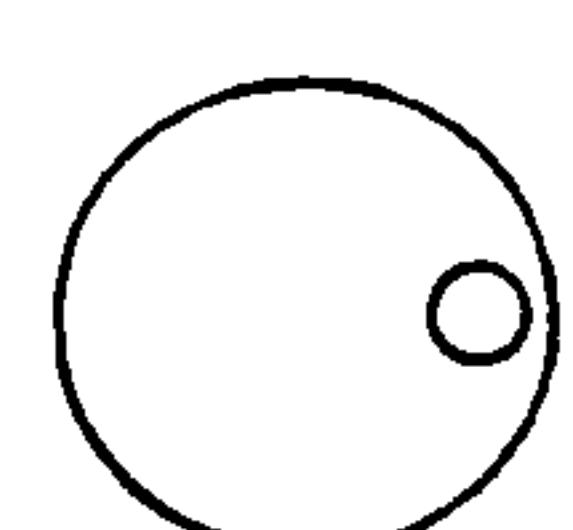


FIG. 5a

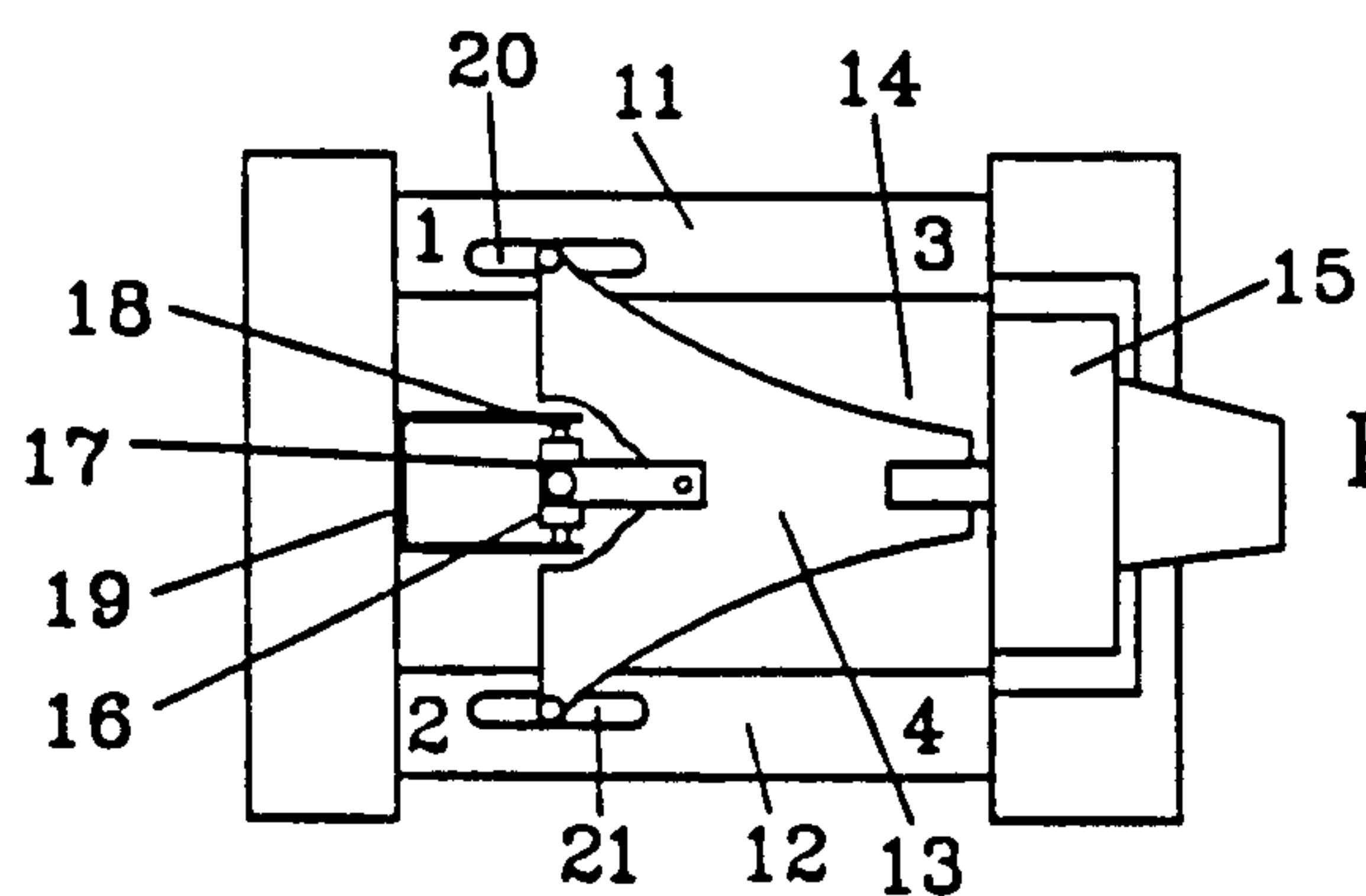


FIG. 6

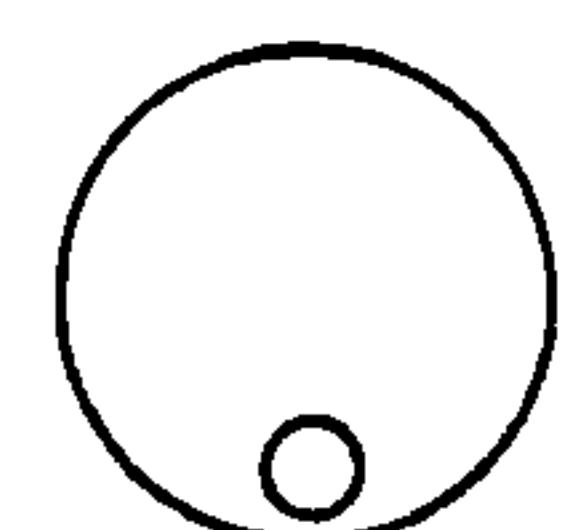


FIG. 6a

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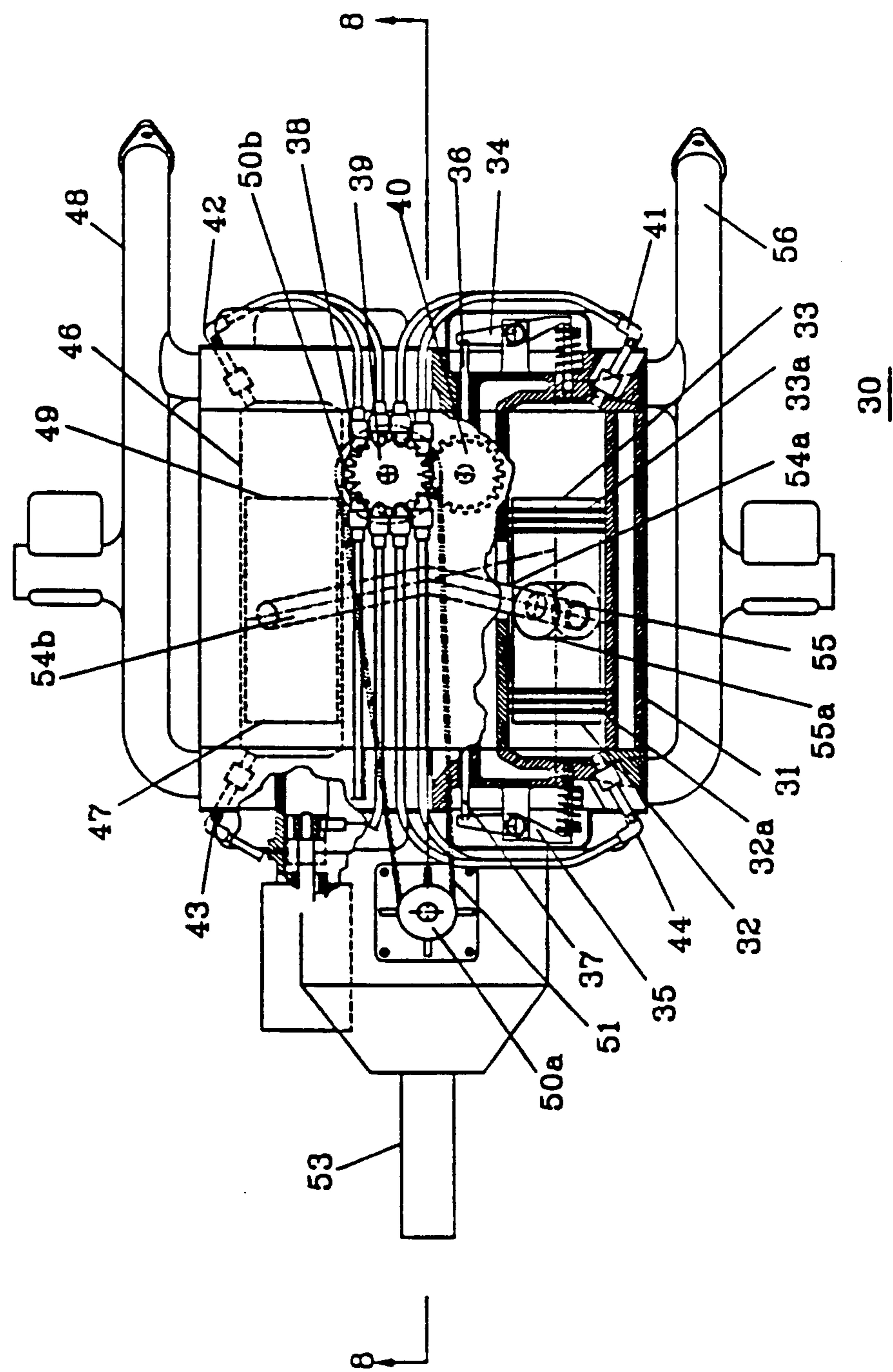


FIG. 7

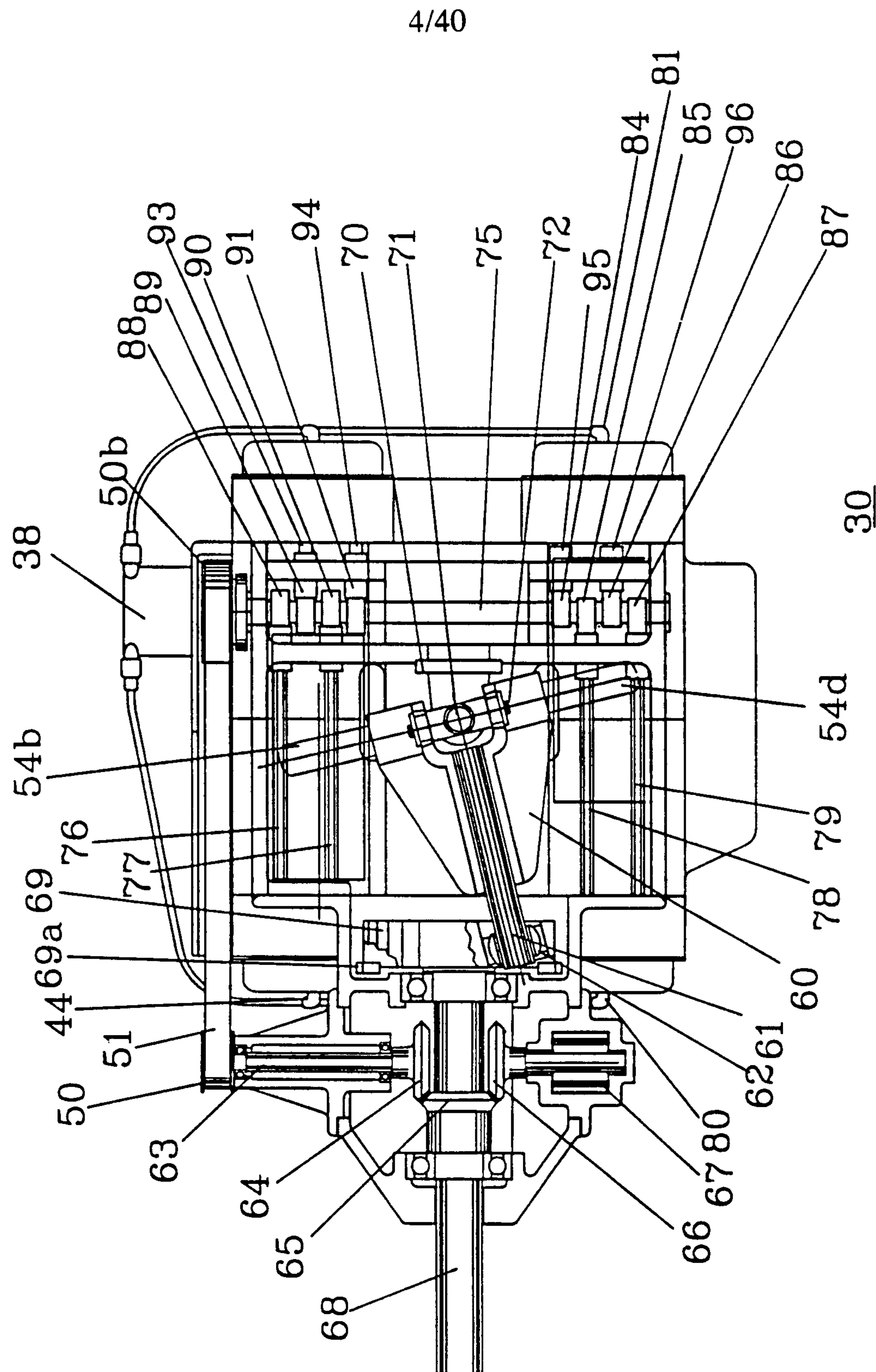


FIG. 8

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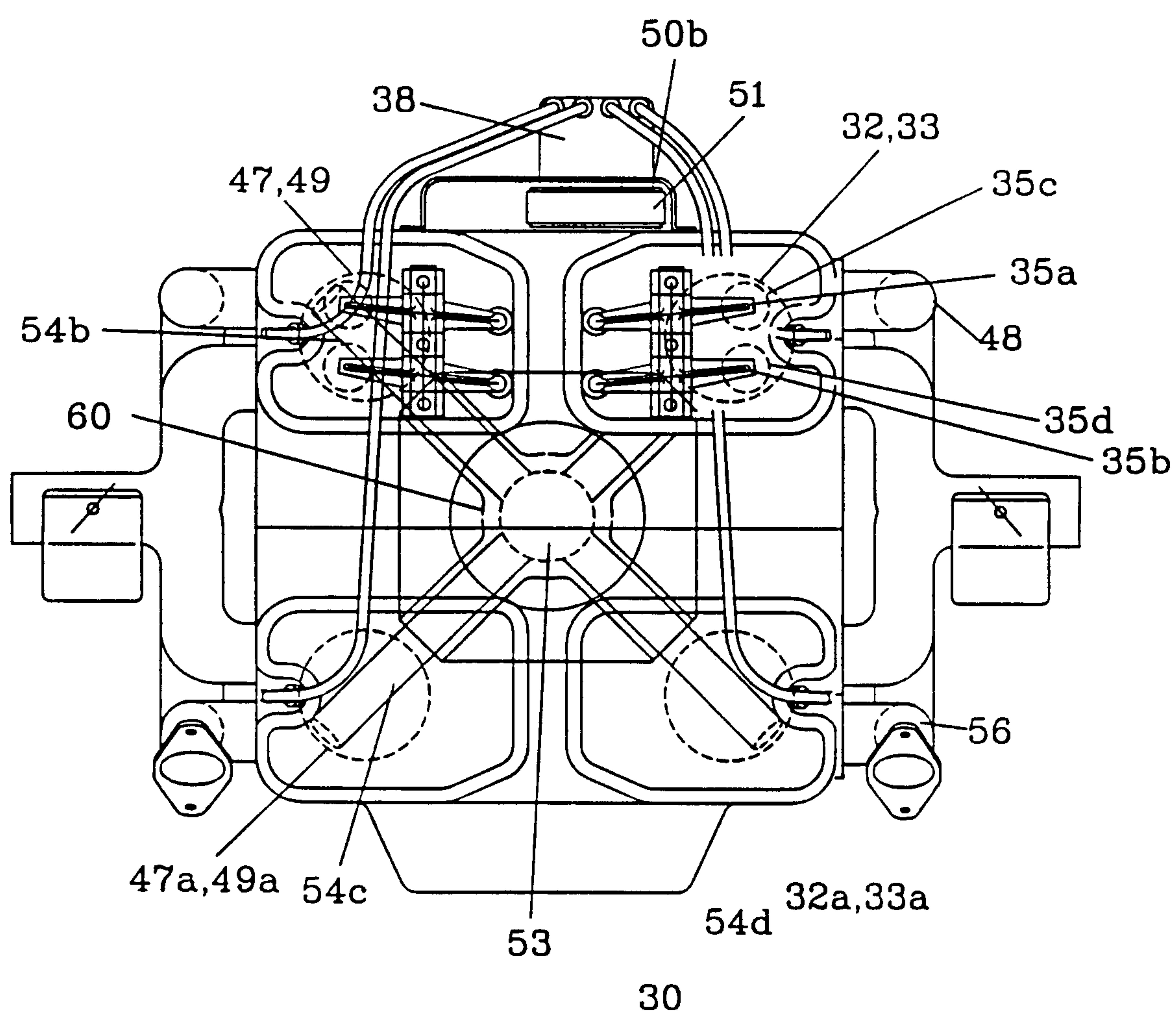
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FIG. 9

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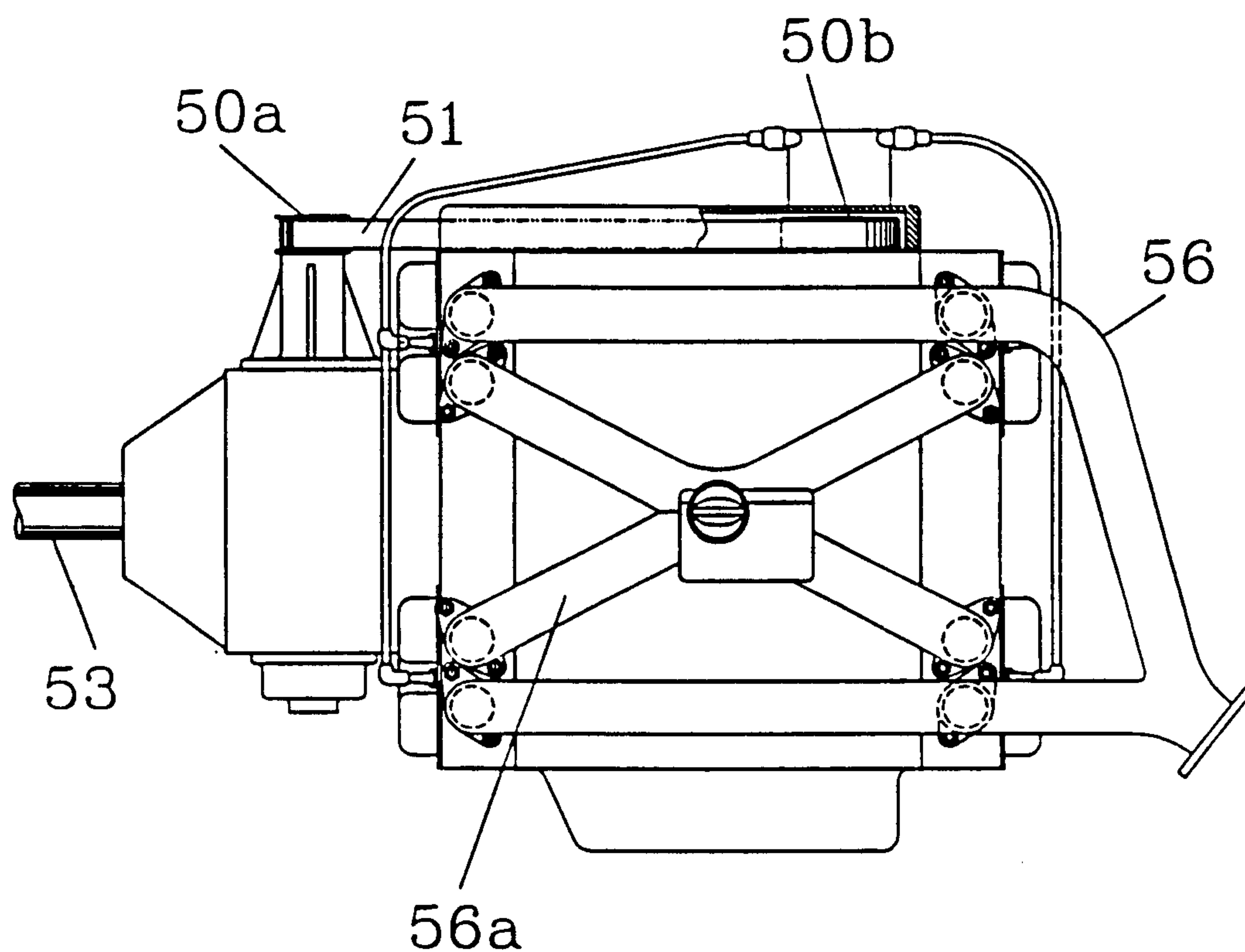


FIG. 10

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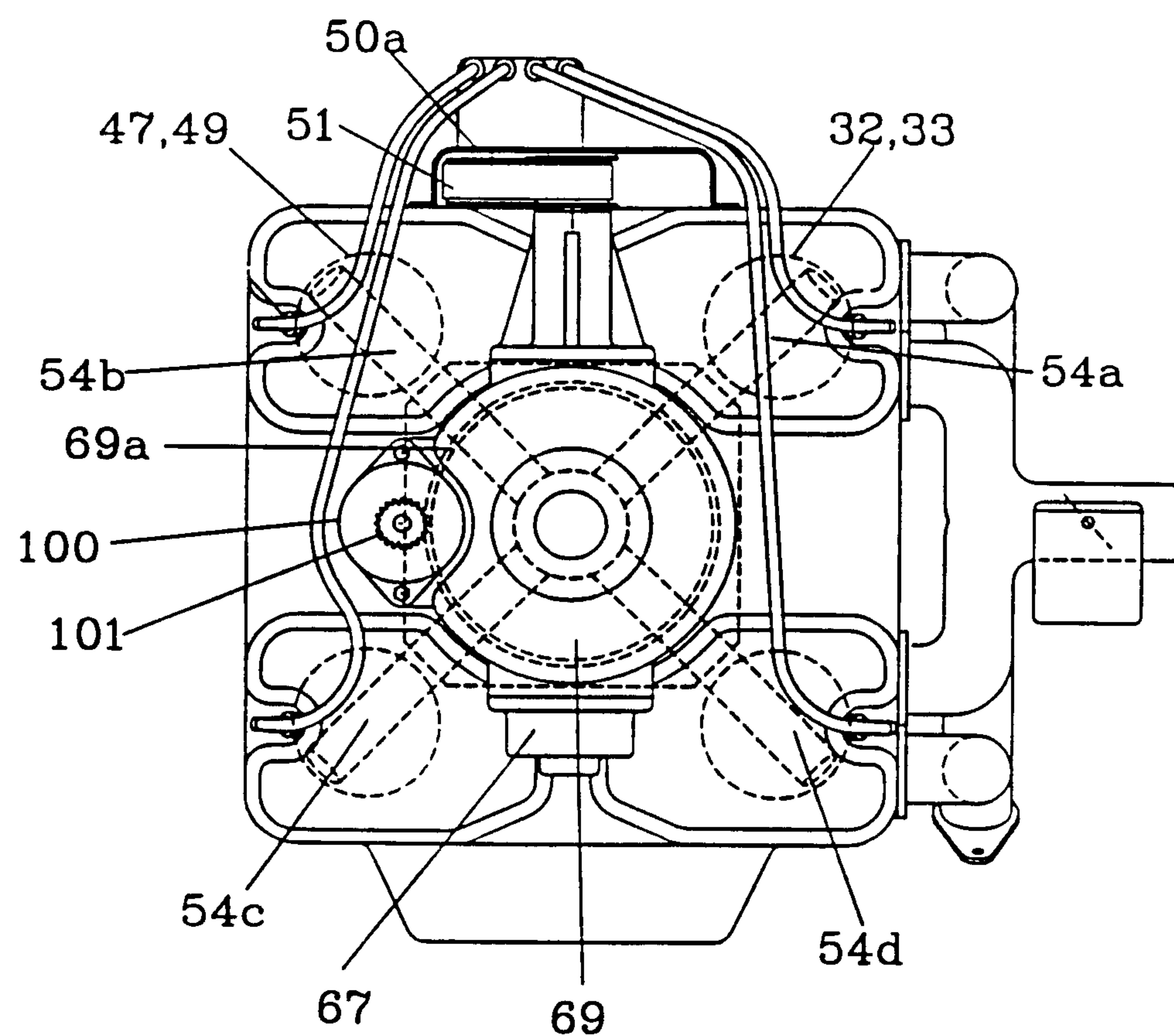


FIG. 11

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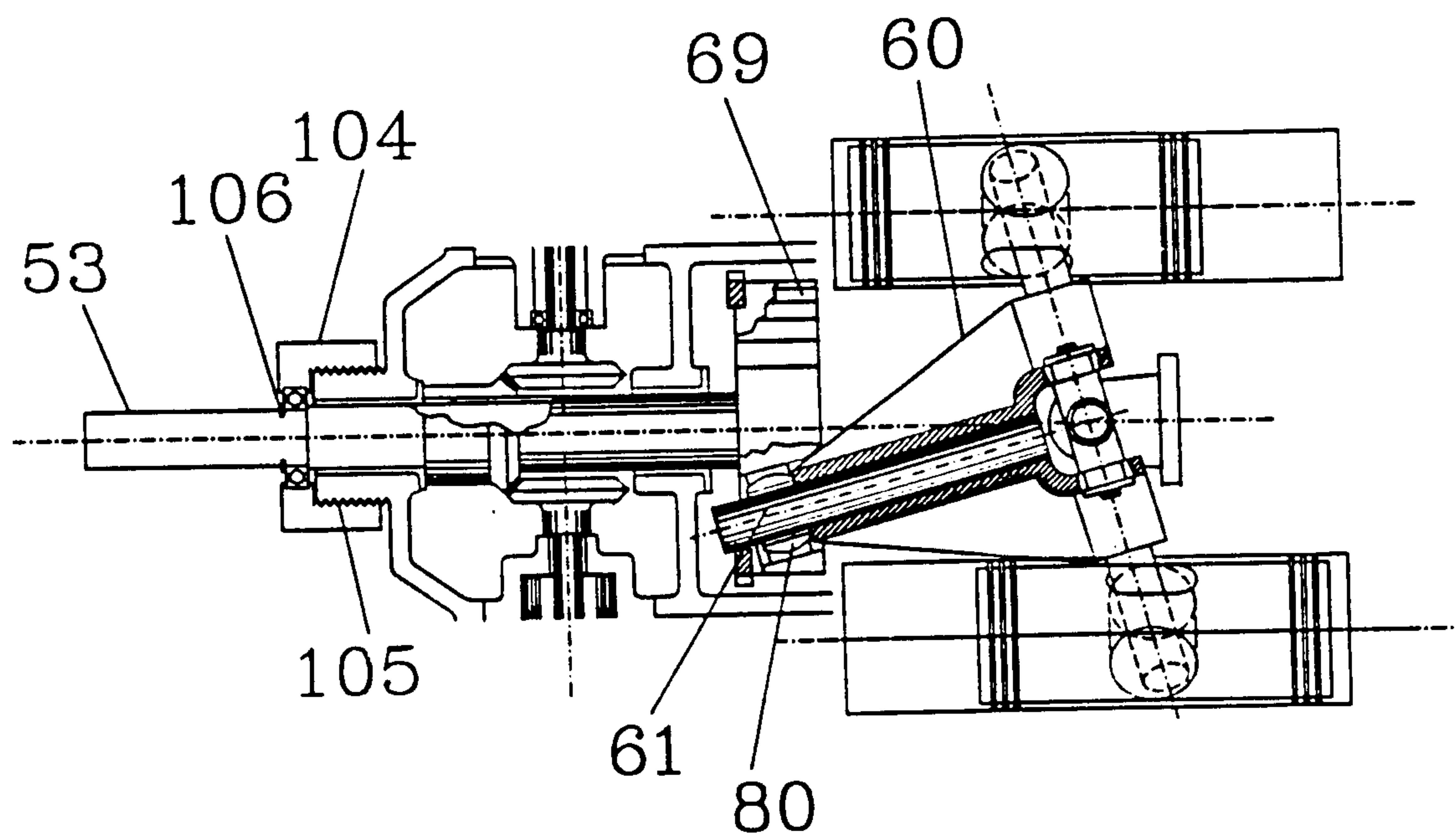


FIG. 12

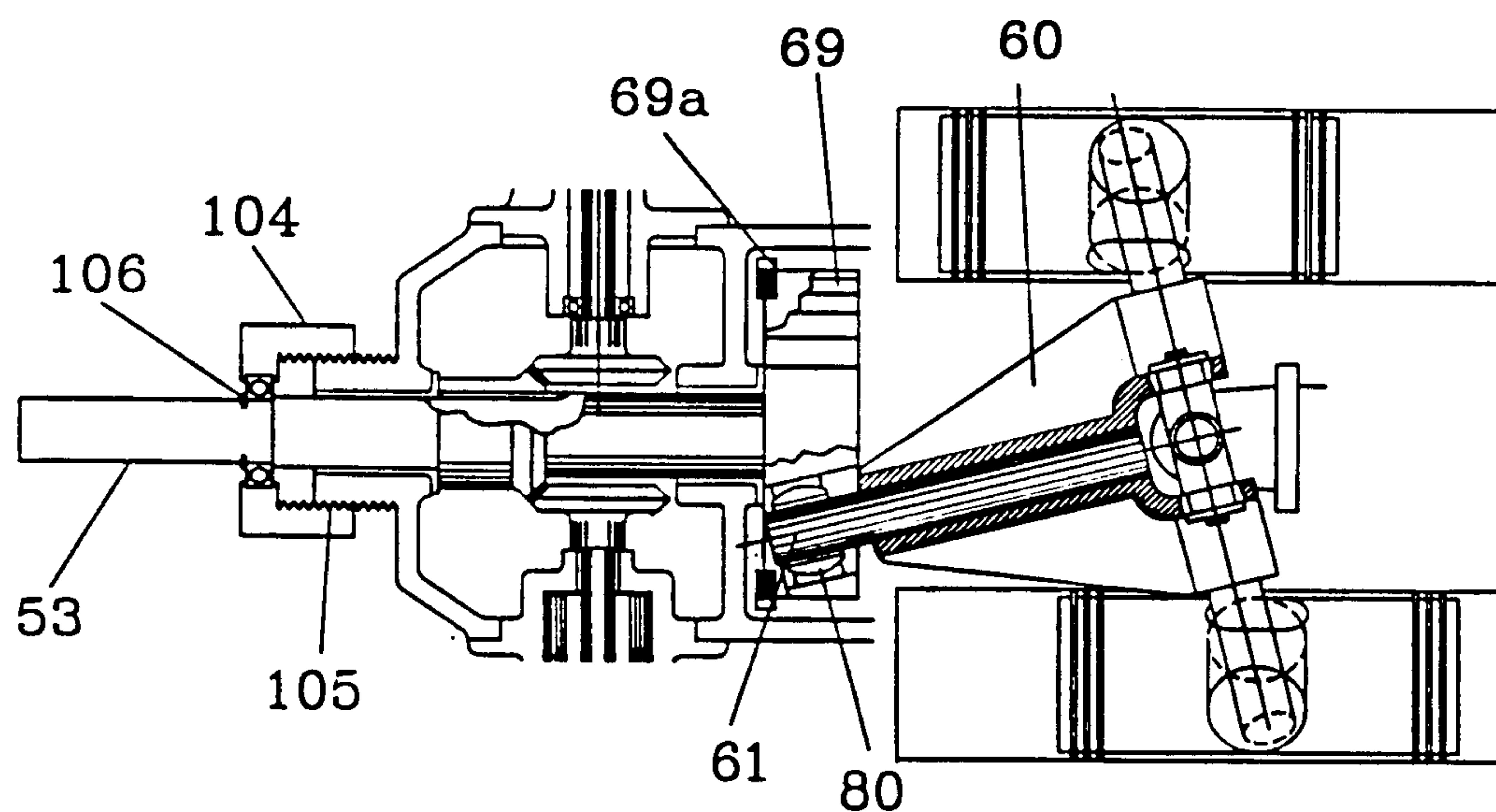
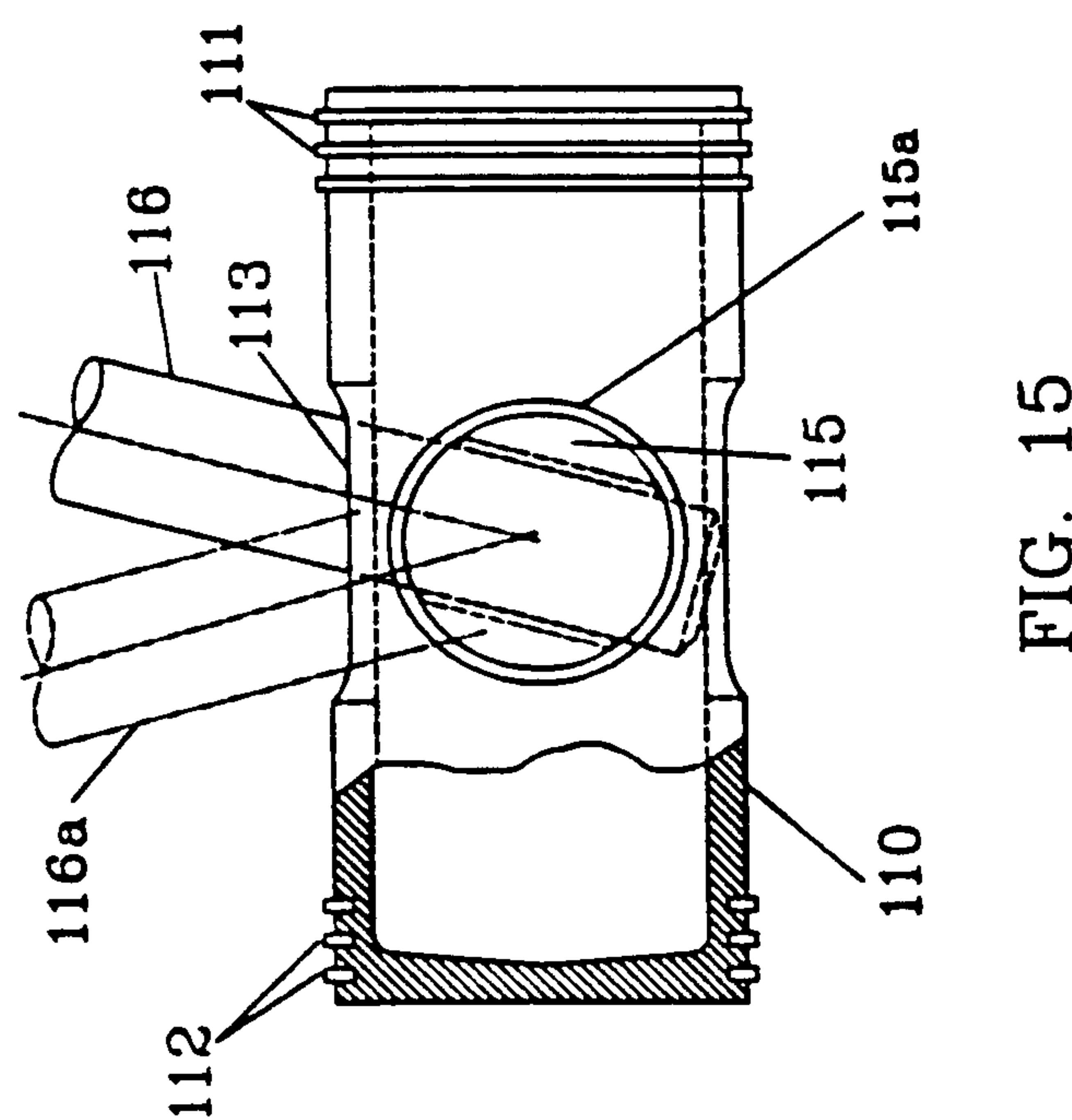
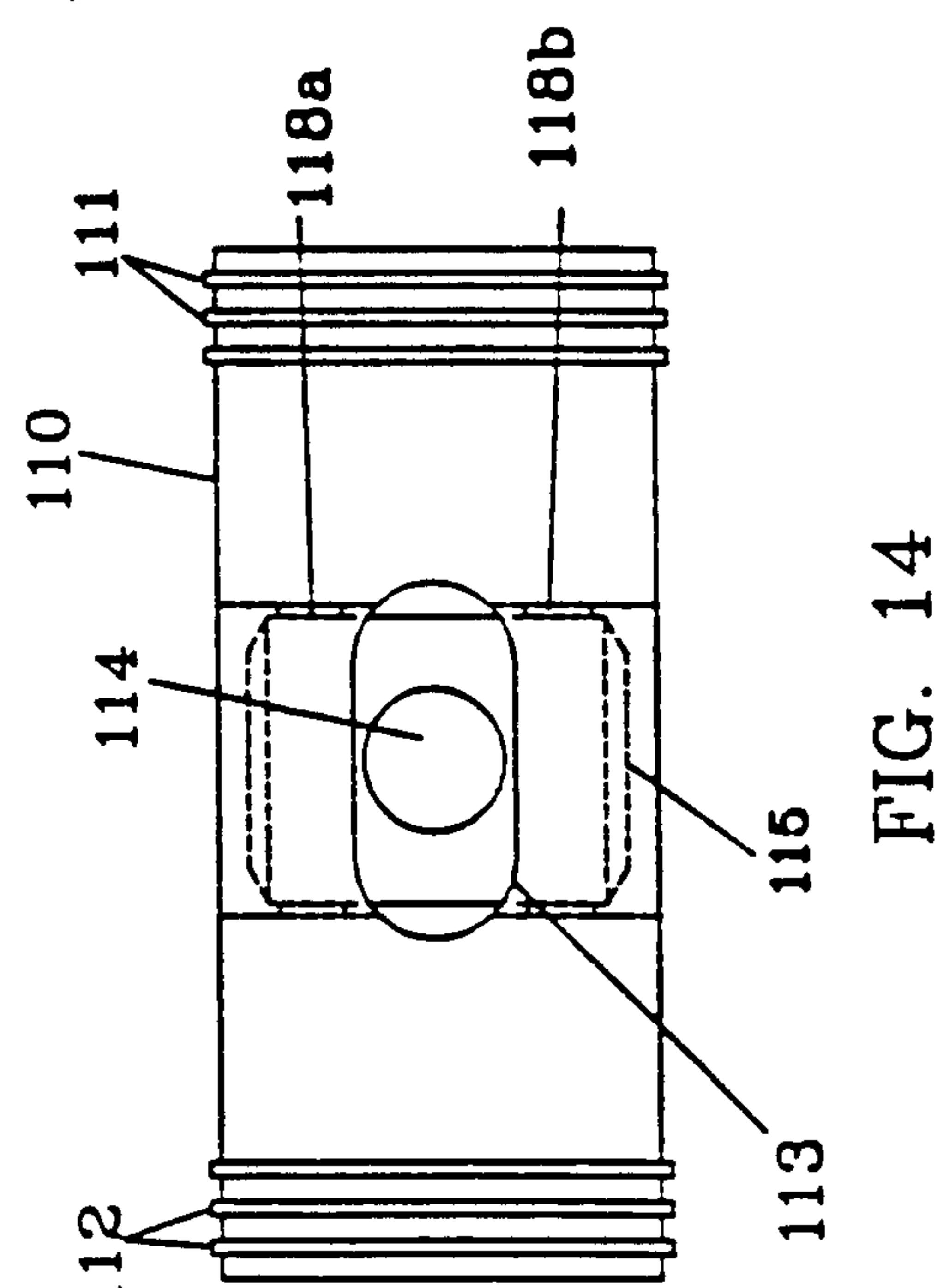
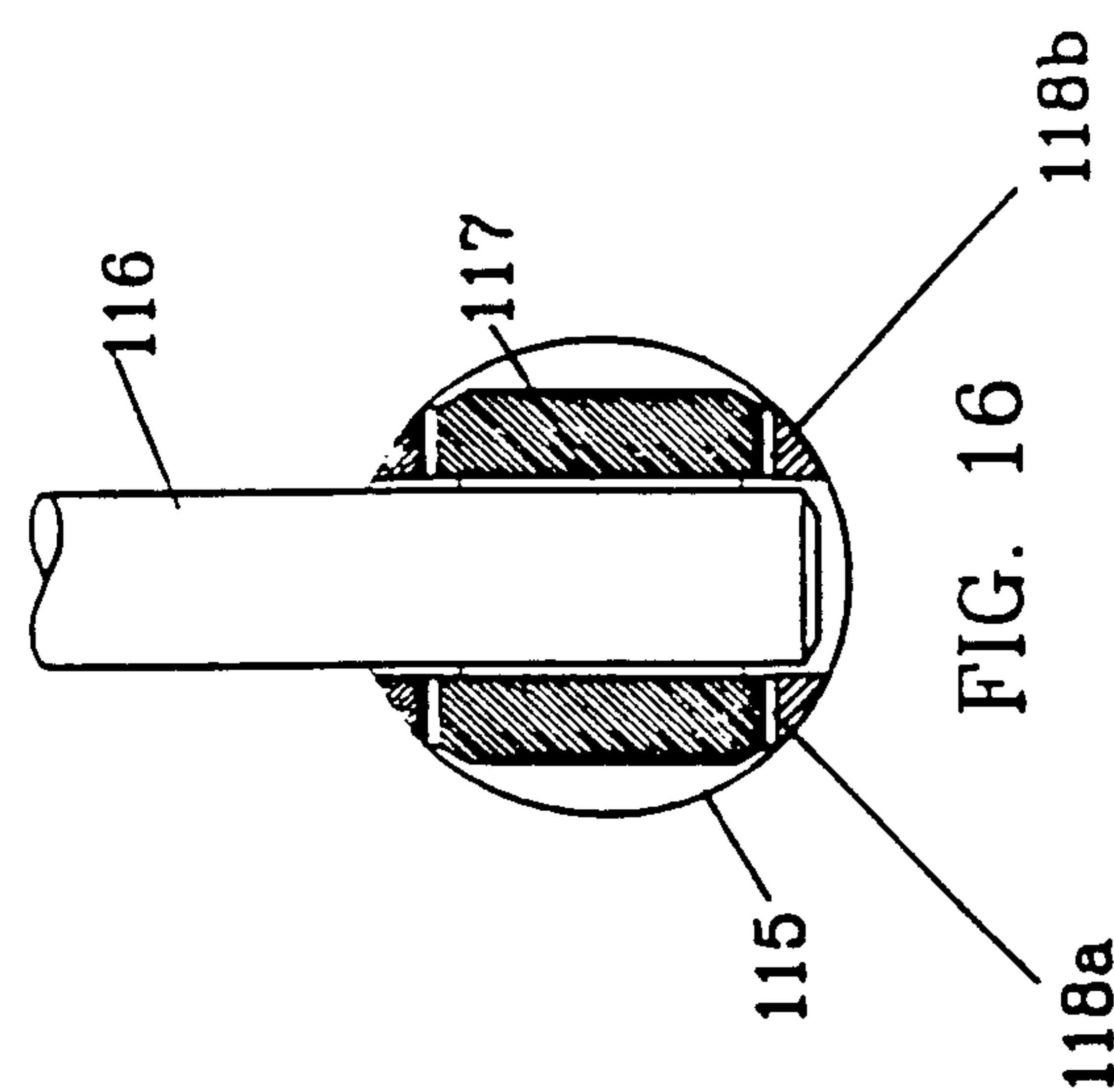


FIG. 13

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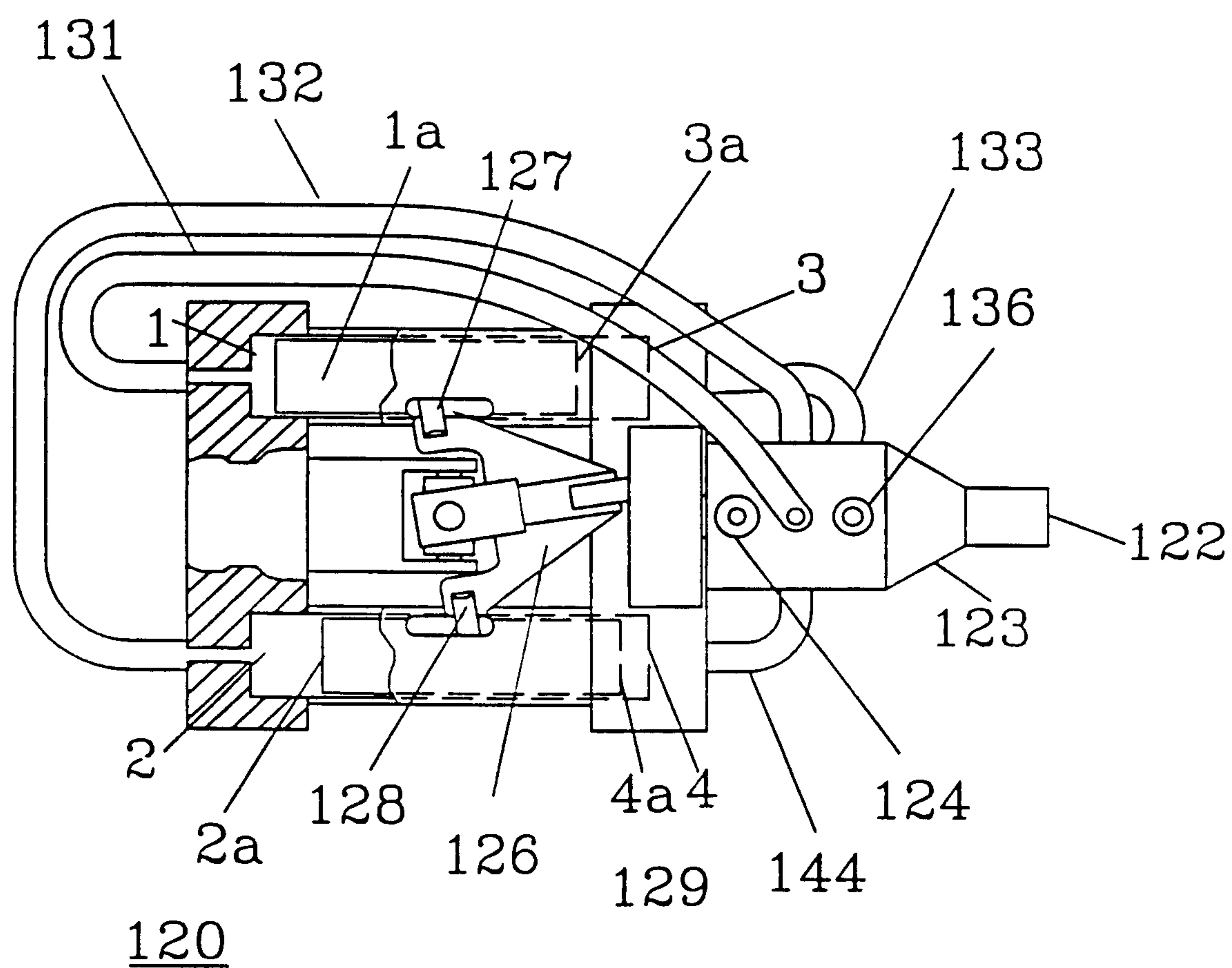


FIG. 17

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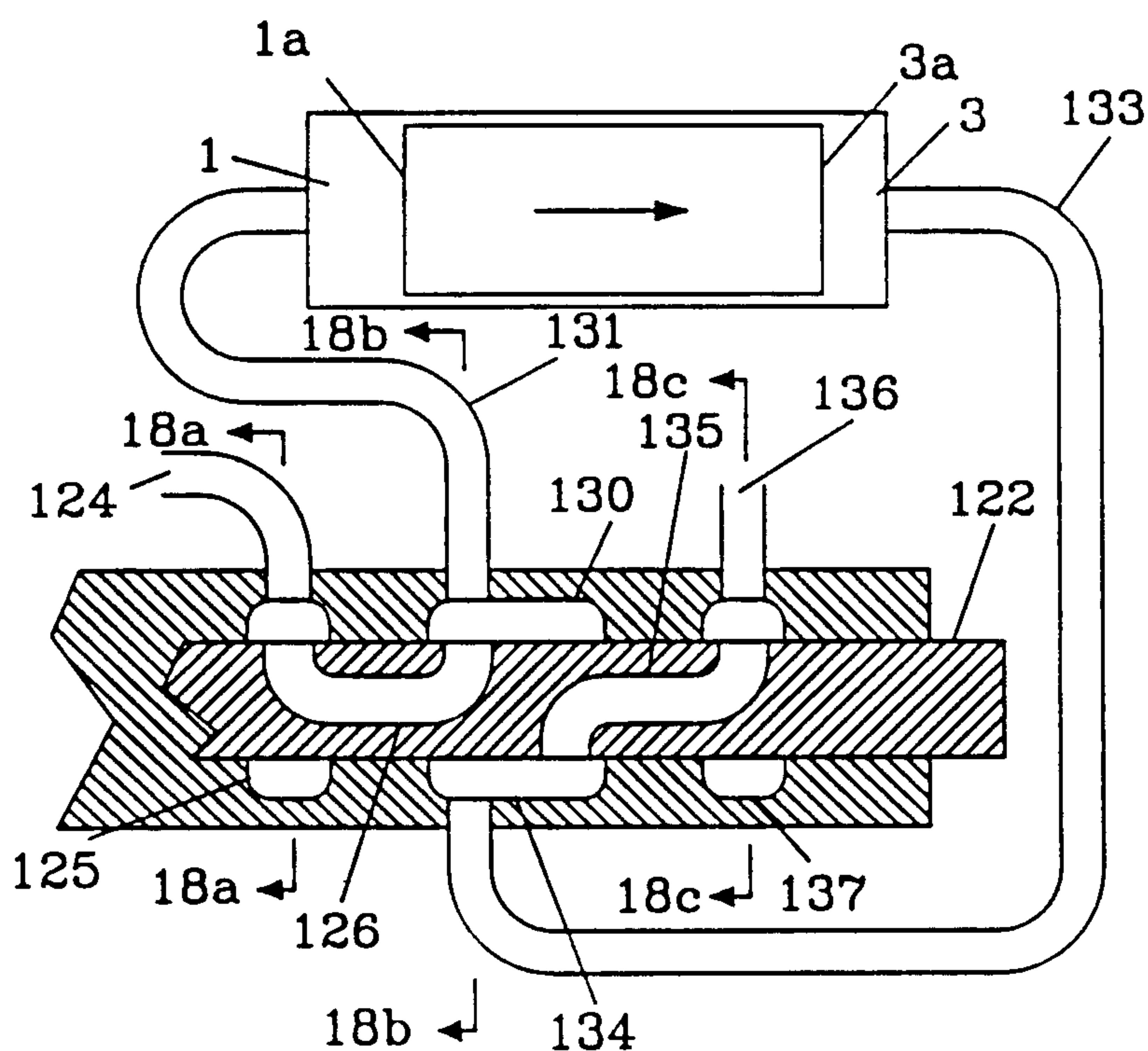


FIG. 18

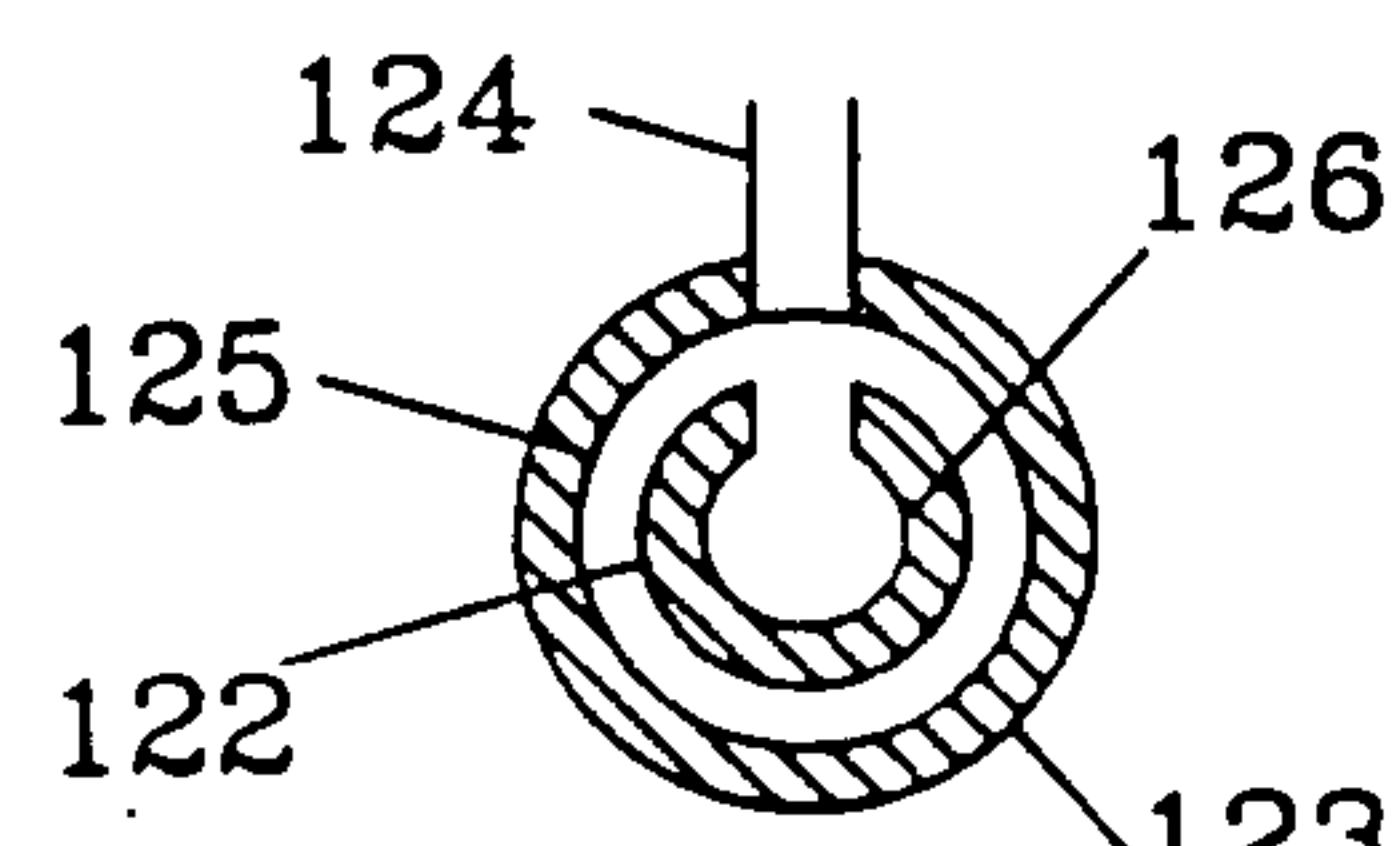


FIG. 18a

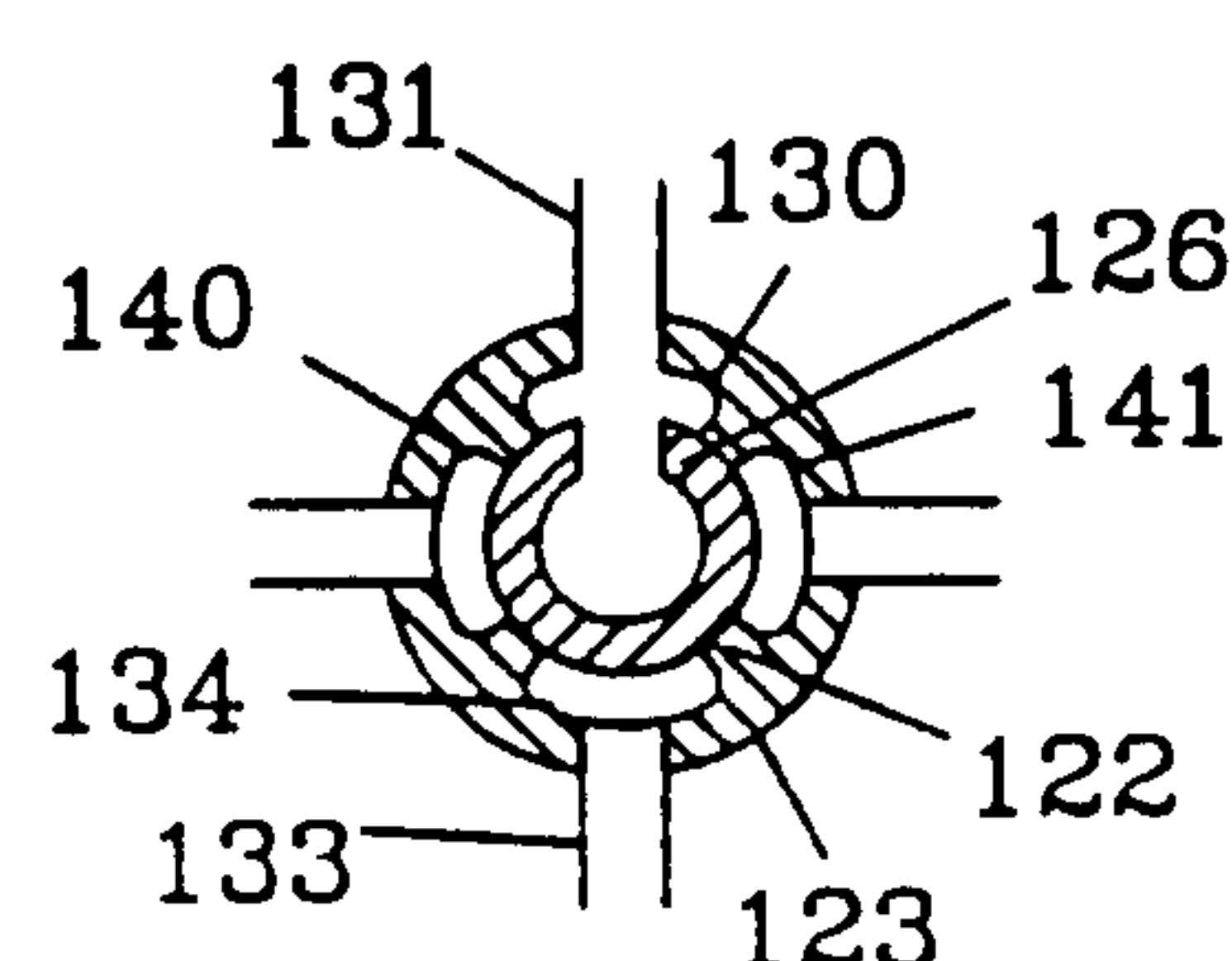


FIG. 18b

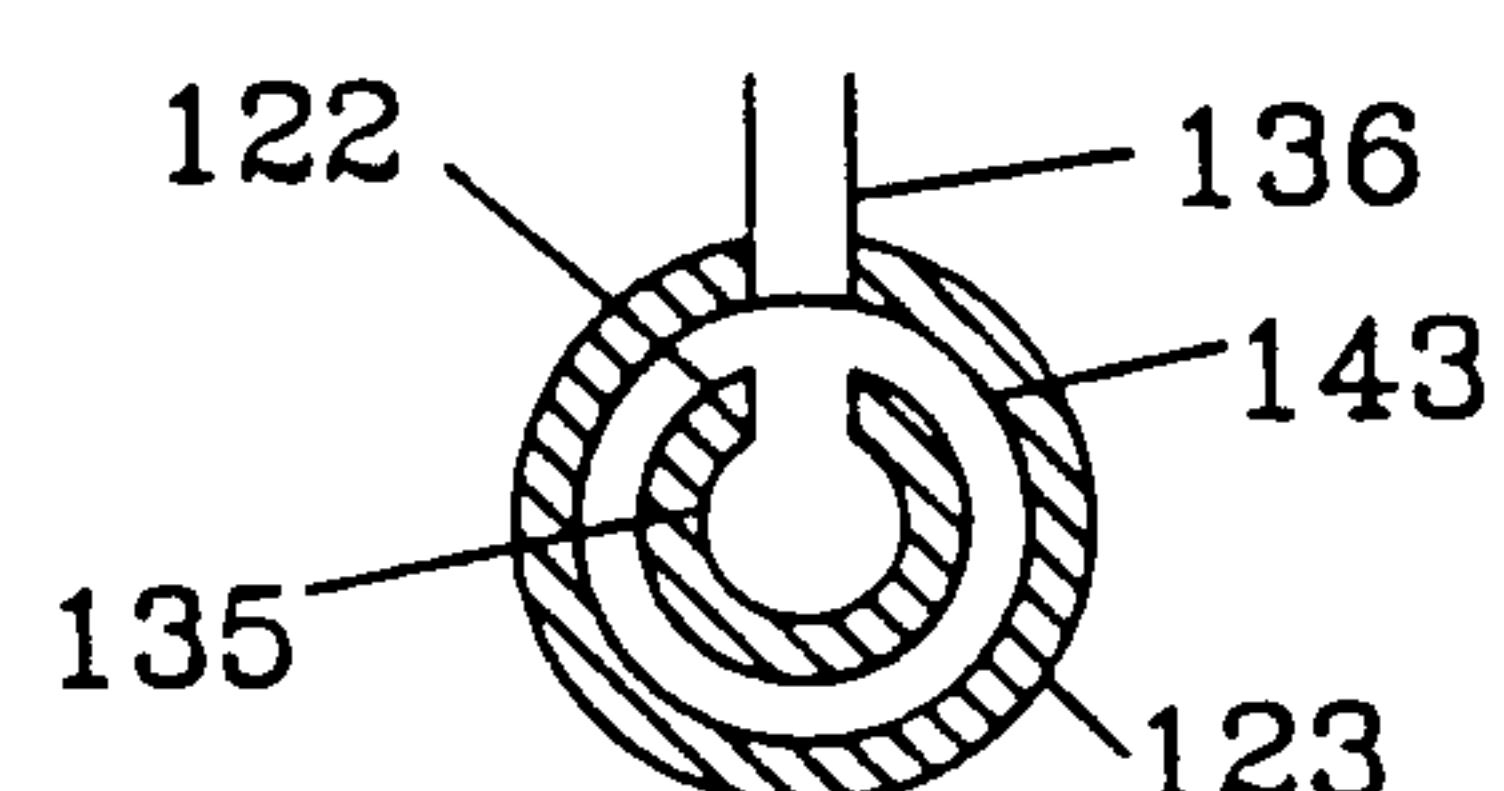


FIG. 18c

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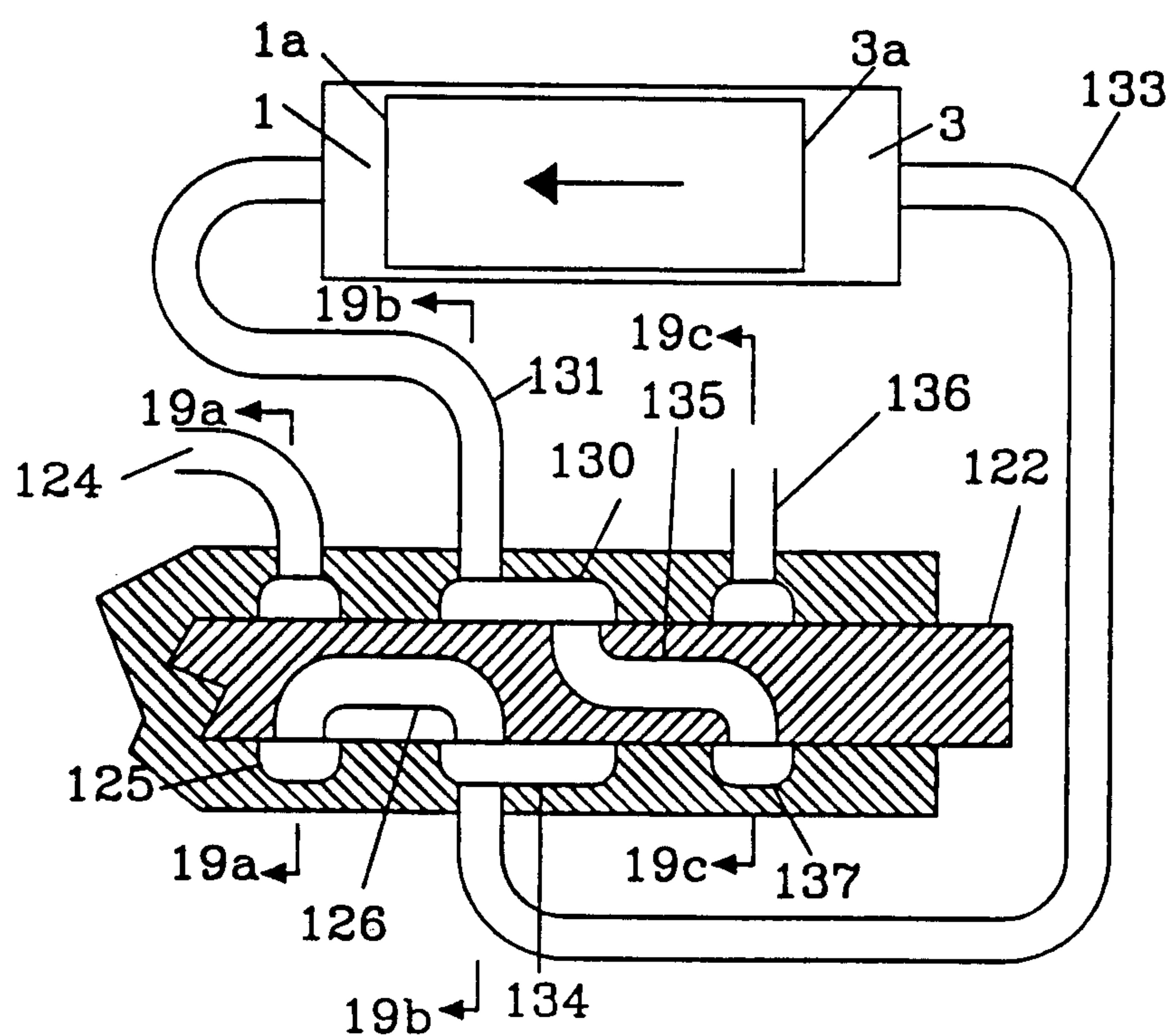


FIG. 19

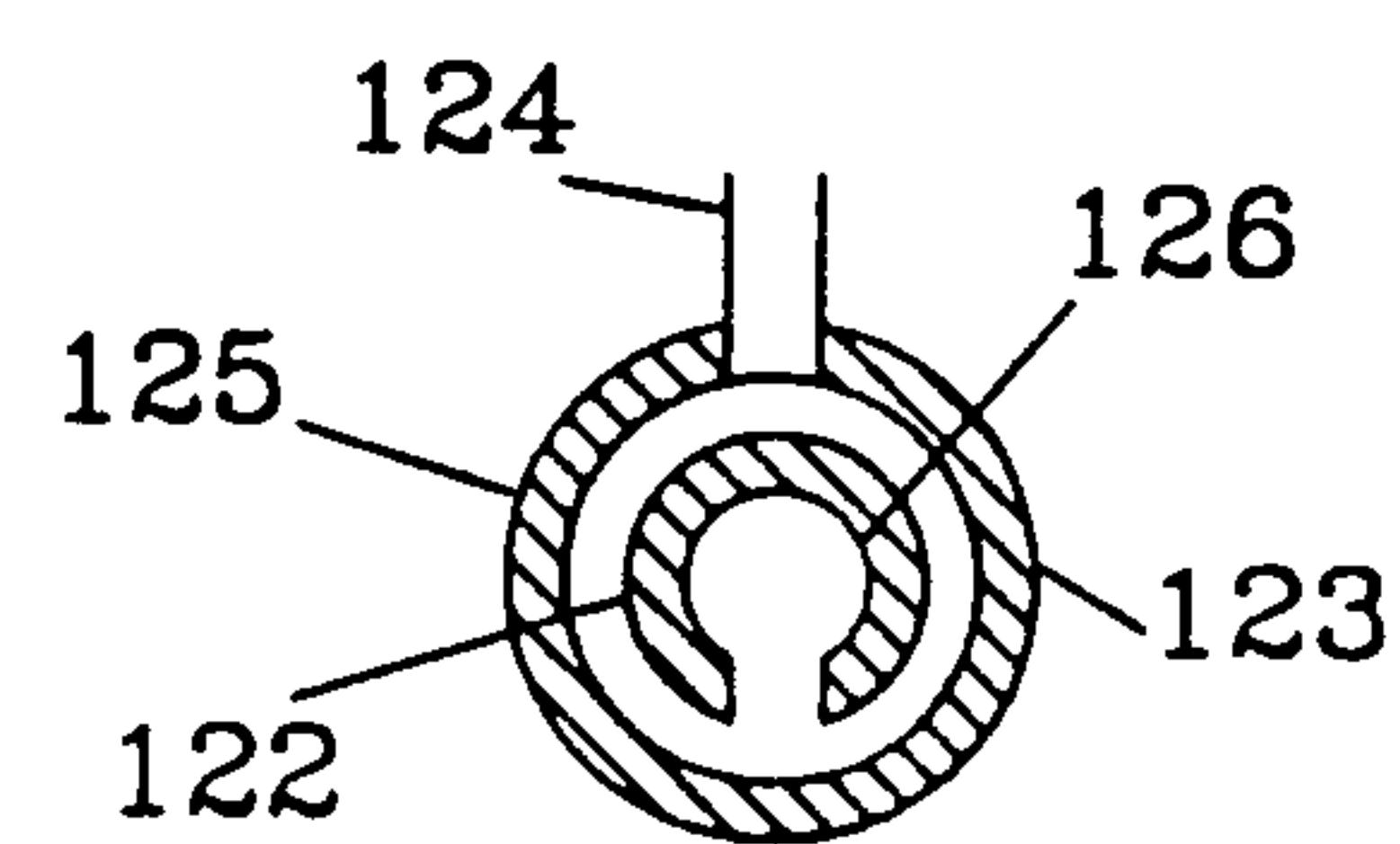


FIG. 19a

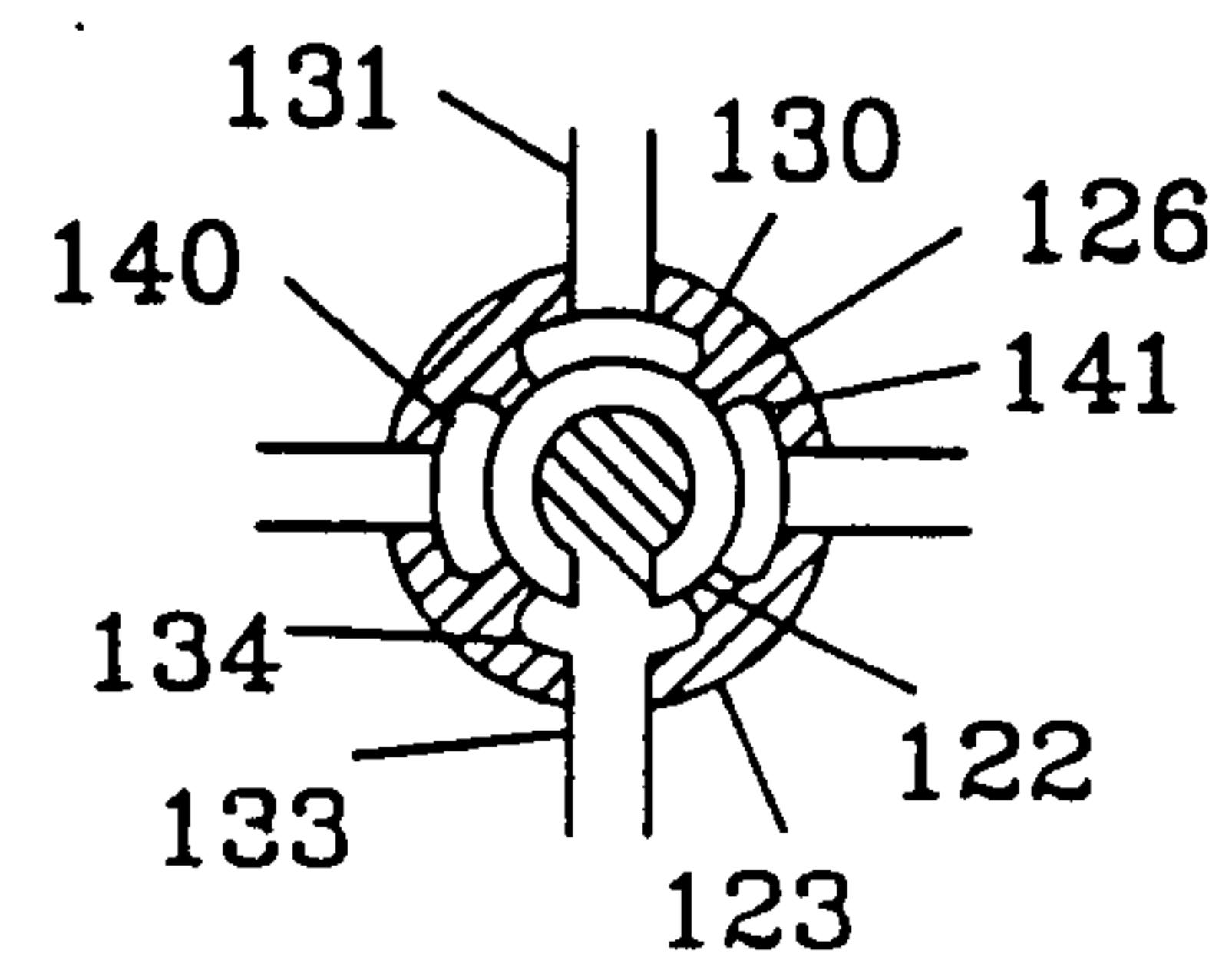


FIG. 19b

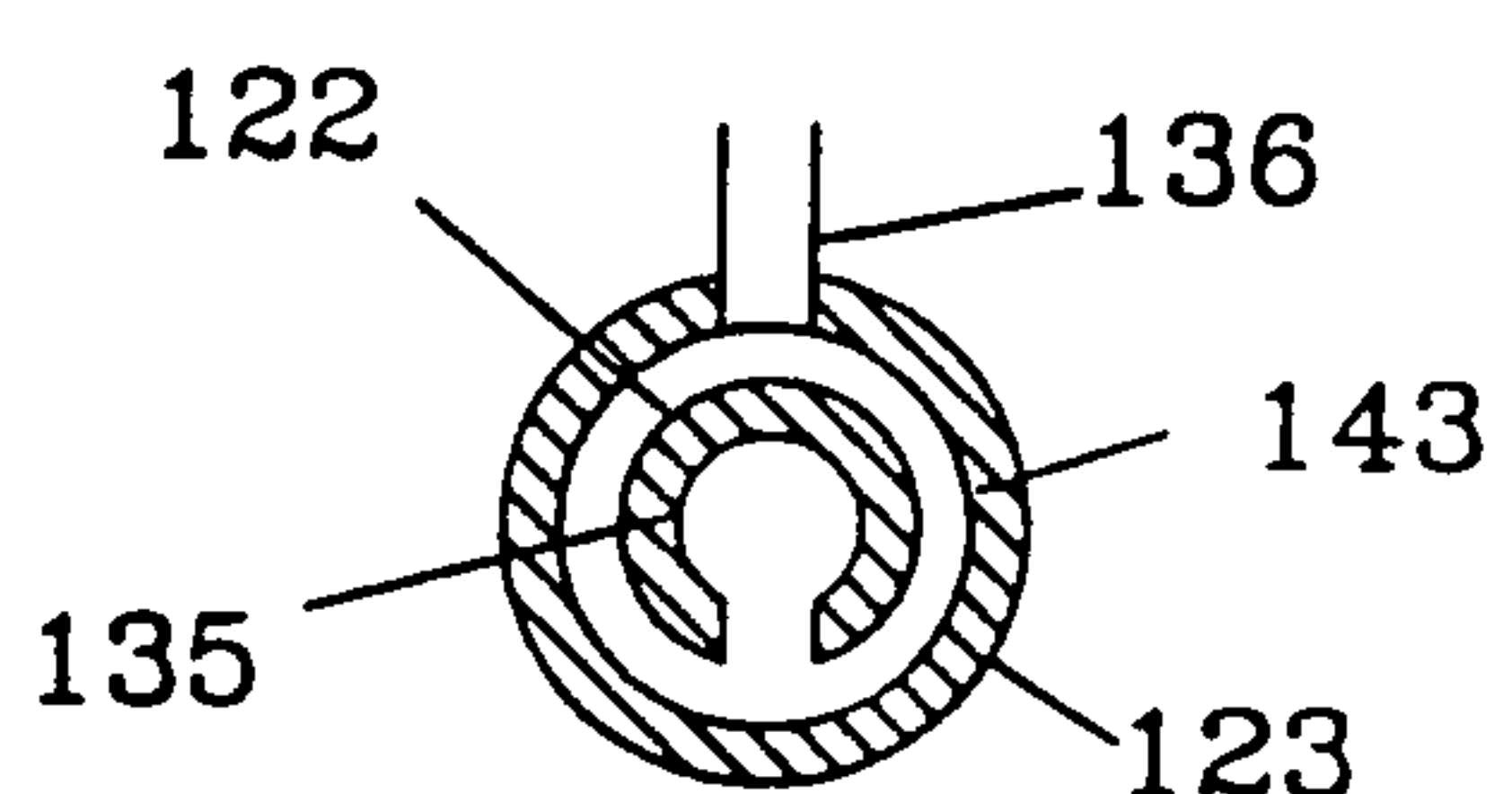


FIG. 19c

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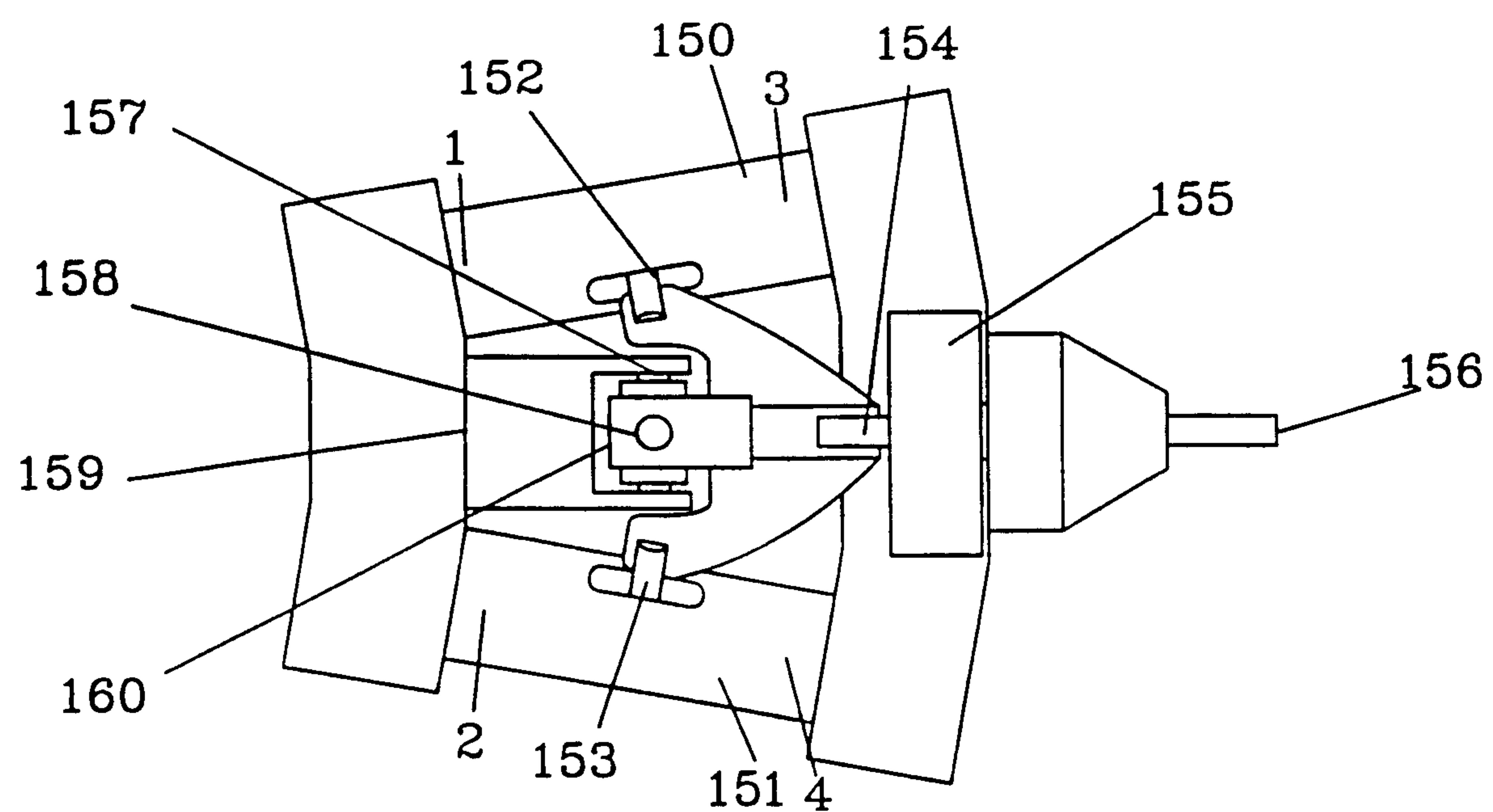


FIG. 20

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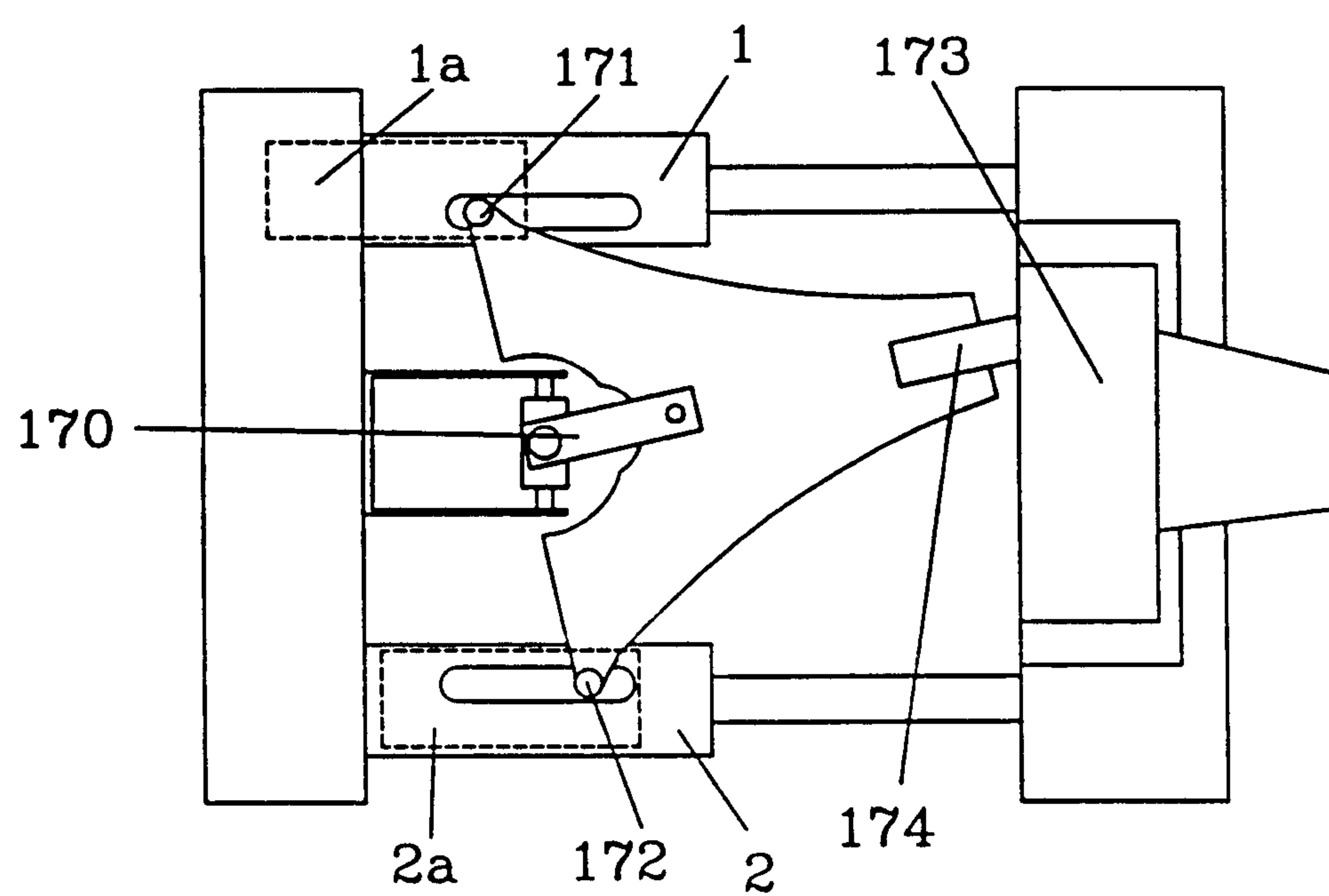


FIG. 21

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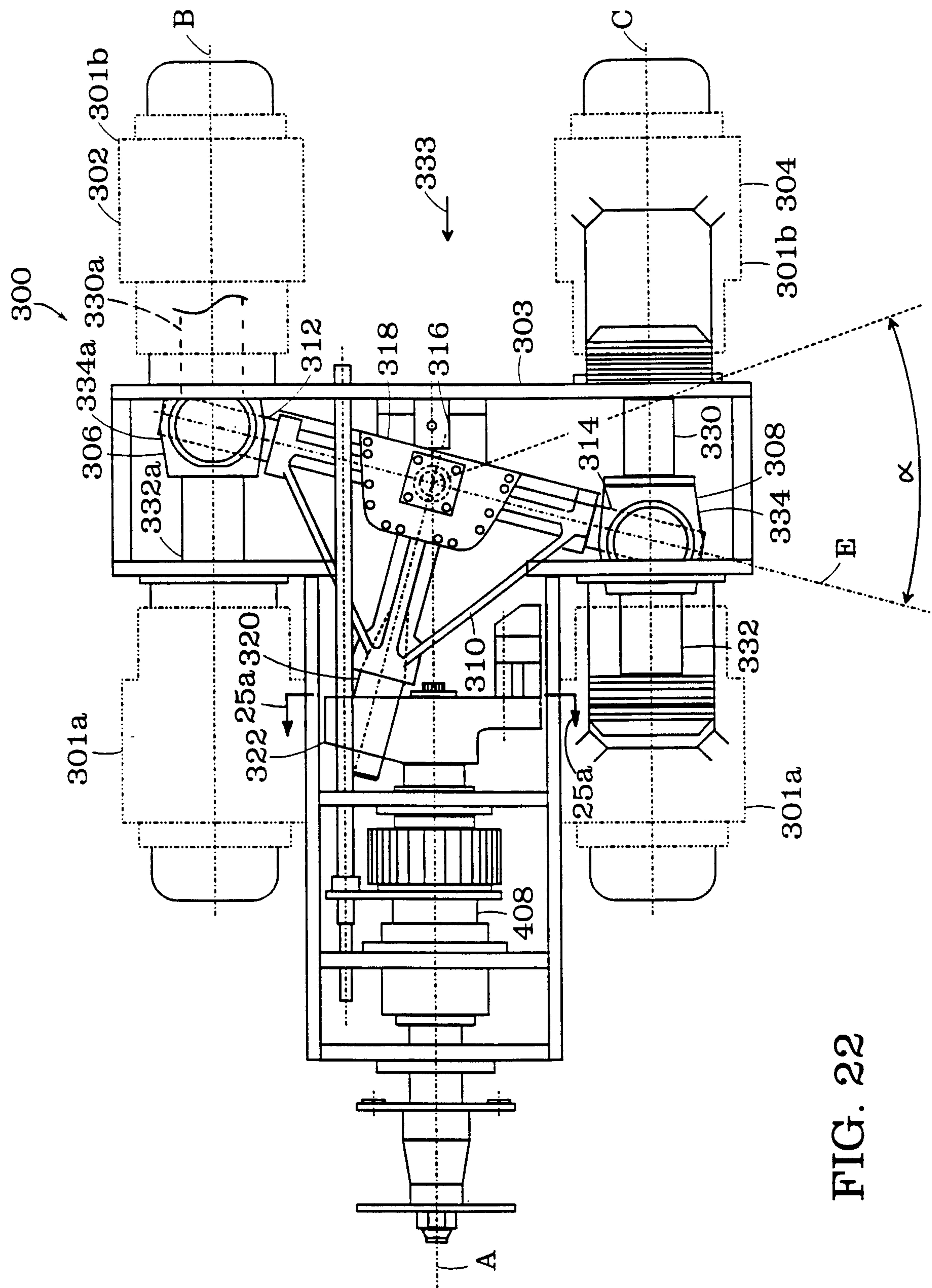
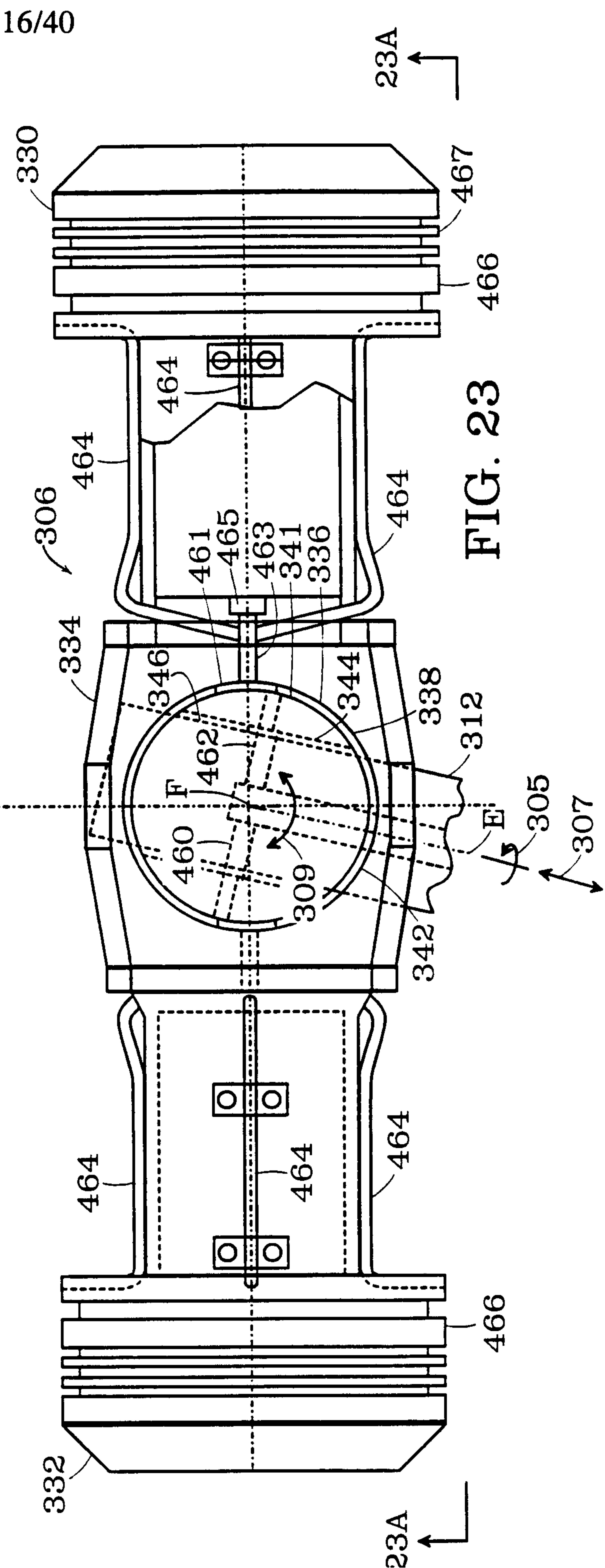
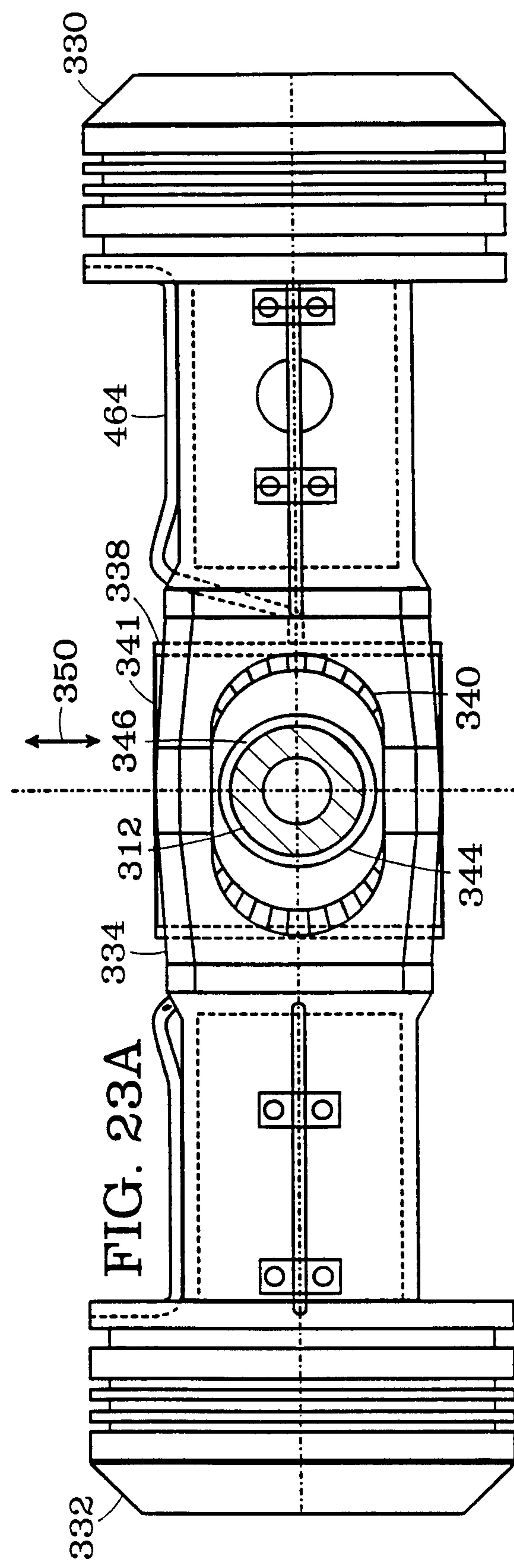
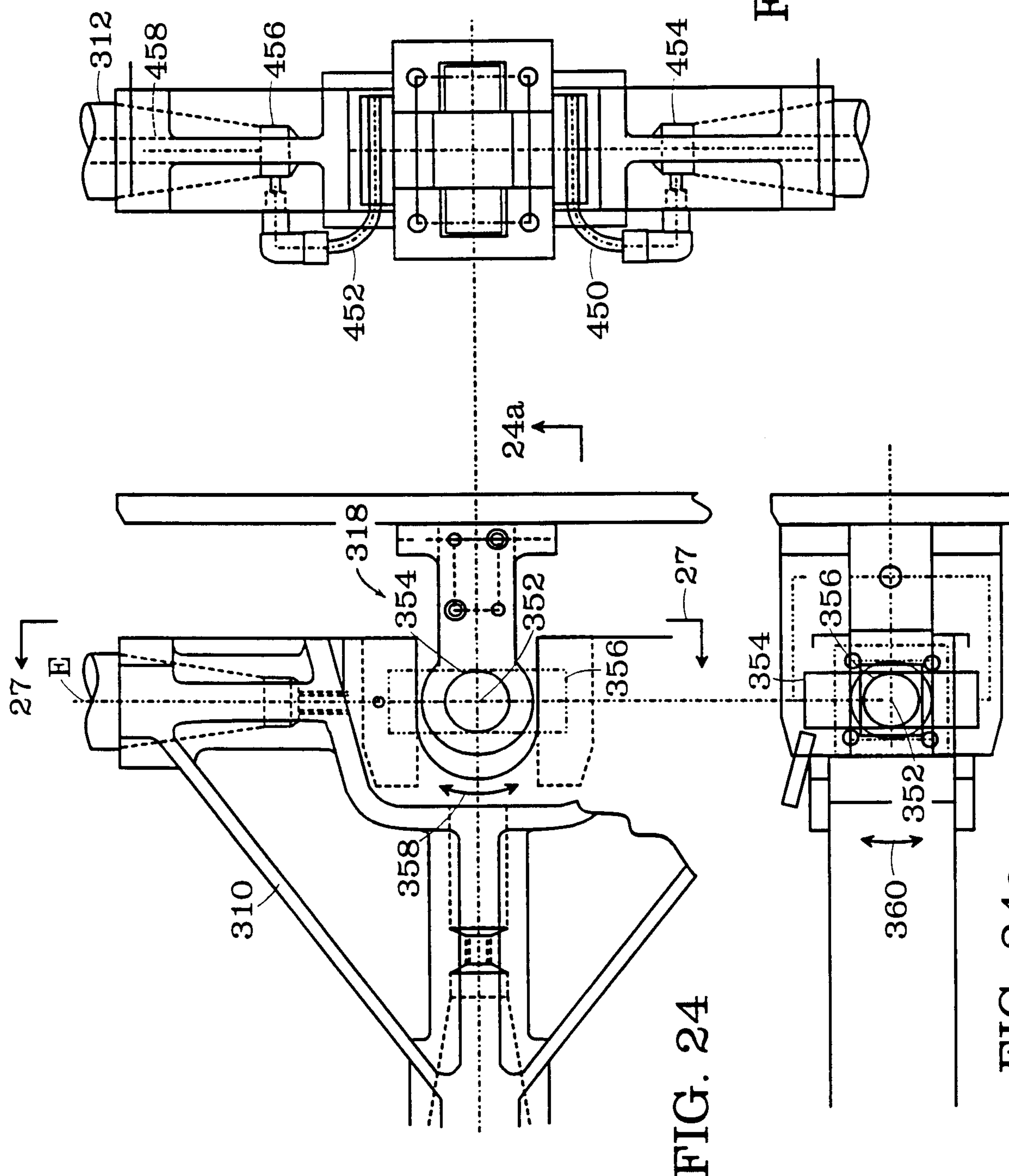


FIG. 22



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SUBSTITUTE SHEET (RULE 26)

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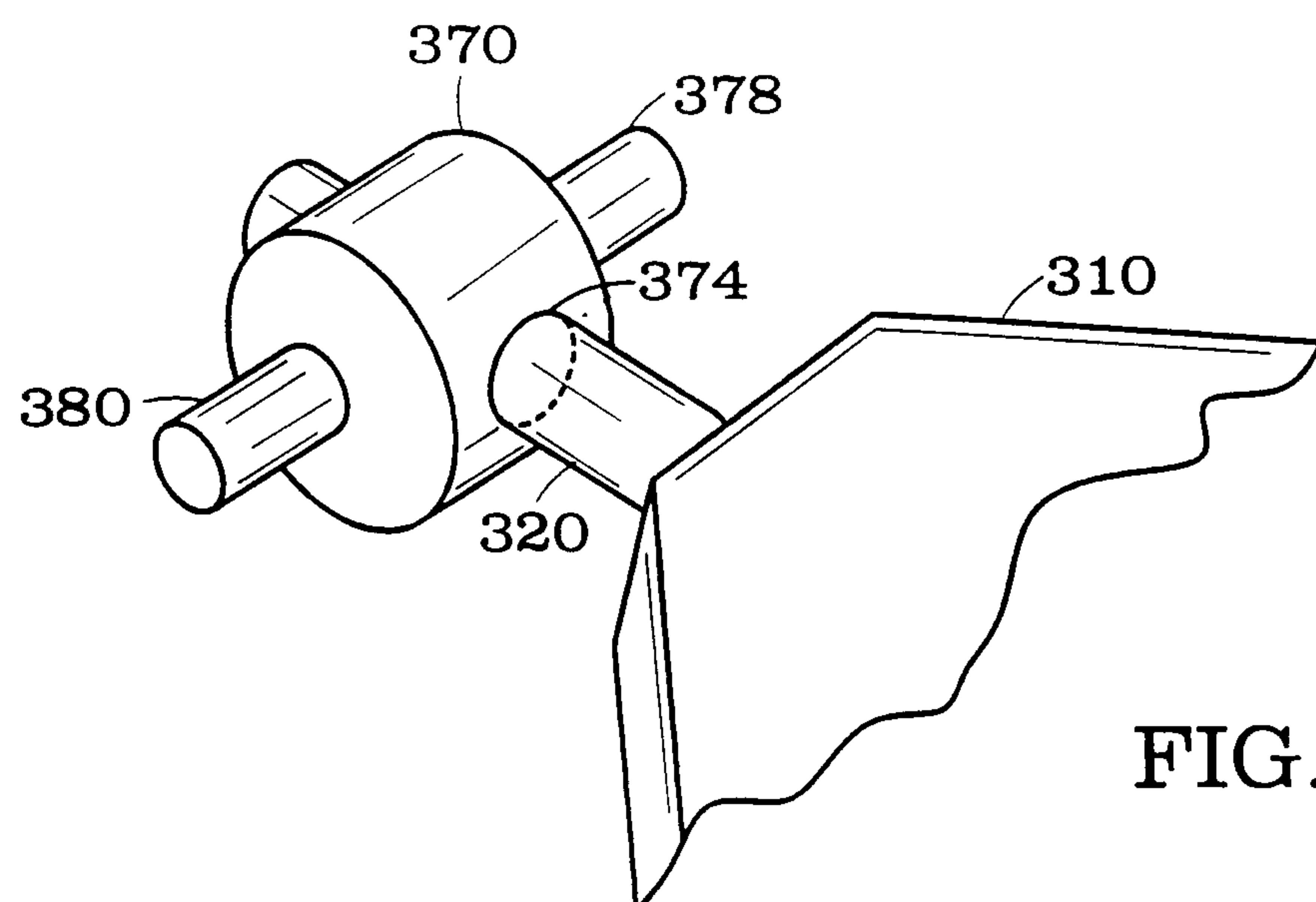
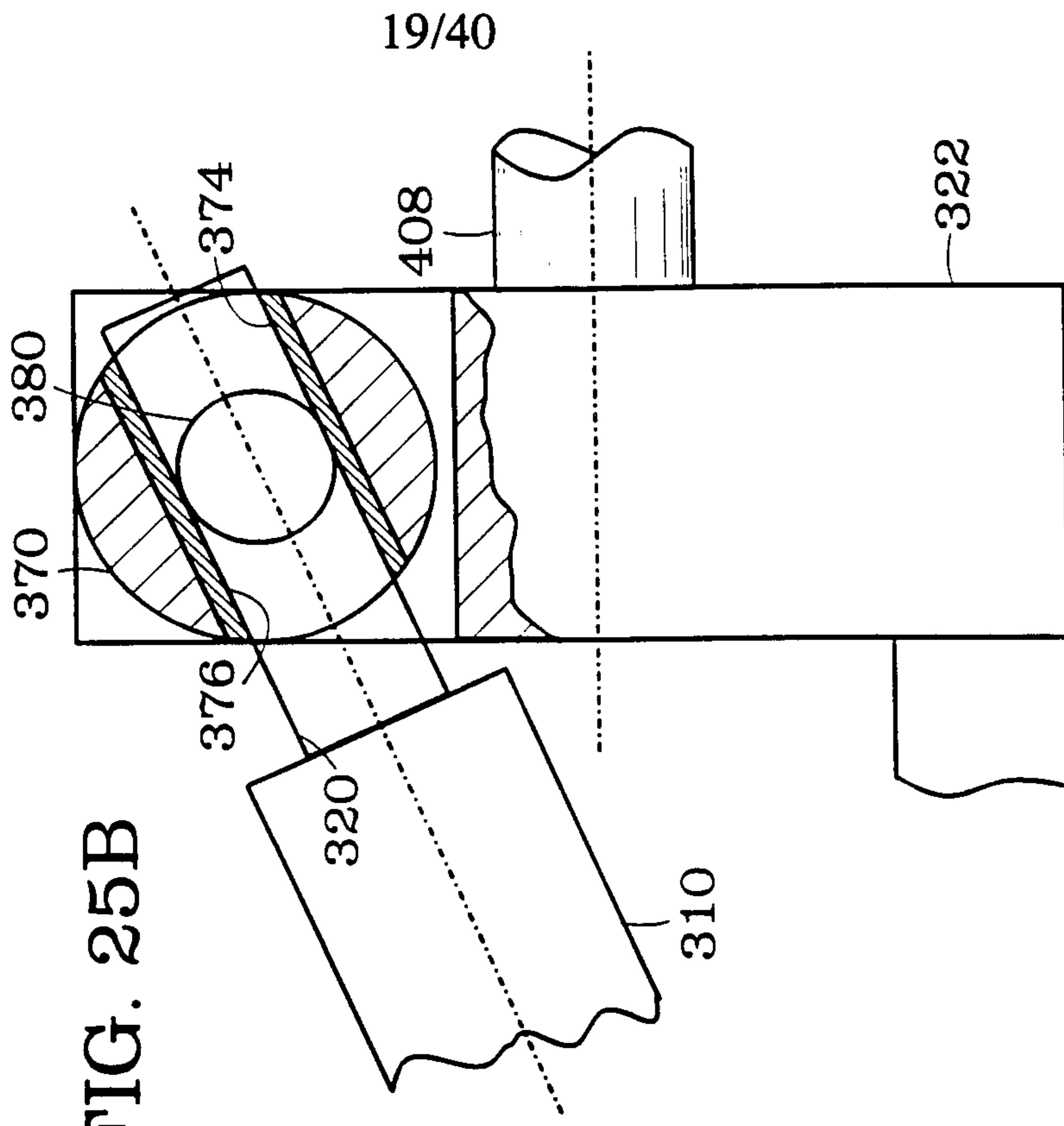
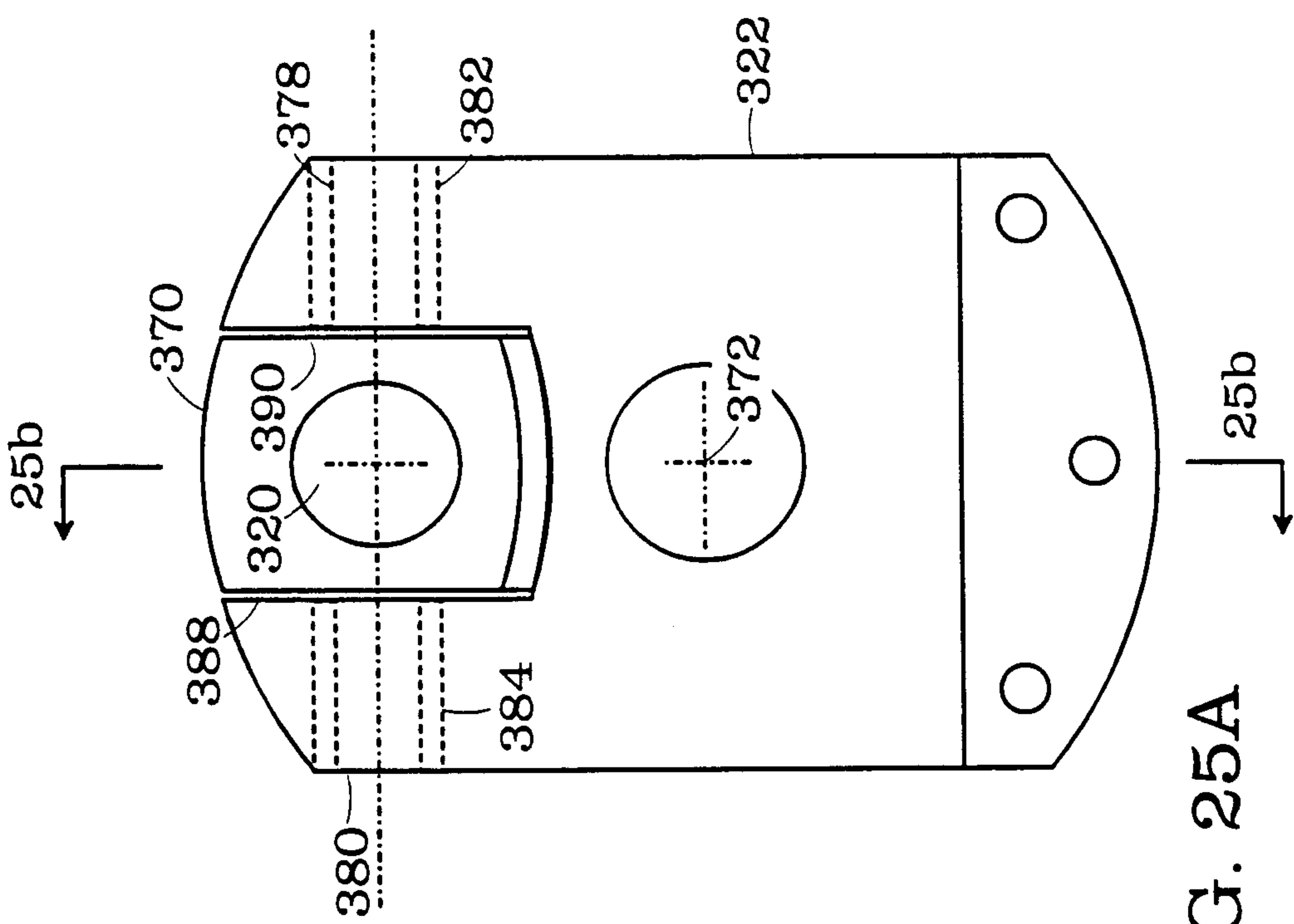


FIG. 25



FIGURE



15A
22
G
T
E

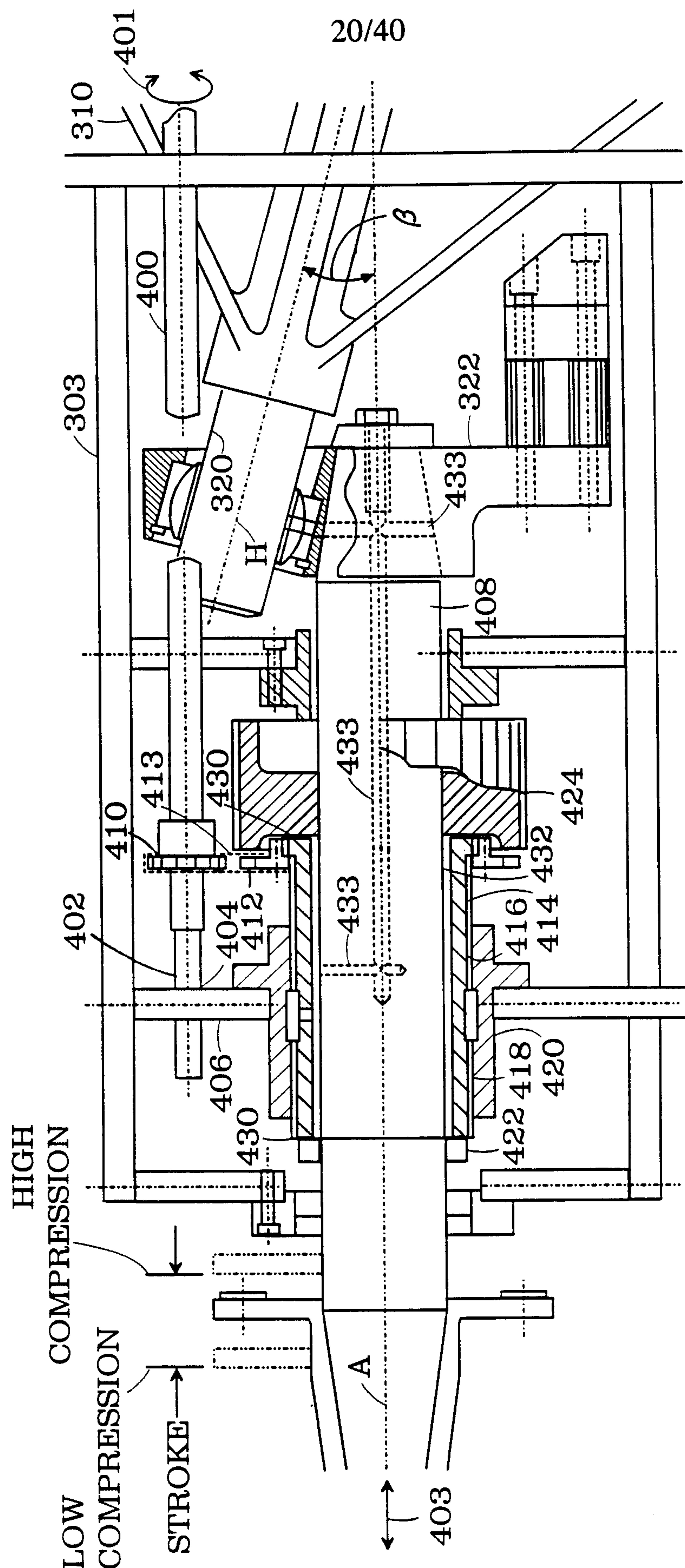


FIG. 26

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FIG. 28a

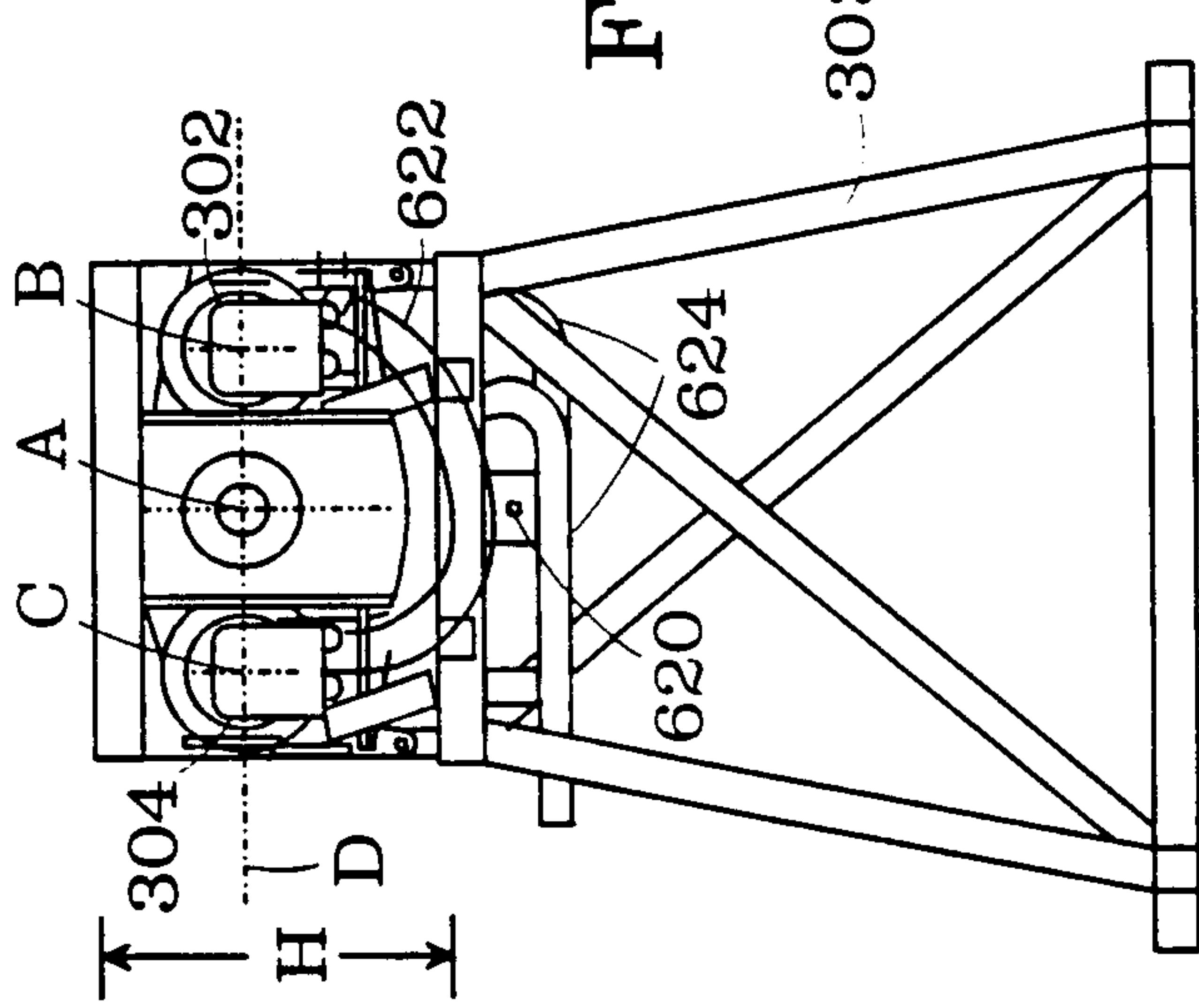


FIG. 28

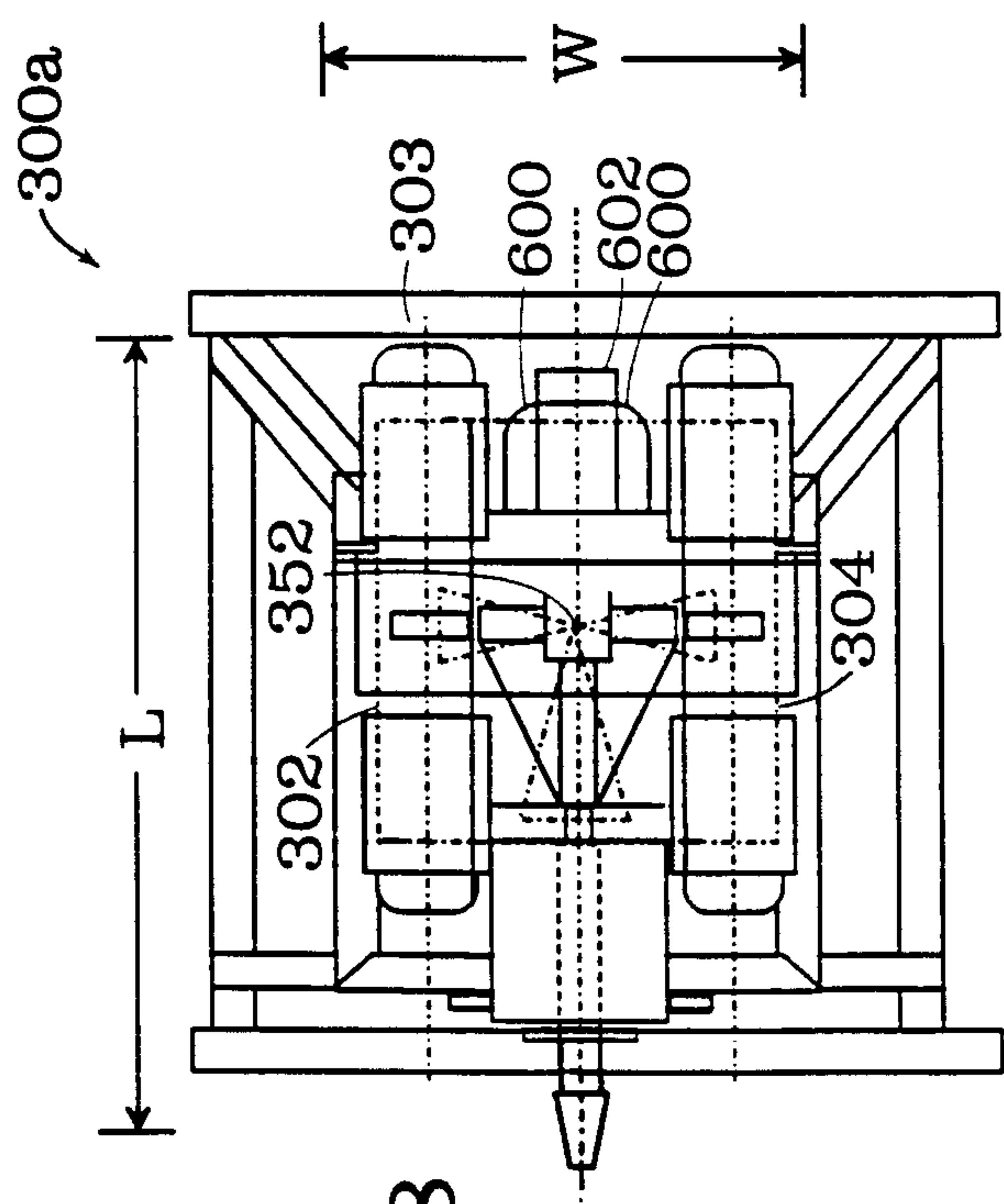
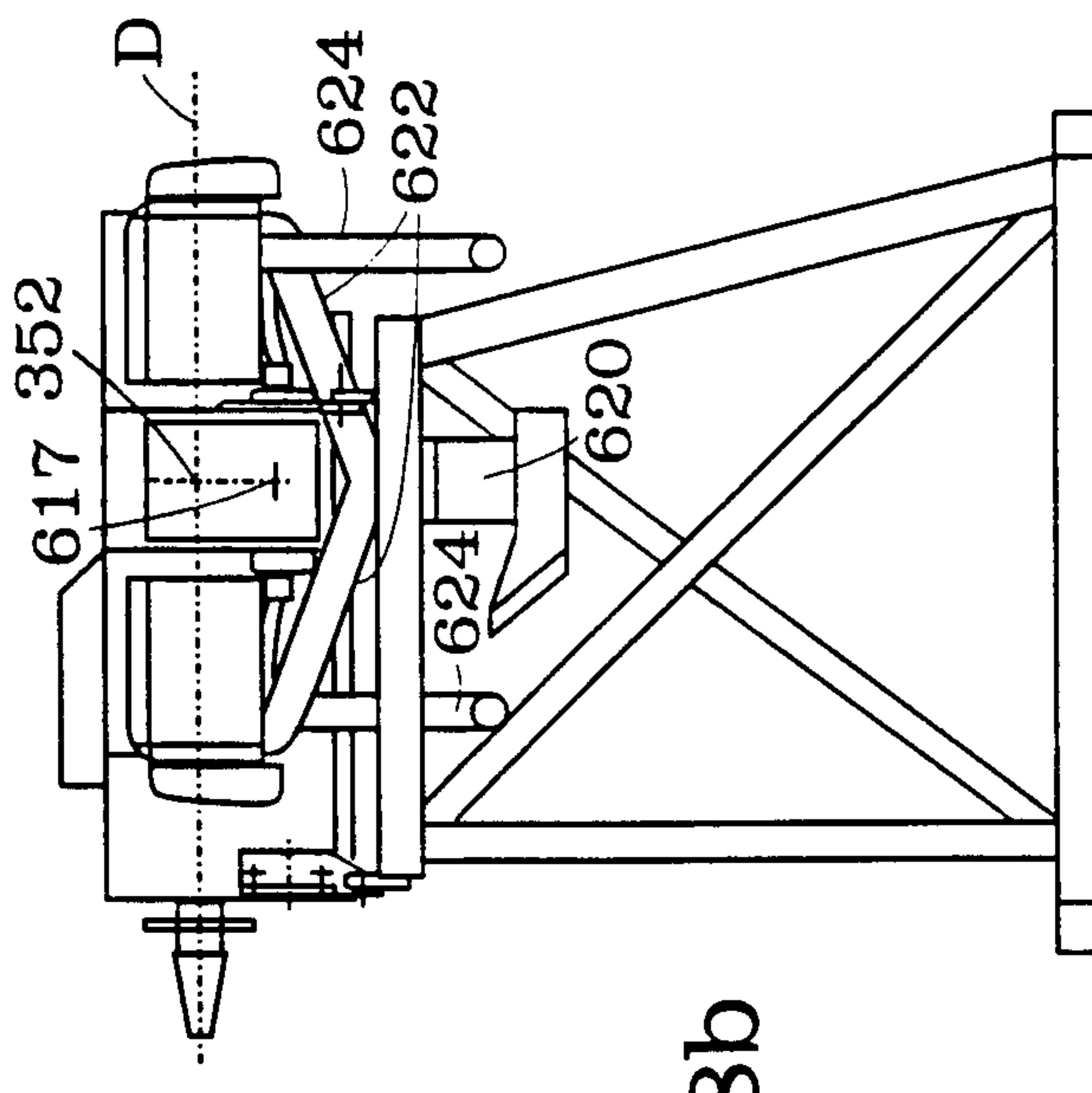
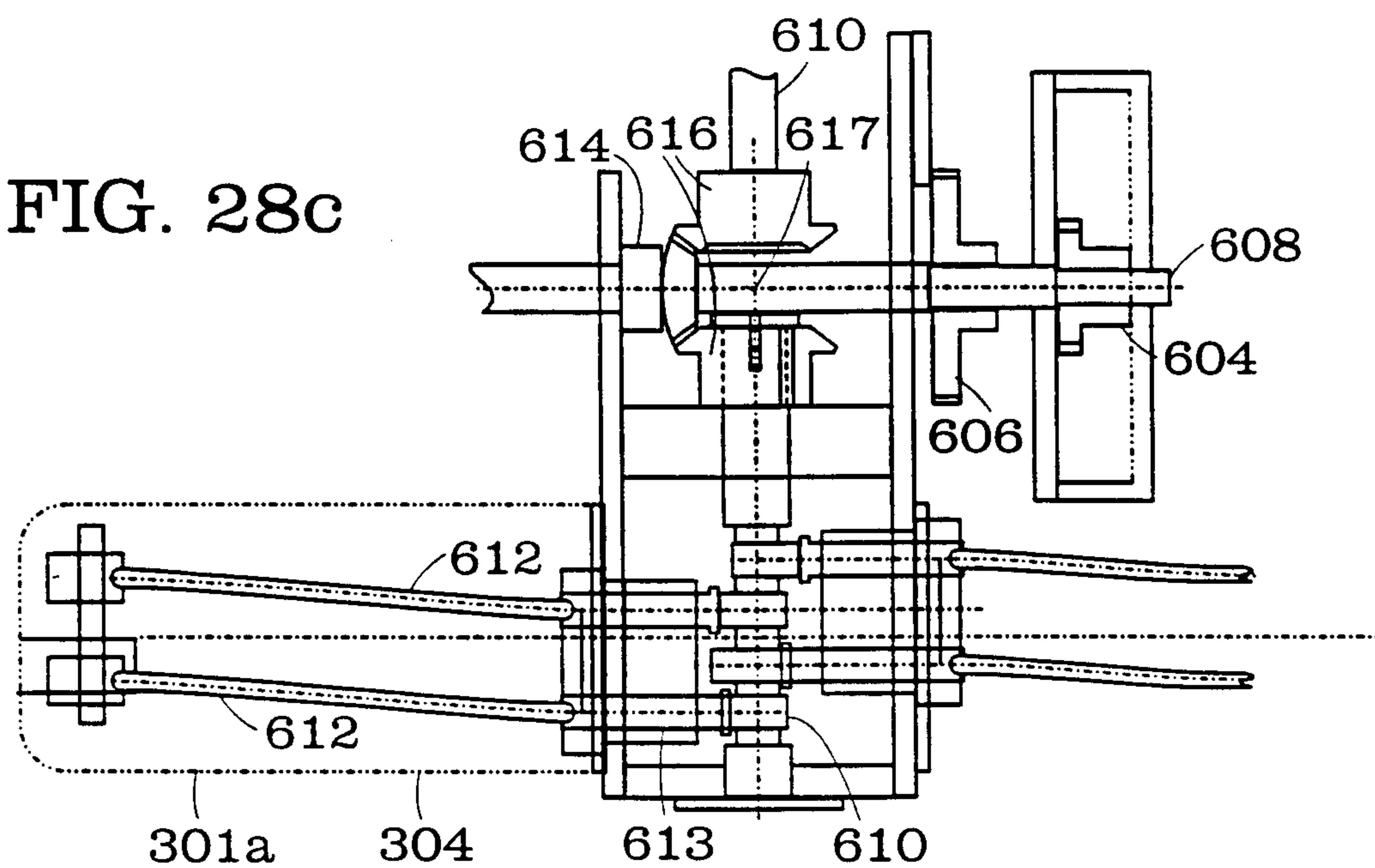


FIG. 28b



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FIG. 28c



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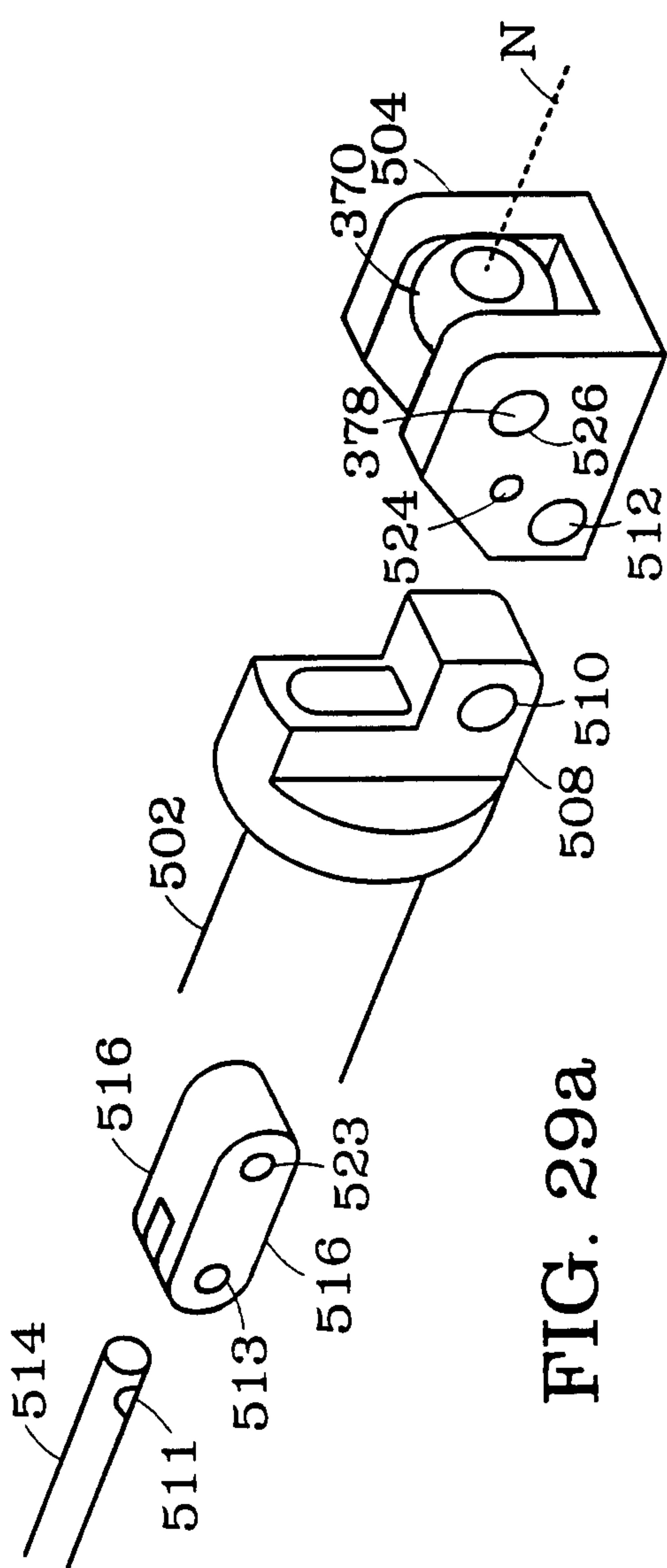
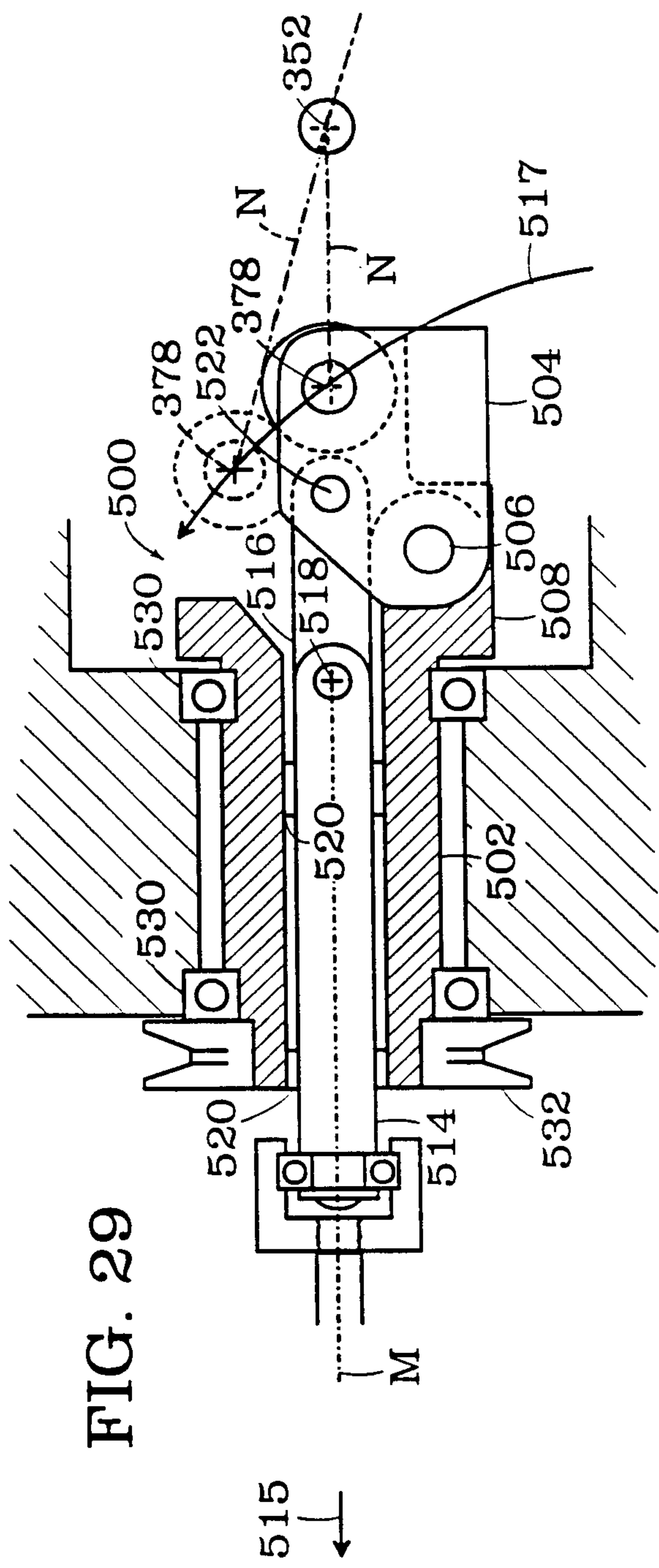


FIGURE EIGHT MOTION OF PISTON ARMS
CROSS U-JOINT, WORST CASE DEVIATION

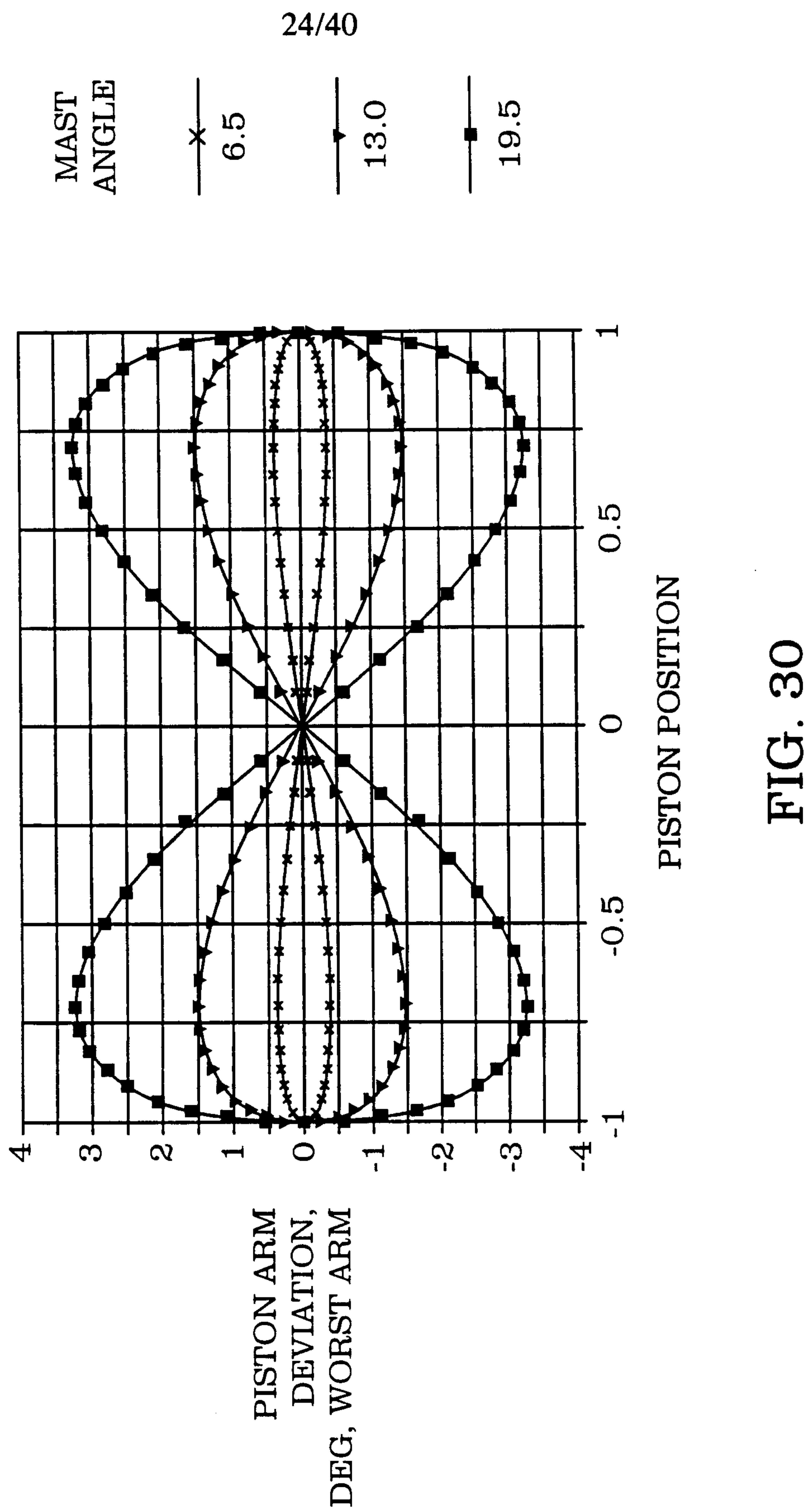


FIG. 30

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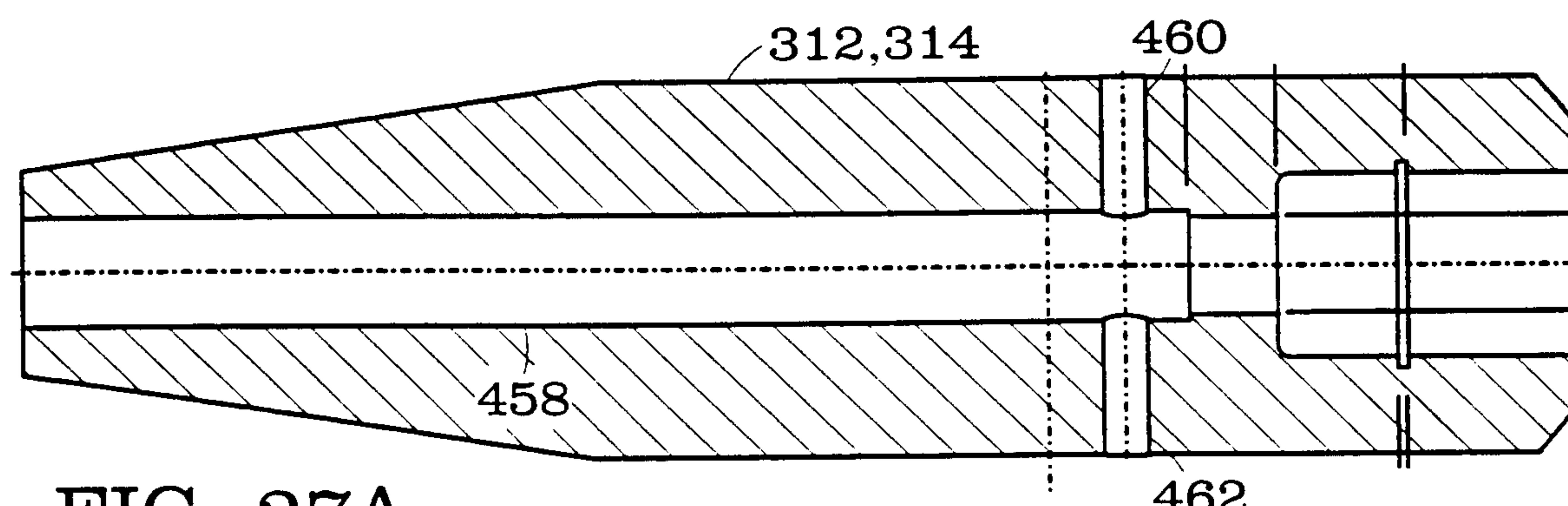


FIG. 27A

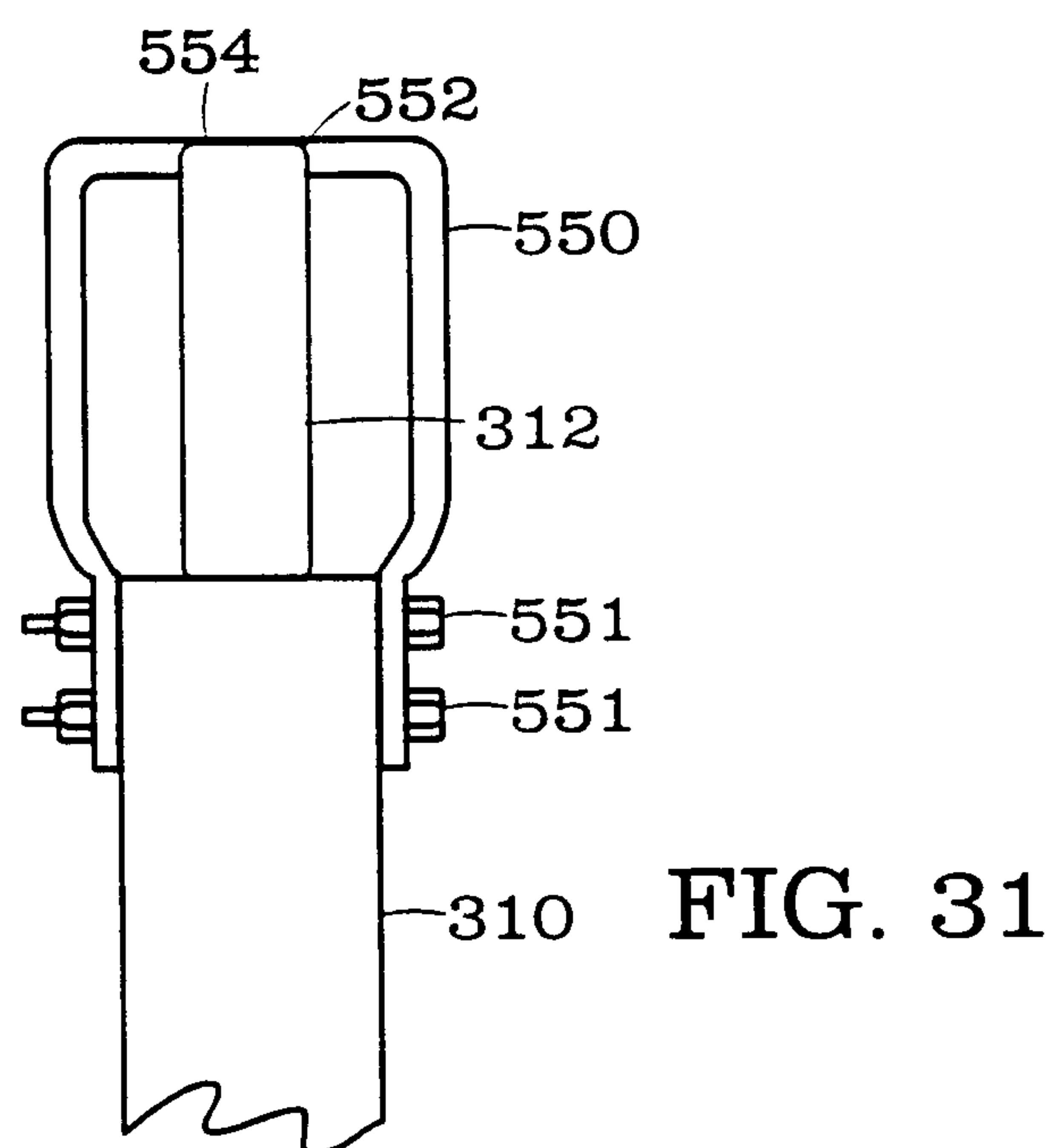


FIG. 31

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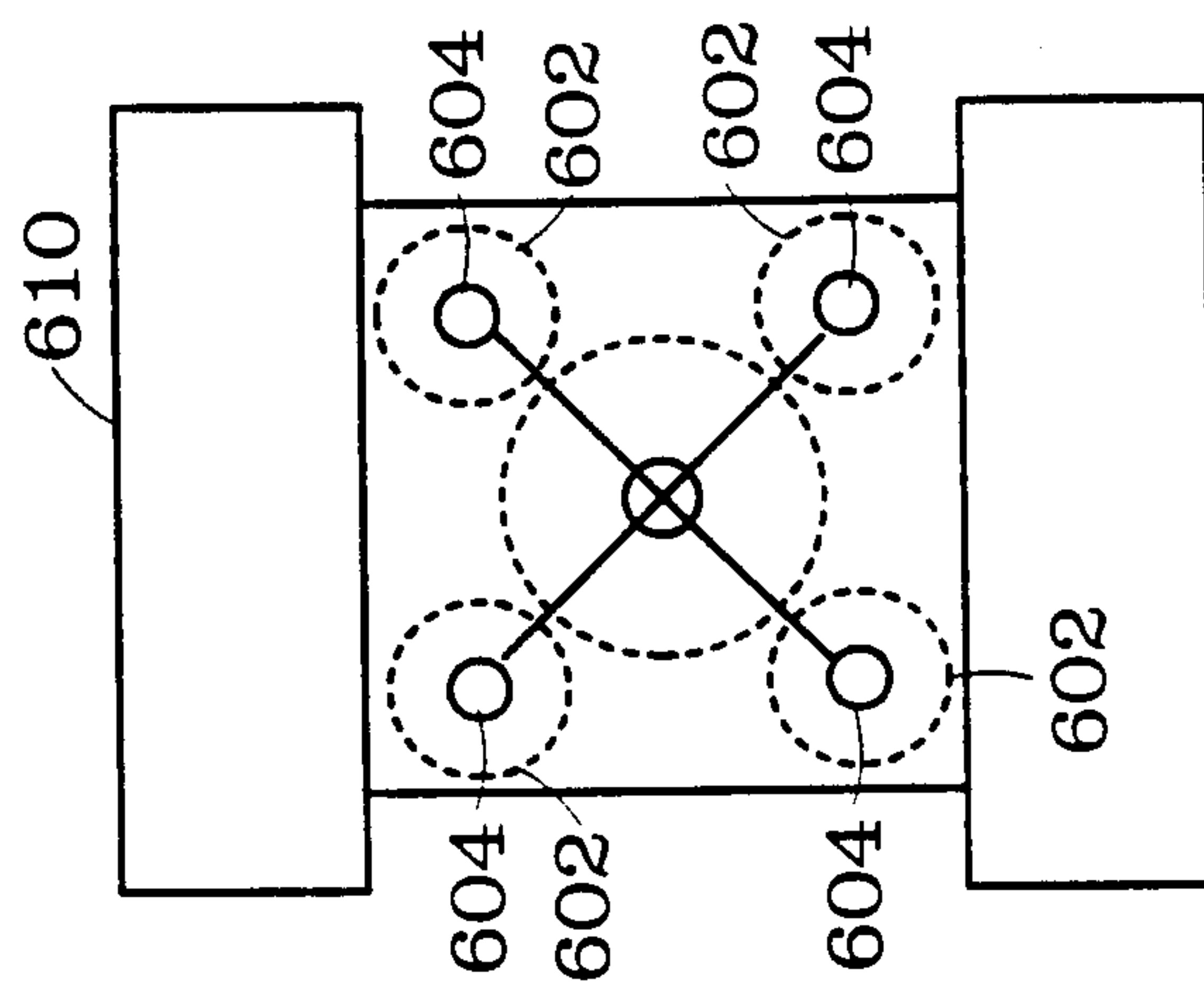


FIG. 32a

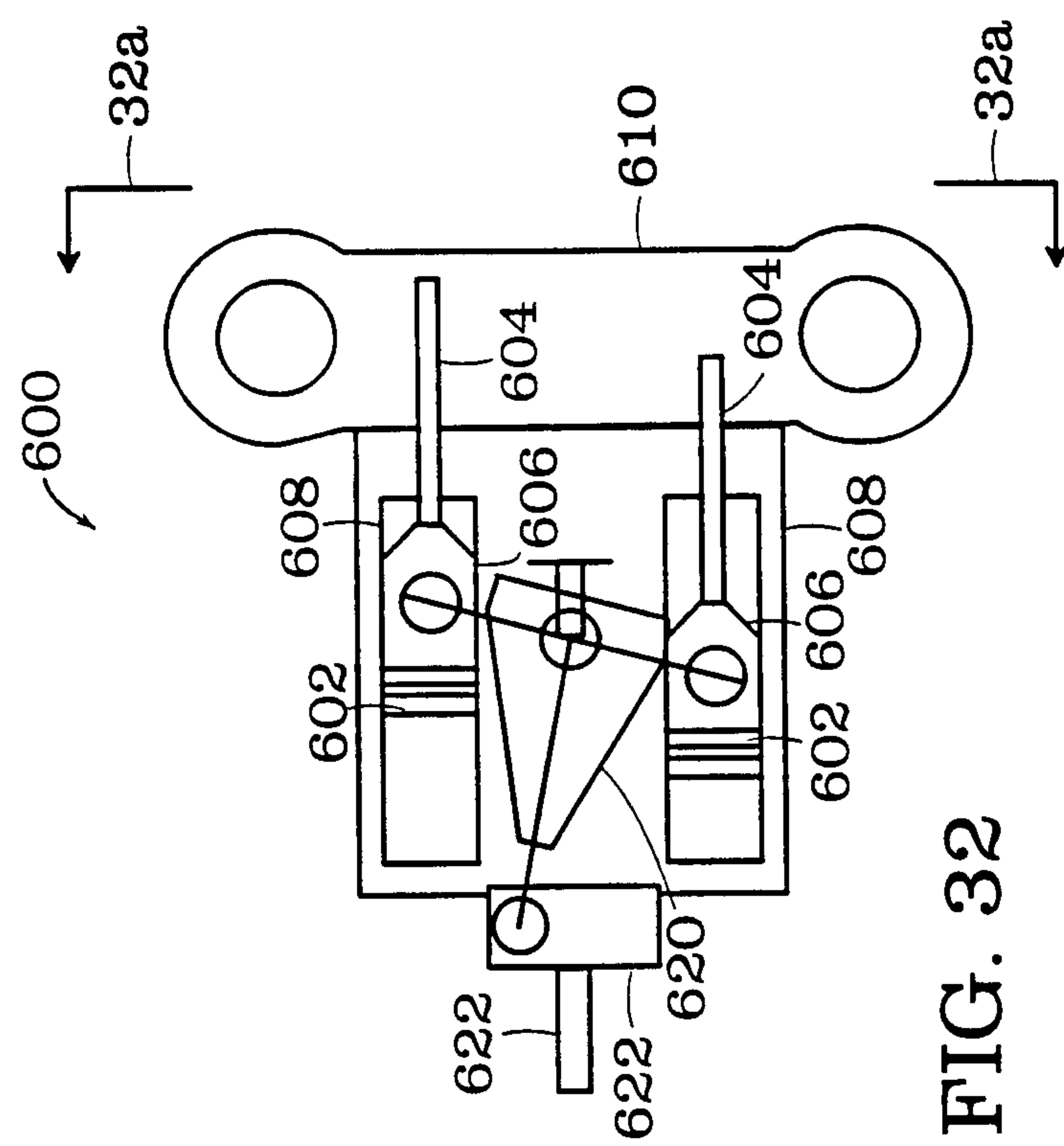
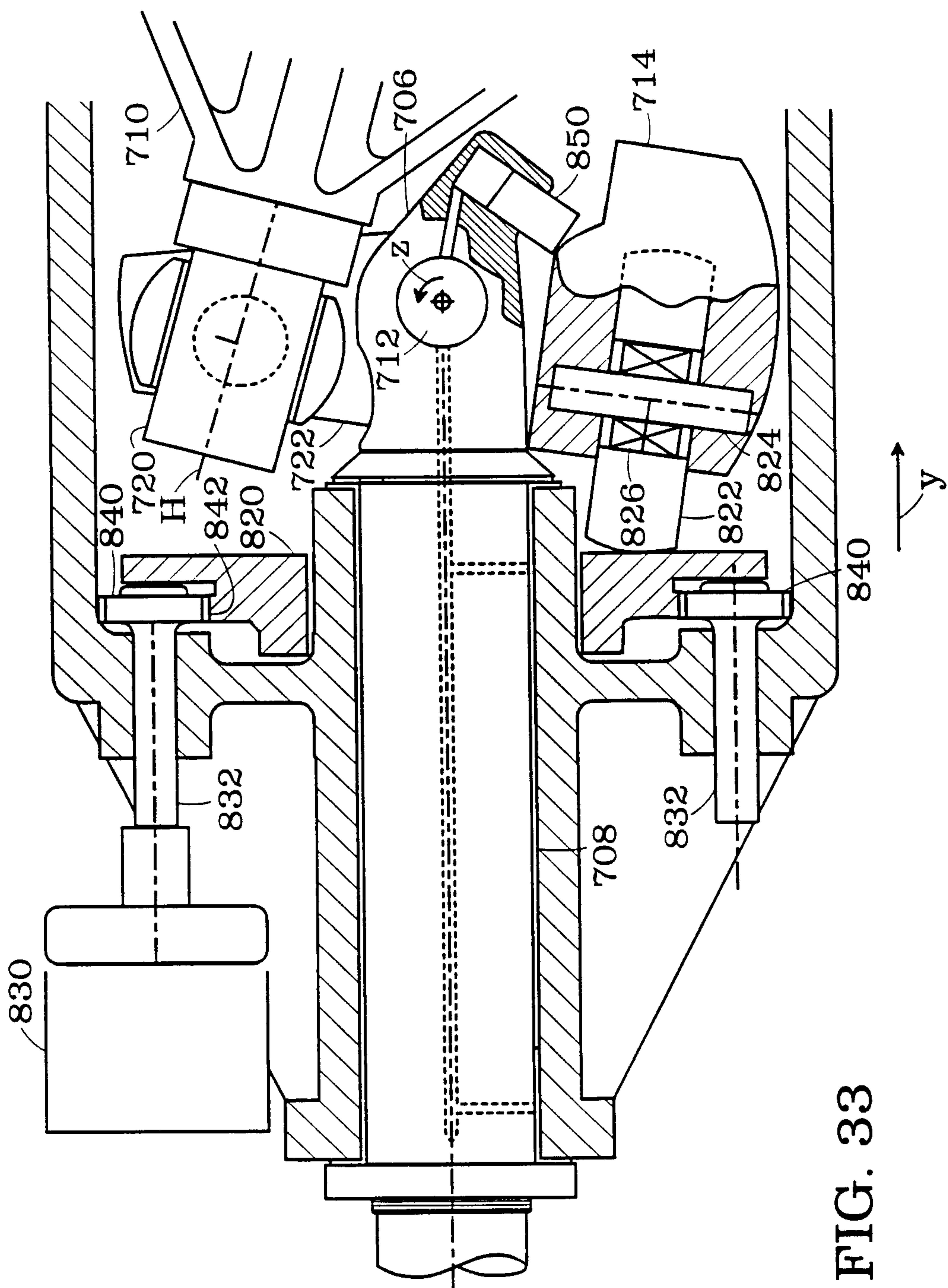


FIG. 32

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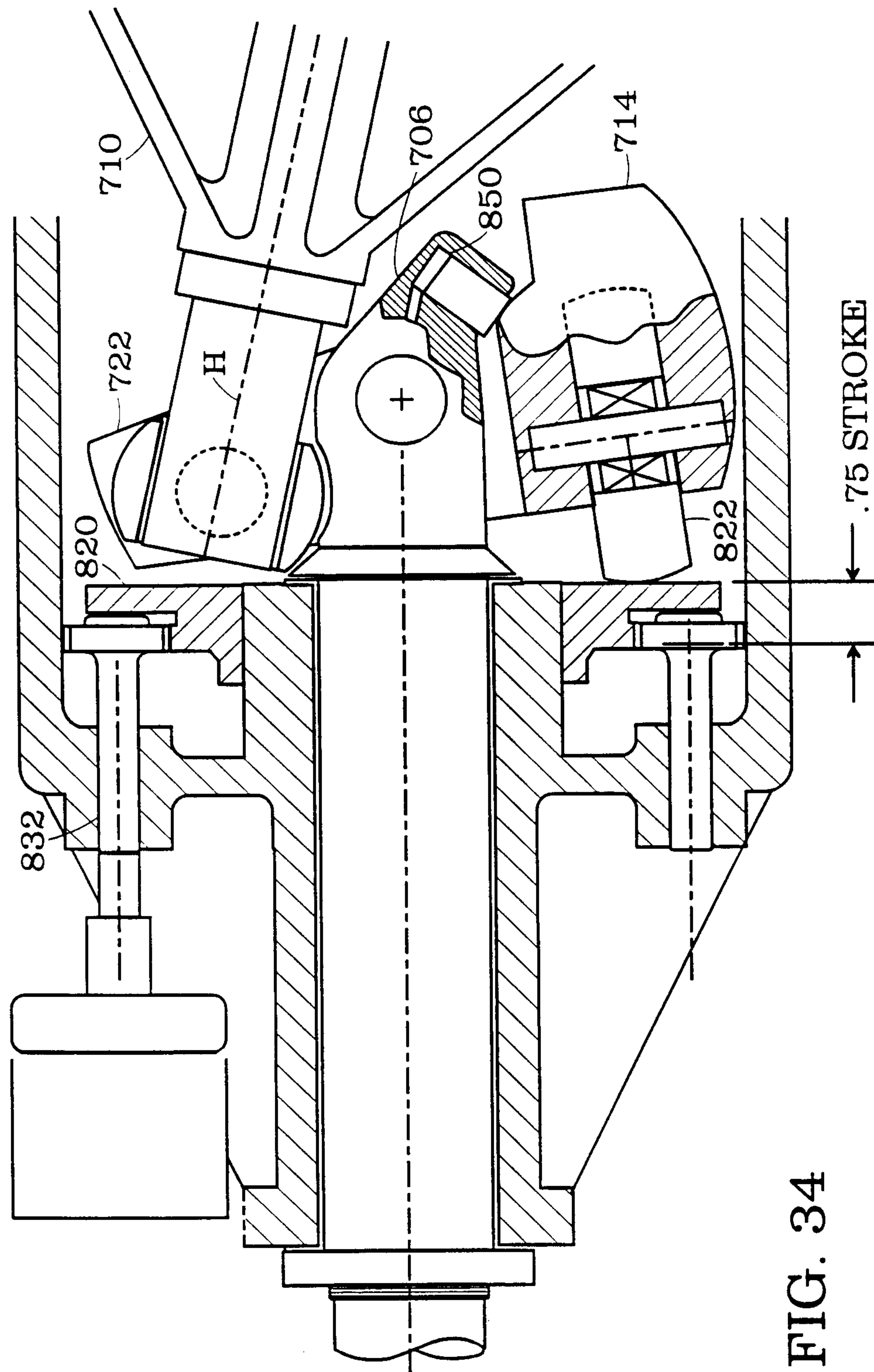


FIG. 34

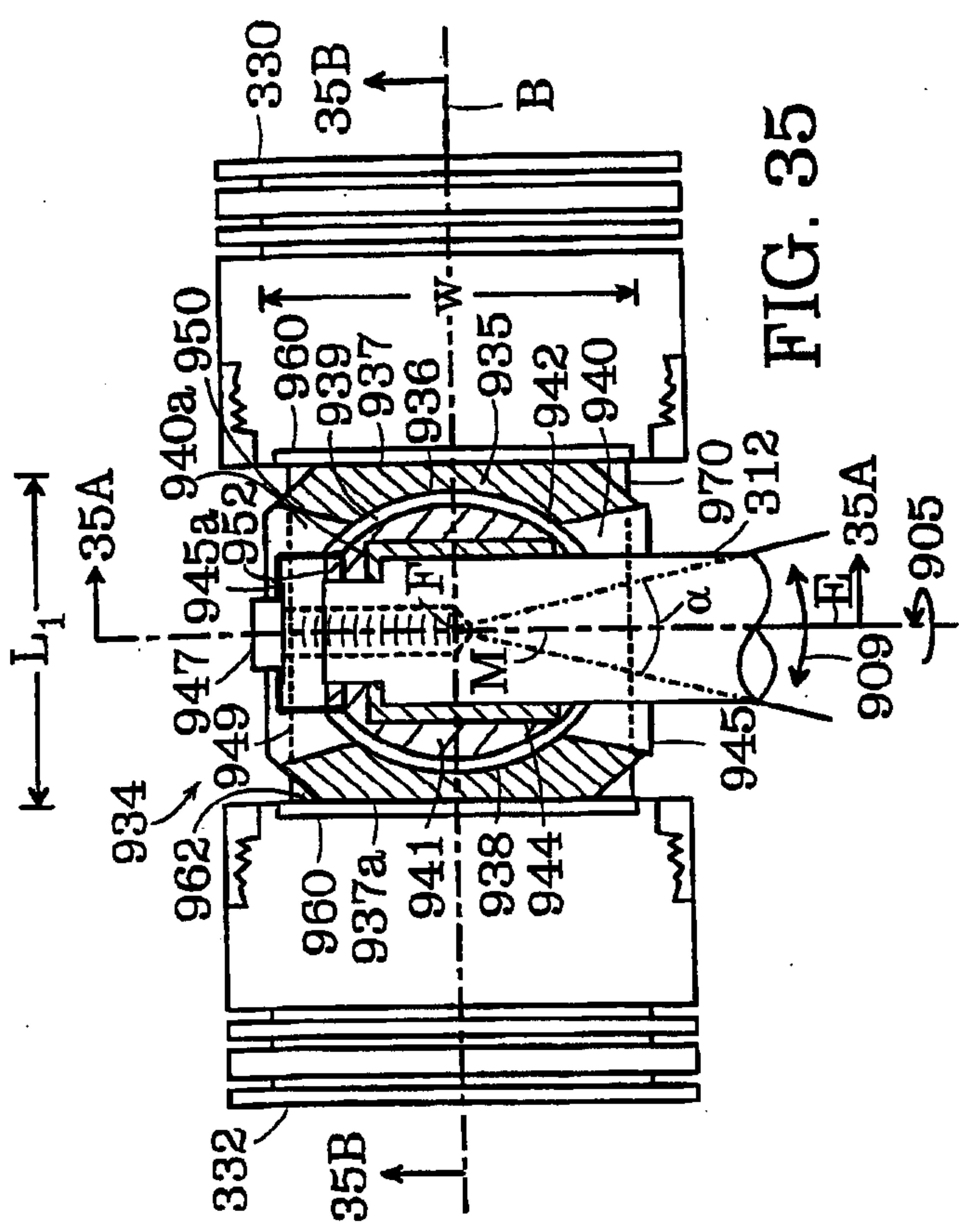


FIG. 35A

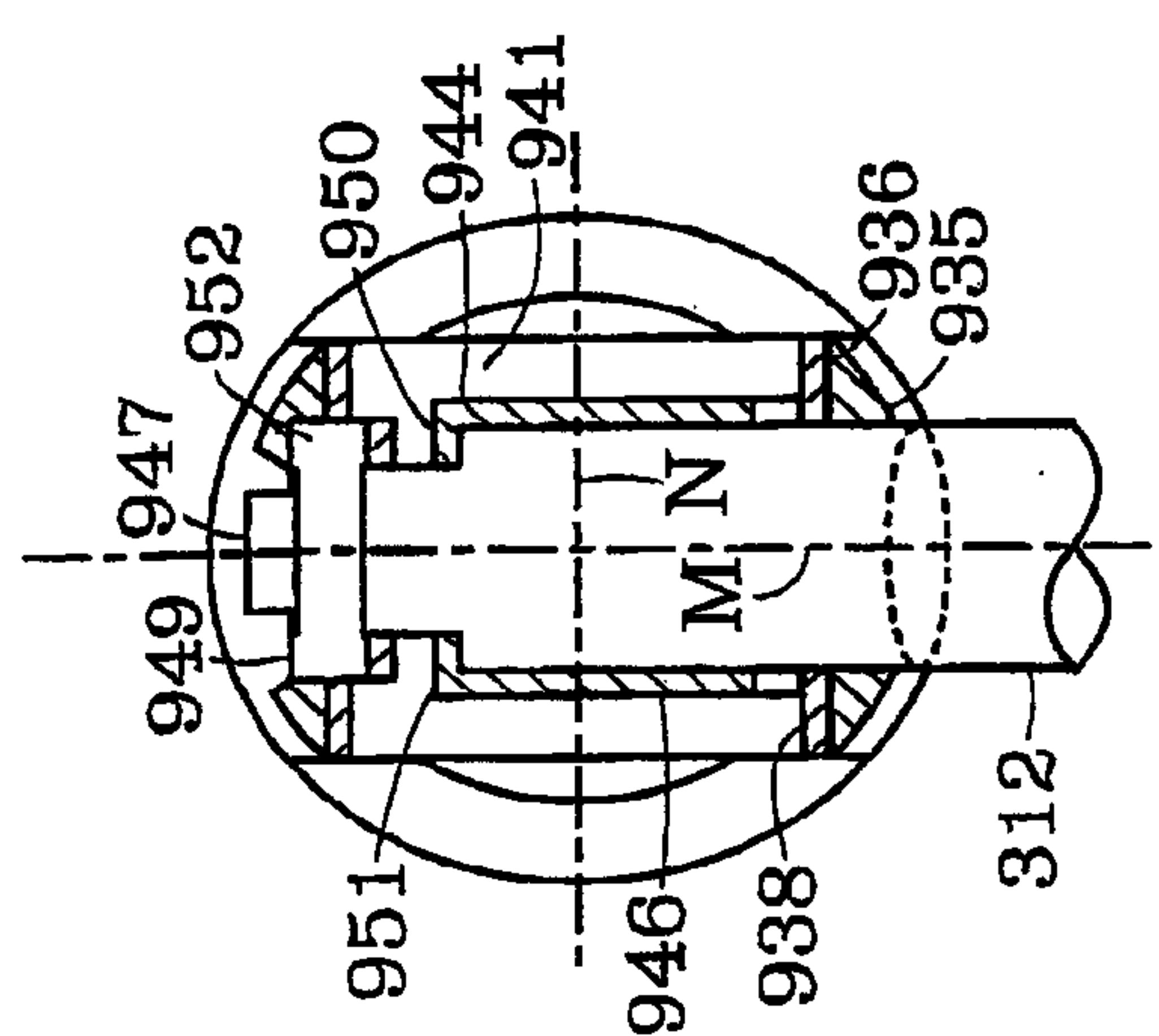
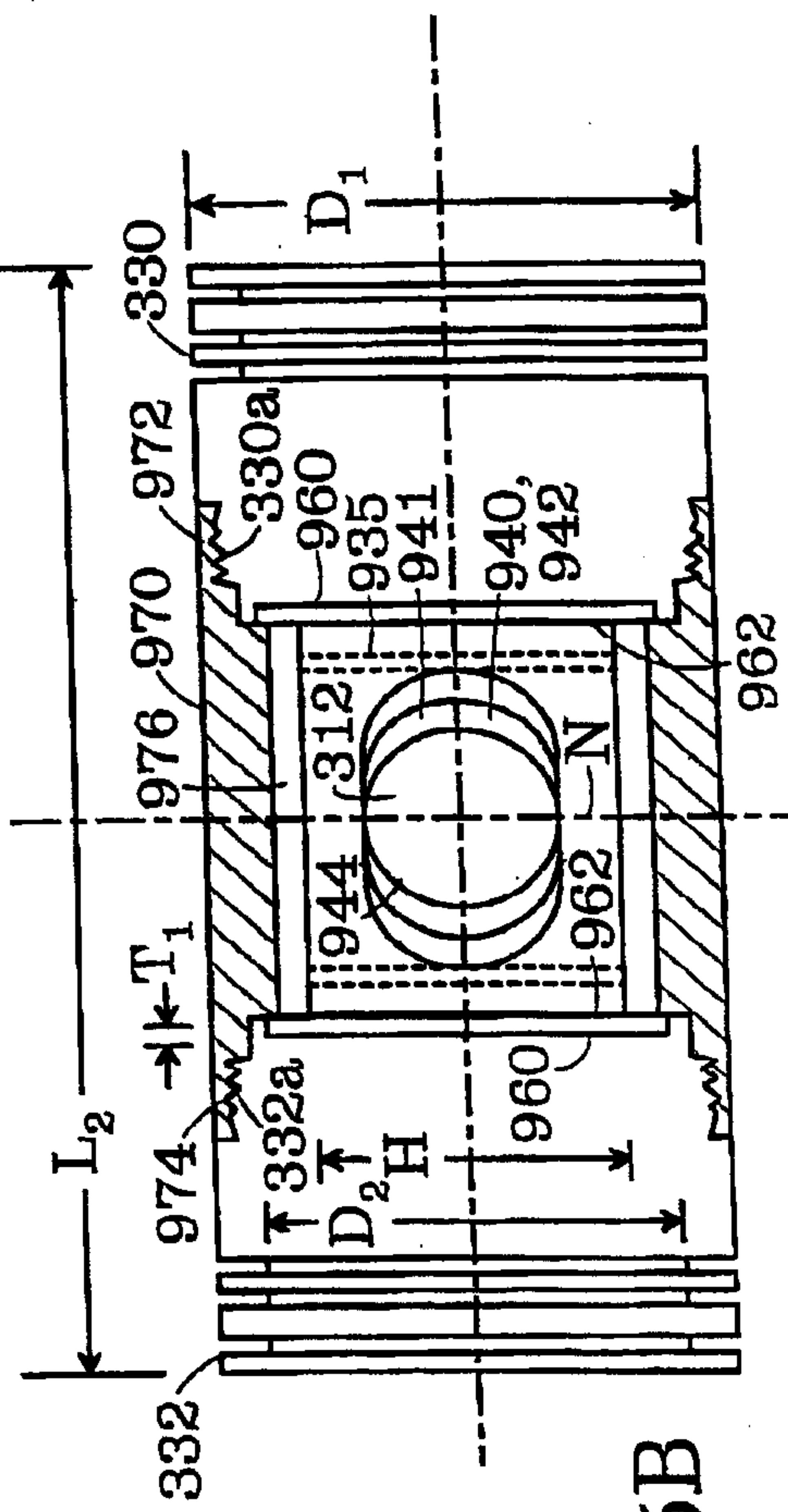


Fig. 3
15
B



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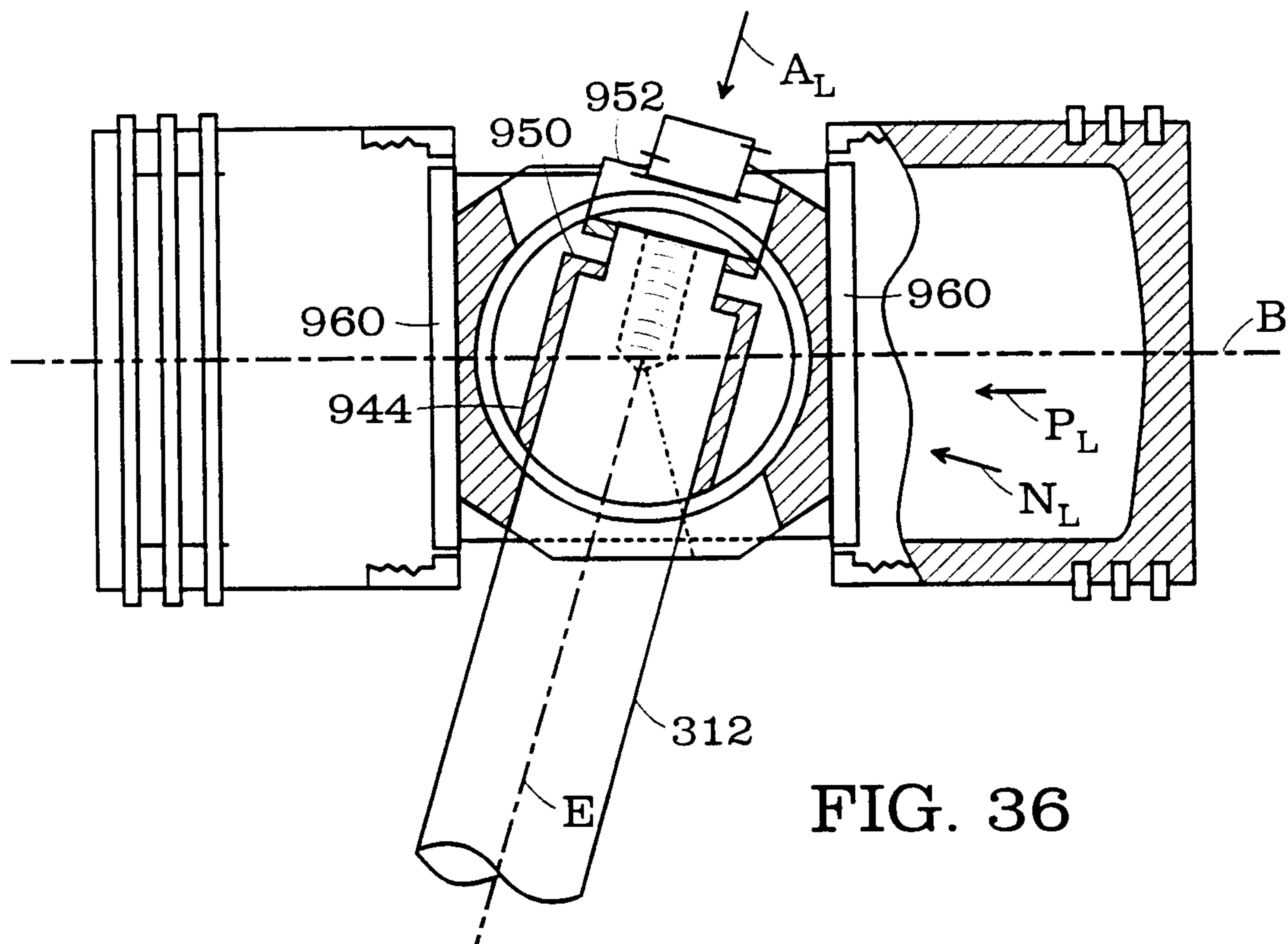


FIG. 36

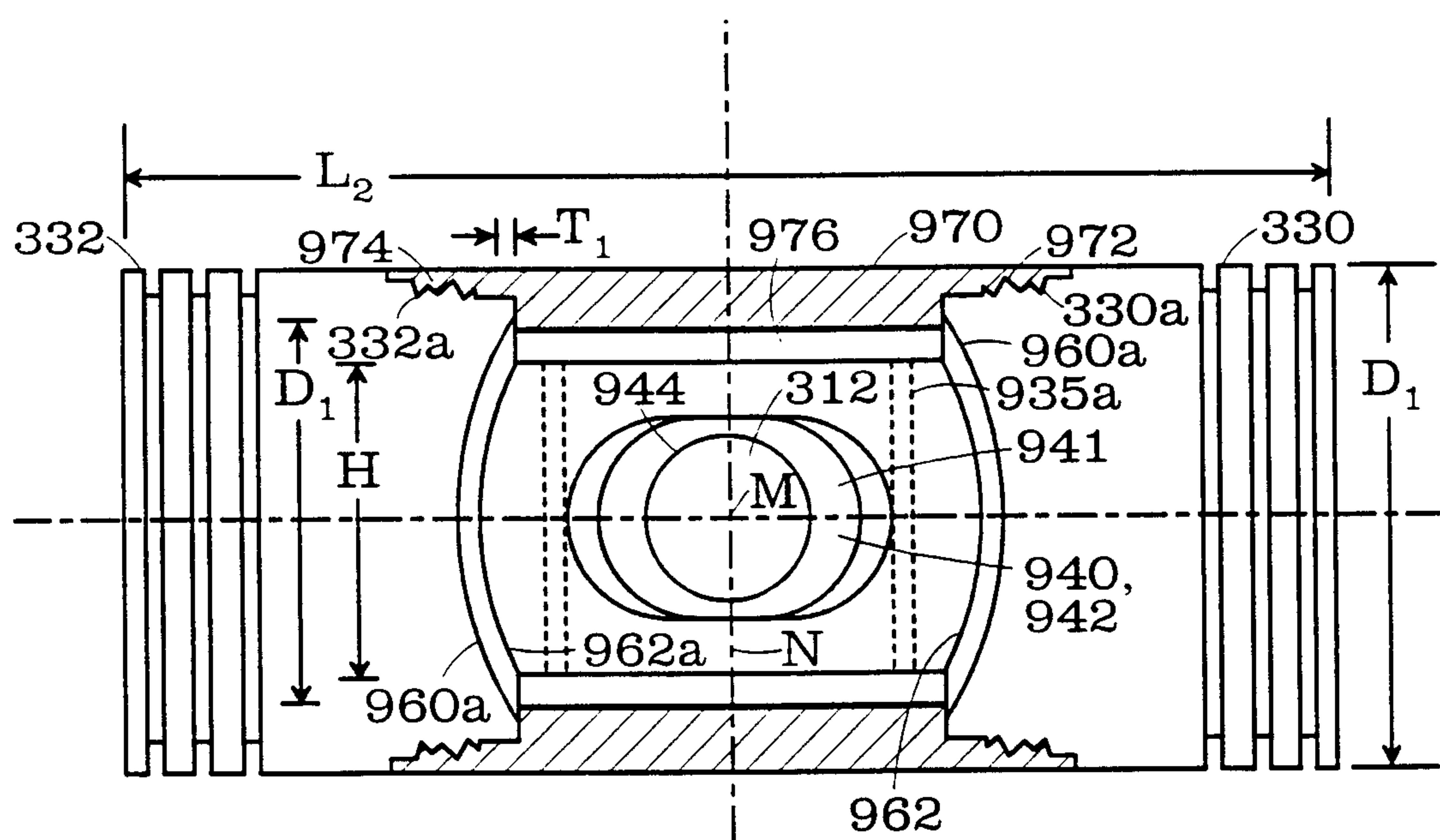


FIG. 37

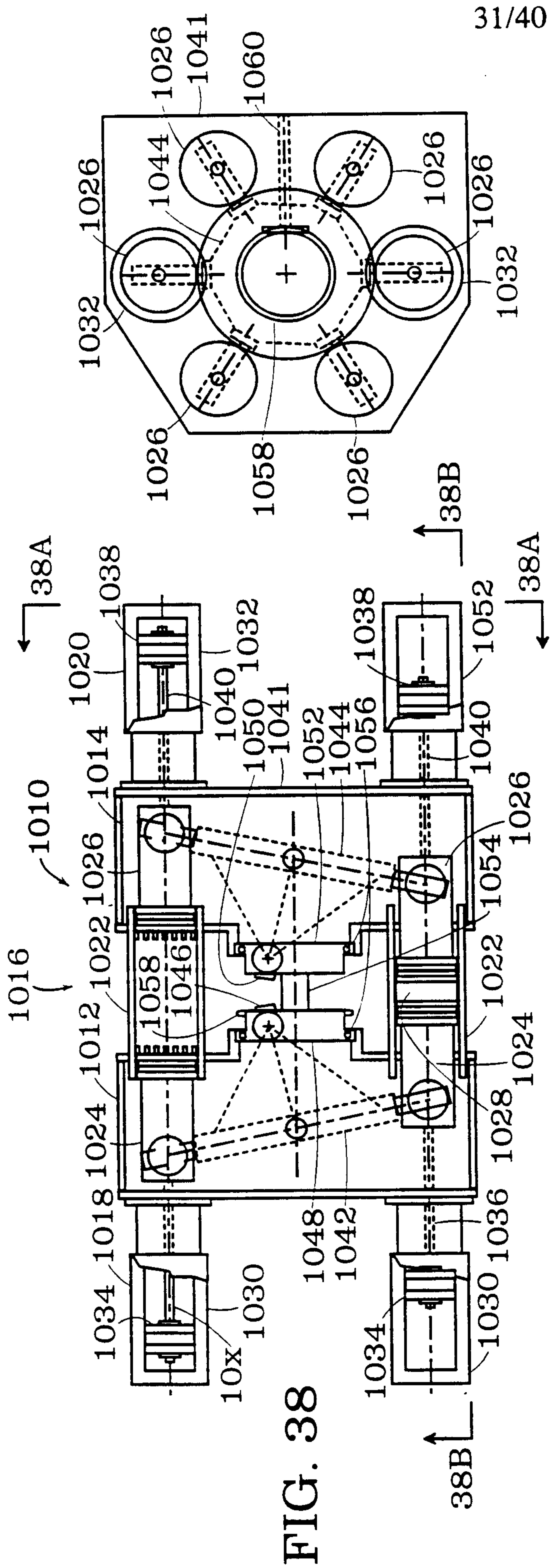


FIG. 38A

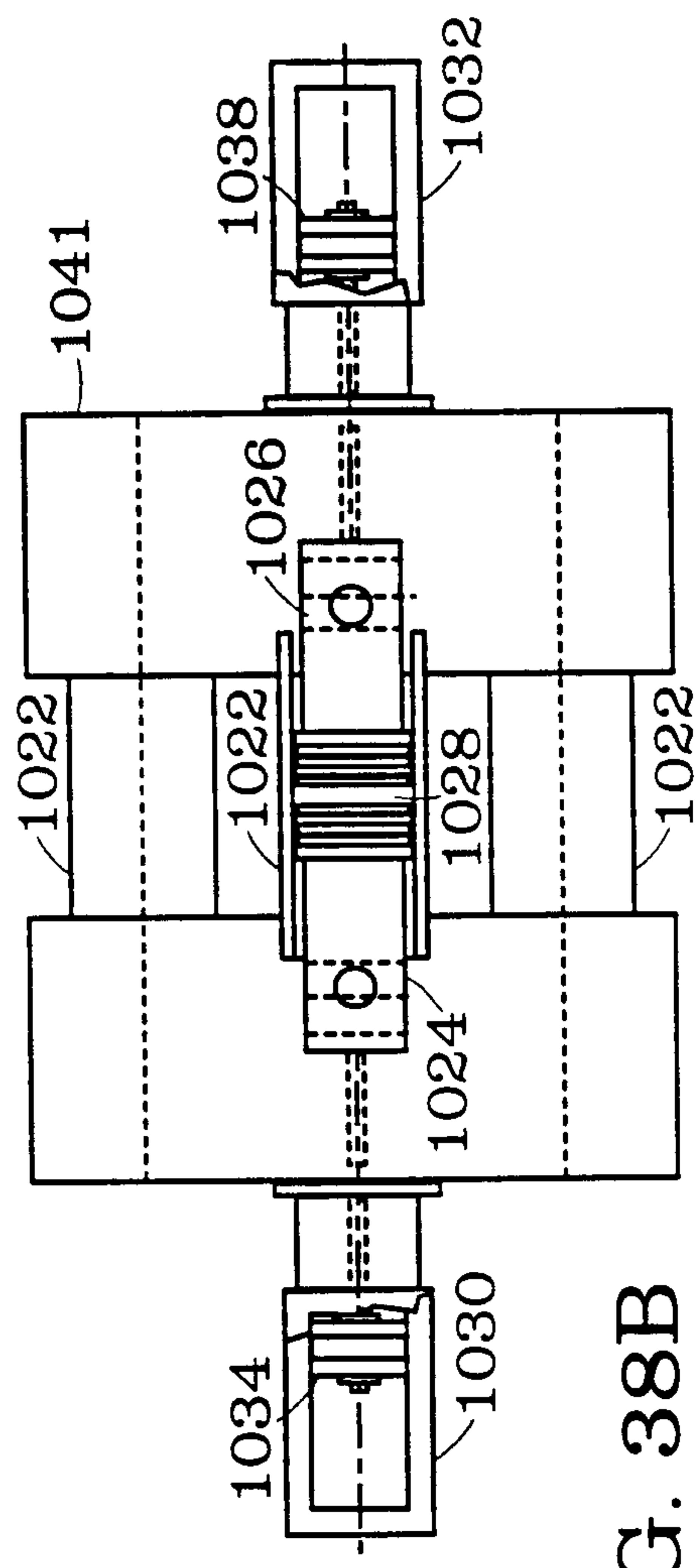


FIG. 38B

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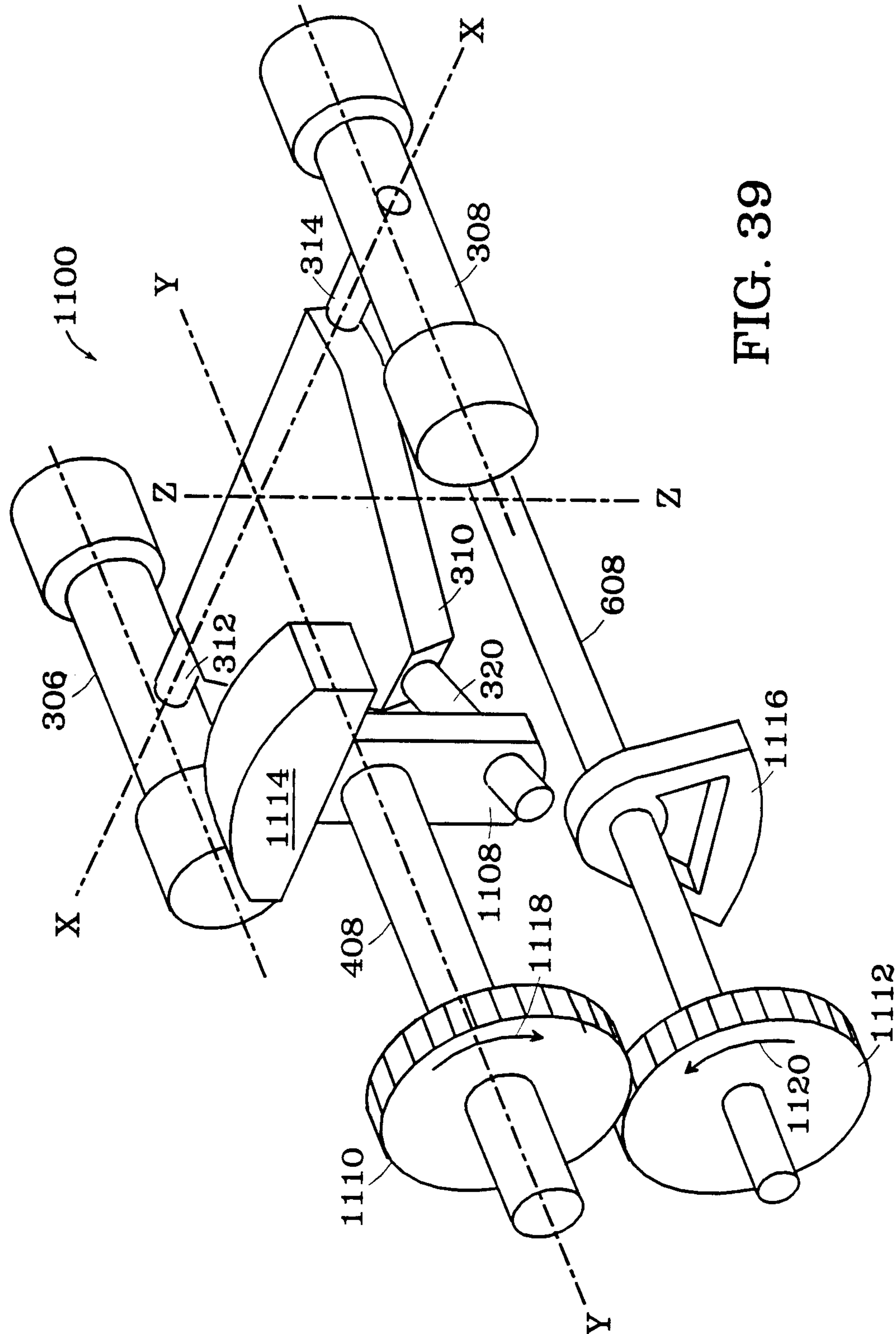


FIG. 39

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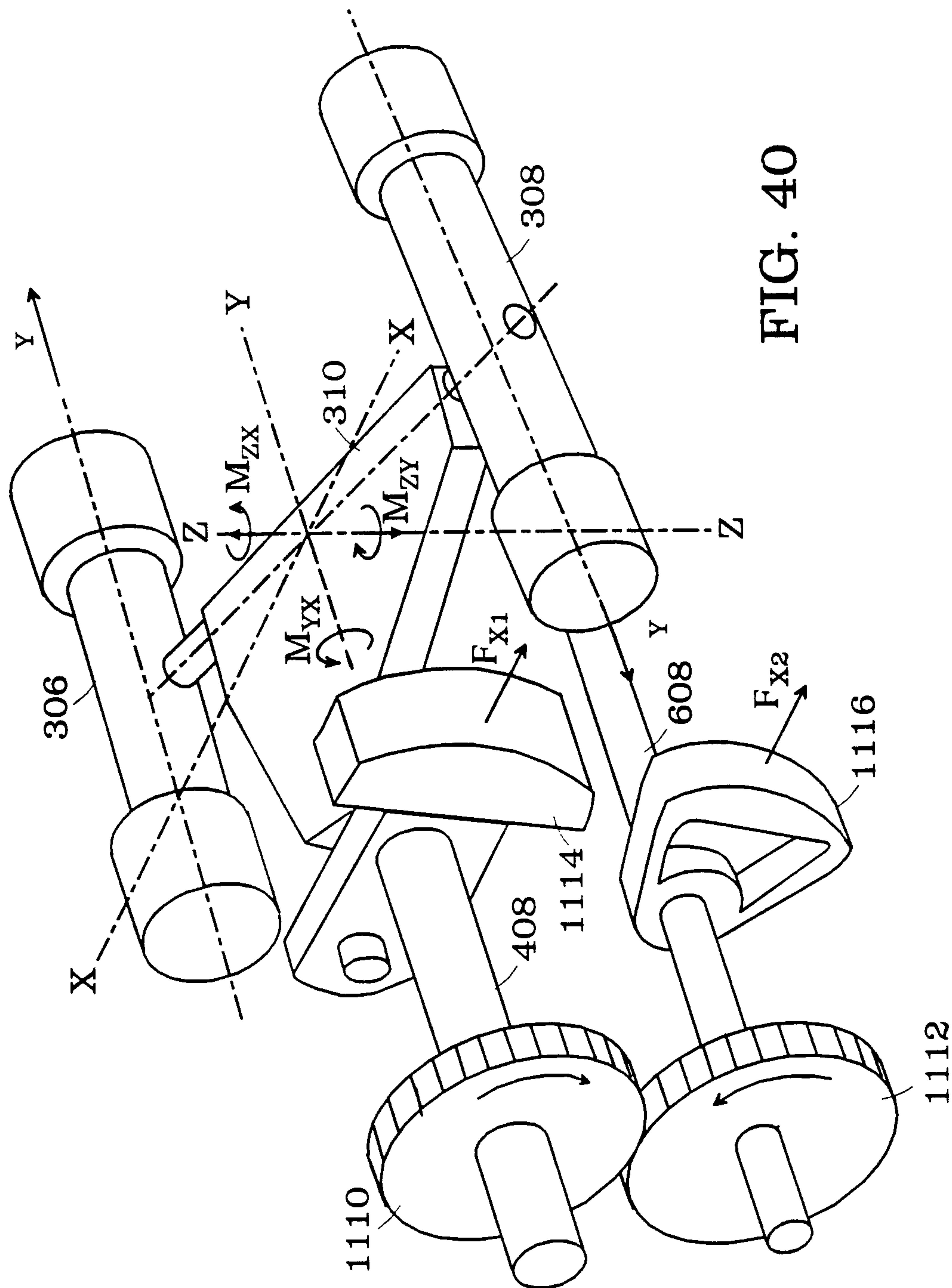


FIG. 40

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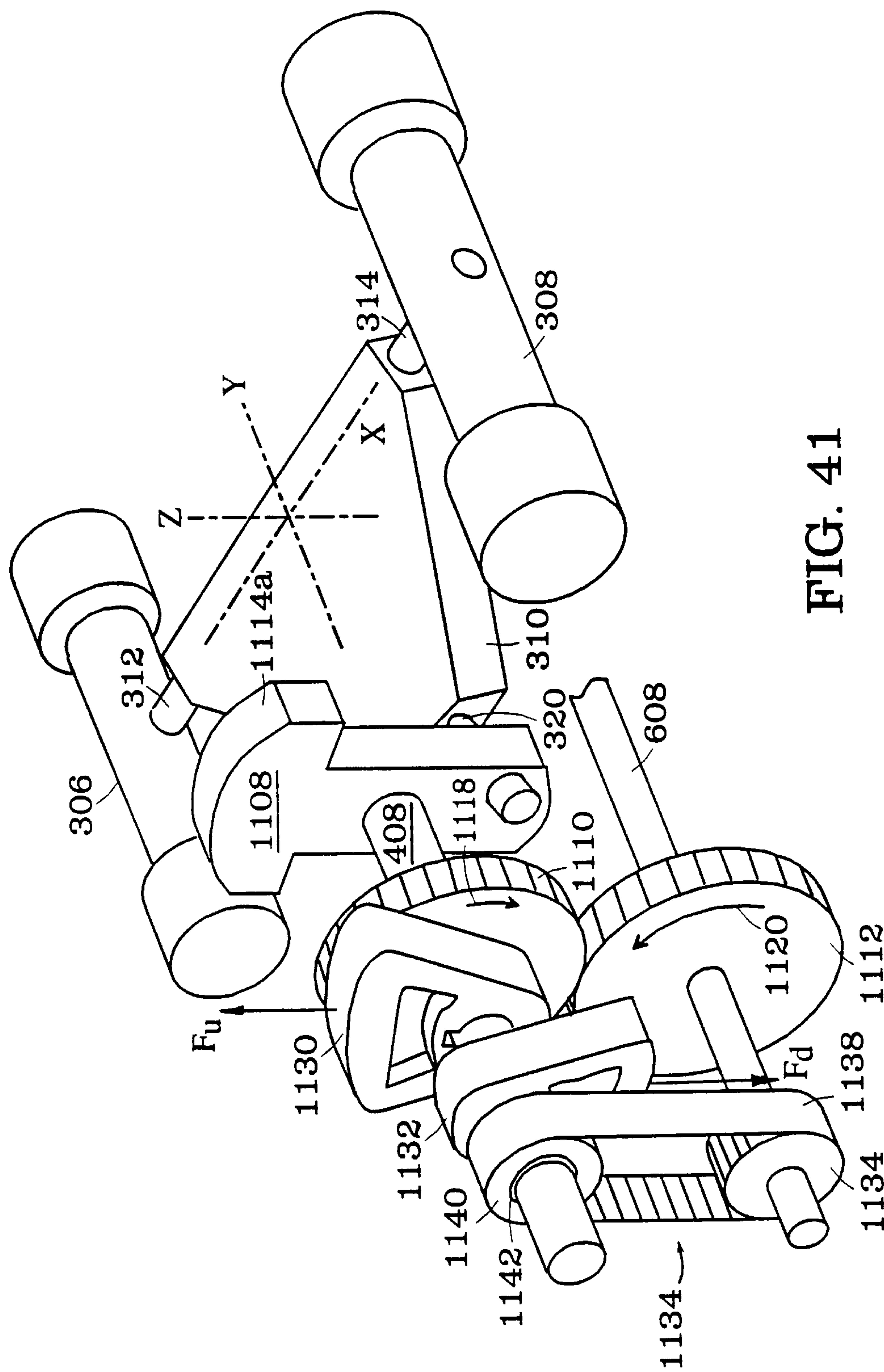


FIG. 41

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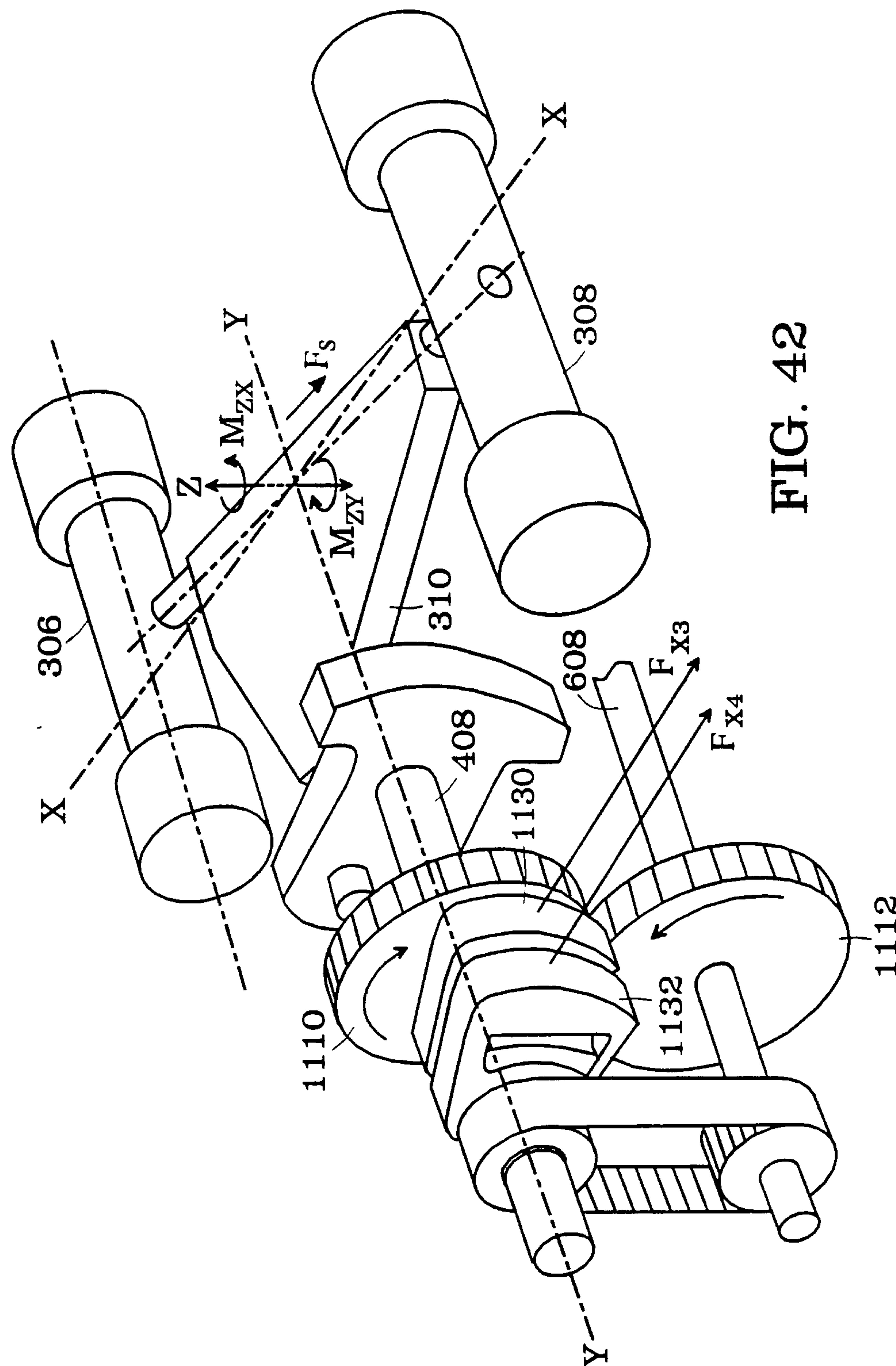
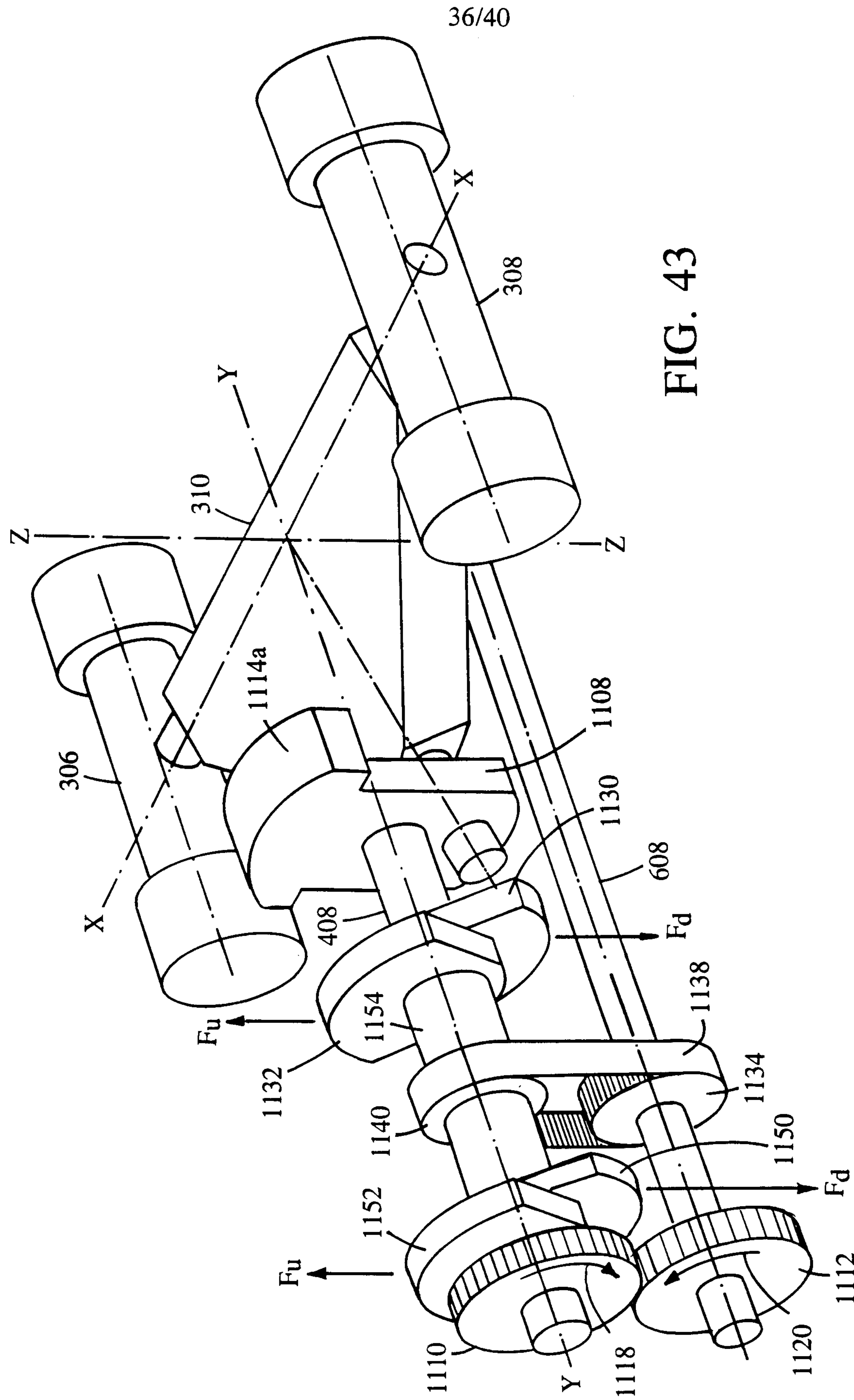


FIG. 42



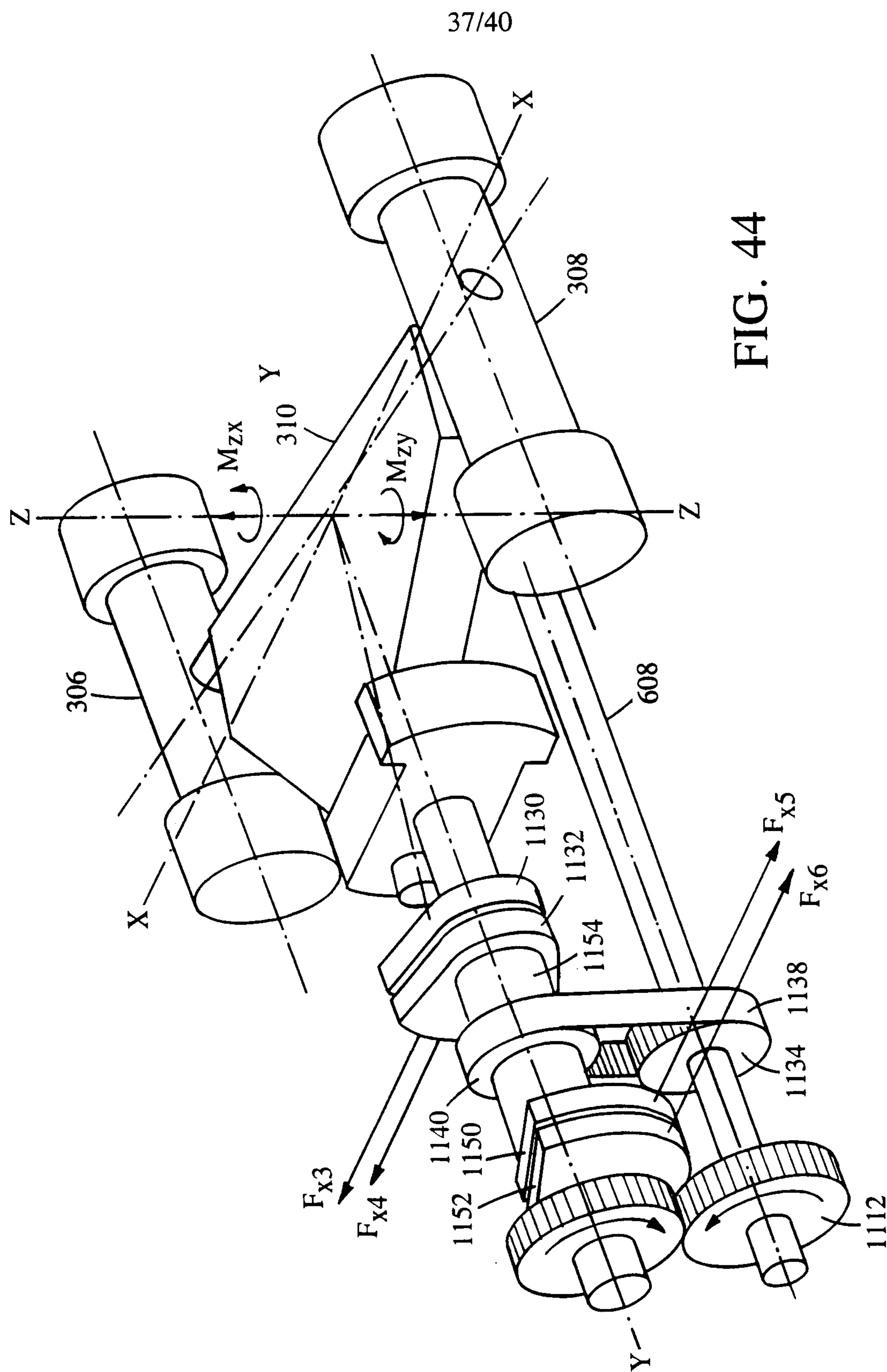
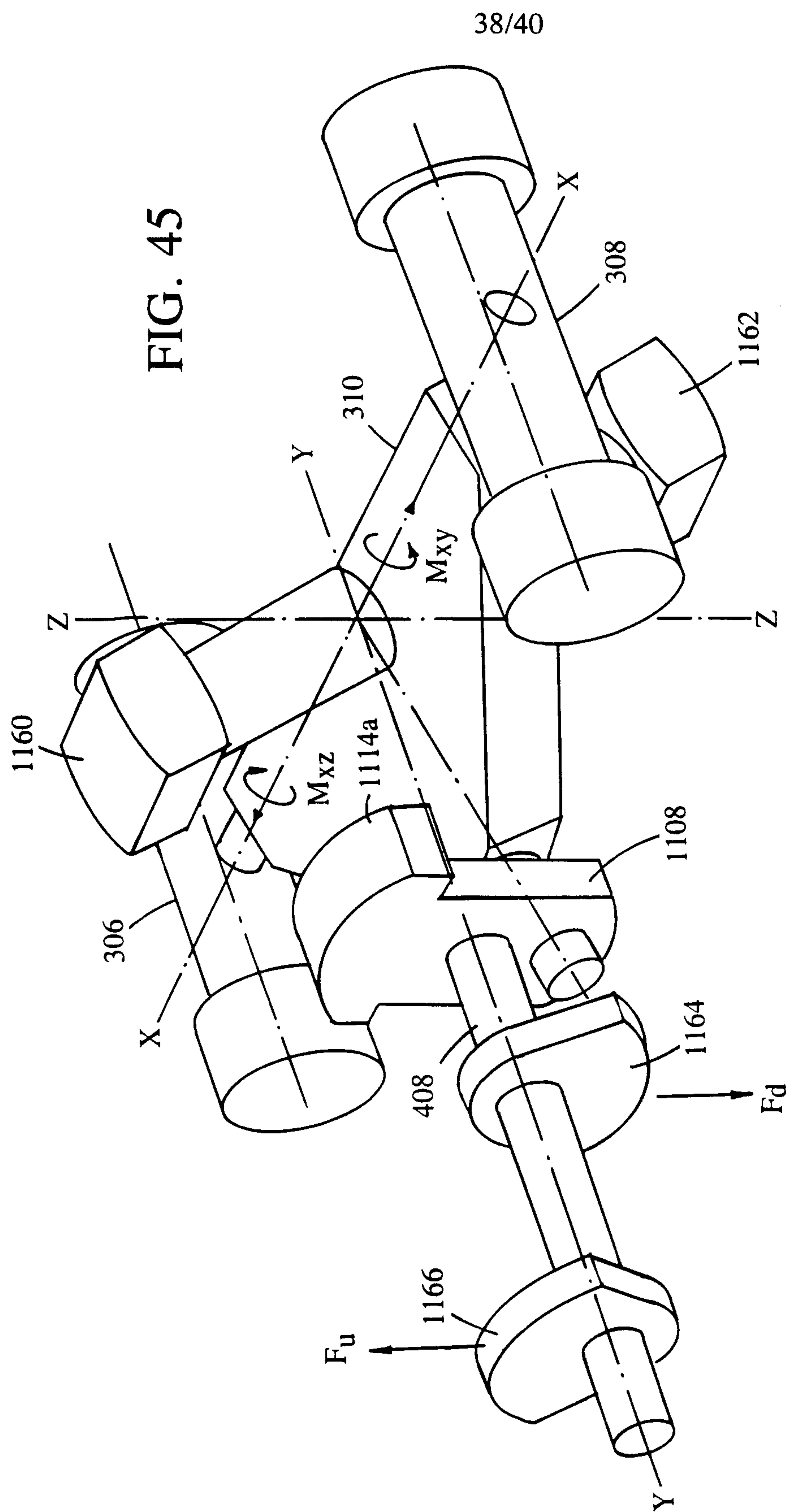
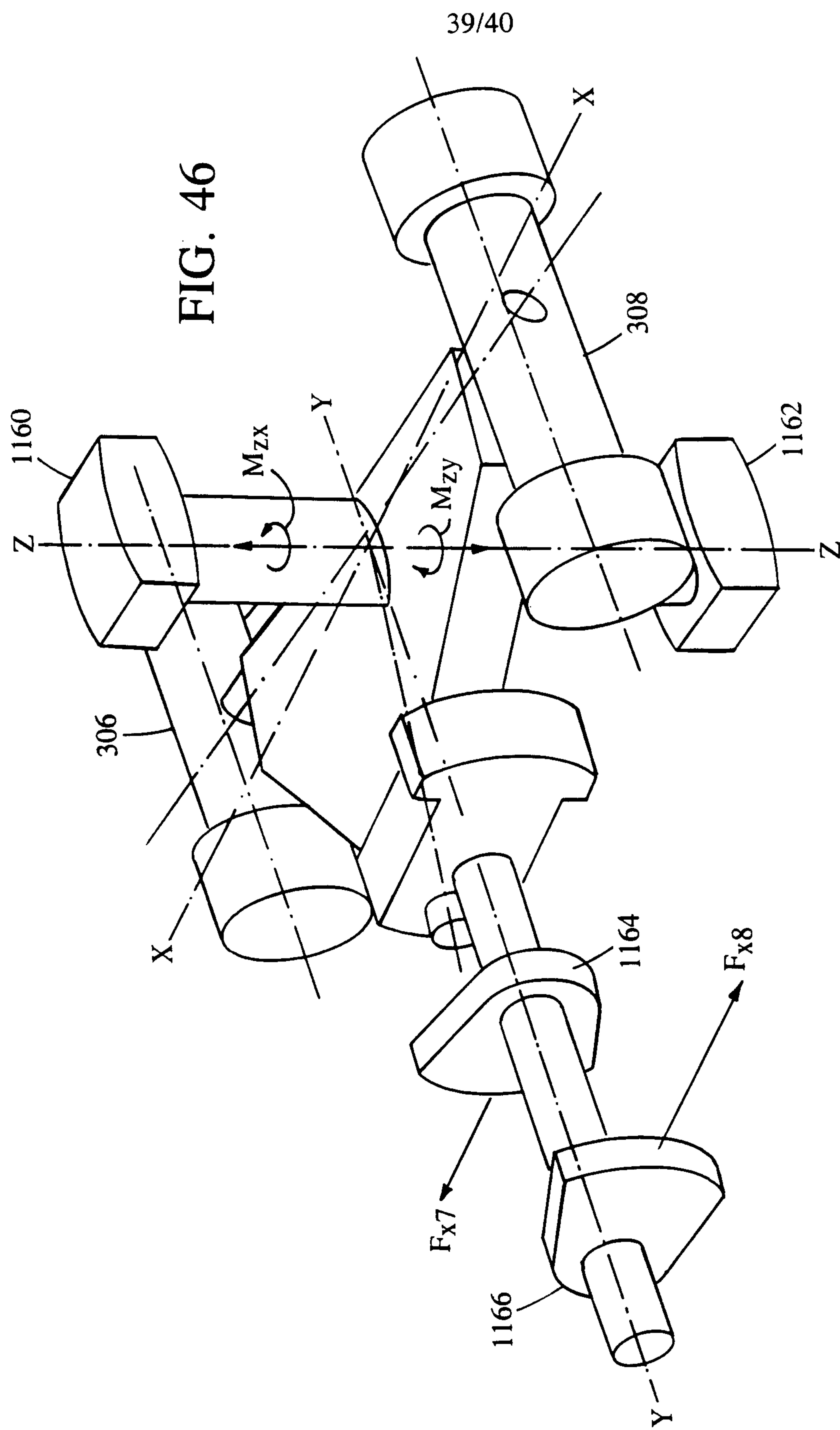


FIG. 45





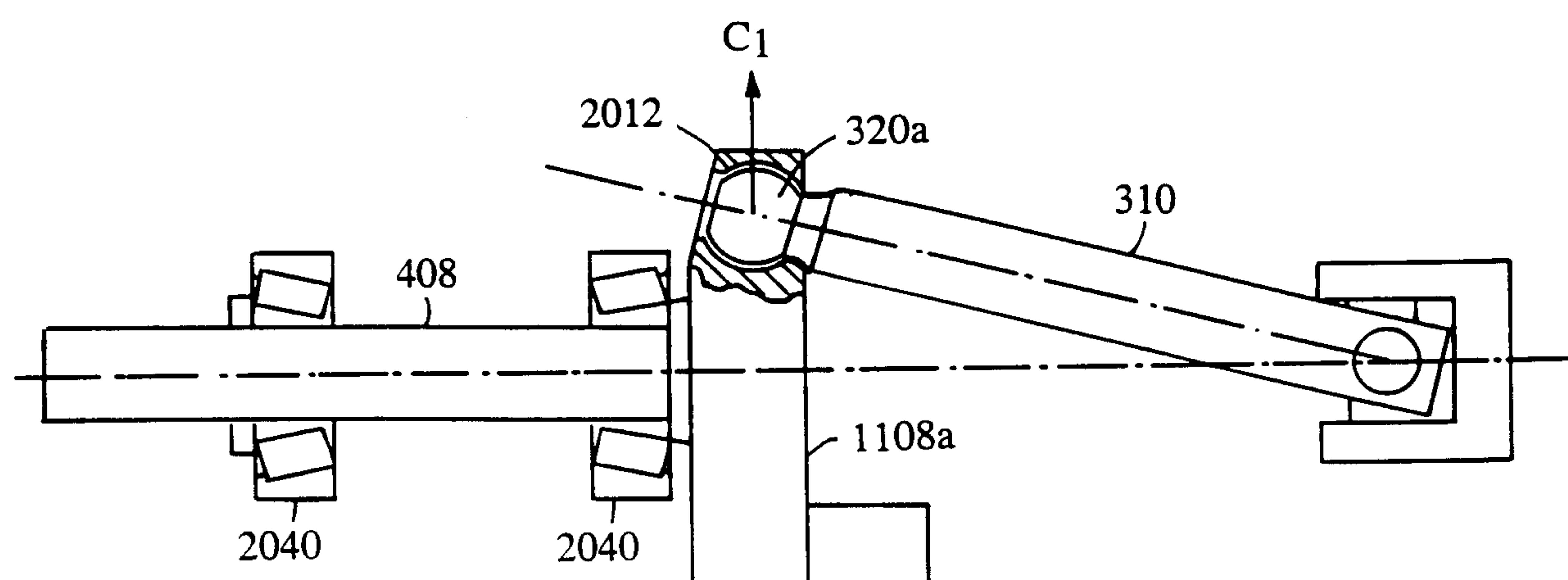
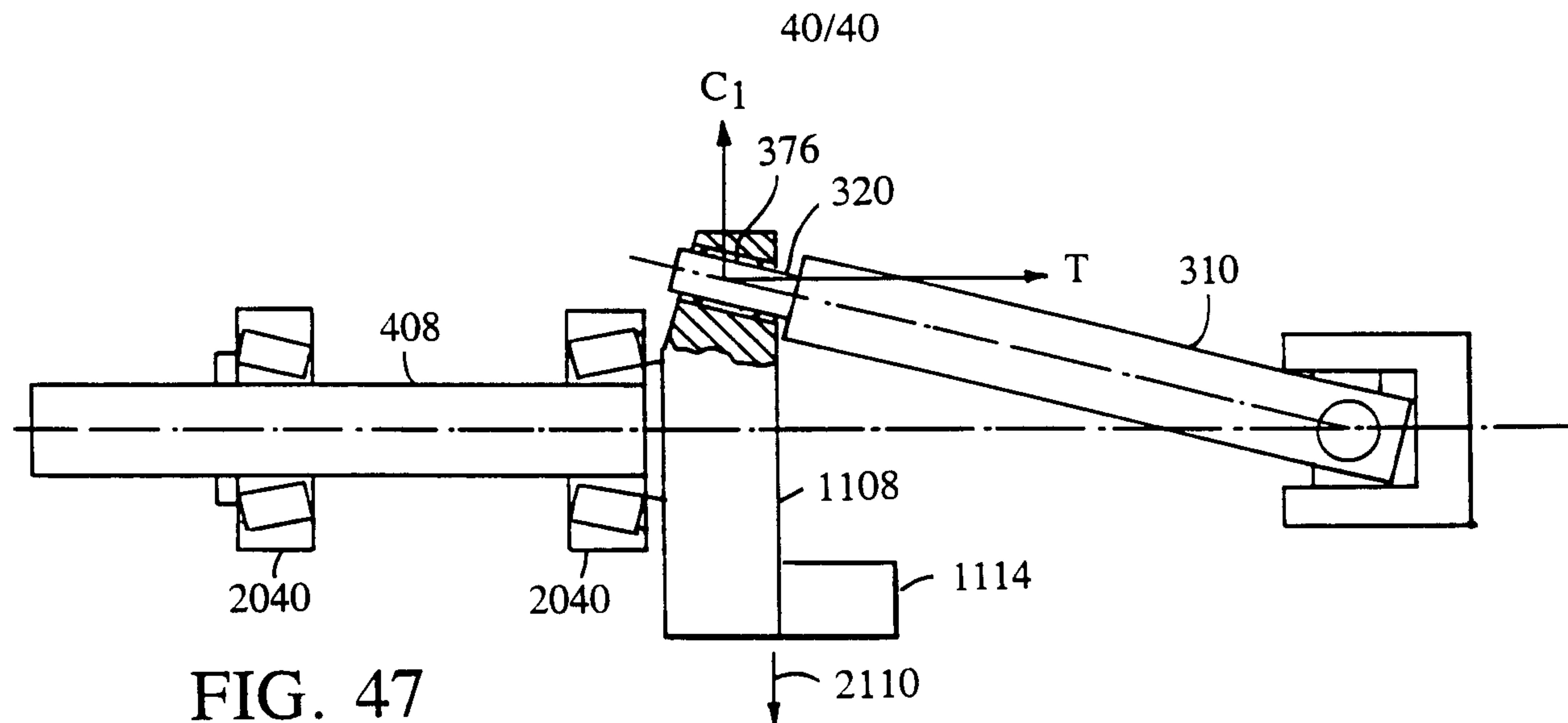


FIG. 48

