

(12) UK Patent Application (19) GB (11) 2 290 000 (13) A

(43) Date of A Publication 06.12.1995

(21) Application No 9510539.1

(22) Date of Filing 24.05.1995

(30) Priority Data

(31) 9410985 (32) 01.06.1994 (33) GB

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(72) and (74) continued overleaf

(51) INT CL⁶

G01S 7/03

(52) UK CL (Edition N)

H4D DRPN DSH D354 D356 D362 D393

H1Q QHX

U1S S1820

(56) Documents Cited

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cont. Short Range FMCW Radar Design & Abstract

volume page 67

(58) Field of Search

UK CL (Edition N) H1Q QHX , H1W WCAX WCX , H4D

DRPA DRPB DRPC DRPN DRPP DRPQ DSH DSX

INT CL⁶ G01S

Online: WPI

(54) Radar transmitter/receivers

(57) A FMCW radar transmitter/receiver arrangement for use, for example, in automotive vehicle cruise control, in which R.F. energy from a frequency modulated oscillator 2 is applied to an antenna for transmission and to one input of a mixer 3 by way of a rat-race device, 5 and RF energy reflected from a target and received at the antenna is applied to another input of the mixer by way of the rat-race device. The rat-race device constitutes a ring of microstrip transmission line $3\lambda/2$ long, with four ports spaced $\lambda/4$, $\lambda/4$, $\lambda/4$, and $3\lambda/4$ apart. The mixer 3 constitutes a second rat-race device 4 and mixer diodes 5, 6.

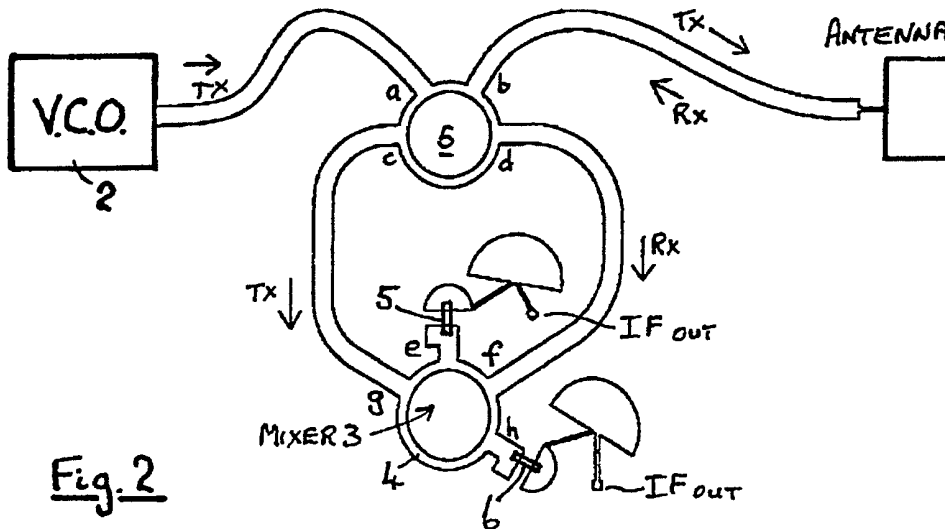


Fig. 2

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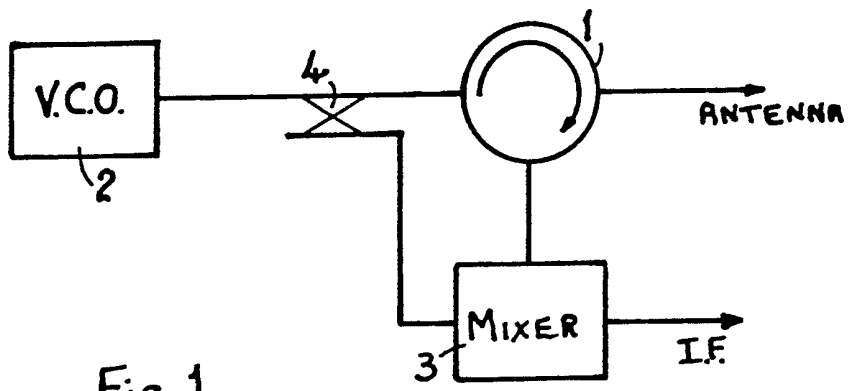


Fig. 1

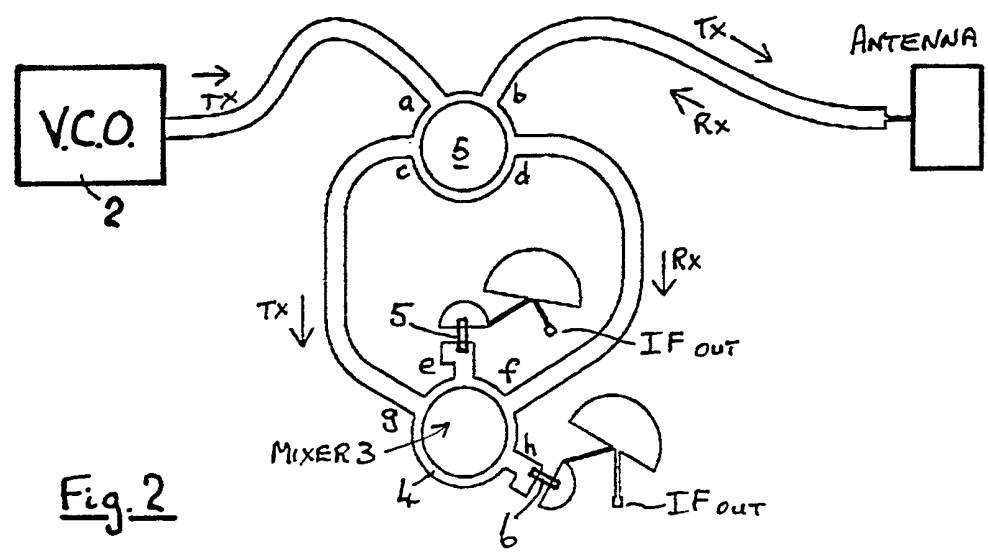


Fig. 2

Radar transmitter/receivers

The present invention relates to radar transmitter/receivers for use for example in automotive vehicles.

5 Various types of distance measuring sensor are presently being considered for use in automotive safety programmes, the principle application being referred to as Autonomous Intelligent Cruise Control (AICC).

A vehicle equipped with conventional cruise control can be made to hold a road speed pre-selected by the driver until the brake pedal is operated, whereupon the vehicle
10 reverts to normal operation. AICC enables a conventional vehicle cruise control function to be extended whereby the braking and throttle functions of cruise control operate without driver intervention. This function is achieved by the sensor on the AICC vehicle being able to determine the distance, lateral position across the carriageway and relative speed of nearby vehicles. Thus, a vehicle operating in
15 autonomous cruise control mode can be automatically brought to a standstill if an object is detected in the path of the vehicle. The pre-selected cruise speed may be resumed once the object is no longer in the path of the AICC vehicle, giving the vehicle autonomous control in stop-go traffic.

One type of radar that is particularly suited to this application is frequency
20 modulated continuous wave (FMCW), primarily because of its simplicity, potential low cost, and relative ease of subsequent signal processing.

In such a radar, a voltage controlled oscillator (VCO) is arranged to generate R.F. energy at nominally 76.5 GHz, which frequency may be varied over a range by applying a voltage ramp of known duration, giving a known frequency ramp rate. If this RF

energy is then transmitted via an antenna to a reflective target, during the time taken for the energy to reach the target and return to the antenna the frequency of the VCO will have changed, and by mixing the reflected signal with the newly generated oscillator frequency used as the local oscillator (L.O.) drive to the mixer the distance-to-target can
5 be calculated from the difference frequency.

In principle there may be two antennae, one for transmit and one for receive. In practice a single antenna is desirable to minimise size and cost, particularly for automotive use. In order to implement an FMCW radar in a single antenna (monostatic) form, it is normally the case that the transmit and receive functions are combined in at
10 the antenna by means of a microwave circulator.

According to one aspect of the present invention in a radar transmitter/receiver arrangement output signals from an electric oscillator are arranged to be applied to an antenna and to a mixer, and signals received at said antenna are arranged to be applied to said mixer, by way of a dual rat-race device.

15 The rat-race device may comprise first, second, third and fourth ports spaced around a ring transmission path having a circumference of substantially one and a half wavelengths at the frequency of operation of the electric oscillator, the spacings between the first and second ports, the second and third ports and the third and fourth ports each being substantially one quarter of a wavelength and the spacing between the fourth and
20 first ports being substantially three quarters of a wavelength at said frequency of operation. The second and third ports may be coupled to said electric oscillator and to said antenna respectively and said first and fourth ports may be coupled to respective inputs of said mixer.

A radar transmitter/receiver arrangement in accordance with the present invention

will now be described by way of example with reference to the accompanying drawing, of which:-

Figure 1 shows schematically a known form of transmitter/receiver arrangement, and

5 Figure 2 shows a transmitter/receiver arrangement in accordance with the present invention.

Referring first to Figure 1, a circulator 1 ideally permits propagation of RF energy from an oscillator 2 only in the direction of the arrow, such that all the RF energy reaching the circulator 1 is transmitted from the antenna port. Similarly, RF energy
10 reflected from a target and received by the antenna (not shown) will propagate only into a mixer 3. RF energy to act as the local oscillator signal for the mixer 3 is derived from the oscillator 2 by way of a directional coupler 4. As well as providing the local oscillator drive for the mixer 3, the coupler 4 also introduces losses and thereby degrades the transmit performance.

15 Imperfections in the circulator 1 occur in two areas, insertion loss and isolation. Imperfect isolation means that a proportion of the transmit power (typically -20dB) enters the mixer receive port and a proportion of the reflected signal returns to the oscillator 2. Imperfect insertion loss means that approximately 0.8dB loss occurs both during transmission to the antenna, and reception from the antenna. These factors
20 degrade performance of a circulator based FMCW radar.

For automotive applications at millimetric frequencies, it is unlikely that this technique could be implemented in a sufficiently low cost manner.

The dual rat-race arrangement illustrated in Figure 2 also facilitates transmission and reception via a single antenna, but in a cost effective manner.

The expensive circulator 1 is replaced by a 3dB hybrid coupler or rat-race coupler 5, yet achieves the same functions. The hybrid coupler 5 can be realised on appropriate low cost microstrip media using photolithographic techniques, so that no additional cost is incurred over that of defining the main microstrip circuit.

5 The length of microstrip transmission line between each of the four ports is:

port a to port b: $\lambda/4$

port b to port d: $\lambda/4$

port d to port c: $3\lambda/4$

port c to port a: $\lambda/4$

10 where λ is the wavelength at -76.5GHz

For an input at port a, power will propagate along the transmission line both clockwise and anti-clockwise. The two components of power arriving at port d will be in anti-phase and so in a perfect rat-race coupler, there will be no output power from port d. The two components of power arriving at port b and port c will be in phase so the power will be split equally into each port. Thus 50% of the oscillator power arrives at port c to provide L.O. drive to the mixer, and 50% is passed to the antenna through port b.

During reception, for a received signal arriving at port b from the antenna, there will be no output from c. The power will split equally into ports d and a. The power emerging from port a is considered to be wasted as it will only be down- converted if it reaches port d, this loss manifesting itself as increased conversion loss. Nevertheless, because both the circulator 1 and L.O. coupler 4, together with their associated insertion loss, are eliminated in this design, the overall performance of the two FMCW radars has been found to be comparable.

Transmitter power from the port c and received signal power from the port d are passed to respective ports g and f of a second rat-race coupler 4 which splits the incoming signal power at each port g and f 50 : 50 between mixer diodes 5 and 6, the transmitter power being applied in opposite phase and the received power being applied in the same phase to the two diodes.

The dual rat-race solution offers identical functionality to the circulator solution, yet it can be realised for a much lower cost than the conventional circulator. Comparative measured performance is summarised below:

	<u>Circulator</u>	<u>Dual rat-race</u>
10 <u>Transmission Loss</u>	6 dB	6 - 7 dB
<u>Conversion Loss</u>	9 dB	12 dB

It will be appreciated that compared to the simple conductor pattern of the microstrip rat-race, the previously proposed circulator arrangement requires an accurately machined hole or recess for a ferrite insert in the substrate on which the transmitter-receiver circuit is to be formed, the ferrite insert itself has to be accurately machined, and the electrical conductors of the circulator have to be accurately positioned with respect to the ferrite insert. These factors tend to slow the production rate and to cause higher reject rates than with the simple photolithographic processes for forming microstrip patterns.

At an operating frequency of 76.5 GHz a microstrip rat-race formed on a 125 micrometre thick quartz substrate, for example, may have a mean diameter of the order of 1mm and be formed with conductors of the order of 0.2mm wide. These dimensions

would of course differ for other substrate materials, depending on the dielectric constant of the material.

CLAIMS

1. A radar transmitter/receiver arrangement wherein output signals from an electric oscillator are arranged to be applied to an antenna and to a mixer, and signals received at said antenna are arranged to be applied to said mixer, by way of a dual
5 rat-race device.
2. A radar transmitter/receiver arrangement in accordance with Claim 1 wherein the rat-race device comprises a first ring transmission path having first, second, third and fourth ports spaced around its circumference.
3. A radar transmitter/receiver arrangement in accordance with Claim 2 wherein the
10 first ring transmission path has a circumference of substantially one and a half wavelengths at the frequency of operation of said electric oscillator, the spacings between the first and second ports, the second and third ports and the third and fourth ports each being substantially one quarter of a wavelength and the spacing between the fourth and first ports being substantially three quarters of a wavelength at said frequency
15 of operation.
4. A radar transmitter/receiver arrangement in accordance with Claim 3 wherein the second and third ports are arranged to be coupled to said electric oscillator and to said antenna respectively, and said first and fourth ports are arranged to be coupled to respective inputs of said mixer.
- 20 5. A radar transmitter/receiver arrangement in accordance with Claim 2, Claim 3 or Claim 4 wherein the first and fourth ports of the first ring transmission path are coupled to respective inputs of said mixer by way of a second ring transmission path having respective first, second, third and fourth ports.
6. A radar transmitter/receiver arrangement in accordance with Claim 5 wherein the

first and fourth ports of said first ring transmission path are coupled to the first and third ports of said second ring transmission path, the second and fourth ports of said second ring transmission path being coupled to respective mixer diodes.

7. A radar transmitter/receiver arrangement substantially as hereinbefore described
- 5 with reference to Figure 2 of the accompanying drawing.



Application No: GB 9510539.1
Claims searched: all

Examiner: E P Plummer
Date of search: 10 August 1995

Patents Act 1977
Search Report under Section 17

Databases searched:

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:
UK Cl (Ed.N): H4D(DSH,DSX,DRPN,DRPP,DRPQ,DRPA,DRPB,DRPC); H1Q(QHX); H1W(WCX,WCAX)
Int Cl (Ed.6): G01S
Other: Online:- WPI

Documents considered to be relevant:

Table with 3 columns: Category, Identity of document and relevant passage, Relevant to claims. Rows include GB2147150A, GB1605254, GB1448266, WO95/04943A1, US4492960, US4377005, US3870960, Radar 92 (IEE Conference Publication No. 365) pp. 288-291: J Kehrbeck et al: A Novel and Inexpensive Short Range FMCW Radar Design.

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