



(19) **United States**

(12) **Patent Application Publication**
Garcia et al.

(10) **Pub. No.: US 2008/0215060 A1**

(43) **Pub. Date: Sep. 4, 2008**

(54) **FASTENER INSERTION METHOD**

Publication Classification

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(51) **Int. Cl.**
A61B 17/58 (2006.01)
A61B 17/16 (2006.01)
(52) **U.S. Cl.** **606/104; 606/80**

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(57) **ABSTRACT**

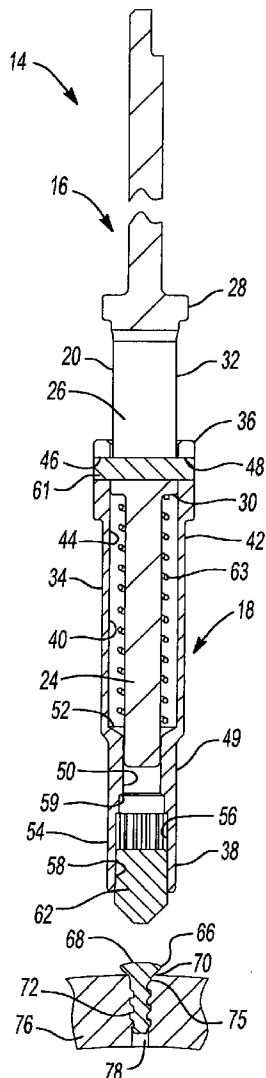
A method may include rotating a threaded fastener at a first rotational speed to provide a kinetic energy force component for the fastener based on the first rotational speed and driving the fastener into a structure based on the rotating. The structure may provide a torsional resistance during the driving greater than a torsional strength of the fastener. The driving may provide a torque force component applied to the fastener. The driving may cut threads into the structure with the fastener. The driving may apply a total force to the structure from the fastener including the kinetic energy force component and the torque force component. The total force applied by the fastener may be greater than or equal to a force required for the cutting. The torque force component may be less than a torsional strength of the fastener.

(21) Appl. No.: **12/040,310**

(22) Filed: **Feb. 29, 2008**

Related U.S. Application Data

(60) Provisional application No. 60/904,678, filed on Mar. 2, 2007, provisional application No. 60/905,157, filed on Mar. 6, 2007.



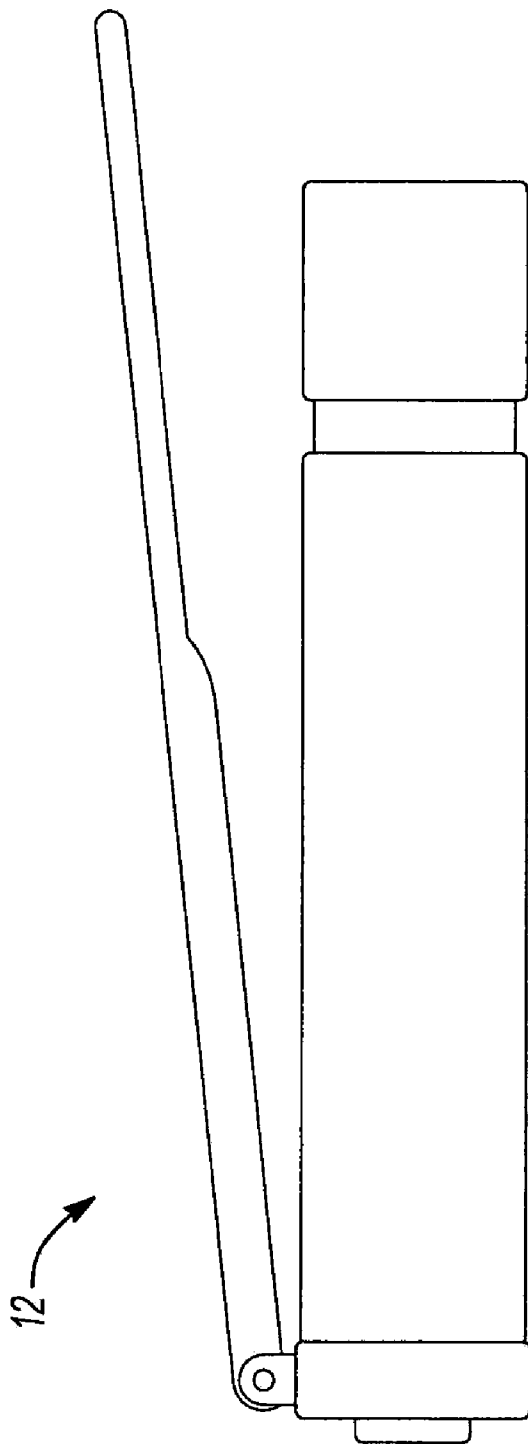
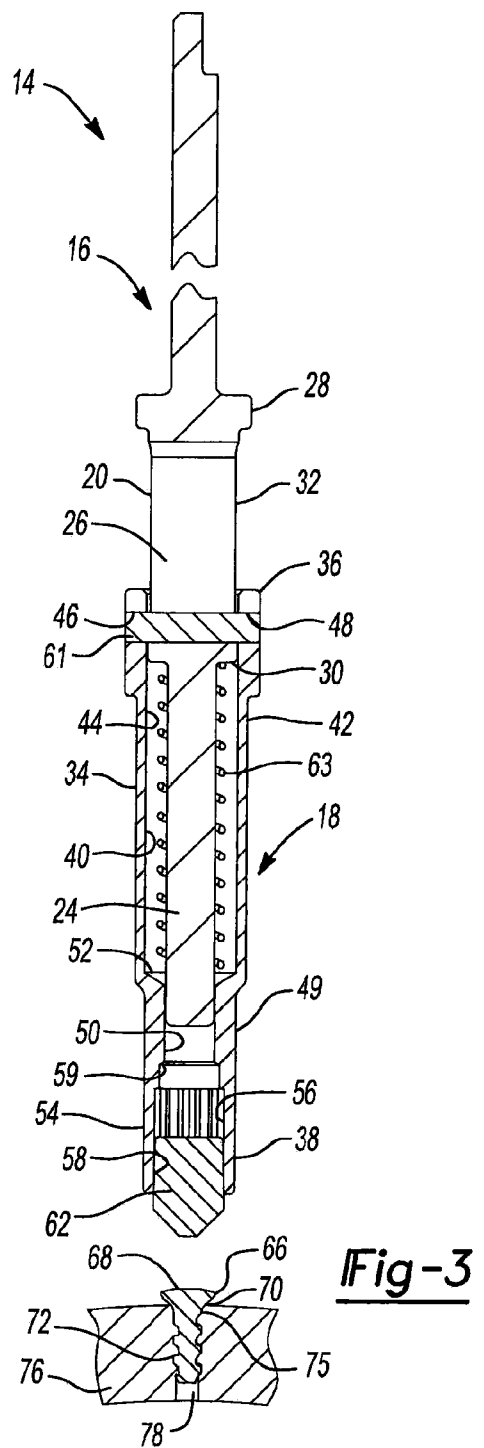
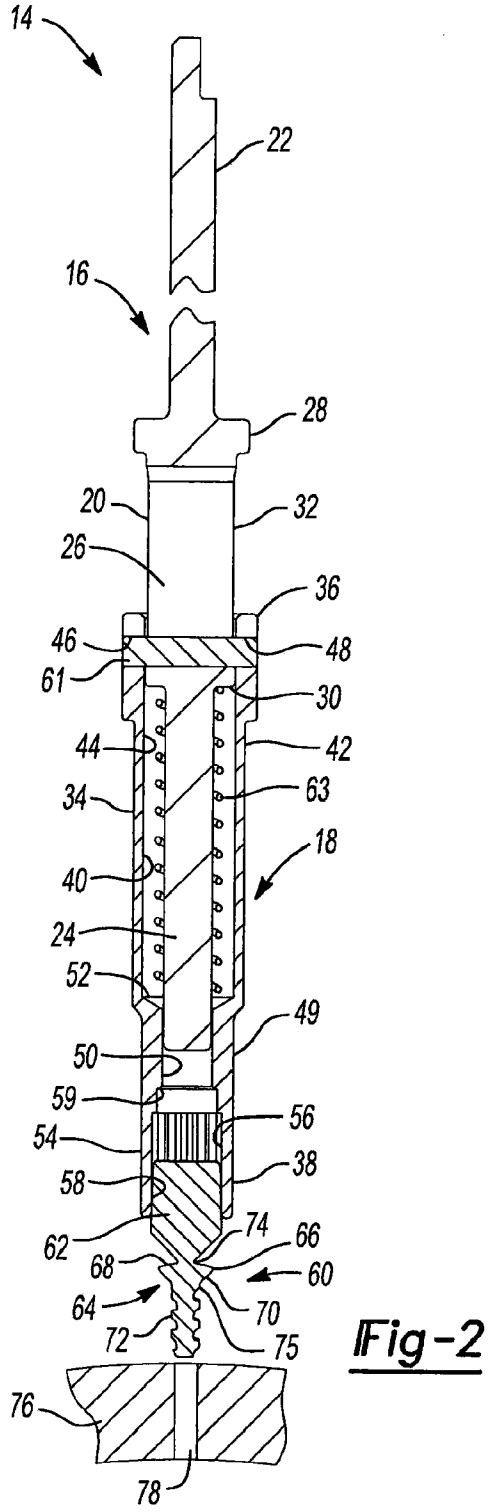


Fig-1



FASTENER INSERTION METHOD

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application claims the benefit of U.S. Provisional Application No. 60/904,678, filed on Mar. 2, 2007 and U.S. Provisional Application No. 60/905,157, filed on Mar. 6, 2007. The disclosures of the above applications are incorporated herein by reference.

FIELD

[0002] The present disclosure relates to threaded fasteners, and more specifically to insertion methods for threaded fasteners.

BACKGROUND

[0003] The statements in this section merely provide background information related to the present disclosure and may not constitute prior art.

[0004] Typical fastener insertion techniques may include applying a torque to a threaded fastener to rotationally drive the fastener into a structure. The torsional strength of the fastener is typically greater than the torque applied to drive the fastener to prevent breaking of the fastener before insertion is completed. The torque applied to the fastener increases when a self-tapping fastener is used due to the additional force required to cut threads into the structure.

SUMMARY

[0005] A method may include rotating a threaded fastener at a first rotational speed to provide a kinetic energy force component for the fastener based on the first rotational speed and driving the fastener into a structure based on the rotating. The structure may be providing a torsional resistance during the driving greater than a torsional strength of the fastener. The driving may provide a torque force component applied to the fastener. The driving may cut threads into the structure with the fastener. The driving may apply a total force to the structure from the fastener including the kinetic energy force component and the torque force component. The total force applied by the fastener may be greater than or equal to a force required for the cutting. The torque force component may be less than the torsional strength of the fastener.

[0006] The method may further include terminating the driving when the fastening portion is inserted a predetermined amount into the structure.

[0007] An apparatus according to the present disclosure may include a threaded fastener having a torsional strength and a driver engaged with the fastener. The driver may be adapted to drive the fastener at a first rotational speed into a structure and apply a torque force component to said fastener. The fastener may be adapted to have a kinetic energy force component based on the first rotational speed and to apply a total force to the structure including the torque force component and the kinetic energy force component. The fastener may cut threads into the structure based on the total force. The total force may be greater than or equal to a force required to cut the threads and the torque force component may be less than the torsional strength of the fastener.

[0008] Further areas of applicability will become apparent from the description provided herein. It should be understood that the description and specific examples are intended for

purposes of illustration only and are not intended to limit the scope of the present disclosure.

DRAWINGS

[0009] The drawings described herein are for illustration purposes only and are not intended to limit the scope of the present disclosure in any way.

[0010] FIG. 1 is a perspective view of a powered driver according to the present disclosure;

[0011] FIG. 2 is a translucent plan view of an adapter assembly and fastener according to the present disclosure; and

[0012] FIG. 3 is an additional translucent plan view of the adapter assembly and fastener of FIG. 2.

DETAILED DESCRIPTION

[0013] The following description is merely exemplary in nature and is not intended to limit the present disclosure, application, or uses.

[0014] With reference to FIGS. 1-3, a driving assembly for a fastener may include a powered driver 12 and an adapter assembly 14. Powered driver 12 may be any driver capable of driving adapter assembly 14 in the manner discussed below. Powered driver 12 shown in FIG. 1 is a powered driver from MicroAire Surgical Instruments L.L.C. of Charlottesville, Va. Adapter assembly 14 may be engaged with and driven by powered driver 12.

[0015] More specifically, adapter assembly 14 may include a plunger 16 and a driving member 18. Plunger 16 may include a central body portion 20, a connection shank 22, and an ejector shaft 24. Central body portion 20 may include a generally cylindrical body 26 having first and second ends 28, 30. An elongate passage 32 may extend radially through cylindrical body 26 and may have an axial extent along cylindrical body 26. Connection shank 22 may extend axially from first end 28 of cylindrical body 26 and may engage powered driver 12 for driving adapter assembly 14. Ejector shaft 24 may be generally cylindrical or may be in the form of a drill bit for drilling a pilot hole, as discussed below, and may extend axially from second end 30 of cylindrical body 26 and may be slidably disposed within driving member 18, as discussed below.

[0016] Driving member 18 may include an elongate body 34 having first and second ends 36, 38. A central opening 40 may extend axially through elongate body 34 and first and second ends 36, 38. A first portion 42 of elongate body 34 may include a first portion 44 of central opening 40 passing therethrough. First portion 44 of central opening 40 may extend through first end 36 and may have a first diameter greater than the diameter of a central portion of cylindrical body 26 and second end 30 thereof and less than the diameter of first end 28 of cylindrical body 26. A set of apertures 46, 48 may extend radially through first portion 42 of driving member 18 near first end 36.

[0017] A second portion 49 of elongate body 34 may include a second portion 50 of central opening 40 passing therethrough. Second portion 50 of central opening 40 may have a second diameter that is less than the first diameter of first portion 44, forming a step 52 therebetween. The second diameter of second portion 50 may be greater than the diameter of ejector shaft 24 and less than the diameter of cylindrical body 26 of plunger 16.

[0018] A third portion **54** of elongate body **34** may include a driving geometry. More specifically, third portion **54** may include a third portion **56** of central opening **40** extending therethrough. Third portion **56** may extend through second end **38** of driving member **18** and may define a series of flats **58** or some other form of driving geometry on an inner wall of third portion **56**. Third portion **56** of central opening **40** may have a third diameter that is greater than the second diameter of second portion **50**, forming a step **59** therebetween.

[0019] Cylindrical body **26** may be disposed in first portion **44** of central opening **40** and a pin **61** may pass through apertures **46, 48** in driving member **18** and elongate passage **32** in plunger **16**, slidably coupling plunger **16** to driving member **18**. Ejector shaft **24** may extend into first and second portions **44, 50** of central opening **40** when plunger **16** is in a retracted position (seen in FIGS. **2** and **3**) and a may be extended into third portion **56** of central opening **40** to abut and/or eject a fastener **60**, as discussed below. A spring **63** may be engaged with step **52** and second end **30** of cylindrical body **26**, urging plunger **16** into the retracted position.

[0020] Fastener **60** may be disposed within third portion **56** of central opening **40**. Fastener **60** may include a torque limiting feature, such as first and second portions that are removable from one another when a predetermined torque limit is exceeded. For example, the first portion may include a breakaway portion **62** and the second portion may include a fastening portion **64**. Breakaway portion **62** may be coupled to fastening portion **64** and may include a series of flats engaged with flats **58** within third portion **56** of central opening **40**, providing for driving of fastener **60** by the driving assembly. Breakaway portion **62** may be retained within third portion **56** of central opening **40** through an interference fit engagement therewith. Fastening portion **64** may include a head **66** having upper and lower portions **68, 70** and a threaded shank **72**. Breakaway portion **62** may be integrally formed with and coupled to upper portion **68** of head **66** at a reduced diameter breakaway region **74** and threaded shank **72** may extend from lower portion **70**. A series of recesses (not shown) may be formed in a perimeter of head **66**.

[0021] Fastener **60** may be formed from a variety of materials including, but not limited to metals (including titanium, titanium alloys, stainless steel, zirconium, and CoCr), bio-compatible non-resorbable materials (including polyetheretherketone (PEEK) and polyetherketoneketone (PEKK)), biocompatible resorbable materials, ceramics, composite materials, allograft or xenograft (including demineralized bone matrix and coral), or combinations thereof.

[0022] The fasteners and fastener insertion method discussed below may include a variety of applications such as to craniofacial procedures, neurosurgical procedures, spinal procedures, orthopedic procedures, suture anchors (Glencord anchors), small bone fixation/anchors, anterior cruciate ligament (ACL) fixation devices (tendon repair devices), and soft tissue anchors. Further, while discussed with respect to powered driver **12**, adapter assembly **14**, and fastener **60**, it is understood that a variety of alternate driving assemblies and fasteners may be used as well.

[0023] As seen in FIGS. **2** and **3**, fastener **60** may be fixed to another structure **76** such as bone, wood, or some other media. A pilot hole **78** may be drilled into structure **76** and fastener **60** may be inserted into pilot hole **78**. More specifically, fastener **60** may cut threads into pilot hole **78**. Fastener **60** may therefore act as a self tapping screw. In order to insert

a self-tapping screw, work is performed on the screw. Work is generally defined as a force imparted over a distance:

$$\text{Work} = F_i \times D;$$

where F_i is force and D is distance.

[0024] In the context of the present disclosure, the force (F_i) noted above in the work definition may generally include a sum of the force (F_c) needed to cut (or tap) threads and the force of friction (F_f) from the threads on structure **76**. The driving assembly may apply the force (F_i) to fastener **60** in order to insert fastener **60** into pilot hole **78**. The force (F_s) applied by fastener **60** may generally include the sum of the force (F_t) from the torque imparted on fastener **60** and the force (F_k) from the kinetic energy of fastener **60**. Therefore, in order to insert fastener **60** into structure **76**, force (F_s) should be greater than force (F_i). When fastener **60** is inserted at low rotational speeds, the kinetic energy force component (F_k) may be small relative to the torque force component (F_t).

[0025] Kinetic energy is generally defined as:

$$K = \frac{1}{2} I \omega^2;$$

where K is kinetic energy, I is moment of inertia, and ω is angular rotational velocity. Angular rotational velocity is directly proportional to rotational speed. Therefore, the kinetic energy force component (F_k) may be directly proportional to the square of the rotational speed that fastener **60** is being driven at. As rotational speed of fastener **60** increases, the torque force component (F_t) needed to drive fastener **60** into structure **76** may be reduced. More specifically, fastener **60** may be driven at a rotational speed that reduces the torque force component (F_t) required to drive fastener **60** into structure **76** below the torsional strength of fastener **60**. As such, fastener **60** may cut threads into structure **76**, even where structure **76** has a torsional resistance that is greater than the torsional strength of fastener **60**.

[0026] However, once fastener **60** is fully inserted into structure **76** and head **66** abuts structure **76**, the force (F_i) required to further insert fastener **60** into structure **76** may be increased by the force of friction (F_f) from head **66** on structure **76**. In order to maintain rotation of fastener **60**, force (F_s) must be increased. If the rotational speed that fastener **60** is being driven at remains constant, the torque force component (F_t) increases. Once the torque force component (F_t) exceeds the torsional strength of breakaway region **74**, breakaway portion **62** may be separated from fastening portion **64**. Alternatively, some other torque limiting feature of fastener **60** or the driving assembly may prevent further transmission of driving torque to fastening portion **64**.

[0027] However, the force (F_s) applied to drive fastener **60** may be limited such that it is greater than the sum of the force (F_c) needed to cut (or tap) threads and the force of friction (F_f) from the threads on structure **76**, but less than a strip-out force (F_{so}), ($F_s > F_c + F_f$). Strip-out may occur when fastener **60** is located within structure **76** and rotationally driven without further insertion into structure **76**. In order to avoid a strip-out condition once fastener **60** is inserted into structure **76** and fastener head **66** is seated against structure **76**, the force applied to fastener **60** (F_s) may be limited such that it is less than the sum of the force (F_c) needed to cut (or tap) threads, the force of friction (F_f) from the threads on structure **76**, and the force of friction (F_f) from head **66** on structure **76**, which is less than the strip-out force (F_{so}), ($F_s > F_c + F_f + F_{f2} > F_s$).

[0028] While discussed with regard to pilot hole **78**, the arrangement discussed above may also be used where fas-

tener 60 is a self-drilling fastener and there is no pilot hole. In the self-drilling configuration, the discussion above applies equally, except the force (F_i) needed to drive fastener 60 may be increased by a drilling force (F_d). Accordingly, the kinetic energy force component (F_k) of fastener 60 may also be increased in order to keep the torque force component (F_t) below the torsional strength of fastener 60.

[0029] Pilot hole 78 may have a diameter that is greater than the minor diameter and less than the major diameter of fastener 60. The rotational speed needed to drive fastener 60 may vary based on the relation between the size of pilot hole 78, the major diameter of fastener 60, the length of threaded shank 72, and the material density of structure 76 relative to the material density of fastener 60.

[0030] More specifically, as the diameter of pilot hole 78 is increased, the rotational speed needed to drive fastener 60 is reduced and as the diameter of pilot hole 78 is decreased, the rotational speed needed to drive fastener 60 is increased. Similarly, as the length of threaded shank 72 is increased, the rotational speed needed to drive fastener 60 is increased and as the length of threaded shank 72 is decreased, the rotational speed needed to drive fastener 60 is decreased. As the material density of structure 76 is increased relative to the material density of fastener 60, the rotational speed needed to drive fastener 60 is increased and as the material density of structure 76 is decreased relative to the material density of fastener 60, the rotational speed needed to drive fastener 60 is decreased.

[0031] In operation, adapter assembly 14 may be coupled to powered driver 12 and a desired driving speed may be selected for powered driver 12. Fastener 60 may be loaded into adapter assembly 14 and an end of fastener 60 may be placed against an opening of pilot hole 78 and fastener 60 may be axially aligned with pilot hole 78. Fastener 60 may then be driven into pilot hole 78, as discussed above.

[0032] More specifically, powered driver 12 may be rapidly actuated, rather than gradually actuated, to quickly generate a desired rotational speed. Downward force may be applied to fastener 60 by displacement of plunger 16 into engagement with fastener 60 once powered driver 12 has been actuated to achieve the desired rotational speed to drive fastener 60 into structure 76. Fastener 60 may be formed from a material that has a greater or lesser torsional strength than the torsional resistance of structure 76. However, even when fastener 60 is formed from a material having a lesser torsional strength than the torsional resistance of structure 76, fastener 60 may still be driven into pilot hole 78 and may tap pilot hole 78 due to the kinetic energy force component (F_k) and the torque force component (F_t) of fastener 60, as discussed above.

[0033] More specifically, when fastener 60 is driven into pilot hole 78 at a high rotational speed, the force (F_s) applied by fastener 60 may be great enough to tap structure 76, such as bone. As indicated above, when the rotational speed of fastener 60 is great enough, the kinetic energy force component (F_k) may reduce the torque force component (F_t) needed to drive fastener 60 to a level below the torsional strength of fastener 60. Since the entire fastener 60 (breakaway portion 62 and fastening portion 64) is rotating at the high rotational speed, a minimal amount of torque is transmitted through fastener 60, allowing fastener 60 to cut threads into structure 76 even when structure 76 has a torsional resistance that is greater than the torsional strength of fastener 60.

[0034] As discussed above, once head 66 of fastener 60 bottoms out on an outer surface of structure 76, an amount of

torque required to drive fastener 60 further into structure 76 becomes too great for the kinetic energy force component (F_k) of fastener 60 and the torque force component (F_t) is increased. Torque may then be transmitted to breakaway region 74 causing breakaway portion 62 to separate from fastening portion 64. Powered driver 12 may then be turned off and breakaway portion 62 may then be ejected from adapter assembly 14 through use of ejector shaft 24.

[0035] Several parameters may be varied for driving fastener 60 in the method discussed above. For example, parameters that may be used for the appropriate fastener and driving arrangement according to the method described above may include the major and minor diameters of the threaded shank 72, the body length of threaded shank 72, the pilot hole diameter, the downward force applied to fastener 60, the speed ramp up of powered driver 12, the set speed of powered driver 12, rate of trigger actuation of powered driver 12, and the material properties of structure 76 and fastener 60, such as material densities. More specifically, Table 1 below includes several configurations and associated parameter values for driving fastener 60 in the manner discussed above. The configurations listed below are examples and may generally apply to structure 76 being bone and fastener 60 being formed from a polymer. As indicated above, fastener 60 may be formed from a material that has a greater or lesser torsional strength than the torsional resistance of structure 76. In the examples listed below, the polymer formed fastener 60 may have a torsional strength less than the torsional resistance of bone.

TABLE 1

| major diameter (mm) | body length (mm) | pilot hole diameter (mm) | driver speed (rpm) |
|---------------------|------------------|--------------------------|--------------------|
| 1.5 | 5 | 1.3 | 12,000 |
| 1.5 | 3 | 1.1 | 20,000 |
| 1.5 | 4 | 1.1 | 25,000-30,000 |
| 1.5 | 4 | 1.2 | 25,000-30,000 |
| 1.5 | 5 | 1.1 | 25,000-30,000 |
| 1.5 | 5 | 1.2 | 25,000-30,000 |
| 1.5 | 8 | 1.3 | 25,000-30,000 |

What is claimed is:

1. A method comprising:

rotating a threaded fastener at a first rotational speed, said rotating providing a kinetic energy force component for the fastener based on the first rotational speed;

driving the fastener into a structure based on said rotating, said structure providing a torsional resistance during said driving greater than a torsional strength of the fastener and said driving providing a torque force component applied to the fastener; and

cutting threads into the structure with the fastener based on said driving, said driving applying a total force to the structure from the fastener including the kinetic energy force component and the torque force component, wherein the total force applied by the fastener is greater than or equal to a force required for said cutting and the torque force component is less than the torsional strength of the fastener.

2. The method of claim 1, wherein the structure includes bone.

3. The method of claim 2, wherein the fastener is formed from one of a polymer, a metal, a biocompatible non-resorb-

able material, a biocompatible resorbable material, a ceramic, a composite material, an allograft and a xenograft.

4. The method of claim 1, further comprising terminating said driving when a predetermined torque limit is applied to the fastener.

5. The method of claim 4, wherein one of the fastener and the driver includes a torque limiting feature that produces said terminating when an engagement between the fastener and the structure provides a frictional force between the fastener and the structure resulting in a torque that is greater than the predetermined torque limit.

6. The method of claim 5, wherein the frictional force includes an engagement between a head of the fastener and the structure.

7. The method of claim 1, further comprising forming a pilot hole having a first diameter greater than a minor diameter of the fastener and less than a major diameter of the fastener, said driving including driving the fastener into the pilot hole.

8. The method of claim 7, wherein a frictional force is applied to the threads of the fastener as the fastener is driven into the structure, the total force applied by the fastener being greater than the force required for said cutting and the frictional force.

9. The method of claim 1, wherein said driving includes drilling a hole in the structure.

10. The method of claim 9, wherein a drilling force is applied to the fastener as the fastener is driven into the structure, the total force applied by the fastener being greater than the force required for said cutting and said drilling.

11. The method of claim 1, wherein the first rotational speed is at least 12,000 revolutions per minute.

12. A method comprising:
applying a kinetic energy force component to a fastener having a torsional strength by rotating the fastener at a first rotational speed;
applying a torque force component to the fastener;
driving the fastener into a structure based on the combination of the kinetic energy and torque force components, wherein the torsional resistance provided by the structure during said driving is greater than a torsional strength of the fastener and the torque force component is less than the torsional strength of the fastener during said driving; and

terminating said driving when the fastening portion is inserted a predetermined amount into the structure.

13. The method of claim 12, wherein said terminating occurs when an additional torque force component is applied to the fastener based on a frictional engagement between a head of the fastener and the structure.

14. The method of claim 12, wherein the structure includes bone.

15. The method of claim 14, wherein the fastener is formed from one of a polymer, a metal, a biocompatible non-resorbable material, a biocompatible resorbable material, a ceramic, a composite material, an allograft and a xenograft.

16. The method of claim 12, further comprising forming a pilot hole having a first diameter greater than a minor diameter of the fastener and less than a major diameter of the fastener, said driving including driving the fastener into the pilot hole.

17. The method of claim 16, wherein a frictional force is applied to the threads of the fastener as the fastener is driven into the structure, the combination of the kinetic energy and torque force components of the fastener being greater than the force required for said cutting and the frictional force.

18. The method of claim 12, wherein said driving includes drilling a hole in the structure.

19. The method of claim 18, wherein a drilling force is applied to the fastener as the fastener is driven into the structure, the combination of the kinetic energy and torque force components of the fastener being greater than the force required for said cutting and said drilling.

20. The method of claim 12, wherein the first rotational speed is at least 12,000 revolutions per minute.

21. An apparatus comprising:
a threaded fastener having a torsional strength; and
a driver engaged with and adapted to drive said fastener at a first rotational speed into a structure and apply a torque force component to said fastener, said fastener adapted to have a kinetic energy force component based on the first rotational speed and to apply a total force to the structure including the torque force component and the kinetic energy force component that cuts threads into the structure, wherein the total force is greater than or equal to a force required to cut the threads and the torque force component is less than the torsional strength of said fastener.

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