



US008781590B2

(12) **United States Patent**  
**Hill et al.**

(10) **Patent No.:** **US 8,781,590 B2**

(45) **Date of Patent:** **Jul. 15, 2014**

(54) **METHOD OF PRODUCING A PROXIMAL CONNECTOR END OF AN IMPLANTABLE LEAD**

USPC ..... 607/36, 37; 600/394  
See application file for complete search history.

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(57) **ABSTRACT**

A connector for an implantable medical lead that is electrically and mechanically connectable to an implantable medical device, has a connector pin made of a first conducting material. A tubular insulator made of an insulating material concentrically surrounds at least a portion of the pin. A connector ring made of a second conducting material is concentrically positioned around at least a portion of the insulator. The insulator is connected to the connector ring by spark plasma sintering in the case of an active fixation lead, and is connected to the ring and the pin by spark plasma sintering in the case of a passive fixation lead.

**10 Claims, 8 Drawing Sheets**

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(\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 76 days.

(21) Appl. No.: **13/557,009**

(22) Filed: **Jul. 24, 2012**

(65) **Prior Publication Data**

US 2012/0290060 A1 Nov. 15, 2012

**Related U.S. Application Data**

(62) Division of application No. 12/741,611, filed as application No. PCT/SE2007/001007 on Nov. 14, 2007, now Pat. No. 8,250,749.

(51) **Int. Cl.**

<b>A61N 1/375</b>	(2006.01)
<b>A61N 1/05</b>	(2006.01)
<b>H01R 43/20</b>	(2006.01)
<b>H01R 24/58</b>	(2011.01)

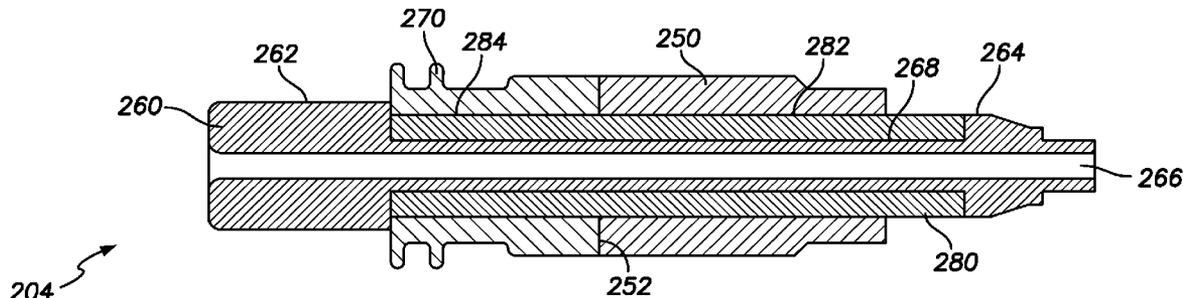
(52) **U.S. Cl.**

CPC **A61N 1/05** (2013.01); **H01R 43/20** (2013.01); **H01R 2201/12** (2013.01); **A61B 2562/227** (2013.01); **A61N 1/3752** (2013.01); **H01R 24/58** (2013.01)

USPC ..... 607/37; 607/36; 600/394

(58) **Field of Classification Search**

CPC ..... A61N 1/3752; A61N 1/3968



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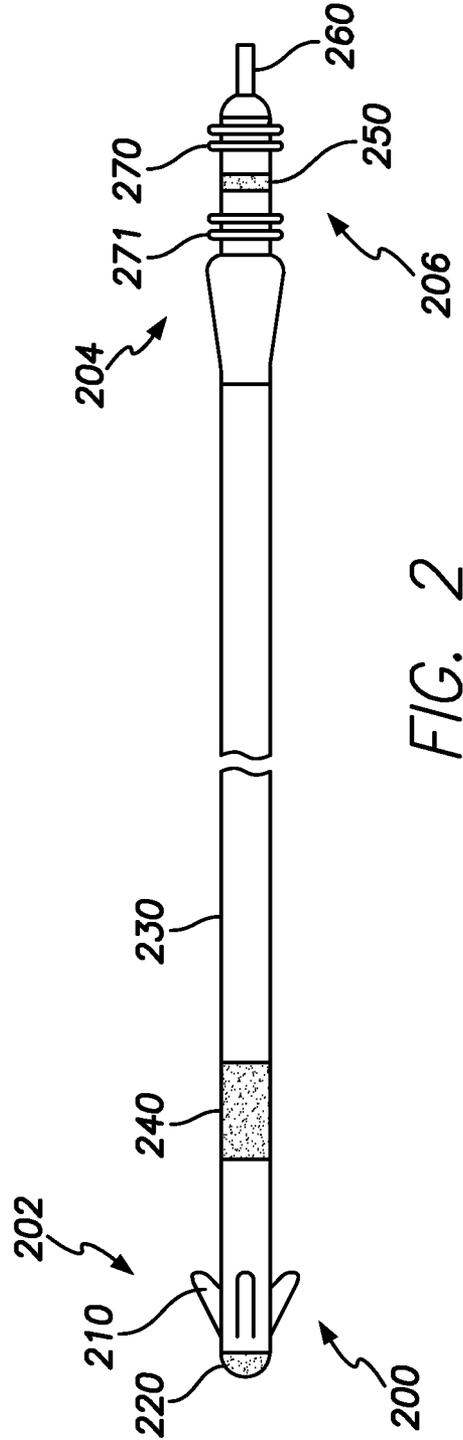
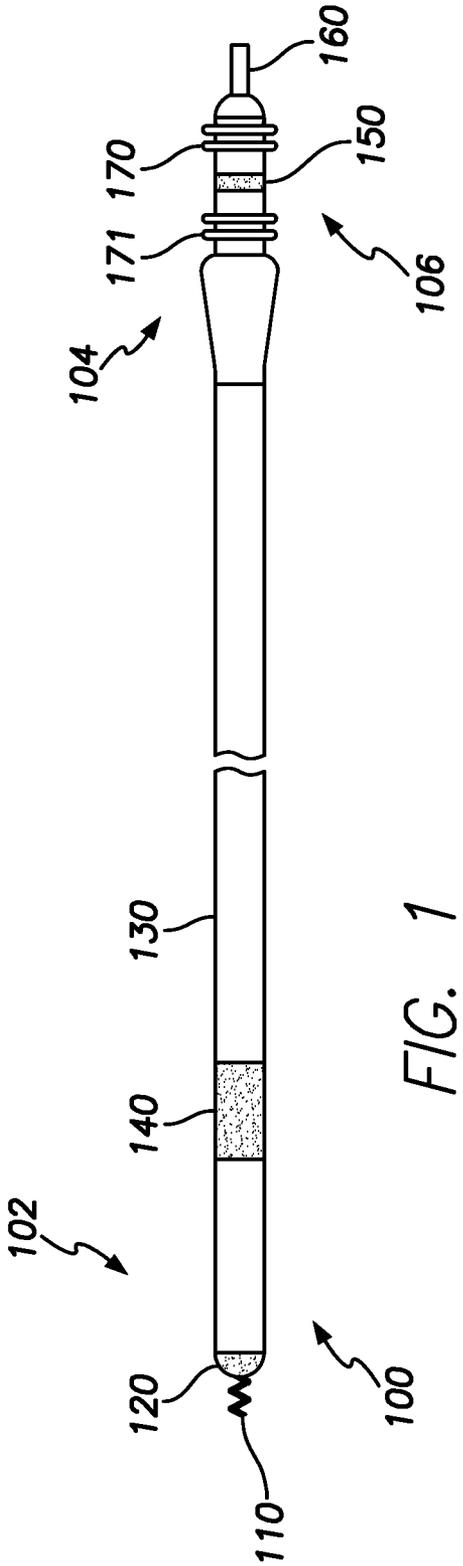
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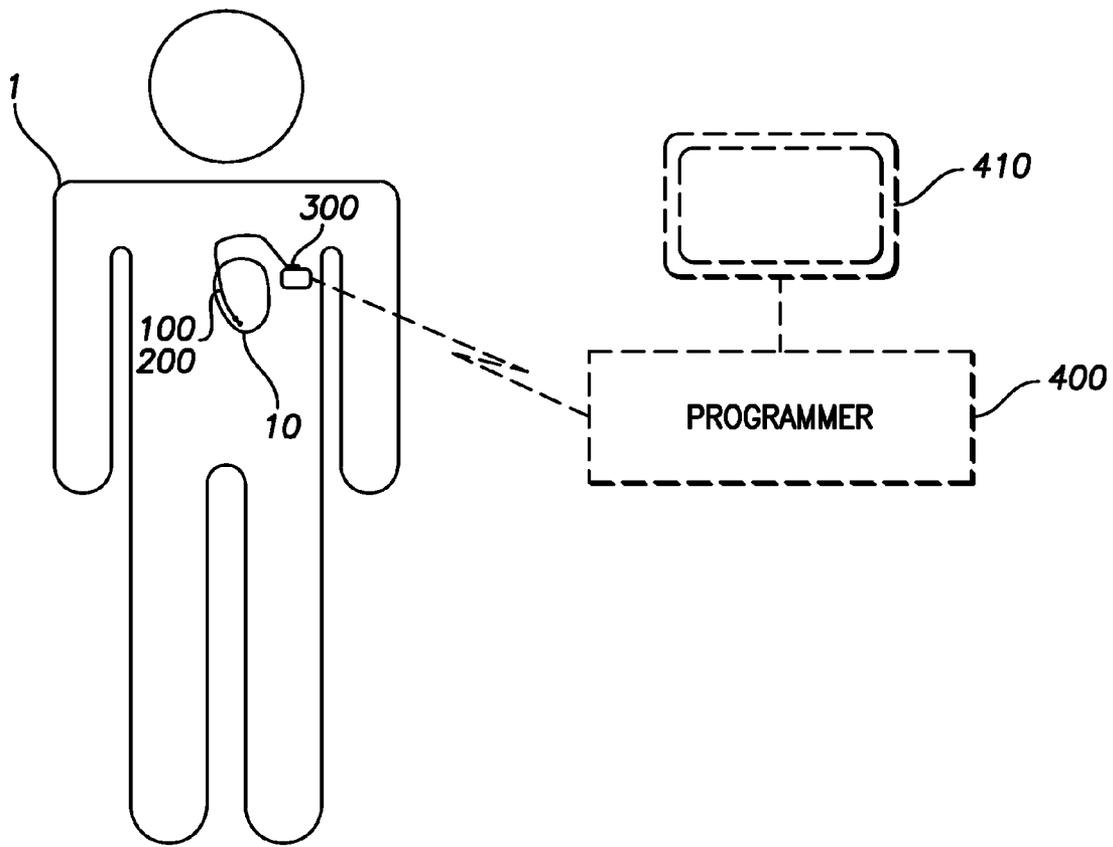


FIG. 3

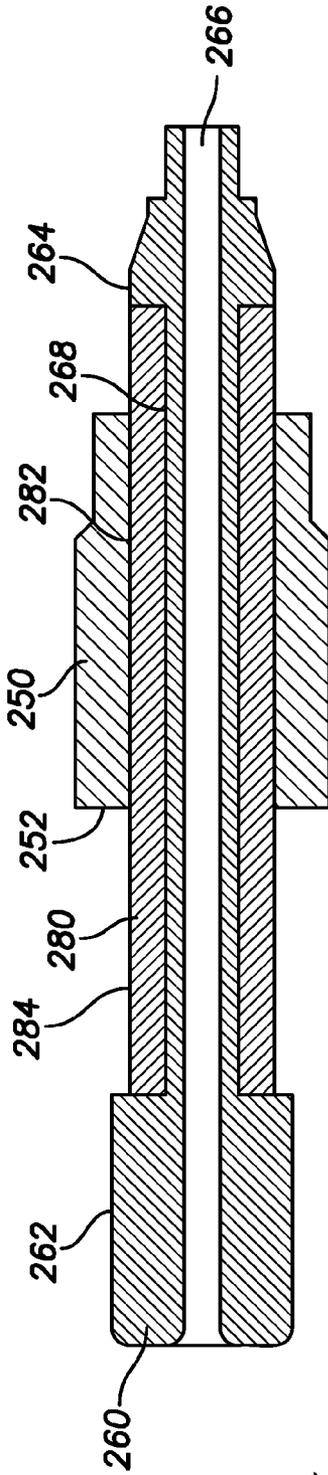


FIG. 4

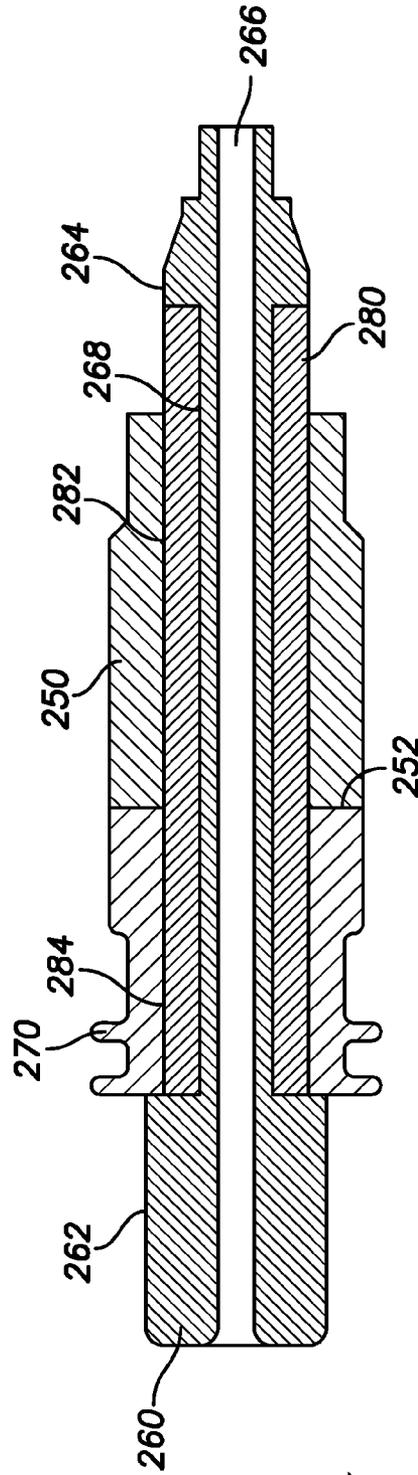
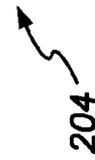


FIG. 5



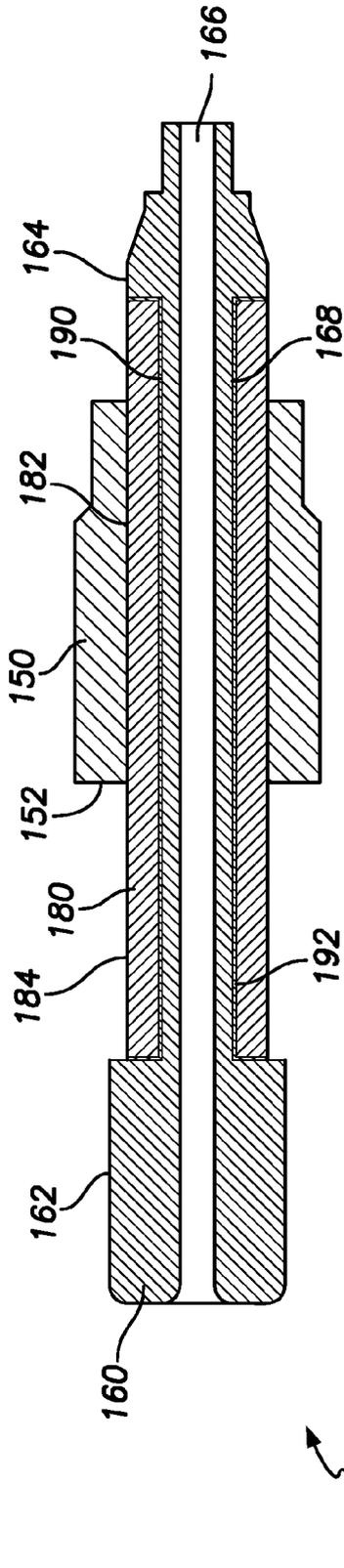


FIG. 6

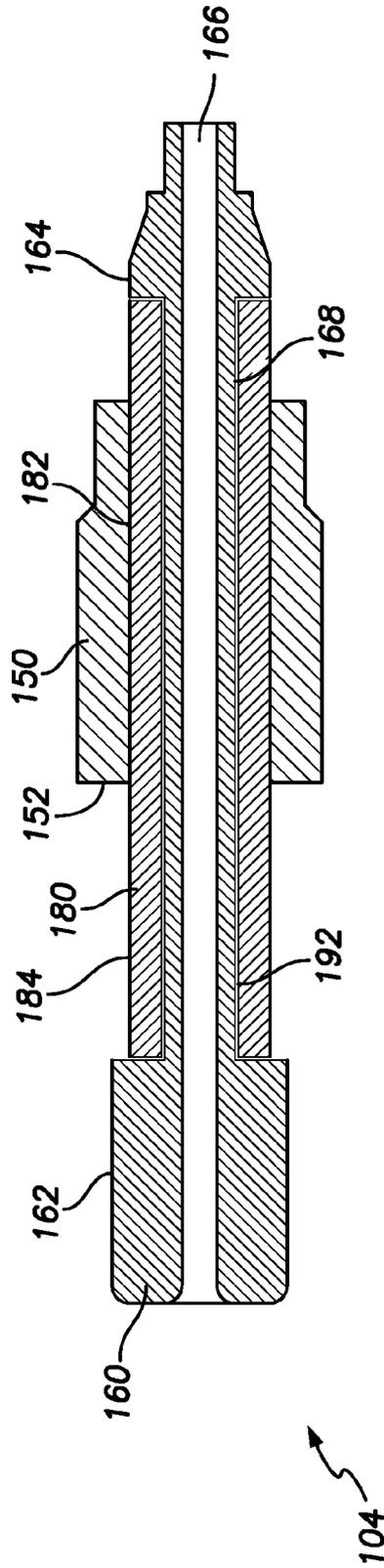


FIG. 7

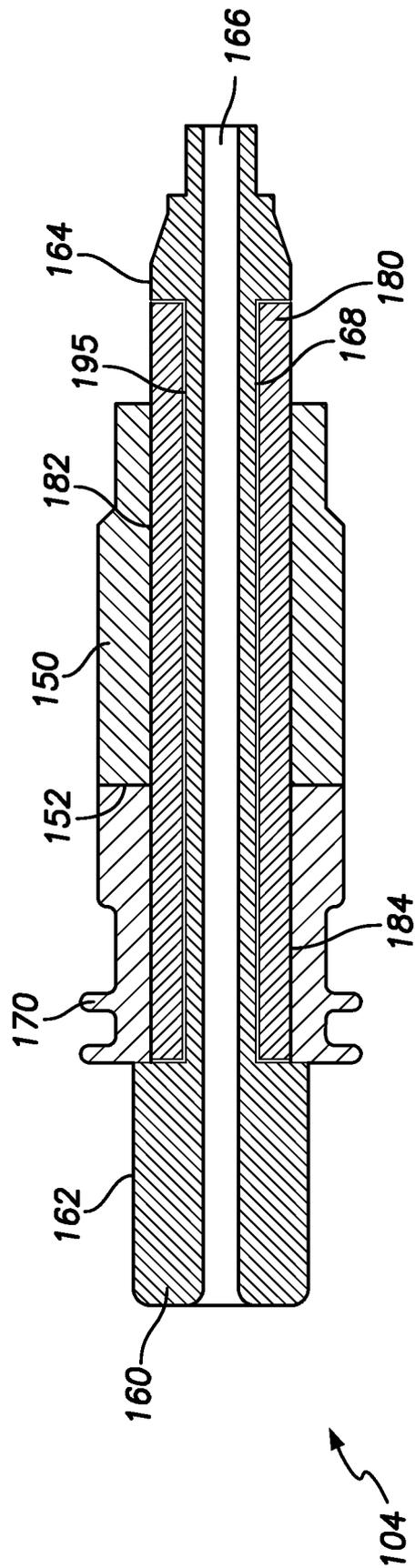


FIG. 8

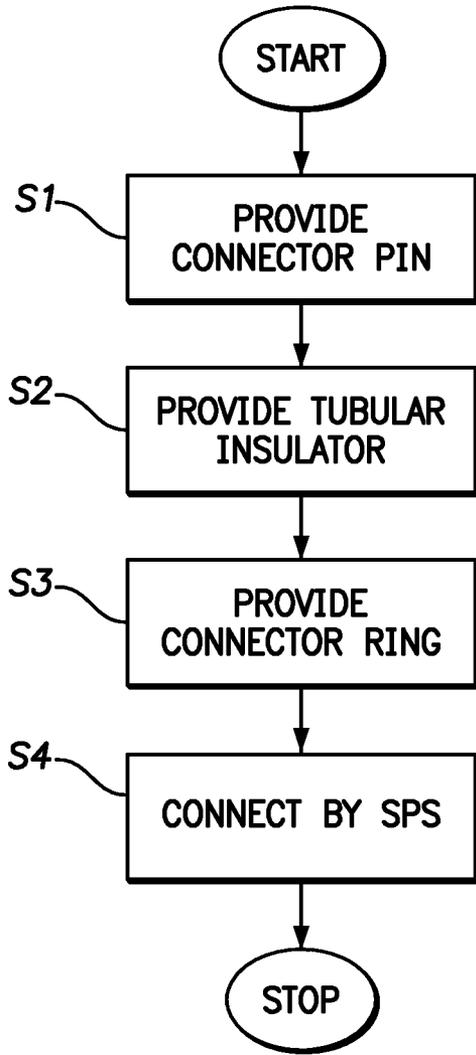


FIG. 9

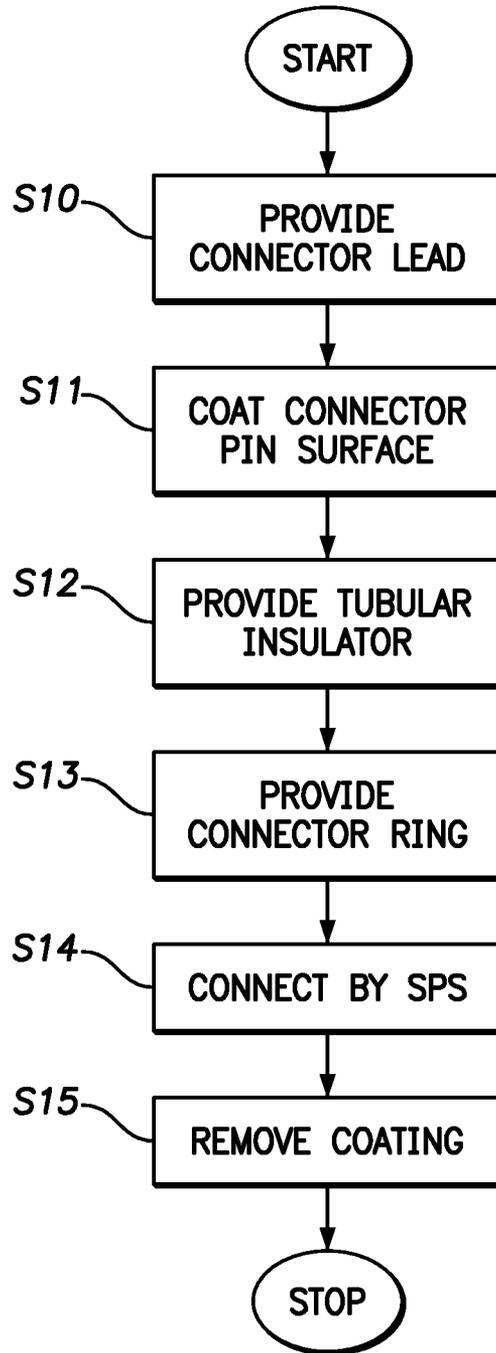


FIG. 10

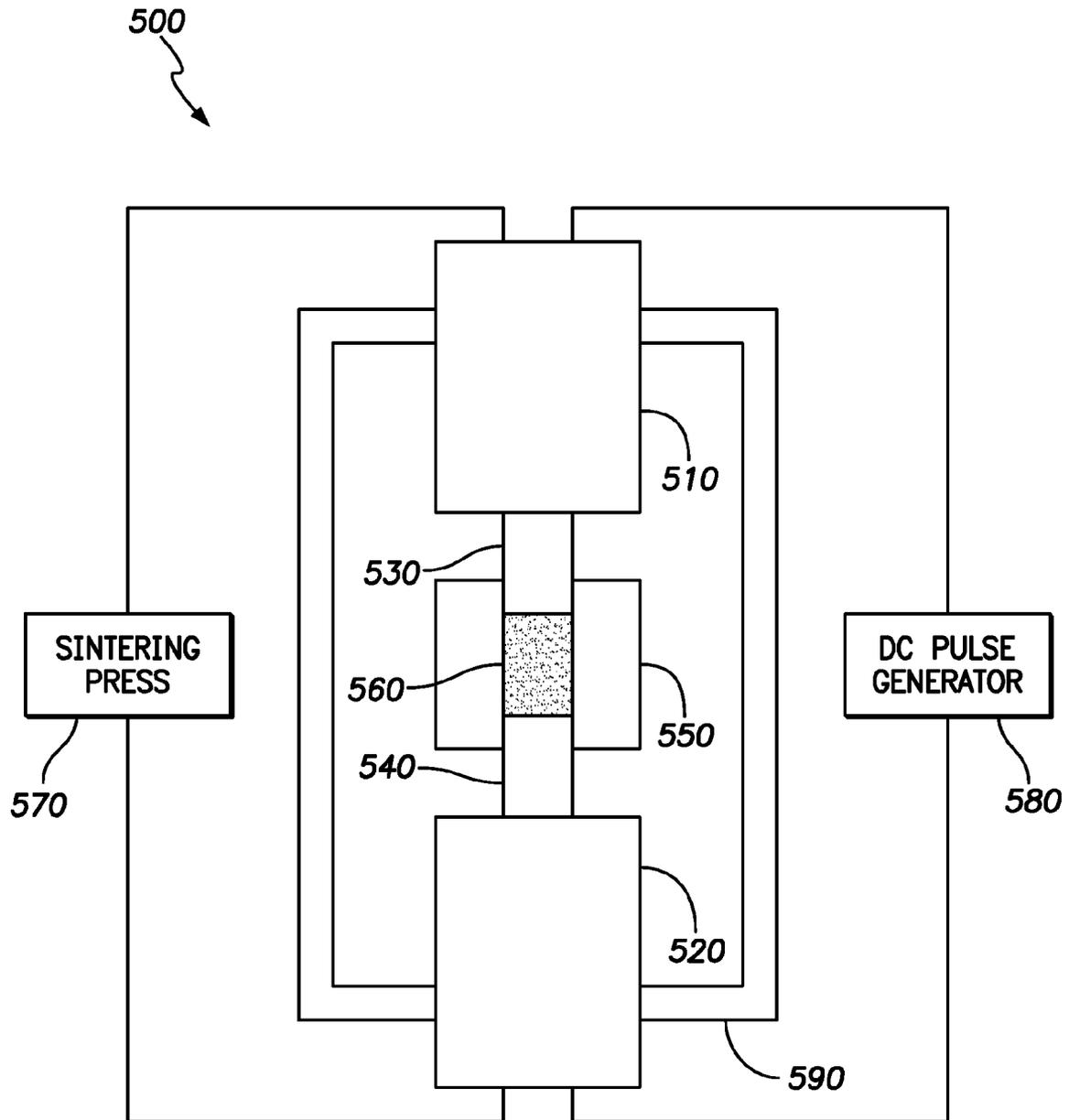


FIG. 11

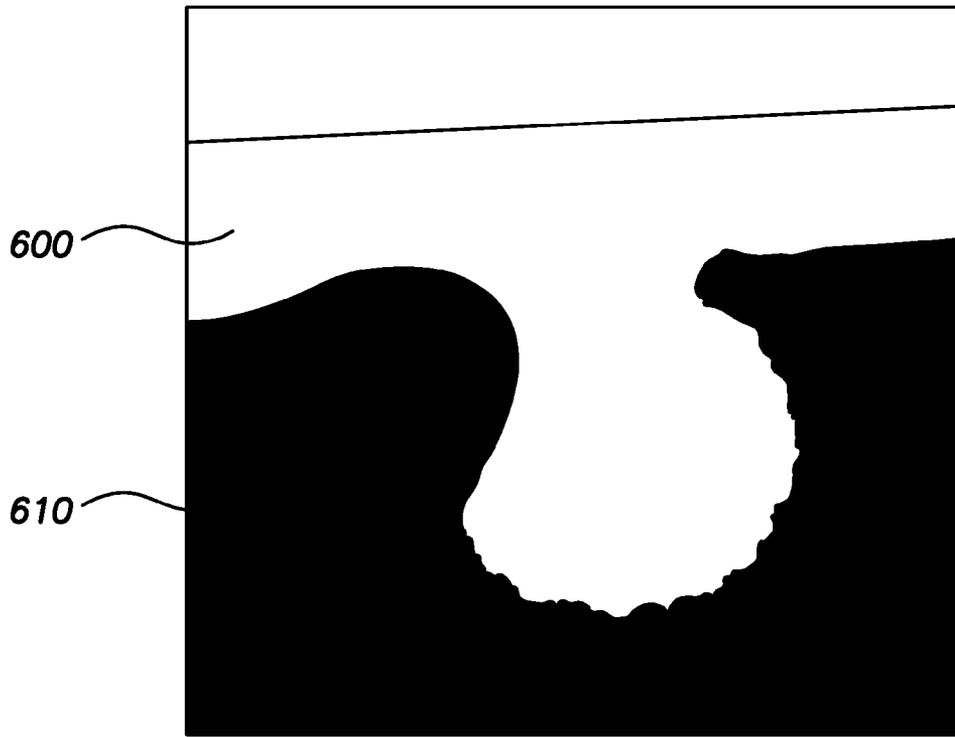


FIG. 12A

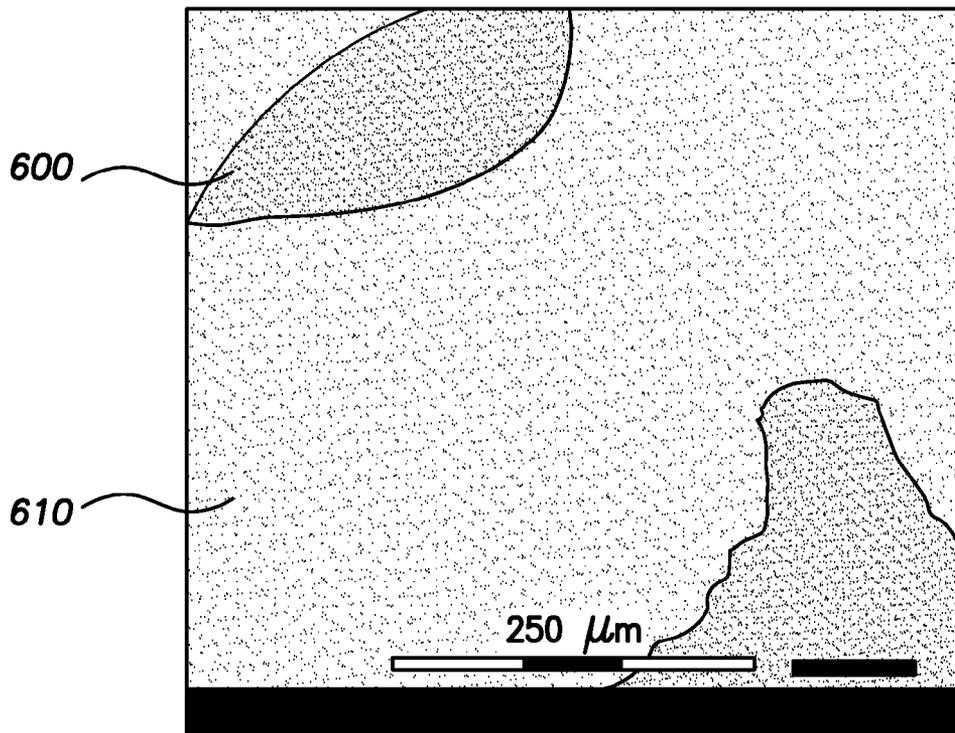


FIG. 12B

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## METHOD OF PRODUCING A PROXIMAL CONNECTOR END OF AN IMPLANTABLE LEAD

### BACKGROUND OF THE INVENTION

#### 1. Field of the Invention

The present invention generally relates to implantable leads, and in particular to proximal end portions for such implantable leads.

#### 2. Description of the Prior Art

Body implantable electrical leads form the electrical connection between an implantable medical device (IMD), such as cardiac pacemaker, cardiac defibrillator or cardioverter, and body tissue, such as the heart, which is to be electrically stimulated. As is well known, the leads connecting the IMD with the tissue may be used for pacing/defibrillation and for sensing electrical signals produced by the tissue.

The implantable leads of today are complex arrangements, generally including multiple different lead elements of different materials and therefore having different characteristics. In particular, connector arrangements or proximal end portions of implantable leads are complex arrangements, generally consisting of a multitude of different lead elements that have to be interconnected to form the final connector. This assembling process is complex and time-consuming having multiple separate sub-assembly steps.

### SUMMARY OF THE INVENTION

There is therefore a need for a lead manufacturing process that allows assembling of proximal lead end portions using few including elements and in few assembly steps. The present invention overcomes these and other drawbacks of the prior art arrangements.

It is a general object of the present invention to provide a lead connector comprising mechanically inter-connected connector elements of different materials.

It is another object of the invention to provide a connector arrangement that can be simply handled in the manufacture of lead connectors for implantable medical leads.

Briefly, the present invention involves a connector assembly of an implantable medical lead for providing a mechanical and electrical connection to an implantable medical device.

The connector assembly has a central connector pin made of a first conducting material, such as stainless steel. In a first embodiment adapted for active fixation implantable leads, at least a portion of the outer lateral pin surface is coated with a protective layer. A tubular insulator is concentrically provided around at least a portion of the coated pin. The insulator is made of an electrically insulating material, such as a ceramic. A connector ring made of a second conducting material, such as stainless steel, is concentrically provided around at least a portion of the outer lateral insulator surface. According to the present invention, spark plasma sintering is applied to the assembly for mechanically connecting the connector ring to the tubular insulator. The protective layer prevents the insulator from mechanically bonding to the connector pin. After removal of the protective layer, a spacing is formed between the outer pin surface and the inner insulator surface. As a consequence, the connector pin is rotatable relative to the mechanically inter-connected sub-assembly consisting of the insulator and the ring electrode. However, due to the design of the pin, i.e. having a waist surrounded by proximal and distal lead portions with comparatively larger diameters, the sub-assembly is longitudinally restricted relative to the connector pin by these proximal and distal pin portions.

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A connector assembly adapted for a passive fixation implantable lead does not have any protective coating on the pin surface. As a consequence, the tubular insulator becomes mechanically connected to both the connector pin and the connector ring.

The invention offers the following advantages:

Requires fewer lead components for manufacturing a lead connector assembly;

Allows reliable mechanical inter-connection of connector elements of different materials;

Simplifies the assembly process;

Provides a rigid connector design; and

Same connector elements and similar manufacturing process can be used for both passive and active fixation lead connectors.

Other advantages offered by the present invention will be appreciated upon reading of the below description of the embodiments of the invention.

### SHORT DESCRIPTION OF THE DRAWINGS

FIG. 1 is a side view of an implantable active fixation lead according to an embodiment of the present invention.

FIG. 2 is a side view of an implantable passive fixation lead according to an embodiment of the present invention.

FIG. 3 is a schematic overview of a subject having an implantable medical device connected to an implantable lead according to an embodiment of the present invention.

FIG. 4 is an axial cross section view of the proximal end portion of an implantable passive fixation medical lead according to an embodiment of the present invention.

FIG. 5 is an axial cross section view of the proximal end portion of an implantable passive fixation medical lead according to FIG. 4 equipped with an insulating seal.

FIG. 6 is an axial cross section view of the proximal end portion of an implantable active fixation medical lead according to an embodiment of the present invention.

FIG. 7 is an axial cross section view of the proximal end portion of an implantable active fixation medical lead according to FIG. 6, in which the protective coating has been removed.

FIG. 8 is an axial cross section view of the proximal end portion of an implantable active fixation medical lead according to FIG. 7 equipped with an insulating seal.

FIG. 9 is a flow diagram illustrating a method of producing a proximal end portion of an implantable passive fixation lead according to an embodiment of the present invention.

FIG. 10 is a flow diagram illustrating a method of producing a proximal end portion of an implantable active fixation lead according to an embodiment of the present invention.

FIG. 11 is a schematic block diagram of a spark plasma sintering apparatus that can be used according to the present invention.

FIGS. 12A and 12B are scanning electron microscope images of a Pt—Al<sub>2</sub>O<sub>3</sub> connection at 500× magnification (FIG. 12A) and 4000× magnification (FIG. 12B).

### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Throughout the drawings, the same reference characters will be used for corresponding or similar elements.

The present invention relates to implantable medical leads or catheters, and in particular to a connector arrangement in the proximal end of such leads. This connector arrangement of the invention is adapted for connection to different

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implantable medical devices (IMDs), such as pacemakers, cardioverters, defibrillators and other implantable electrical medical devices.

FIG. 1 is a schematic illustration of an implantable lead **100** according to an embodiment of the present invention. The lead **100** comprises a lead body **130** extending a long a central, longitudinal axis. The lead **100** has a proximal end **106** carrying a connector assembly **104** for electrically connecting the lead body **130** to an IMD. The lead **100** also has a distal end **102** comprising a header with electrodes **120**, **140** and fixation elements **110**. The lead **100** has non-limitedly been illustrated in the form of a so-called active fixation medical lead **100**, implying that the fixation element **110** is in the form of a helical, screw-in fixation element **110** adapted to be extended so as to project from the distal end of the header. The helical screw-in fixation element **110** is preferably active electrically so as to function as an electrode when implanted to stimulate selected tissue, such as cardiac tissue, and/or sense electrical activity of the tissue. Consistent with teachings well known in the art, one or more portions of such a helical electrode **110** may be electrically insulated along its length. The helical electrode **110** not only has a stimulating and/or sensing function but also serves to anchor or stabilize the distal lead portion **102** relative to the tissue.

The distal lead portion **102** also has a ring electrode **140** or indifferent electrode for electrically stimulating adjacent tissue and/or for sensing electrical activity of tissue. An optional tip electrode **120** may be provided at the most distal end **102** of the lead **100** as is well known in the art. The tip electrode **120** may optionally be made of a radiopaque material for facilitating monitoring implantation of the lead **100** into a patient body.

The connector assembly **104** at the proximal lead end **106** is adapted to electrically and mechanically couple the lead body **130** to the IMD. The assembly comprises terminal contacts in the form of a tubular, rotatable pin terminal contact **160**, often denoted connector pin **160**, and a ring terminal contact **150**, generally referred to as connector ring **150**. These two contacts **150**, **160** are positioned to engage corresponding electrical terminals within a receptacle in the IMD. In order to prevent ingress of body fluid into the IMD receptacle, the connector assembly may be provided with spaced-apart sets of seals **170**, **171**, well known in the art.

FIG. 2 is an illustration of another embodiment of a lead **200** to which the teachings of the present invention can be applied. This lead **200** is a so called passive fixation lead, where the helical screw-in fixation element has been replaced by, for instance a collar, fines or, as in the figure, tines **210** for anchoring the lead body **230** to a selected tissue.

The passive fixation lead **200** has a distal end **202** with an optional, preferably radiopaque, tip electrode **220** and a ring electrode **240**. The proximal lead end **206** has a connector assembly **204** according to the present invention with an electrically conducting connector pin **260** and connector ring **250**. These two terminals **250**, **260** are adapted for connection to matching electrical terminal in a receptacle of the IMD. The connector **204** preferably also comprises seal rings **270**, **271** for preventing body fluids from entering the IMD receptacle.

In clear contrast to the connector pin of the active fixation lead in FIG. 1, the connector pin **260** does not have to be rotatable relative the lead body **230** in this embodiment as no screwing fixation element is present.

FIG. 3 is a schematic overview of a subject **1** equipped with an IMD **300** connected to the subject's heart **10**. The IMD **300** is illustrated as a device that monitors and/or provides therapy to the heart **10** of the patient **1**, such as a pacemaker, defibril-

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lator or cardioverter. However, the present invention is not limited to cardiac-associated IMDs but may also be practiced with other implantable medical devices, such as drug pumps, neurological stimulators, physical signal recorders, oxygen sensors, or the like, as long as the IMD **300** is equipped with or is connected to at least one medical lead **100**, **200** according to the present invention.

The IMD **300** can wirelessly communicate with an external device **400**, non-limitedly illustrated as a programmer **400** in the figure. The external device **400** could alternatively be a physician's workstation, a home monitoring device or actually any data processing unit having capability of receiving data collected by the IMD **300** and preferably sending instructions and commands to the IMD **300**. The external device **400** is preferably connected to a display screen **410** allowing display of the collected diagnostic parameters and data.

The present invention provides a novel bonding technique used for mechanically connecting connector elements of different material to obtain a robust and reliable mechanical connection. Traditionally, a multitude of different connecting techniques have been used in the art, including snap-fit solutions, adhesions, welds, etc. These known connecting techniques have pros and cons. A general problem is that the assembly generally becomes time-consuming and complex, as an operator has to simultaneously handle multiple separate lead components that are to be inter-connected. Furthermore, the number of connecting techniques in the prior art of implantable lead assembly when connecting conducting metal-based lead elements with non-conducting non-metal elements has been rather limited. Generally, one may be limited to using different adhesions and like, making the assembly processes complex and time-consuming.

The present invention takes a radically different approach by utilizing spark plasma sintering for mechanically inter-connecting different connector elements to achieve a highly robust, reliable and corrosion- and strain-resisting connection. The spark plasma sintering technique has the further advantage in not being limited to be applied to metal and metal-based materials but can also be used for inter-connecting a conducting element, such as made of metal (alloy) material, to a non-conducting element, for instance made of a ceramic material.

FIG. 4 is a cross-sectional view of a proximal connector end **204** of a passive fixation implantable lead according to the present invention. The connector assembly **204** comprises a connector pin **260** made of a first conducting material. This material is selected from the group including metals, such as platinum, titanium, tantalum, iridium and niobium, and different alloys thereof, such as titanium alloys or platinum/iridium (Pt/Ir) alloys, including Pt/Ir 90/10 or Pt/Ir 80/20. Also other metal alloy materials can be used, including nickel-cobalt-chromium-molybdenum alloys, such as MP35N® (trademark of SPS Technologies, Inc.) or 35NLT® (trademark of Fort Wayne Metals Research Products Corp.), or iron-nickel-cobalt alloys, such as Kovar® (trademark of Carpenter Technology Corp.). Further suitable materials include stainless steel, preferably stainless steel of medical grade, such as medical grade 316L stainless steel.

The proximal end portion **262** of the connector pin **260** is adapted for electrical connection to a mating terminal at a receptacle of the IMD. The distal end portion **264** of the pin **260** is adapted for connection to an inner conductor coil that runs through the length of the lead body for connection with one of the electrodes (tip or ring electrode) at the lead header.

The connector pin **260** has a longitudinally running bore **266** through which a stylet or guide wire can be inserted

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through the bore **266** of the pin **260** and into a longitudinal passageway within the lead body for the purpose of delivering and steering the distal portion of the lead during implantation.

A tubular insulator **280** made of an insulating material is concentrically positioned around a portion **268** of the connector pin **260**. The insulator **280** is, in this embodiment of the invention, mechanically connected to the pin **260** by spark plasma sintering. Thus, an inner surface of the insulator **280** is at least partly connected to the lateral surface of a portion **268** of the connector pin **260**. The insulator **280** preferably covers an intermediate portion **268** of the pin lateral surface between the proximal end **262** for electrical connection to an IMD terminal and the distal end **264** for mechanical and electrical connection to the inner conductor coil. In a preferred embodiment, the covered pin portion **268** presents a smaller outer diameter as compared to the end portions **262**, **264**. As a consequence, tubular insulator **280** can be formed and connected to the pin **260** in a waist of the connector pin **260**.

The tubular insulator **280** is made of an insulating material that can be spark plasma sintered to the conducting material of the connector pin **260**. Preferred such insulating materials include ceramic materials, including alumina oxide ( $\text{Al}_2\text{O}_3$ ), zirconium dioxide ( $\text{ZrO}_2$ ) and potassium sodium niobate (KNN) ceramics ( $\text{K}_x\text{Na}_y\text{NbO}_3$ ). Other possible insulating materials include hydroxylapatite ( $\text{Ca}_5(\text{PO}_4)_3(\text{OH})$ ), magnesium oxide ( $\text{MgO}$ ) and silicon dioxide ( $\text{SiO}_2$ ). Also mixtures of any combination of at least two of the above-mentioned insulating materials can be used according to the invention.

The connector assembly **204** also comprises a connector ring **250** made of a second conducting material concentrically positioned around at least a portion **282** of the tubular insulator **280**. The connector ring **250** is adapted for electrical connection to an electrode terminal in the IMD receptacle. A distal end of the connector ring **250** is adapted for mechanical and electrical connection to an outer conductor coil that will run through the length of the lead body and end at the ring electrode or tip electrode in the lead header.

The connector ring **250** is mechanically connected to the tubular insulator **280** by spark plasma sintering to achieve a reliable and robust connection even though the two connector elements are made of different materials. The tubular insulator **280** electrically separates the two conducting elements **250**, **260** and therefore effectively functions as an insulator therebetween.

The connector ring **250** preferably only covers a sub-portion **282** of the lateral surface of the insulator **280**. As a consequence, a remaining portion **284** is bare and may be covered by a seal **270**, which is illustrated in FIG. 5. The seal **270**, which may be of silicone rubber, polyurethane, a Elast-Eon® polymer (trademark of Aor Tech International, a polymer of silicone with polyurethane), such as Elast-Eon® 2A, 2D, 3A, 3LH or HF, or like, is preferably attached to the surface of remaining insulator portion **284** and the proximal end surface **252** of the connector ring **250** utilizing a medical glue or adhesive.

The second conducting material of the connector ring **250** may be selected from the group including metals, such as platinum, titanium, tantalum, iridium and niobium, and different alloys thereof, such as titanium alloys or platinum/iridium (Pt/Ir) alloys, including Pt/Ir 90/10 or Pt/Ir 80/20. Also other metal alloy materials can be used including a nickel-cobalt-chromium-molybdenum alloy, such as MP35N® (trademark of SPS Technologies, Inc.) or 35N LT® (trademark of Fort Wayne Metals Research Products Corp.), or an iron-nickel-cobalt alloy, such as Kovar® (trademark of Carpenter Technology Corp.). Further suitable materials include stainless steel, preferably stainless steel of medical

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grade, such as medical grade 316L stainless steel. The ring **250** can advantageously be made of the same conducting material as the connector pin **260**.

In this embodiment, the connector ring **250**, tubular insulator **280** and connector pin **260** are mechanically interconnected by spark plasma sintering to form a connector assembly **204**. Thus, spark plasma sintering is used for connecting an outer surface of a portion **268** of the connector pin **260** to an inner surface of the insulator **280** and for connecting an outer surface of a portion **282** of the insulator **280** to an inner surface of the connector ring **250**. The connector assembly **204** can then be handled as a single unit during the remaining lead assembling process, which thereby significantly reduces the complexity and time of the lead manufacturing.

In the above-described connector embodiment all the connector elements are mechanically connected and thereby cannot be separately moved or rotated relative each other. Such connectors are useful for passive fixation leads in which there is no need for being able to extend or retract a helical screw-in fixation element at the distal lead end by manipulating the proximal lead end.

A connector assembly **104** useful in active fixation leads is illustrated in FIGS. 6 to 8. The connector **104** includes the connector pin **160** made of the first conducting material, preferably having a central bore or channel **166**. A proximal pin end **162** is adapted for connection to a terminal at the IMD receptacle with a distal pin end **164** is to be mechanically and electrically connected to the inner conductor coil of the lead, electrically inter-connecting the connector pin **160** to an electrode, typically the helix electrode, at the lead header.

A tubular insulator **180** made of an insulating material is concentrically provided around a portion **168** of the connector pin **160**. However, in clear contrast to the connector assembly illustrated in FIGS. 4 and 5, the insulator **180** does not become mechanically connected to the connector pin **160** during the spark plasma sintering process in this embodiment. The reason for this is that a protective layer **190** (see FIG. 6) is coated on the lateral surface of at least a portion **168** of the connector pin **160** before initiating the spark plasma process. The coating **190** is also applied to the end surfaces of the proximal pin **162** and the distal pin end **164** facing each other. Alternatively, the whole outside surface of the connector pin **160** is coated with the protective layer **190**. This protective layer **190** is then removed after the SPS-process to thereby create a gap **195** (see FIGS. 7 and 8) between the tubular insulator **180** and the pin **160**. The usage of such a protective layer **190** means that the inner diameter of the insulator **180** is slightly larger than the outer diameter of the insulated waist portion **168** of the connector pin **160**. As a consequence, the pin **160** is rotatable relative the insulator **180** thereby forming a bearing.

The proximal **162** and distal **164** pin portions having larger outer diameters than the intermediate insulated pin portion **168** prevents any significant longitudinal movement of the tubular insulator **180** relative the connector pin **160**. The insulator **180** is thereby longitudinally limited in the pin waist. The pin end portions **162**, **164** can therefore be regarded as radially protruding shoulders or flanges, which will limit any longitudinal movement of the insulator **180**.

The connector ring **150** made of the second conducting material is then concentrically positioned around at least a portion **182** of the tubular insulator **180**. The ring **150** is furthermore mechanically connected to the insulator **160** through spark plasma sintering. Thus, an inner surface of the connector ring **150** is mechanically connected to the lateral surface of at least a portion **182** of the insulator **180**. As the

connector ring **150** becomes attached and anchored to the insulator **180**, the connector pin **180** is also rotatable relative to the connector ring **150**.

A remaining non-covered surface **184** of the tubular insulator **180** is then preferably covered by one or more seals **170** as is illustrated in FIG. **8**.

FIG. **9** is a flow diagram illustrating a method of producing a proximal connector assembly of an implantable passive fixation lead according to the present invention. The method involves providing an at least partly fabricated connector pin made of a first conducting material in step **S1**.

According to the present invention "at least partly fabricated" means a sub-assembly that is either a completely fabricated connector element or at least a partly fabricated raw or start material that can be formed into a fabricated element. As a consequence, at least partly fabricated encompasses providing powder, grain, granule or granulate particles of the relevant material compacted to a shape from which the final shape of the element can be fabricated and formed to a continuous body by spark plasma sintering. At least partly fabricated also encompasses a finally fabricated element that is to be connected, such as by spark plasma sintering, to another element of the connector assembly. The expression also covers element bodies between these two extremes such as an continuous element body of the conducting (in the case of connector pin and connector ring) or non-conducting (in the case of tubular insulator) material that is connected, such as by spark plasma sintering, to another element of the connector assembly but having a shape different from the final shape of the element. In such a case, the element body can be further processed, such as turned, ground, etched, subjected to electrical discharge machining (EDM), milled, sawed, drawn, tumbled, swaged, forged, welded, following the connection to form the desired final shape and/or surface treatment.

Step **S1** can therefore involve, for instance, providing powder particles of the first conducting material and forming, in a sintering die, the particles to a desired shape. Alternatively, a fabricated connector pin body of the first material, such as illustrated in FIG. **4** or **5**, is provided in step **S1**. Furthermore, the step **S1** can involve provided a continuous body, such as a cylinder or tubular body, of the first conducting material, where the body has a shape different from the final shape of the connector pin.

A next step **S2** involves concentrically providing an at least partly fabricated tubular insulator made of a non-conducting material around at least a portion of the connector pin. This step **S2** can, in consistency with step **S1**, involve providing powder particles of the non-conducting material and compacting them to a desired shape. Alternatively, a fabricated tubular insulator having a shape as illustrated in FIG. **4** or **5**, but having a longitudinal opening allowing the connector pin to be inserted into the lumen of tubular insulator is provided in step **S2** or alternatively a continuous but not finally processed tubular insulator body.

Step **S3** concentrically provides an at least partly fabricated connector ring made of a second conducting material around at least a portion of the tubular insulator. The connector ring can be provided in the form of particles of the second material compacted around the body or the compacted powder of the tubular insulator. Alternatively, the connector ring can be a body having final shape or a partly fabricated continuous body in which the tubular insulator and the connector pin are threaded.

A next step **S4** involves mechanically connecting the tubular insulator to the connector pin and to the connector ring by spark plasma sintering. Furthermore, in the case any of the providing steps **S1** to **S3** involved providing material par-

articles, the spark plasma sintering operation performed in step **S4** also includes forming a continuous body of the material in addition to inter-connecting the connector assembly elements.

"Spark plasma sintering" or "SPS" is a sintering technique that applies, in addition to pressure, DC current/voltage pulses directly through a die containing a sample to be formed or samples to be inter-connected. The DC current pulses not only pass through the die but also through the actual sample(s) in the case of conductive samples. As a consequence, heat is generated internally through spark discharge between the particles occurring in the initial stage of the current-voltage pulse. The generation of spark impact pressure, Joule heat and the action of the electric field will result in efficient heating, plastic deformation promotion, high-speed diffusion and material transfer that give an opportunity to conduct low-temperature, short-time sintering of hard-to-sinter materials and bonding of dissimilar materials.

Spark plasma is formed initially of the sintering process and necks between the particles are created. After the initial process, surface, grain-body and volume-diffusion-processes and plastic flow contribute to densification while avoiding coarsening. SPS also facilitates a very high heating or cooling rate (several hundred ° K/minute), hence the sintering process is very fast. SPS is also sometimes denoted field assisted sintering technique (FAST) or pulsed electric current sintering (PECS) in the art.

Thus, the expression "spark plasma sintering" as used herein relates to a technique for forming bonds between conducting (metal (alloy)) and non-conducting (ceramic) material bodies through the application of pressure and DC current/voltage pulses through the die and the at least partly fabricated connector assembly elements of the invention.

FIG. **11** is a schematic a SPS device **500** that can be used according to the present invention. The device **500** has an upper punch electrode **510** connected to an upper punch **530**. A corresponding lower punch electrode **520** is connected to a lower punch **540**. The connector assembly elements **560** of the invention to be mechanically connected by SPS according to the present invention are provided in a sintering (graphite) die **550** between the two punches **530**, **540**. The sample **560** is enclosed together with the punches **530**, **540** and the die **550** into a vacuum chamber **590**. A DC pulse generator **580** is connected to the upper **510** and lower **530** punch electrode to thereby apply DC current/voltage pulses over the die **550** and through the electrode elements **560**. A sintering press **570** is arranged for controlling an exerted pressure applied by the punches **530**, **540** to the connector elements **560**.

FIG. **10** is a corresponding flow diagram illustrating a method of producing a proximal connector assembly of an implantable active fixation lead according to the present invention. The method starts in step **S10**, where an at least partly fabricated connector pin made of a first conducting material. This step **S10** corresponds to step **S1** of FIG. **9** and is not further described. A next step **S11** coats or covers at least a portion of an outer surface (lateral surface) of the connector pin with a protective layer. This protective layer is provided to prevent the formation of a mechanical bonding between the connector lead and the tubular insulator. The coating can be applied to only those portions of the connector pin that otherwise would come into contact with insulator material in the SPS process. Alternatively, the whole connector pin surface or at least a major portion thereof can be provided with a protective coating or layer.

There is a vast amount of materials that can be used as protective layer for preventing formation of the mechanical bonding. A first example is salt materials, such as sodium

chloride (NaCl) or potassium chloride (KCl). In such a case, a thin coating of the salt can be applied to at least a portion of the outer surface of the connector pin. The application can be in the form of immersing the connector pin in a (high concentration) saline solution and then evaporating away the solvent. Another possible non-salt, protecting material is graphite.

The main characteristic of this protecting material is that it should prevent the insulator from becoming mechanically attached to the connector pin during the SPS and that the shape of the protective layer should be preserved during the SPS process. Furthermore, the protecting material must be removable after the SPS process, without damaging the connector element materials. Any materials that fulfill these requirements can be used according to the invention.

An at least partly fabricated tubular insulator made of a non-conducting material is concentrically provided around at least a portion of the coated portion of the connector pin in step S12. The discussion in connection with step S2 of FIG. 9 applies mutatis mutandis to step S12. Step S13 involves concentrically providing an at least partly fabricated connector ring made of a second conducting material around at least a portion of the tubular insulator. This step S13 corresponds to step S3 of FIG. 9.

The tubular insulator is then mechanically connected to the connector ring by spark plasma sintering in step S14. In addition, if any of the connector elements were provided in the form of material particles, the spark plasma sintering also forms continuous material bodies having a defined (final or processable) shape. In clear contrast to the spark plasma sintering step S4 of FIG. 9, the tubular insulator and the connector pin do not become attached to each other in this step S14 due to the presence of the protective coating. The coating is removed in step S15 from the outer surface of the connector pin to form a spacing between the inner insulator surface and the outer pin surface.

The coating can be removed through different operations, depending on the particular coating material. If the coating consists of a salt layer, the connector assembly can be immersed into a solvent, in which the salt dissolves. Any remaining salt particles can be rinsed of with further solvent, such as water. For non-salt materials, non-aqueous solvents may be required including organic solvents, such as chloroform, alcohols, etc.

Another possible operation can to oxidize away the protective layer together with (mild) heating. For example, a graphite layer can be removed through oxidization at about 400-500° C.

In either case, the coating particle will escape through the (thin) spacings between the short ends of the tubular insulator and the proximal and distal pin portions, respectively.

In an implementation of the invention, the connector pin is provided in the form of a continuous body of the first conducting material, where the body can have the final shape of the connector pin or a more crude shape from which the final shape can be obtained by further processing. The connector pin material can be made of any of the previously mentioned material examples, such as stainless steel of medical grade.

The tubular insulator is preferably provided in the form of non-conducting material particles that are deposited and compacted around a portion of the connector pin. The particles can, for instance, be in the form of spark plasma sinterable ceramic grain/powder/granule/granulate particles, such as Al<sub>2</sub>O<sub>3</sub> particles.

The connector ring can then be in the form of a partly fabricated or finally fabricated body of the second conducting material or in the form of conducting material particles that

are deposited and compacted around a portion of the tubular insulator. The body or particles are preferably made of the same material as the connector pin, such as stainless steel of medical grade.

In another implementation, also the connector pin is provided in the form of conducting material particles that are deposited and compacted in the sintering die in the form of cylinder, preferably hollow cylinder, or more closely to the final pin shape.

A further implementation uses the three connector elements in the form of continuous bodies of the respective materials.

A test body made of a suitable conducting material of the connector pin and/or connector ring, i.e. platinum, and a preferred non-conducting material of the tubular insulator, i.e. Al<sub>2</sub>O<sub>3</sub>, have been spark plasma sintered at a temperature of 1175° C. for 5 minute. The test bodies had a diameter of 10 mm and a height of 3 mm and were sintered from Al<sub>2</sub>O<sub>3</sub> and platinum powder. FIGS. 12A and 12B are scanning electron microscope images of the joint between the platinum material 610 and the Al<sub>2</sub>O<sub>3</sub> material 600 at 500× magnification (FIG. 12A) and 4000× magnification (FIG. 12B). As can be seen from the drawings, spark plasma sintering can be used for providing a seamless connection between the two different materials 600, 610 without the formation of any cracks or voids in the joint.

The SPS procedure of the present invention results in a diffusion-based joint between the materials. In a small transition zone around the joint, particles of the materials become inter-mixed to form the diffusion-based, seamless joint.

As is well known in the art, the temperature of the SPS process is dependent on, among others, the particular materials to be sintered and the thickness of the materials or the size of the material particles. Briefly, the sintering temperature should be below the lowest melting point of the materials to be sintered. Furthermore, the smaller the diameter of the material particles, generally the lower sintering temperature can be used. Care must also be taken for materials that are subject to phase transitions so that not an unaccepted, from mechanical and/or electrical properties point of view, is formed in the SPS process. The pressure that is applied during the SPS process is also material dependent and depends on the size of the sintered materials. Generally, the pressure per surface area is rather constant for a given material.

Examples of suitable sintering temperature for some of the materials useful according to the invention include ~1100° C. for Al<sub>2</sub>O<sub>3</sub>, 1000-1100° C. for ZrO<sub>2</sub>, 700-500° C. for SiO<sub>2</sub> and hydroxylapatite, <1100° C. for steel.

The optimal SPS sintering parameters can be determined by the person skilled in the art through routine tests and table look-ups regarding the particular material combinations. The above described parameter settings can be used as starting points in such an optimization process.

It will be understood by a person skilled in the art that various modifications and changes may be made to the present invention without departure from the scope thereof, which is defined by the appended claims.

What is claimed is:

1. A proximal connector end of an implantable lead comprising:

- a connector pin made of a first conducting material;
- a tubular insulator made of an electrically insulating material concentrically positioned around at least a portion of the connector pin;
- a protective layer coating a surface of the connector pin such that the protective layer is disposed between the connector pin and the tubular insulator; and

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a connector ring made of a second conducting material concentrically positioned around at least a portion of the tubular insulator;

wherein the connector pin, tubular insulator, and connector ring are at least partly connected by spark plasma sintering, wherein the protective layer prevents formation of a mechanical bonding between the connector pin and the tubular insulator, and wherein the protective layer is removed after the spark plasma sintering to create a gap between the tubular insulator and the connector pin to allow rotation of the connector pin relative to the tubular insulator.

2. The proximal connector end according to claim 1, wherein the tubular insulator and the connector ring are collectively rotatable relative to the connector pin.

3. The proximal connector end according to claim 2, wherein the at least a portion of the connector pin constitutes a pin waist flanked by a proximal pin portion and a distal pin

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portion restricting longitudinal movement of the tubular insulator and the connector ring relative to the connector pin.

4. The proximal connector end according to claim 1, wherein the tubular insulator is connected to the connector pin at least partly by spark plasma sintering.

5. The proximal connector end according to claim 1, wherein the first conducting material is stainless steel.

6. The proximal connector end according to claim 1, wherein the second conducting material is stainless steel.

7. The proximal connector end according to claim 1, wherein the insulating material is a ceramic material.

8. The proximal connector end according to claim 1, wherein the protective layer is a salt material.

9. The proximal connector end according to claim 8, wherein the salt material is sodium chloride (NaCl).

10. The proximal connector end according to claim 8, wherein the salt material is potassium chloride (KCl).

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