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DESCRIPTION

BACKGROUND

1. Field of the Technology

[0001] The present application relates generally to torque power tools.

2. Description of the Related Art

[0002] Torque power tools are known in the art and include those driven pneumatically, electrically, hydraulically, manually, by a torque multiplier, or otherwise powered. All torque power tools have a turning force and an equal and opposite reaction force. Often this requires the use of reaction fixtures to abut against viable and accessible stationary objects to stop the housing of the tool from turning backward, while a fastener, such as for example a nut, turns forward. The stationary object must be viable in that it must be able to absorb the reaction force and be accessible in that it must be nearby for the reaction fixture to abut against it. The reaction fixture may be connected around an axis or the housing, and a mechanism is provided to hold the fixture steady relative to the tool housing during operation. This may be achieved with splines, polygons, or other configurations. DE 200 26 612 U1 discloses a variable support system comprising a plurality of rotatable axes that can be used for bolting devices. The support system comprises a support member that is mounted to a bolting device, the support member having a close-pitch fluting used for receiving a counter bracket. EP 0 879 670 A1 discloses a device for tightening up a plurality of threaded members at the same time with proper torque according to the preamble portion of claim 1 without necessitating the cumbersome procedure of rotating the members one by one through a specified small angle at a time and without unequivalent tightening of the members.

[0003] Present reaction fixtures limit tool functionality. Those connected about a turning force axis, on the one hand, allow for complete rotation of a tool housing about the turning force axis without changing the abutment point. On the other hand, they are limited to coaxial abutment against stationary objects. Those connected at the housing, on the one hand, allow for abutment against stationary objects positioned in various circumferential and spatial locations relative to the nut to be turned. On the other hand, they prevent complete rotation of the tool housing about the turning force axis without changing the abutment point.

[0004] Adjustability of present reaction fixtures is limited to about a single axis which precludes the use of a single tool in assemblies having viable stationary objects in non-accessible locations. Operators commonly need several tools at a workstation each having a reaction fixture oriented differently to abut against a viable and accessible stationary object. Alternatively, operators must disassemble the tool, reposition the reaction fixture and reassemble the tool. The former solution is expensive while the latter solution is time consuming.

[0005] If present reaction fixtures cannot abut against viable and accessible stationary objects properly, custom reaction fixtures need to be engineered. Reengineering of the tool connection means to accommodate custom reaction fixtures is prohibitively expensive, unsafe and time consuming. Tool manufacturers offer several commercially available reaction fixture constructions for these reasons.

[0006] During operation of tools, twisting forces are induced on the housing along the turning force axis by the transfer of the reaction force through the reaction fixture to the stationary object. The reaction force for tools with torque output of 13558,2 Nm (10,000 ft.lbs.) can be as high as 54232,7 Nm (40,000 lbs.) and is applied as a side load to the stationary object in one direction and to the fastener to be turned in an opposite direction. Large reaction forces bend and increase the turning friction of the fastener.

[0007] Twisting forces are limited and least destructive when the reaction force is transferred to a stationary object perpendicular to the turning force axis. The ideal abutment point is perpendicular to the turning force axis and on the same plane as the fastener to be turned. Tools operating with sockets that reach down to the same plane as the fastener cause twisting forces. Twisting forces exacerbate fastener-bending forces roughly by a distance H between the attachment point of the socket to the tool and the fastener plane. These twisting and fastener-bending forces are limited and least destructive when the reaction force is transferred perpendicular to the turning force axis in a plane roughly the distance H above the fastener plane. Thus the ideal abutment pressure point is perpendicular to the turning force axis in the plane distance H above the fastener plane. Rarely do

present reaction fixtures transfer the reaction force to the ideal abutment pressure point. Reaction fixtures must be adjustable to minimize twisting and fastener-bending forces so as to avoid the tool from jumping off of the job or from failing.

[0008] Present reaction fixtures are not adjustable around multiple axes due to concerns regarding total tool weight. Tools need to be portable for the majority of fasteners. The maximum tool weight to be carried safely by an operator should not exceed 13,6 kg (30 lbs). For larger fasteners, the maximum tool weight to be carried safely by two operators should not exceed 27,2 kg (60 lbs). For applications where the only viable and accessible stationary object requires custom reaction fixtures, these weights are exceeded and crane use is required. Crane use to support the tool is expensive and is economical only for large fasteners.

[0009] Other tools provided with reaction fixtures of the prior art are disclosed, for example, in U.S. Pat. Nos. 3,361,218, 4,549,438, 4,538,484, 4,607,546, 4,619,160, 4,671,142, 4,706,526, 4,928,558, 5,027,932, 5,016,502, 5,142,951, 5,152,200, 5,301,574, 5,791,619, 6,260,443.

[0010] Accordingly, what are needed are reaction force transfer mechanisms which overcome the deficiencies of the prior art.

SUMMARY

[0011] According to the invention, an apparatus for tightening or loosening fasteners is provided as defined by the features of claim 1.

[0012] Advantageously, inadvertent injury to the operator; bolt load variances caused by frictional differences from one fastener to another; fastener bending and thread galling from nonsymmetrical absorption of the side load; and fastener replacement caused by fastener bending and thread galling are substantially decreased. The reaction forces from the apparatus substantially cancel themselves out at the ideal abutment pressure point. And the portability of the apparatus is increased. Furthermore the ability to simultaneously tighten or loosen two fasteners increases efficiency and productivity.

BRIEF DESCRIPTION OF THE DRAWINGS

[0013]

FIG. 1 is a side view of a tool having a reaction adaptor;

FIG. 2 is a plan view FIG. 1;

FIG. 3 is a three-dimensional view of FIG. 1 having the reaction adaptor adjusted to abut against a stationary object about a pipe flange;

FIG. 4 is a flowchart which describes an exemplary method of using the reaction adaptor and the tool having the reaction adaptor;

FIGs. 5A-5C are perspective views of alternative embodiments of a third and a fourth connecting means of a first and a second force-transmitting element and a fourth connecting means of a second force-transmitting element of the reaction adaptor including bores and threaded nuts, bores and detents, and polygonal configurations;

FIG. 6 is a display of commercially available reaction fixtures usable with portions of the reaction adaptor;

FIG. 7 is a side view of an apparatus for tightening or loosening fasteners according to the invention having a torque output regulation system;

FIG. 8 is a three dimensional view of apparatus of FIG. 1 having an additional reaction adaptor. FIG. 9 is a three-dimensional view of a first and a second pneumatically, electrically, hydraulically or manually driven torque power tool attached by a reaction adaptor;

FIG. 10 is a three-dimensional view of another exemplary embodiment of a reaction adaptor for the tool; and

FIG. 11 is a three-dimensional view of another exemplary embodiment of a reaction adaptor for another tool.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0014] FIG. 1 shows a side view of an exemplary embodiment of a reaction adaptor 150 for a torque power tool 100. FIG. 2 is a plan view of FIG. 1. Tool 100 includes a housing 101 having two housing portions, a cylinder portion 102 and a driving portion 103.

[0015] Cylinder-piston means 104 are arranged in cylinder portion 102 and include a cylinder 105, a piston 106 reciprocatingly movable in cylinder 105 along a piston axis A_1 , and a piston rod 107 connected with piston 106. A known lever-type ratchet mechanism 108 is arranged in driving portion 103, connected to and drivable by cylinder-piston means 104, and includes a ratchet 109. Ratchet 109 is turnable about a turning force axis B_1 which is perpendicular to piston axis A_1 . Ratchet 109 is connected with a driving element 110 which receives a first turning force 190 acting about turning force axis B_1 in one direction 192 during operation of tool 100 (see also FIG. 2). Turning force 190 turns a hex socket 111 attached to driving element 110 which turns a nut 131.

[0016] A reaction support portion 114, formed on a part of cylinder portion 103 receives second turning force 191 acting about turning force axis B_1 in another direction 193 during operation of tool 100. Reaction support portion 114 is formed of an annular polygonal body 115 having a plurality of outer splines 116. Outer splines 116 are positioned circumferentially around annular body 115 and extend radially outwardly from a central axis A_2 which is coaxial with piston axis A_1 .

[0017] A reaction support portion 120, connected to driving portion 103, also receives second turning force 191 acting about turning force axis B_1 in another direction 193 during operation of tool 100. Reaction support portion 120 is formed of an annular polygonal body 121 having a plurality of outer splines 123. Outer splines 123 are positioned circumferentially around annular body 121 and extend radially outwardly from a central axis B_2 which is coaxial with turning force axis B_1 .

[0018] Reaction adaptor 150, when attached to reaction support portion 120, receives second turning force 191 acting in another direction 193 during operation. First and second turning forces 190 and 191 are equal to and in opposite directions to each other. First turning force 190 turns fastener 131 while reaction adaptor 150 transfers second turning force 191 to a stationary object at abutment pressure point P_1 , in this case, a neighboring nut 133.

[0019] Reaction adaptor 150 generally includes a first force-transmitting element 160, when engaged with tool 100, being rotatable about turning force axis B_1 ; and a second force-transmitting element 170, when engaged with first element 160, being one of rotatable about, extensible and retractable along, and rotatable about and extensible and retractable along at least a distal portion 165 of first element 160. First element 160 includes a proximal portion 161 formed of an annular polygonal body 162 having a plurality of inner splines 163, and distal portion 165 formed of a tubular member 166 having an internal bore 167 with a plurality of inner splines 168. Second element 170 includes a proximal portion 171 formed of a tubular member 172 having a plurality of outer splines 173, and a distal portion 175 formed of a rectangular body 176. First element 160, when attached to tool 100, extends substantially perpendicular to and has a first force-transmitting axis C_1 substantially perpendicular to turning force axis B_1 . Second element 170, when attached to first element 160, extends substantially perpendicular to and has a second force-transmitting axis D_1 substantially perpendicular to first force-transmitting axis C_1 .

[0020] First element 160 is shown non-rotatably attached to reaction support portion 120 in a first position and held in place by a locking mechanism 180. First element 160 is engageable and attachable separately, individually, and independently to tool 100. Inner splines 163 are positioned circumferentially around the inside of annular body 162 and extend radially inwardly toward a central axis B_3 . Annular body 162 is of such inner width and annular body 121 is of such outer width that inner splines 163 mesh with outer splines 123. Annular body 121 and proximal portion 161 include first and second connecting means 124 and 164. Reaction support portion 120 and first element 160 are attachable to each other by attaching first and second connecting means 124 and 164. Locking mechanism 180 may include a bore and pin or other well known configuration like a spring loaded reaction clamp at the base of reaction support portion 120 and receiving grooves on proximal portion 161. Axes B_1 , B_2 , and B_3 are coaxial when first element 160 and reaction support portion 120 are attached to each other and to tool 100.

[0021] Second element 170 is shown non-rotatably attached to first element 160 in a second position and held in place by a locking mechanism 181. Second element 170 is engageable and attachable separately, individually, and independently to first element 160. Inner splines 168 are positioned circumferentially around the inside of internal bore 167 and extend radially inwardly toward a central axis C_2 . Outer splines 173 are positioned circumferentially around tubular member 172 and extend radially outwardly from a central axis C_3 . Internal bore 167 is of such inner width and tubular member 172 is of such outer width that inner

splines 168 mesh with outer splines 173. Internal bore 167 receives tubular member 172 in a telescoping arrangement. Distal portion 165 includes third connecting means 169 which comprises tubular member 166, internal bore 167, and inner splines 168. Proximal portion 171 includes fourth connecting means 174 which comprises tubular member 172 and outer splines 173. First and second elements 160 and 170 are attachable to each other by attaching third and fourth connecting means 169 and 174 which are held in place by locking mechanism 181. Locking mechanism 181 may include a bore and pin or other well known configuration like a spring loaded reaction clamp on distal portion 165 and receiving grooves on proximal portion 171. Axes B_1 , B_2 , and B_3 are coaxial and C_1 , C_2 , and C_3 are coaxial when second element 170, first element 160 and reaction support portion 120 are attached to each other and to tool 100. Rectangular body 176 of distal portion 175 as shown extends substantially perpendicular to tubular member 172 and first element 160.

[0022] Tool 100 is prepared to turn nut 131 threaded on a lug 132 to connect flanges (not shown). Reaction adaptor 150 is attached to tool 100 in a reaction force transfer position to transfer turning force 191, the reaction force, to nut 133 at abutment pressure point P_1 during operation. As turning force 190 turns hex socket 111 on nut 131, rectangular body 176, supported by distal portion 175, bears against abutment pressure point P_1 on the walls of nut 133. This prevents ratchet 109 from rotating inwardly relative to nut 131. Thus nut 131 is turned by hex socket 111 to a desired torque.

[0023] Nut 31 to be turned is located in the center, abutment pressure point P_1 for reaction adaptor 150 is arranged left of center, and nut 135 is arranged right of center. Since action and reaction are equal but opposite, reaction adaptor 150 pushes its abutment area backwards from the center (see FIG. 2). Side loads applied to driving portion 103 are reduced but not eliminated.

[0024] FIG. 3 is a three-dimensional view of FIG. 1 having a reaction adaptor 350 abutted against a piping segment 302 of a pipe flange 300. Reaction adaptor 350 is similar to reaction adaptor 150 of FIGs. 1-2 in all material ways except that second element 370 has been rotated counterclockwise to abut against piping segment 302 at an abutment pressure point P_3 . As discussed previously, tool 100 operates with hex socket 111 which reaches down to a fastener plane 141. Twisting forces exacerbate fastener-bending forces by a distance H roughly between the attachment point of socket 111 to tool 100 at plane 140 and fastener plane 141 (see FIG. 1). In this embodiment, axes C_1 , C_2 , C_3 and D_1 lie in plane 140 at distance H above plane 141. The twisting and fastener-bending forces are limited and least destructive when turning force 191, the reaction force, is transferred perpendicular to turning force axis B_1 in plane 140. Thus the ideal abutment pressure point P_3 for reaction adaptor 350 is perpendicular to turning force axis B_1 in plane 140.

[0025] Advantageously, first element 160 is engageable and attachable separately, individually and independently to tool 100 and second element 170 is engageable and attachable separately, individually and independently to first element 160. The portability of tool 100 is maximized while the weight of tool 100 is minimized. Commercially available reaction fixtures may be used with or in replacement of portions of first and second elements 160 and/or 170, rather than custom reaction fixtures, thereby reducing costs and increasing safety. Reaction adaptor 150 is adjustable to minimize twisting and fastener-bending forces so as to avoid tool 100 from jumping off of the job or from failing. Reaction adaptor 150, when engaged with tool 100, is adjustable to abut against viable and otherwise inaccessible stationary objects at the ideal abutment pressure point P_3 . Reaction adaptor 150, when attached to tool 100, transfers turning force 191 to at the ideal abutment pressure point P_3 during operation. Operators no longer need several tools at the workstation each having a reaction fixture oriented differently to abut against viable stationary objects for each application. Nor do operators need to completely disassemble tool 100, reposition reaction adaptor 150 and reassemble tool 100 for each application. Also, reaction adaptor 150 allows for complete rotation of housing 101 about turning force axis B_1 without changing abutment point P_3 thereby avoiding any circumferential obstructions in a rotation plane of housing 101.

[0026] FIG. 4 is a flowchart which describes an exemplary method of using the reaction adaptor and the tool having the reaction adaptor FIGs. 1-3 will be referenced with the flowchart steps of FIG. 4.

[0027] Beginning with step 404 of FIG.4, tool 100 is provided by providing housing 101 having cylinder portion 102 and driving portion 103; arranging, in cylinder portion 102, cylinder-piston means 104 movable along piston axis A_1 ; arranging, in driving portion 103, ratchet mechanism 108 connected to and drivable by cylinder-piston means 104; providing, in ratchet mechanism 108, ratchet 109 turnable about turning force axis B which is perpendicular to piston axis A_1 ; and providing driving element 110, connected to ratchet 109, receiving first turning force 190 acting about turning force axis B_1 in one direction 192 during operation of tool 100.

[0028] Next, in step 406 of FIG. 4, first element 160 is engaged with tool 100 by bringing proximal portion 161 substantially

adjacent to reaction support portion 120 and substantially aligning axes B₁, B₂, and B₃. Annular body 162 is passed over driving element 110.

[0029] In step 408 of FIG. 4, first element 160 is rotated about turning force axis B₁ to a first position. The first position is chosen based on the proximity of a viable and accessible stationary object that may be found in various circumferential and spatial locations relative to nut 131. First element 160, when engaged with tool 100, is rotatable about turning force axis B₁ because inner splines 163 and outer splines 123 have not yet been meshed.

[0030] In step 410 of FIG. 4, first element 160 is attached to reaction support portion 120 in the first position by meshing inner splines 163 and outer splines 123 and activating locking mechanism 180. In steps not shown in FIG. 4, hex socket 111 is attached to driving element 110, and tool 100 is placed on nut 131.

[0031] In step 412 of FIG. 4, second element 170 is engaged with first element 160 by bringing proximal portion 171 substantially adjacent to distal portion 165 and substantially aligning axes C₁, C₂, and C₃.

[0032] In step 414 of FIG. 4, second element 170 is positioned to abut against the stationary object in a second position by rotating it about and then retracting it along distal portion 165. The second position is chosen based on the proximity of the viable and accessible stationary object. Second element 170, when engaged with first element 160, is rotatable about distal portion 165 because inner splines 168 have not yet been meshed with outer splines 173. Second element 170 is rotated about distal portion 165 to one of a plurality of extension angles; inner splines 168 and outer splines 173 are meshed when internal bore 167 receives tubular member 172 in a telescoping arrangement; and second element 170 is retracted along distal portion 165 to one of a plurality of extension lengths. Reaction adaptor 150, in the second position, abuts against the viable and accessible stationary object, nut 133. In step 416 of FIG. 4, second element 170 is attached to first element 160 in the second position by activating locking mechanism 181. Reaction adaptor 150 is now in reaction force transfer position.

[0033] When necessary to disassemble tool 100 or adjust reaction adaptor 150 to another abutment pressure point, second element 170 is detached from first element 160 by deactivating locking mechanism 181. Second element 170 is extended along distal portion 165 until inner splines 168 and outer splines 173 are no longer meshed and second element 170 is no longer substantially adjacent first element 160. Tool 100 may be displaced from nut 131 and hex socket 111 may be detached from driving element 110. First element 160 is detached from reaction support portion 120 by deactivating locking mechanism 180, unmeshing inner splines 163 and outer splines 123, and removing it from reaction support portion 120. The steps of FIG. 4 are then repeated.

[0034] In an alternative method of using the reaction adaptor and the tool having the reaction adaptor, the second element is engaged with the first element prior to the first element being engaged with the tool. The reaction adaptor is fully assembled and pre-adjusted and may be abutted against a viable and accessible stationary object prior to being engaged with the tool.

[0035] Alternative Structures of the First and Second Connecting Means. Reaction support portion 120 may have a height such that first element 160, when engaged with reaction support portion 120, is also slideable along reaction support portion 120. Distance H and thus plane 140 may be varied by sliding first element 160 along reaction support portion 120.

[0036] Proximal portion 161 may have a hinged annular body 162 such that annular body 162 is not passed over driving element 110 in step 406 of FIG. 4. First element 160 is engaged with tool 100 by bringing proximal portion 161 substantially adjacent to reaction support portion 120, unhinging annular body 162, and substantially aligning axes B₁, B₂, and B₃. Note that a similar structure may be used for other tool and reaction adaptor components.

[0037] Alternative Structures of the Third and Fourth Connecting Means. FIGs. 5A-5C are perspective views of alternative structures of the third and fourth connecting means of the first and second elements including bores and threaded nuts, bores and detents, and polygonal configurations. Referring back to FIGs. 1-4, distal portion 165 and proximal portion 171 include third and fourth connecting means 169 and 174 which are splined configurations. First and second elements 160 and 170 are attachable to each other by attaching third and fourth connecting means 169 and 174.

[0038] FIG. 5A is a perspective view of a second structure of a third and fourth connecting means 569_A and 574_A. Generally discussion related to FIGs. 1-3 applies to FIG. 5A. A portion of distal portion 565_A of first element 160 is shown formed of a tubular member 566_A having an internal bore 567_A and at least three sets of a plurality of radially directed, circumferentially spaced, threaded-through bores 568_{A1}, 568_{A2}, and 568_{A3}. A portion of proximal portion 571_A of second element 170 is shown

formed of a tubular member 572_A having at least three sets of a plurality of radially directed, circumferentially spaced, inwardly tapered attachment bores 573_{A1}, 573_{A2}, and 573_{A3}, so as to operatively engage with first element 160. Bore sets 568_{A1}-568_{A3}, are of such size as to receive a threaded end of threaded bolts 582 and bore sets 573_{A1}-573_{A3} are of such size so as to receive a tapered end of bolts 582_A at one of a plurality of extension angles and extension lengths. Internal bore 567_A is of such inner width and tubular member 572_A is of such outer width that bore sets 568_{A1}-568_{A3} align with bore sets 573_{A1}-573_{A3}. Internal bore 567_A receives tubular member 572_A in a telescoping arrangement. Distal portion 565_A includes third connecting means 569_A which comprises tubular member 566_A, internal bore 567_A, and bore sets 568_{A1}-568_{A3}. Proximal portion 571_A includes fourth connecting means 574_A which includes tubular member 572_A and bore sets 573_{A1}-573_{A3}. First and second elements 160 and 170 are attachable to each other by attaching third and fourth connecting means 569_A and 574_A.

[0039] Generally discussion related to the method of FIG. 4 applies to FIG. 5A. In step 412 of FIG. 4, second element 170 is engaged with first element 160 by bringing proximal portion 571_A substantially adjacent to distal portion 565_A, substantially aligning axes C₁, C₂, and C₃, and inserting proximal portion 571_A into distal portion 565_A in a telescoping arrangement.

[0040] FIG. 5B is a perspective view of a third structure of a third and fourth connecting means 569_B and 574_B. Generally discussion related to FIGs. 1-3 applies to FIG. 5B. A portion of distal portion 565_B of first element 160 is shown formed of a tubular member 566_B having an internal bore 567_B and at least three sets of a plurality of radially directed circumferentially spaced bores 568_{B1}, 568_{B2}, and 568_{B3}. A portion of proximal portion 571_B of second element 170 is shown formed of a tubular member 572_B having at least three sets of a plurality of radially directed, circumferentially spaced bores 573_{B1}-573_{B3}. At least three sets of a plurality of detents 582_{B1}-582_{B3} project through bore sets 568_{B1}-568_{B3} and are biased radially outwardly by spring mechanisms (not shown) so as to operatively engage with first element 160. Bore sets 568_{B1}-568_{B3} are of such size as to receive detent sets 582_{B1}-582_{B3} at one of a plurality of extension angles and extension lengths. Internal bore 567_B is of such inner width and tubular member 572_B is of such outer width that bore sets 568_{B1}-568_{B3} align with bore sets 573_{B1}-573_{B3}. Internal bore 567_B receives tubular member 572_B in a telescoping arrangement. Distal portion 565_B includes third connecting means 569_B which includes tubular member 566_B, internal bore 567_B, and bore sets 568_{B1}-568_{B3}. Proximal portion 571_B includes fourth connecting means 574_B which includes tubular member 572_B, bore sets 573_{B1}-573_{B3}, and detent sets 582_{B1}-582_{B3}. First and second elements 160 and 170 are attachable to each other by attaching third and fourth connecting means 569_B and 574_B.

[0041] Generally discussion related to the method of FIG. 4 applies to FIG. 5B. In step 412 of FIG. 4, second element 170 is engaged with first element 160 by bringing proximal portion 571_B substantially adjacent to distal portion 565_B, substantially aligning axes C₁, C₂, and C₃, and inserting proximal portion 571_B into distal portion 565_B in a telescoping arrangement.

[0042] FIG. 5C is a perspective view of a fourth structure of a third and fourth connecting means 569_C and 574_C. Generally discussion related to FIGs. 1-3 applies to FIG. 5C. A portion of distal portion 565_C of first element 160 is shown formed of a tubular member 566_C having an internal bore 567_C with a polygonal inner wall 568_C (not shown). A portion of proximal portion 571_C of second element 170 is shown formed of a tubular member 572_C having a polygonal outer wall 573_C. Internal bore 567_C is of such inner width and tubular member 572_C is of such outer width that internal bore 567_C receives tubular member 572_C in a telescoping arrangement and polygonal inner wall 568_C meshes with polygonal outer wall 573_C at one of a plurality of extension angles and extension lengths. Distal portion 565_C includes third connecting means 569_C which includes tubular member 566_C, internal bore 567_C, and polygonal inner wall 568_C. Proximal portion 571_C includes fourth connecting means 574_C which includes tubular member 572_C and polygonal outer wall 573_C. First and second elements 160 and 170 are attachable to each other by attaching third and fourth connecting means 569_C and 574_C.

[0043] Generally discussion related to the method of FIG. 4 applies to FIG. 5C. In step 412 of FIG. 4, second element 170 is engaged with first element 160 by bringing proximal portion 571_C substantially adjacent to distal portion 565_C and substantially aligning axes C₁, C₂, and C₃.

[0044] Note that other structures of the third and fourth connecting means may be used including a bores and pins and hinged body configuration.

[0045] Alternative Structures of Portions of the First and Second Elements. In the exemplary embodiment of FIGs. 1-3, at least

portions of first and second elements 160 and 170 extend perpendicular to each other. Alternatively, at least distal portion 165 of first element 160, when attached to tool 100, may extend substantially at an angle of 45°-135° to turning force axis B₁. First force-transmitting axis C₁ would be of a similar angle to turning force axis B₁. Further, at least distal portion 175 of second element 170, when attached to first element 160, may extend substantially collinear to at least distal portion 165. In other structures, at least distal portion 175 of second element 170, when attached to first element 160, may extend substantially at an angle of 45°-135° to at least distal portion 165. Second force-transmitting axis D₁ would have similar angle to first force-transmitting axis C₁.

[0046] These and other alternative structures of portions of first and second elements 160 and 170 envision the use of commercially available and custom manufactured reaction fixtures with or in replacement of portions of first and/or second elements 160 and 170. FIG. 6 is a display of such commercially available reaction fixtures, including: splined, bore and nut, bore and detent, polygonal, bore and pin, hinged and other connecting means. Examples of some of these commercially available and custom manufactured reaction fixtures include: a dual reaction fixture 602; a standard reaction arm 604; an extended collinear reaction arm 606; a tubular reaction fixture 608; an extended reaction arm 610; a reaction pad 612; a cylinder reaction arm 614; a turbine coupling reaction fixture 616; a three position reaction roller 618; a cylinder reaction foot 620; and an extended reaction roller 622. Other commercially available and custom manufactured reaction fixtures exist and may be adapted to use with portions of first and second elements 160 and 170.

[0047] Generally discussion related to FIGs. 1-6 applies to FIGs. 7 and 8. FIG. 7 is a side view of an apparatus 7 for tightening or loosening fasteners which includes: a first and a second receiving member 111 and 711, rotatably supported in apparatus 7, for receiving a first and a second fastener 131 and 731; a first and a second device for effecting rotation of the respective receiving members (i.e., at least portions of a first and a second torque power tool 100 and 700) to tighten or loosen the respective fasteners; and a device for controlling a first and a second torque output level 127 and 727 or other operation parameter of the respective devices for effecting rotation (i.e., at least portions of a torque output regulation system 759) to maintain a difference in the torque output levels within a predetermined value.

[0048] Generally, reaction adaptor 750 includes a first and a second force-transmitting element 160 and 770 engageable with and attachable to tools 100 and 700. Tool 100 produces a first turning force 190 acting about a first turning force axis B₁ in one direction 192 during operation. Second tool 700 produces a second turning force 790 acting about a second turning force axis B₄ in one direction 192 during operation. First element 160, when attached to first tool 100, receives a first reaction turning force 191 acting in another direction 193 during operation. Second element 770, when attached to second tool 700, receives a second reaction turning force 791 acting in another direction 193 during operation. First and second turning forces 190 and 790 turn fasteners 131 and 731.

[0049] First and second turning forces 190 and 790 may be substantially equal to each other, in opposite directions to first and second reaction turning forces 191 and 791. This likely occurs where bolt loads and friction values of fasteners 131 and 731 are similar. Reaction adaptor 150 receives reaction turning forces 191 and 791 in another direction 193, thus substantially negating them. The twisting and fastener-bending forces are limited and least destructive when reaction turning forces 191 and 791 are transferred perpendicular to turning force axes B₁ and B₄ in plane 140 at ideal abutment pressure point P₇. The usual side load; fastener bending, thread galling and bolt damage are reduced or negated. Efficiency and productivity is increased.

[0050] As previously discussed, tool 100 includes a housing 101 having two housing portions, a cylinder portion 102 and a driving portion 103. Cylinder-piston means 104 are arranged in cylinder portion 102 and include a cylinder 105, a piston 106 reciprocatingly movable in cylinder 105 along piston axis A₁, and a piston rod 107 connected with piston 106. Hydraulic fluid, under pressure, is delivered to tool 100 via a conduit 119 through a fluid supply line 149 from an hydraulic pump 135. A known lever-type ratchet mechanism 108 is arranged in driving portion 103, connected to and drivable by cylinder-piston means 104, and includes a ratchet 109. Ratchet 109 is turnable about turning force axis B₄, perpendicular to piston axis A₁ and A₂. Ratchet 109 is connected with a driving element 110 which receives first turning force 190. First turning force 190 turns hex socket 111 attached to driving element 110 to turn fastener 131.

[0051] A reaction support portion 120 connected to driving portion 103 receives first reaction turning force 191. Reaction support portion 120 is formed of annular polygonal body 121 having the plurality of outer splines 123. Outer splines 123 are positioned circumferentially around annular body 121 and extend radially outwardly from central axis B₂ which is coaxial with first turning force axis B₁.

[0052] Tool 700 includes a housing 701 having two housing portions, a cylinder portion 702 and a driving portion 703. Cylinder-piston means 704 are arranged in cylinder portion 702 and include a cylinder 705, a piston 706 reciprocatingly movable in

cylinder 705 along a piston axis A_2 , and a piston rod 707 connected with piston 706. Hydraulic fluid, under pressure, is delivered to tool 700 via a conduit 719 through a fluid supply line 749 from hydraulic pump 135. A known lever-type ratchet mechanism 708 is arranged in driving portion 703, connected to and drivable by cylinder-piston means 704, and includes a ratchet 709. Ratchet 709 is turnable about second turning force axis B_4 , perpendicular to piston axes A_1 and A_2 and parallel to first turning force axis B_1 . Ratchet 709 is connected with a driving element 710 which receives second turning force 790 acting about turning force axis B_4 . Second turning force 790 turns hex socket 711 attached to driving element 710 to turn fastener 731.

[0053] A reaction support portion 720 connected to driving portion 703 receives a second reaction turning force. Reaction support portion 720 is formed of an annular polygonal body 721 having a plurality of outer splines 723. Outer splines 723 are positioned circumferentially around annular body 721 and extend radially outwardly from a central axis B_5 which is coaxial with second turning force axis B_4 .

[0054] Reaction adaptor 750 includes first force-transmitting element 160, which when engaged with tool 100 is rotatable about turning force axis B_1 . Reaction adaptor 150 also includes a second force-transmitting element 770, which when engaged with first element 160 is either rotatable about, extensible and retractable along, or rotatable about and extensible and retractable along at least distal portion 165. Second force-transmitting element 770, when engaged with tool 700, is rotatable about turning force axis B_4 .

[0055] First element 160 includes proximal portion 161 formed of an annular polygonal body 162 having plurality of inner splines 163, and a distal portion 165 formed of a tubular member 166 having an internal bore 167 with a plurality of inner splines 168. Second element 770 includes a proximal portion 771 formed of a tubular member 772 having a plurality of outer splines 773, and a distal portion 775 formed of an annular polygonal body 776 having a plurality of inner splines 777. As shown in FIG. 7, first element 160, when attached to tool 100, extends substantially perpendicular to and has a force-transmitting axis C_1 , which is substantially perpendicular to turning force axis B_1 . Second element 770, when attached to tool 700, extends substantially perpendicular to and has force transmitting axis C_1 substantially perpendicular to turning force axis B_2 . First and second elements 160 and 770, when attached to each other, extend substantially collinear to force-transmitting axis C_1 .

[0056] First element 160 is shown non-rotatably attached to reaction support portion 120 in first position and held in place by locking mechanism 180. First element 160 is engageable and attachable separately, individually, and independently to tool 100 and second element 770. Inner splines 163 are positioned circumferentially around the inside of annular body 162 and extend radially inwardly toward central axis B_3 . Annular body 162 is of such inner width and annular body 121 is of such outer width that inner splines 163 mesh with outer splines 123. Annular body 121 and proximal portion 161 include first and second connecting means 124 and 164. Reaction support portion 120 and first element 160 are attachable to each other by attaching first and second connecting means 121 and 164. Axes B_1 , B_2 , and B_3 are coaxial when first element 160 and reaction support portion 120 are attached to each other and to tool 100.

[0057] Second element 770 is shown non-rotatably attached to first element 160 in a second position and held in place by a locking mechanism 780. Second element 770 is engageable and attachable separately, individually and independently to first element 160. Inner splines 168 are positioned circumferentially around the inside of internal bore 167 and extend radially inwardly toward a central axis C_2 . Outer splines 773 are positioned circumferentially around tubular member 772 and extend radially outwardly from a central axis C_3 . Internal bore 167 is of such inner width and tubular member 772 is of such outer width that inner splines 168 mesh with outer splines 773. Internal bore 167 receives tubular member 772 in a telescoping arrangement. Distal portion 165 includes third connecting means 169 which comprises tubular member 166, internal bore 167, and inner splines 168. Proximal portion 771 includes fourth connecting means 774 which comprises tubular member 772 and outer splines 773. First and second elements 160 and 770 are attachable to each other by attaching third and fourth connecting means 169 and 774 which are held in place by locking mechanism 181. Axes B_1 , B_2 , and B_3 are substantially coaxial and C_1 , C_2 , C_3 and D_1 are substantially coaxial when tool 100 with reaction support portion 120, first element 160, second element 770 and tool 700 with reaction support portion 720 are attached to each other.

[0058] Second element 770 is also shown non-rotatably attached to reaction support portion 720 in second position and held in place by locking mechanism 780. Second element 770 is engageable and attachable separately, individually and independently to tool 700. Inner splines 777 are positioned circumferentially around the inside of annular body 776 and extend radially inwardly toward central axis B_6 . Annular body 776 is of such inner width and annular body 721 is of such outer width that inner splines 777 mesh with outer splines 723. Annular body 721 and distal portion 775 include fifth and sixth connecting means 724 and 779. Reaction support portion 720 and second element 770 are attachable to each other by attaching fifth and sixth connecting means

724 and 779. Axes B₄, B₅, and B₆ are coaxial when second element 770 and reaction support portion 720 are attached to each other and to tool 700.

[0059] An operation parameter regulation system 759 is shown exterior to pump 735, however the whole of system 759 or parts thereof may be found within pump 735. Operation parameter regulation system 759 regulates torque outputs of tools 100 and 700. Torque output regulation system 759 includes a first and a second switch 734 and 736 attached to hydraulic pump 735 and pressurized fluid supply lines 149 and 749. Switches 734 and 736 are activated by a control system 737, which controls torque output levels 127 and 727 of tools 100 and 700 to maintain a difference in the torque output levels within a predetermined torque difference value 758. Switches 734 and 736 may include: pushbutton, rocker, toggle, rotary coded DIP, rotary DIP, key lock, slide, snap action or reed switches; or air, back flow preventer, ball, butterfly, check, control, diverter, drain, shut-off, gas, gas-pressure, globe, hydraulic regulator, hydraulic, mixing, needle, pinch, plug, pressure regulator, pressure relief, servo, shut-off, slide, poppet or solenoid valves. If an electric motor is used, switches 734 and 736 may include any of the above electrical control switches.

[0060] Torque output regulation system 759 may include torque transducers such as a first and a second ferromagnetic sensor 144 and 744. Ferromagnetic sensors 144 and 744 include: couplings 145 and 745 for connection to control system 737; stationary Hall effect or similar magnetic field sensing units 146 and 746; and ferromagnetic parts 148 and 748 coupled to tools 100 and 700. Note that other components known in the art may be used.

[0061] Ferromagnetic sensors 144 and 744 measure torque output levels 127 and 727 of tools 100 and 700. A first and a second conduit 151 and 751 carry a first and a second torque data signal 152 and 752 including output torque levels 127 and 727 to control system 737. A conduit 757 carries input data 758 from an input device 739 to control system 737. A conduit 728 carries an output data 729 to an output device 738. A conduit 755 carries power 756 from a power supply 733 to control system 737. Power supply 733 may be any suitable source (e.g., battery, solar cell, fuel cell, electrical wall socket, generator, motor, etc.). Input device 739 may be any suitable device (e.g., touch screen, keypad, mouse, remote, etc.). An operator may input a predetermined torque difference value, input data 758, into input device 739. Predetermined torque difference value 758 is carried through conduit 757 to control system 737. Control system 737 may transmit output data 729 through conduit 728 to output device 738. Output data 729 may include predetermined torque difference value 758 and/or torque output levels 127 and 727 from tools 100 and 700. Output device 738 may be any suitable device (e.g., screen, liquid crystal display, etc.). Control system 737 may send switch control signals 154 and 754 through conduits 153 and 753 to switches 734 and 136.

[0062] Torque output regulation system 759 may monitor torque output levels 127 and 727 by any of the following operation parameters (i.e., torque data signals 152 and 752) including: hydraulic or pneumatic fluid pressures or flow rates; electrical circuit parameters such as current, voltage or magnetic field; direct measurement of torque output; or a combination of such. These operation parameters may be measured or sensed by various types of: strain gauges; rotary encoders; torque sensors; clutches; load cells; or position, flow, force or pressure meters, sensors or valves. Note that other components known in the art may be used. For example, clutches may be configured to slip respectively to maintain the difference in the torque output levels within the predetermined torque difference value 758.

[0063] Apparatus 7 operates by activating pump 735 and control system 737 to regulate torque output levels 127 and 727. The difference in torque output levels 127 and 727 may exceed predetermined torque difference value 758. If so control system 737 regulates torque output levels 127 and 727 of tools 100 and 700 by either: lowering the torque output level of the tool with the higher torque output level; raising the torque output level of the tool with the lower torque output; or both raising and lowering the torque output levels of the tools until the difference in the torque output levels returns to within the predetermined torque difference value.

[0064] FIG. 8 is a three dimensional view of portions of FIG. 7. Tools 100 and 700 are prepared to turn fasteners 131 and 731 threaded on lugs 132 and 732 to connect plates of a flange. Reaction adaptor 750 is attached to tools 100 and 700 in a reaction force transfer position to transfer reaction turning forces 191 and 791 to ideal abutment pressure point P₇. Turning forces 190 and 790, acting in the clockwise one direction 192, turn hex sockets 111 and 711 on fasteners 131 and 731. And first and second elements 160 and 770 of reaction adaptor 750 receive reaction turning forces 191 and 791, acting in the counterclockwise another direction 193. This prevents ratchets 109 and 709 from rotating inwardly relative to fasteners 131 and 731, which are turned to a desired torque.

[0065] A method of using the apparatus may include: an operator inputs predetermined torque difference value 758 into input device 739; output device 738 displays predetermined torque difference value 758; the operator activates tools 100 and 700; control system 737, using ferromagnetic sensors 144 and 744, measures torque output values 127 and 727 and maintains a difference in the torque output values 127 and 727 within predetermined torque difference value 758. If the difference in the

torque output values 127 and 727 exceeds the predetermined torque difference value 758, control system 737 either: lowers the torque output level of the tool with the higher torque output level; raises the torque output level of the tool with the lower torque output; or both raises and lowers the torque output levels of the tools until the difference in the torque output levels returns to within predetermined torque difference value 758.

[0066] The following discussion relates to alternative embodiments of apparatus 7. Note that for ease of discussion, the components are referenced in the plurality but alternatively may be in the singular.

[0067] The receiving members commonly known in the art as 'sockets', receive at least a portion of the fasteners. The receiving members are shaped so that they correspond to the shape of at least a portion of the fasteners. Once such a portion is received, it and the receiving member are rotationally fast with each other. It will be appreciated by those skilled in the art that there are many shapes that a fastener may be, and an appropriately shaped receiving member must be selected for use with a particular fastener. Thus the receiving members may be removably connectable to the devices for effecting rotation to permit interchangeability of differently shaped receiving members.

[0068] The devices for controlling may include clutches which are configured to slip to maintain the difference in the torque output levels or other operation parameters within the predetermined value. The devices for sensing operation parameters may be in the form of angle or rotary encoders which send signals to the devices for effecting rotation. In use, the respective devices for effecting rotation either maintain, slow, stop, or speed up to regulate the difference in the torque output levels to within the predetermined value. Such a clutch mechanism may selectively couple and uncouple the cylinder and driving or other related portions of the respective tools. An actuator, operated by pressure of a working medium for pressing the clutch mechanism into engagement so that a torque can be transferred from the driving shaft to the driven shaft, would be needed. A control unit for controlling the pressure of the working medium supplied to the actuator clutch and for stopping the motor when the actuator clutch is disengaged and a working medium source for supplying the working medium to the actuator clutch would also be needed.

[0069] Note that other operation parameters may be used to regulate the apparatus including: hydraulic or pneumatic fluid pressures or flow rates; electrical circuit parameters such as current, voltage or magnetic field; rotation speeds of the devices for effecting rotation of the respective receiving members; or a combination of such. If the difference in the operation parameters exceed the predetermined value the device for controlling regulates the operation parameter of the respective devices for effecting rotation by either: lowering the operation parameter of the device with the higher operation parameter; raising the operation parameter of the device with the lower operation parameter; or both raising and lowering the operation parameter of the respective devices until the difference in the operation parameters returns to within the predetermined value.

[0070] Note that other regulation methods may be used, including turning the tools on and off manually or at a fixed or variable frequency until the difference in the operation parameters returns to within the predetermined value.

[0071] In another embodiment of the apparatus of the present invention motors, current detecting means and rotation angle detection means may be used. The current detecting means (e.g., an ammeter) senses current flowing to the motors and the rotation angle detecting means (e.g. a rotary encoder) senses relative rotation angles of the devices for effecting rotation. The device for controlling regulates the devices for effecting rotation to maintain the difference between the operation parameters within the predetermined value.

[0072] An operator may manage the apparatus of the present application by a device for managing the tightening or loosening of the fasteners. The device for managing may include a microcomputer having a CPU, a ROM, a RAM and an I/O. The ROM of the microcomputer stores a control program to automatically maintain the difference in the torque outputs or other operation parameters within a predetermined value. The device for managing may further include a memory. Note that an operator may set and store in the memory preset ranges of hydraulic or pneumatic fluid pressures or flow rates, electrical circuit parameters such as current, voltage or magnetic field, torque output, rotation speeds, a combination of such; or other parameters disclosed or known in the art.

[0073] The components of the device for managing and the apparatus in general may be connected communicably to each other. The memory of the management system may store the determination result transmitted from the communicating means. It should be appreciated that a plurality of management tasks may be performed, including: the simultaneous tightening or loosening of a plurality of fasteners; the simultaneous testing of a plurality of fasteners; determining the normality of tightening or loosening of the fasteners; storing of data of tightening, loosening and testing operations over a range of operation periods; and determining the extent of wear of components of the tightening and testing apparatus; etc.

[0074] Another embodiment of the apparatus may include a reaction adaptor and/or a reaction hub to tighten or loosen a plurality of fasteners.

Alternative Embodiments of the Placement and Quantity of the Reaction Adaptor.

[0075] Tool 100 may have a first and a second reaction adaptor. Generally discussion related to FIGs. 1-8 applies to this embodiment. The second reaction adaptor, similar to first reaction adaptor 150, has a third force-transmitting element, when engaged with tool 100, being rotatable about a piston axis of the tool; and a fourth force-transmitting element, when engaged with the third element, being either rotatable about, extensible and retractable along, and rotatable about and extensible and retractable along at least a distal portion of the third element.

Alternative Types of Tools Which May Utilize the Reaction Adaptors.

[0076] Torque power tools are known in the art and include those driven pneumatically, electrically, hydraulically, manually, by a torque multiplier, or otherwise powered. FIG. 9 shows a first hand-held torque power wrench 900_A and a second hand-held torque power wrench 900_B attached by a reaction adaptor 950, similar to that of reaction adaptor 750. First wrench 900_A has a housing 901_A which accommodates a motor 902_A driven pneumatically, electrically, hydraulically, manually, by a torque multiplier, or otherwise powered. Motor 902_A produces a turning force 990_A acting about a turning force axis B₉ in one direction 992_A which turns driving element 910_A and provides rotation of a corresponding fastener. First wrench 900_A may be provided with torque intensifying means (not shown) for increasing a torque output from motor 902_A to driving element 910_A. The torque intensifying means may be formed as planetary gears which are located in housing 901_A. Generally discussion related to first wrench 900_A applies to second wrench 900_B. Generally discussion related to reaction adaptor 750 applies to reaction adaptor 950.

Further Embodiments.

[0077] FIG. 10 shows a three-dimensional perspective view of tool 100 with a reaction adaptor 1050, an alternative embodiment of reaction adaptors of the present application. Generally all previous discussion applies to FIG. 10. Tool 100 tightens or loosens a fastener (not shown) during operation. Reaction adaptor 1050 transfers reaction force 191 to another fastener (not shown). It has a first force-transmitting element 1060 attachable to reaction support portion 114; a second force-transmitting element 1070 slidably attachable to first element 1060; and second element 1070 has a receiving member 1011 for receiving the other fastener.

[0078] First element 1060 includes a proximal portion 1061 formed of an annular polygonal body 1062 having a plurality of inner splines 1063, and a distal portion 1065 formed of a polygonal body 1066 having a substantially T-shaped track plate 1067. Second element 1070 includes a proximal portion 1071 formed of a polygonal body 1072 having a substantially C-shaped track plate 1073, and a distal portion 1075 formed of a cylindrical body 1076. First element 1060, when attached to reaction support portion 114, extends substantially collinear to and has a first force-transmitting axis A₅ substantially collinear to piston axis A₁. Second element 1070, when attached to first element 1060, extends substantially perpendicular to and has a second force-transmitting axis E₄ substantially perpendicular to first force-transmitting axis A₅.

[0079] First element 1060 is shown rotatably engaged with reaction support portion 114 in a first position. Note that reaction support portion 114 is away from turning force axis B₁ and reaction support portion 120. First element 1060 may be non-rotatably attached to reaction support portion 114 in numerous positions and held in place by a locking mechanism 1080 (not shown). Locking mechanism 1080 may include a bore and pin or other well known configuration like a spring loaded reaction clamp, a catch lever assembly or a fixed link pin with snap rings. First element 1060 is engageable and attachable separately, individually, and independently to tool 100. Inner splines 1063 are positioned circumferentially around the inside of annular body 1062 and extend radially inwardly toward central axis A₂. Annular body 1062 is of such inner width and annular body 115 is of such outer width that inner splines 1063 mesh with outer splines 116. Annular body 115 and proximal portion 1061 are part of additional connecting means. Reaction support portion 114 and first element 1060 are attachable to each other by attaching the additional connecting means. Axes A₁, A₂, and A₅ are substantially coaxial when first element 1060 and reaction support portion 114 are attached to each other and to tool 100.

[0080] Note that reaction support portion 114 has a height such that first element 1060, when engaged with tool 100, may be slid

along reaction support portion 114. In this variation, annular body 1062 may also have a height such that first element 1060 is extensible and retractable along reaction support portion 114.

[0081] Second element 1070 is shown slideably attached to first element 1060 in a second position and held in place by a locking mechanism 1081 (not shown). Locking mechanism 1081 may include a bore and pin or other well known configuration like a spring loaded reaction clamp, a catch lever assembly or a fixed link pin with snap rings. Additionally a set screw may be used to hold first element 1060 in place. Second element 1070 is engageable and attachable separately, individually, and independently to first element 1060. T-shaped track plate 1067 and C-shaped track plate 1073 are both complementary and of such dimensions that they mesh to form a slideable T&C connector. Note that other connector shapes may be used.

[0082] The hex socket and reaction adaptor 1050 are shown disassembled from tool 100. Tool 100 turns the fastener and reaction adaptor 1050 transfers reaction force 191 to the other fastener at an abutment pressure point during operation. Distal portion 1075 extends downward, substantially perpendicular to first element 1060 and receives the other fastener. Cylindrical body 1076 bears against the abutment pressure point on the walls of the other fastener as turning force 190 turns the hex socket on the fastener. This prevents the ratchet from rotating inwardly relative to the fastener. Thus the fastener is turned by the hex socket to a desired torque.

[0083] Driver 110 may rotate different fastener engagement means 111 depending on the fastener to be turned including: alien key; castellated or impact socket driver; hex reducer; square drive adaptor; or any other reasonable geometry or configuration. Similarly receiving member 1077 may be round, square, hexagonal or any reasonable geometry or configuration, depending on the fastener which absorbs reaction force 191. Receiving member 1077 may surround, engage or abut the other fastener. Receiving member 1077 may surround, engage or abut other structures to achieve an ideal abutment pressure point. Further receiving member 1077 either may be an abutment portion, polygonal or otherwise, a socket, an allen key or another type of fastener engagement means. Both tool 100 and reaction adaptor 1050 may include a tool pattern for mounting a handle for an operator.

[0084] Generally discussion related to the method of FIG. 4 applies to FIG. 10.

[0085] In step 412 of FIG. 4, second element 1070 is engaged with first element 1060 by bringing proximal portion 1071 substantially adjacent to distal portion 1065 and substantially aligning T-shaped track plate 1067 and C-shaped track plate 1073 to form a slideable T&C connector.

[0086] Tool 100 is prepared to turn the fastener about turning force axis B_1 with turning force 190 in the one direction 192. In step 414 of FIG. 4, tool 100 is positioned to receive the other fastener by sliding second element 1070 along distal portion 1065 to an extension length which corresponds to the proximity of the other fastener. In step 416 of FIG. 4, second element 1070 is attached to first element 1060 in the second position by activating locking mechanism 1081. Reaction adaptor 1050 is now in reaction force transfer position. In steps not shown in FIG. 4, socket 111 is attached to the driving element, and tool 100 is placed on the fastener to be turned.

[0087] Advantageously, first element 1060 is engageable and attachable separately, individually and independently to tool 100 and second element 1070 is engageable and attachable separately, individually and independently to first element 1060. Portability of tool 100 is maximized while weight of tool 100 is minimized. Commercially available reaction fixtures may be used with or in replacement of portions of first and second elements 1060 and 1070, rather than custom reaction fixtures, thereby reducing costs and increasing safety. Reaction adaptor 1050 is adjustable to minimize twisting and fastener-bending forces so as to avoid tool 100 from jumping off of the job or from failing. Reaction adaptor 1050, when engaged with tool 100, is adjustable to surround, engage or abut against viable fasteners or stationary objects at the ideal abutment pressure point. Reaction adaptor 1050, when attached to tool 100, transfers reaction force 191 to the ideal abutment pressure point during operation. Operators no longer need several tools at the workstation each having a reaction fixture oriented differently to abut against viable stationary objects for each application. Nor do operators need to completely disassemble tool 100, reposition reaction adaptor 1050 and reassemble tool 100 for each application.

[0088] FIG. 11 shows a three-dimensional perspective view of a tool 1100 with a reaction adaptor 1150, alternative embodiments of tools and reaction adaptors of the present application. Tool 1100 may be a limited clearance hydraulic torque multiplier and/or tension tool. Generally all previous discussion applies to FIG. 11.

[0089] Tool 1100, as configured, tightens or loosens a fastener (not shown), likely an allen bolt, during operation. A driver 1110 may rotate different fastener engagement means 1111 depending on a fastener to be turned including: allen; castellated or

impact socket driver; hex reducer; square drive adaptor; or any other reasonable geometry or configuration.

[0090] Reaction adaptor 1150, transfers reaction force 1191 to another fastener (not shown). It has a first force-transmitting element 1160 attachable to a reaction support portion 1114; a second force-transmitting element 1170 slideably attachable to first element 1160; and second element 1170 has receiving member 1177 for receiving the other fastener.

[0091] First element 1160 includes a proximal portion 1161 formed of a polygonal body 1162 having a recess or removed portion 1163, and a distal portion 1165 formed of a polygonal body 1166. A substantially T-shaped track plate 1167 runs along first element 1160 encompassing most of proximal portion 1161 and all of distal portion 1166. Second element 1170 includes a proximal portion 1171 formed of a polygonal body 1172 having a substantially C-shaped track plate 1173, and a distal portion 1175 formed of a polygonal or cylindrical body 1176 with a receiving member 1177. First element 1160, when attached to tool 1100, extends the length of reaction support portion 1114. In this example, first element 1160 extends from reaction support portion 1114 such that first element 1160 extends substantially at an angle of 135° to reaction support portion 1114. Receiving member 1177 is substantially coplanar with driver 1110. First element 1160 may substantially extend at an angle of 45° - 180° to reaction support portion 1114 and have a first force-transmitting axis substantially along itself. Second element 1170, when attached to first element 1160, extends substantially perpendicular to and has a second force-transmitting axis substantially perpendicular to the first force-transmitting axis.

[0092] First element 1160 is shown attached to reaction support portion 1114 in a first position. Note that reaction support portion 1114 is away from the turning force axis. First element 1160 may be attached to reaction support portion 1114 in numerous user chosen positions and held in place by a locking mechanism 1180 (not shown). Locking mechanism 1180 may include a bore and pin or other well known configuration like a spring loaded reaction clamp, a catch lever assembly or a fixed link pin with snap rings. Additionally a set screw may be used to hold first element 1160 in place. First element 1160 is engageable and attachable separately, individually, and independently to tool 1100. Recess 1163 receives part of reaction support portion 1114, both of which are part of additional connecting means. Reaction support portion 1114 and first element 1160 are attachable to each other by attaching the additional connecting means. First element 1160, when engaged with tool 1100, may be slid along reaction support portion 1114 depending on the length of first element 1160 and the angle and length of recess 1163.

[0093] Second element 1170 is shown slideably attached to first element 1160 in a second position. Second element 1170 is engageable and attachable separately, individually, and independently to first element 1160. T-shaped track plate 1167 and C-shaped track plate 1173 are both complementary and of such dimensions that they mesh to form a slideable T&C connector. Note that other connector shapes maybe used.

[0094] Receiving member 1177 may be round, square, hexagonal or any reasonable geometry or configuration, depending on the other fastener, the fastener which absorbs reaction force 1191. Receiving member 1177 may surround, engage or abut the other fastener. Receiving member 1177 may surround, engage or abut other structures to achieve an ideal abutment pressure point. Further receiving member 1177 either may be an abutment portion, polygonal or otherwise, a socket, an allen key or another type of fastener engagement means. Both tool 1100 and reaction adaptor 1150 may include a tool pattern for mounting a handle for a user.

[0095] Advantageously, first element 1160 is engageable and attachable separately, individually and independently to tool 1100 and second element 1170 is engageable and attachable separately, individually and independently to first element 1160. Portability of tool 1100 is maximized while weight of tool 1100 is minimized. Commercially available reaction fixtures may be used with or in replacement of portions of first and second elements 1160 and 1170, rather than custom reaction fixtures, thereby reducing costs and increasing safety. Reaction adaptor 1150 is adjustable to minimize twisting and fastener-bending forces so as to avoid tool 1100 from jumping off of the job or from failing. Reaction adaptor 1150, when engaged with tool 1100, is adjustable to surround, engage or abut against viable fasteners or stationary objects at the ideal abutment pressure point. Reaction adaptor 1150, when attached to tool 1100, transfers reaction force 1191 to the ideal abutment pressure point during operation. Operators no longer need several tools at the workstation each having a reaction fixture oriented differently to abut against viable stationary objects for each application. Nor do operators need to completely disassemble tool 1100, reposition reaction adaptor 1150 and reassemble tool 1100 for each application.

Combinations and Variations of All Embodiments and Modes.

[0096] Combinations and variations of all of embodiments and modes discussed in relation to FIGs. 1-11 may find useful applications. In one combination and variation, for example, a tool similar to tool 900_A is attached to a tool similar to tool 100 by a

first reaction adaptor similar to reaction adaptors 750 and/or 950 and a second reaction adaptor similar to reaction adaptor 850 is attached to tool 100 at reaction support portion 114. In another combination and variation, for example, a first and a second tool similar to tool 900_A and a third and a fourth tool similar to tool 100 are attached to a reaction hub by a first, a second, a third and a fourth reaction adaptor similar to reaction adaptors 750 and/or 950. Further, a fifth and a sixth tool similar to tool 100 are attached to the third and fourth tools by a fifth and a sixth reaction adaptor similar to reaction adaptors at the reaction support portions of tools. In such combinations and variations, a plurality of tool types may be used with a plurality of reaction adaptor and hub types. In additional combination and variations, multiple force-transmitting elements may be utilized by reaction adaptors similar to reaction adaptors 150, 350, 750, 950, 1050, 1150 and the reaction hub and by tools similar to tools 100 and 900. Indeed, elaborate and complex tool, reaction adaptor and force-transmitting elements, etc. combinations may be utilized as the need arises. Note that discussion related to FIGs. 7 and 8 are applicable to these combinations and variations of all embodiments and modes.

Miscellaneous Information.

[0097] Reaction adaptors, tools, and other force-transmitting components of the present application may be made from any suitable material such as aluminum, steel, or other metal, metallic alloy, or other alloy including non-metals. Tools of the present application may have: load bolt sizes from 12,7 to 203,3 mm (½ in. to 8 in.); have drive sizes from 12,7 to 203,3 mm (½" to 8 in.); have hex sizes from 12,7 to 203,3 mm (½" to 8"); have torque output ranges of 135,5 to 54232,7 Nm (100 ft.lbs. to 40,000 ft.lbs); bolt load ranges of 4536 to 680400 kg (10,000 lbs. - 1,500,000 lbs.); and have operating pressures from 103,42 to 689,475 bar (1,500 psi to 10,000 psi). Tools of the present application may include Tension, Torque-Tension, and Torque machines, and may include those driven pneumatically, electrically, hydraulically, manually, by a torque multiplier, or otherwise powered. Dimensions of reaction adaptors of the present application may range from 76 x 25,4 x 63,5 mm (3 in. x 1 in. x 2.5 in.) to 609 x 203,2 x 609 mm (24 in. x 8 in. x 24 in.) and weigh from 1,3 to 226,8 kg (3 lbs. to 500 lbs). Dimensions of tools of the present application may range from 152,4 x 50,8 x 127 mm (6 in. x 2 in. x 5 in.) to 584,2 x 304,8 x 355,6 mm (23 in. x 12 in. x 14 in.) and weigh from 1,3 to 226,8 kg (3 lbs. to 500 lbs). Note that reaction adaptors and tools of the present application may substantially diverge, both positively and negatively, from these representative ranges of dimensions and characteristics.

[0098] Note that reaction adaptors and apparatus of the present application may be used with different types of fasteners including screws, studs, bolts, stud and nut combinations, bolt and nut combinations, allen bolts, and any other geometries and configurations of fasteners known in the art. Further fasteners may have engagement means which protrude from, are flush with or are recessed from its end face, or are shaped as caps, discs, cups, tool engagement means, feet, and other rotatable structures of varying dimensions and geometries.

REFERENCES CITED IN THE DESCRIPTION

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- US6260443B [0009]

Patentkrav

1. Indretning til at fastspænde eller løsne fastgørelsesmidler (131, 731), omfattende:

5 et første og et andet optagelsesled (111, 711), som er roterbart lejret i indretningen, til optagelse af et første og et andet fastgørelsesmiddel (131, 731); en første og en anden anordning udført som et første og et andet kraftdrevet drejningsmomentværktøj (100, 700) til fremkaldelse af rotation af de respektive optagelsesled (111, 711) til at fastspænde eller løsne de respektive fastgørelsesmidler (131, 731); hvor anordningerne til fremkaldelse af rotation enten er pneumatisk eller hydraulisk drevne,
10 en anordning til styring af en driftsparameter af hver anordning til fremkaldelse af rotation for at fastholde en forskel mellem driftsparametrene inden for en forudbestemt værdi, hvilke driftsparametre omfatter enten hydrauliske eller pneumatiske væsketryk eller strømningsrater, elektriske kredsløbsparametre såsom strøm, spænding eller magnetisk felt, værdier af den afgivne effekt af drejningsmoment, rotationshastigheder eller en kombination deraf,
15 hvor under driften, hvis forskellen i driftsparametrene overstiger den forudbestemte værdi, anordningen til styring regulerer driftsparameteren af de respektive anordninger til fremkaldelse af rotation ved enten sænkelse af driftsparameteren af anordningen med den højere driftsparameter, forøgelse af driftsparameteren af anordningen med den lavere driftsparameter eller både forøgelse og sænkelse af driftsparameteren af de respektive anordninger, indtil forskellen i driftsparametrene vender tilbage til inden for den forudbestemte værdi,

25 **kendetegnet ved, at** anordningerne til fremkaldelse af rotation (100, 700) er forbundet, hvilket forbindelsesmiddel omfatter:

et første kraftoverførende element (160), som kan fastgøres roterbart omkring en drejekraftakse (B1) af den første anordning til fremkaldelse af rotation (100);

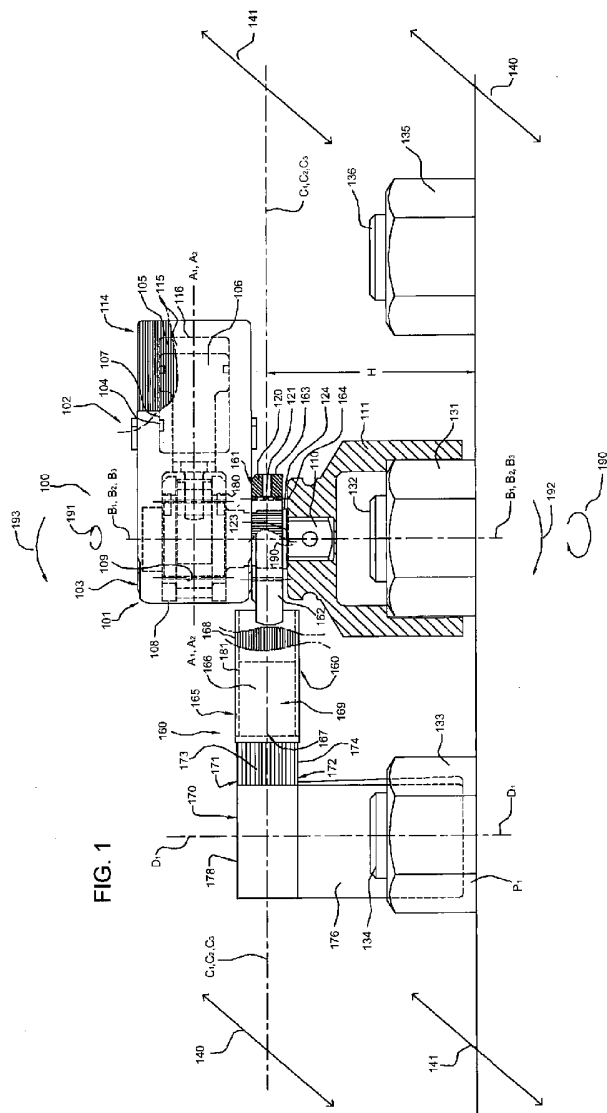
30 et andet kraftoverførende element (770), som kan fastgøres roterbart omkring en drejekraftakse (B4) af den anden anordning til fremkaldelse af rotation (700); og

35 hvor det andet kraftoverførende element (770) enten kan fastgøres roterbart omkring, kan fastgøres udtrækkeligt og tilbagetrækkeligt langs eller kan fast-

gøres roterbart omkring og kan fastgøres udtrækkeligt og tilbagetrækkeligt langs mindst en distal del af det første kraftoverførende element (160).

- 5 **2.** Indretning ifølge krav 1, hvor anordningen til styring omfatter en anordning til registrering af driftsparameteren.
- 10 **3.** Indretning ifølge krav 1 eller 2, hvor driftsparameteren er den afgivne effekt af drejningsmoment, og hvor under driften, hvis forskellen i de afgivne effekter af drejningsmoment overstiger den forudbestemte værdi, anordningen til styring regulerer den afgivne effekt af drejningsmoment af de respektive anordninger til fremkaldelse af rotation ved enten sænkelse af den afgivne effekt af drejningsmoment af anordningen med den højere afgivne effekt af drejningsmoment, forøgelse af den afgivne effekt af drejningsmoment af anordningen med den lavere afgivne effekt af drejningsmoment eller både forøgelse og sænkelse af de afgivne effekter af drejningsmoment af de respektive anordninger, indtil forskellen i de afgivne effekter af drejningsmoment vender tilbage til inden for den forudbestemte værdi.
- 15 **4.** Indretning ifølge krav 1, 2 eller 3, hvor anordningerne til fremkaldelse af rotation samtidigt fastspænder eller løsner fastgørelsesmidlerne (131, 731).
- 20 **5.** Indretning ifølge krav 1, 2, 3 eller 4, hvor en første og en anden reaktionsdrejekraft af den første og den anden anordning til fremkaldelse af rotation er i det væsentlige er ophævet.
- 25 **6.** Indretning ifølge krav 1, 2, 3, 4 eller 5, omfattende en anordning til styring af fastspænding eller løsning af fastgørelsesmidlerne (131, 731), omfattende en anordning til kommunikation mellem anordningerne til fremkaldelse af rotation og anordningen til styring.
- 30

DRAWINGS



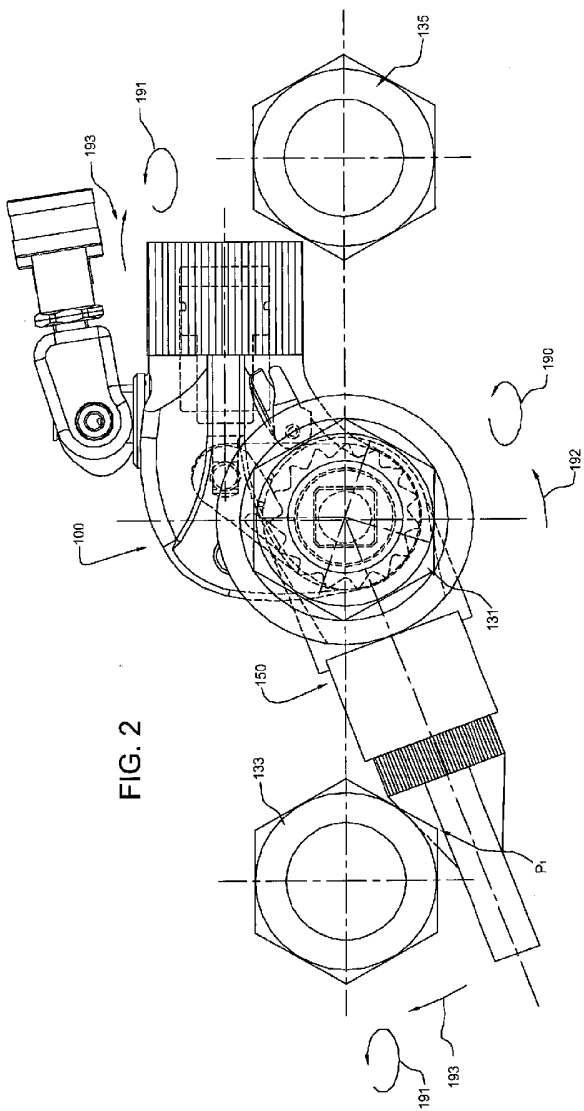
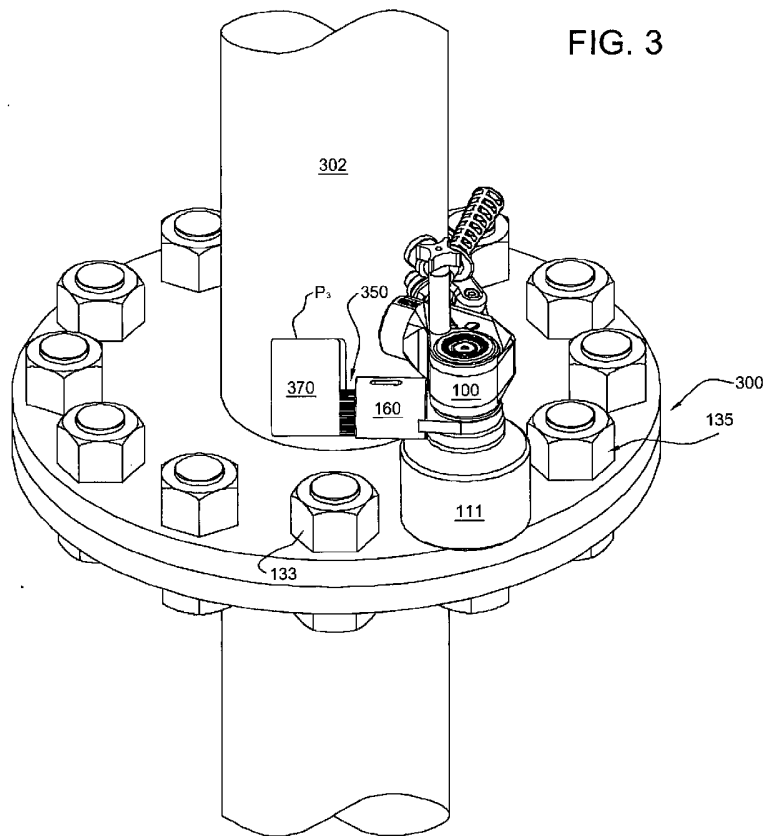


FIG. 3



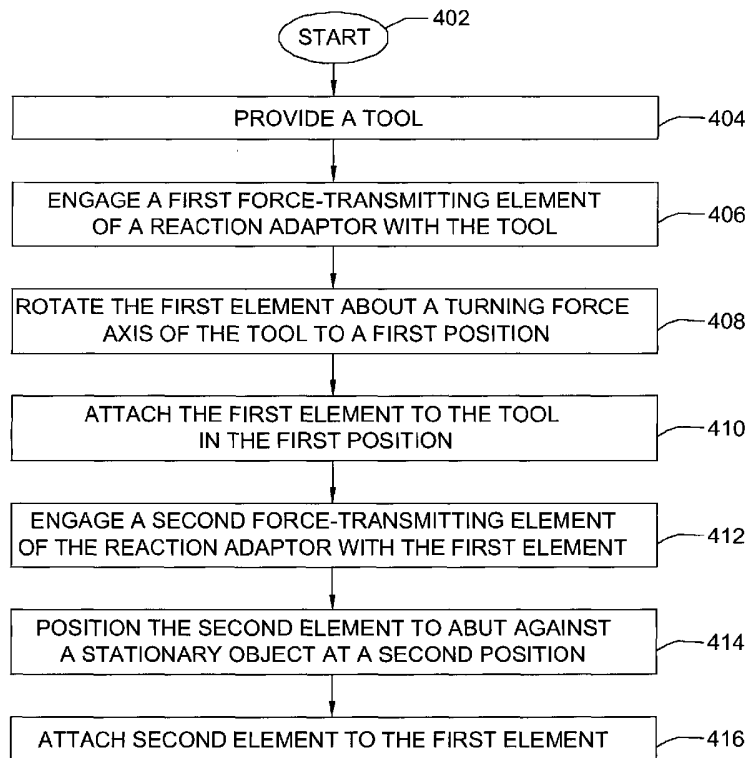


FIG. 4

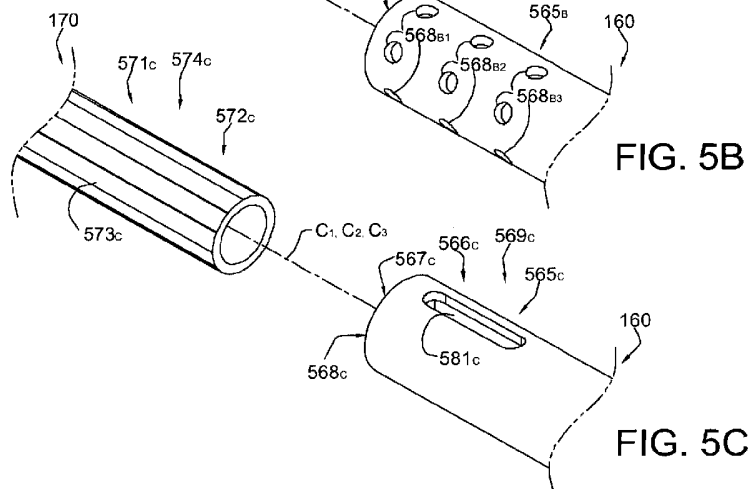
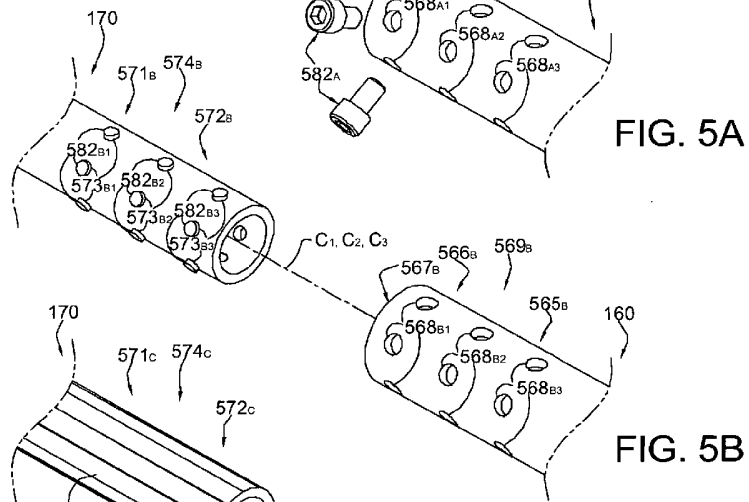
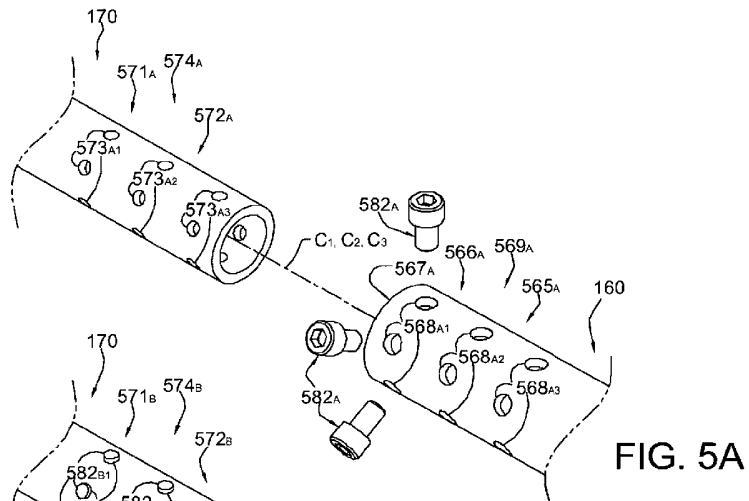
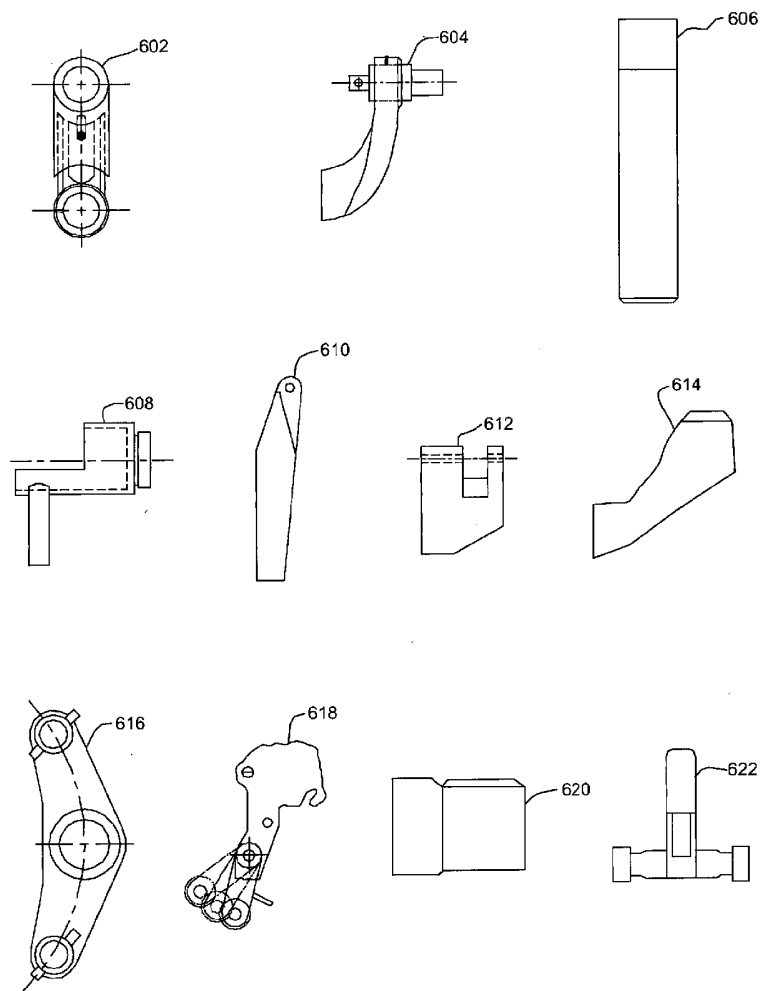
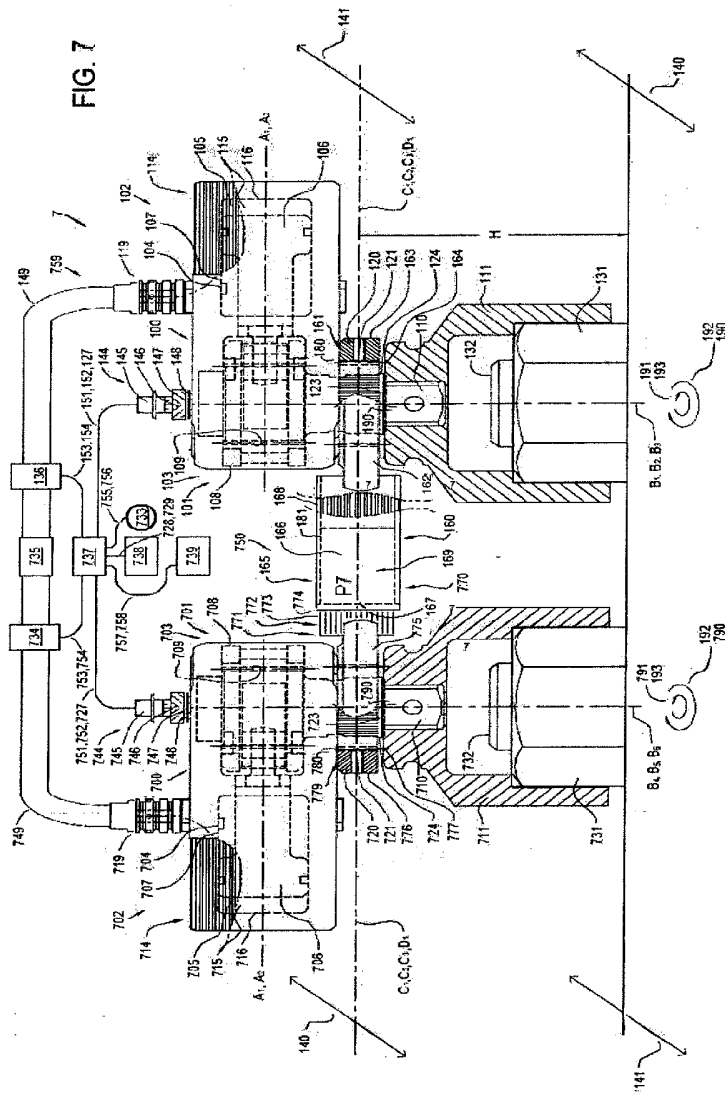
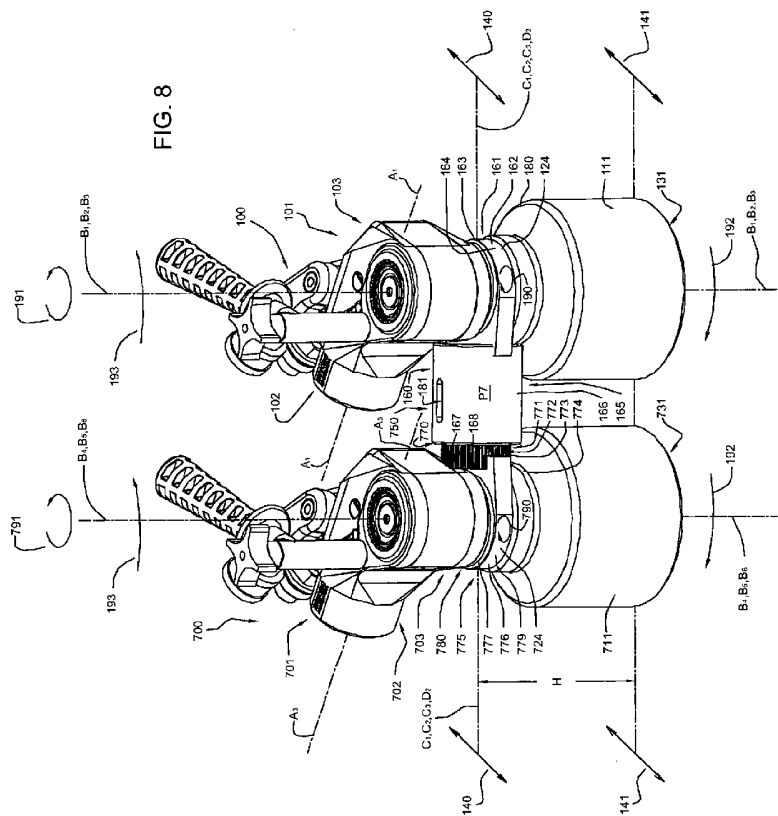


FIG. 6







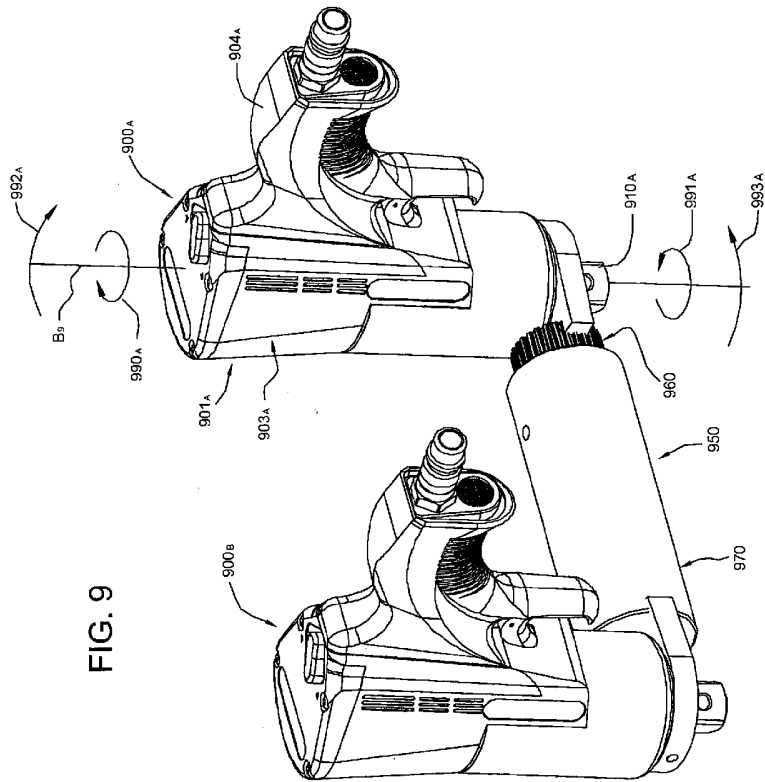


FIG. 9

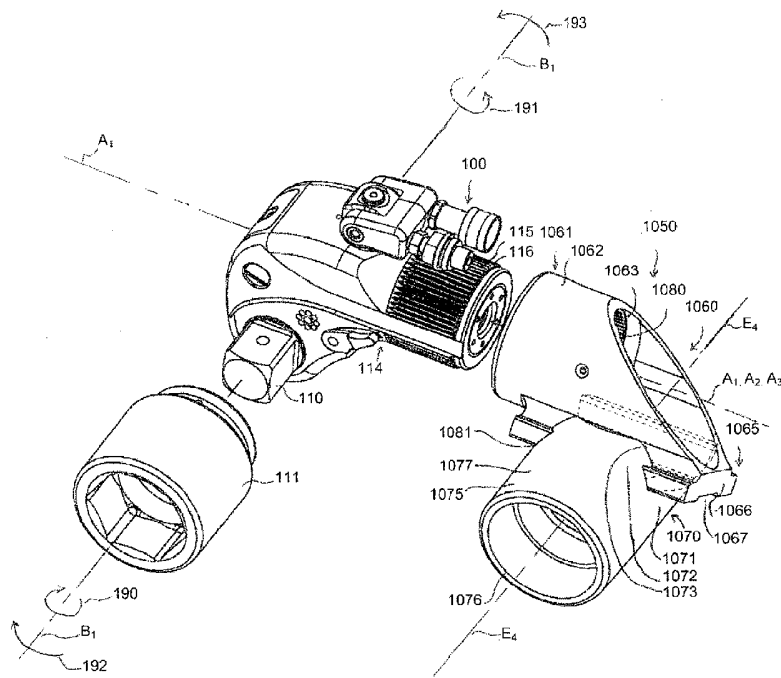


FIG. 10

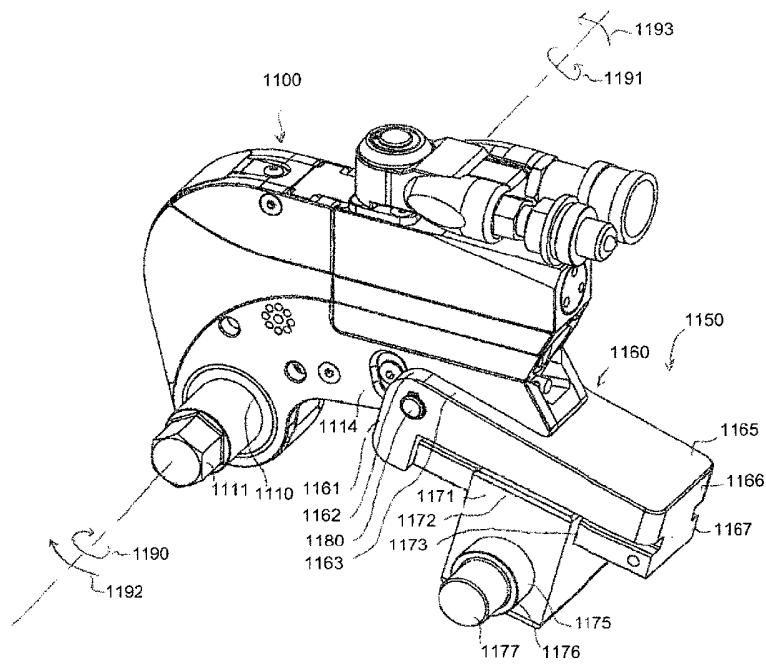


FIG. 11