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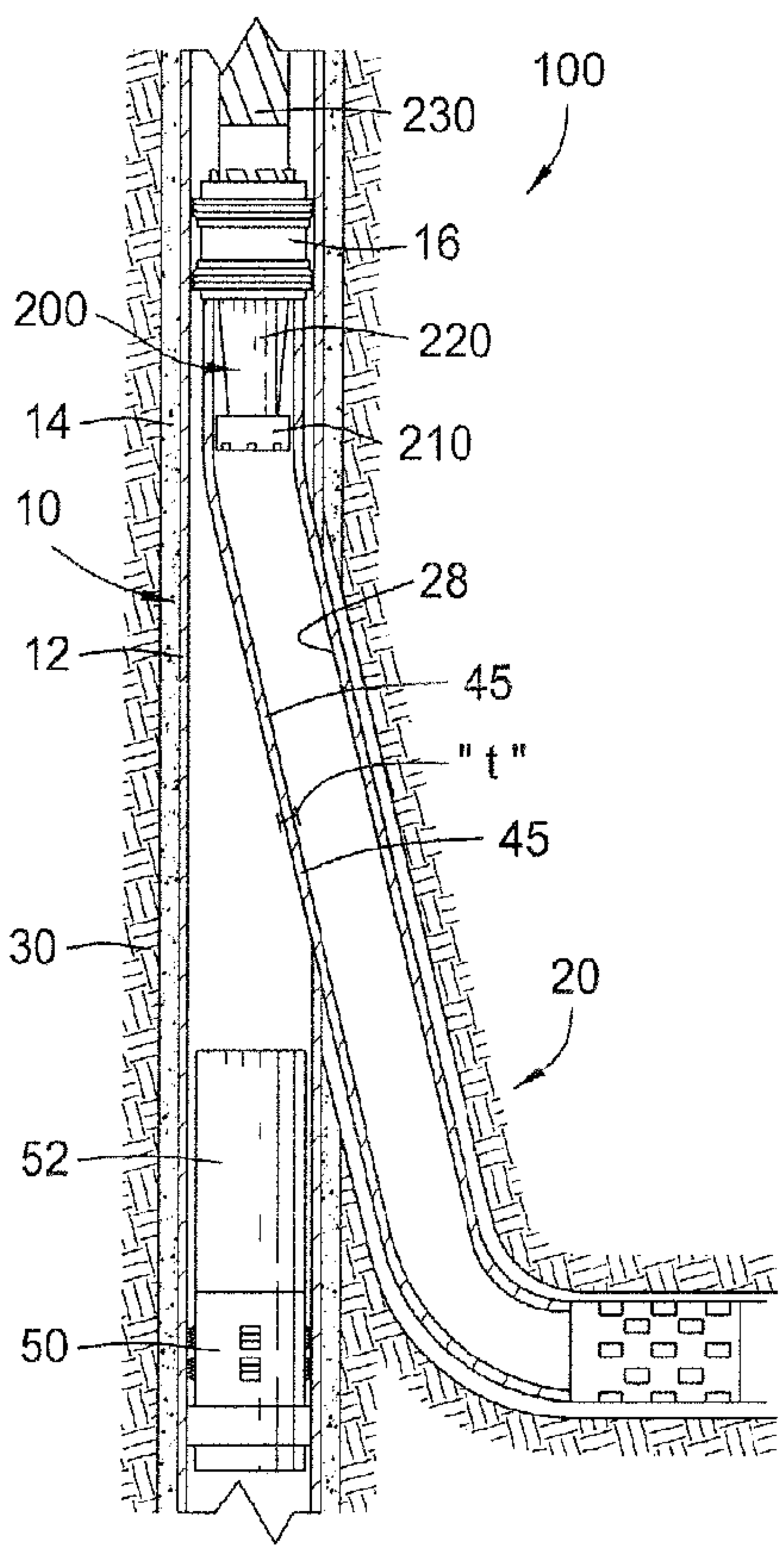
(54) Titre : METHODE DE DEVELOPPEMENT D'UNE REENTREE DANS UN PUITS PRINCIPAL A PARTIR D'UN PUITS LATERAL, ET ENSEMBLE DE FOND DE PUITS POUR LE FRAISAGE

(54) Title: METHOD OF DEVELOPING A RE-ENTRY INTO A PARENT WELLBORE FROM A LATERAL WELLBORE, AND BOTTOM HOLE ASSEMBLY FOR MILLING



(57) Abrégé/Abstract:
A method is provided that allows the operator to re-enter a primary wellbore from a lateral wellbore after the lateral wellbore has been completed. The method generally comprises the steps of locating a cutting device such as a milling bit adjacent a tubular

(57) Abrégé(suite)/Abstract(continued):

such as a liner within a wellbore, rotating the milling bit while maintaining an axial position of the milling bit relative to the liner to initiate an opening, and rotating and axially advancing the milling bit to complete the opening. In addition, a bottom hole assembly that facilitates re-entry into the primary wellbore from a lateral wellbore is provided. The bottom hole assembly generally includes a drill collar or other heavy pipe structure, and a mill. The mill has a body and cutting structures. The cutting structures apply lateral force against a surrounding pipe to form an initial lip through the wall of the pipe.

ABSTRACT OF THE DISCLOSURE

A method is provided that allows the operator to re-enter a primary wellbore from a lateral wellbore after the lateral wellbore has been completed. The method generally comprises the steps of locating a cutting device such as a milling bit adjacent a tubular such as a liner within a wellbore, rotating the milling bit while maintaining an axial position of the milling bit relative to the liner to initiate an opening, and rotating and axially advancing the milling bit to complete the opening. In addition, a bottom hole assembly that facilitates re-entry into the primary wellbore from a lateral wellbore is provided. The bottom hole assembly generally includes a drill collar or other heavy pipe structure, and a mill. The mill has a body and cutting structures. The cutting structures apply lateral force against a surrounding pipe to form an initial lip through the wall of the pipe.

METHOD OF DEVELOPING A RE-ENTRY INTO A PARENT WELLBORE FROM A LATERAL WELLBORE, AND BOTTOM HOLE ASSEMBLY FOR MILLING

BACKGROUND OF THE INVENTION

Field of the Invention

Embodiments of the present invention generally relate to the practice of sidetrack drilling for hydrocarbons. More specifically, this invention pertains to a method of developing a re-entry into a parent wellbore from a lateral wellbore. The present invention also relates to a bottom hole assembly for providing re-entry into a parent wellbore.

Description of the Related Art

In recent years, technology has been developed which allows an operator to drill a primary vertical well, and then drill an angled lateral borehole off of the primary well at a chosen depth. Generally, the primary vertical wellbore is first cased with a string of casing and cemented. Then a tool known as a whipstock is positioned in the casing at the depth where deflection is desired. The whipstock is specially configured to divert milling bits and then a drill bit in a desired direction for forming a lateral borehole. This process is sometimes referred to as sidetrack drilling.

Figures 1A-1G present sequential steps for one known method of forming a lateral wellbore. **Figure 1A** presents a partial cross-sectional view of a wellbore **100**. The wellbore **100** in this initial step comprises only a primary wellbore **10**. The primary wellbore **10** is an essentially vertically formed wellbore extending downward through the earth formation **30**. The primary wellbore, or "parent" wellbore **10**, is lined with generally tubular casing **12**. A cement column **14** fills an annular area radially between the casing **12** and the earth **30**.

An anchoring device **50** such as an anchor-packer has been set in the primary wellbore **10**. The packer **50** grippingly engages the surrounding casing **12**, enabling the packer **50** to act as an anchor against which tools above it may be urged to activate different tool functions. The illustrative packer **50** of **Figure 1A** includes an orientation indicating member **52** secured at its top. The orientation indicating member's **52** orientation is checked by running a tool such as a gyroscope indicator or measuring-while-drilling device into the primary wellbore **10**.

A whipstock **40** has also been run into the wellbore **100**. The whipstock **40** preferably has a stinger **74** (see **Figure 1F**) located at the bottom of the whipstock **40**. The stinger engages the orientation indicating member **52** of the packer **50**. In one procedure, splined connections between the stinger and the orientation indicating member facilitate correct stinger orientation. The stinger allows a concave face **42** of the whipstock **40** to be oriented so as to direct the milling operation in the proper azimuth. In this way, the whipstock **40** is oriented onto the packer **50** so that the upper concave face **42** is downwardly inclined in a desired direction for milling a window **18** through the casing **12** and for drilling the lateral wellbore **20**.

A working string **70** has also been lowered into the wellbore **100**. The working string **70** may be coiled tubing, drill collars, or other tubular member. A pilot mill **72** is shown attached to a bottom end of the working string **70**. The pilot mill **72** includes blades around a radial body of the mill **72** for engaging and cutting the casing **12**. In this respect, the milling bit **72** is lowered into the parent wellbore **10** and urged against the upper face **42** of the whipstock **40**, thereby forcing the milling bit **72** to deflect in the desired direction to form a window through the casing **12** and the cement **14**.

In one illustrative procedure, the whipstock **40** includes an upper pilot lug **41**. The working string **70** lowers the milling bit **72** and the whipstock **40** into the primary wellbore **10** together by means of a temporary connection with the pilot lug **41**. **Figure 1A** shows a shearable setting stud **43** between the pilot mill **72** and the pilot lug **41**. In this way, the need for separate trips for running various tools is avoided.

U.S. Patent No. 6,112,812 discloses a mill which is releasably secured at the top of the whipstock, e.g. with a shearable setting stud connected to a pilot lug on the whipstock. The mill and whipstock can then be lowered into the wellbore together. Rotation of the string rotates the mill, and causes shearing of the connection with the whipstock. In addition, U.S. Patent No. 6,695,056 provides methods for single-trip milling and drilling of a window and lateral wellbore.

Figure 1B shows a next step in the formation of a lateral wellbore 20, in one embodiment. Here, the milling bit 72 is being urged against the whipstock 40 so as to frictionally engage the surrounding casing 12. Rotation of the string 70 with the pilot mill 72 rotates the mill 72, causing the connection, e.g., a single bolt shear lug (not shown), with the whipstock 40 to be sheared. The mill 72 is moved downwardly while contacting the pilot lug 41 and then the concave face 42. This urges the starting mill 72 into contact with the casing 12. Milling of the casing 12 is achieved by rotating the tool 72 against the inner wall of the casing 12 while at the same time exerting a downward force on the drill string 70 against the concave face 41 of the whipstock 40. In Figure 1B, the milling bit 72 has breached the surrounding casing 12 of the primary wellbore 10. The milling bit 72 will continue to work against the casing 12 until a window 18 begins to be formed.

It is not uncommon for the operator to deploy a series of milling bits during a window formation operation. Figure 1C shows that the original milling bit 72 has been removed from the wellbore 10, and that the working string has been again run into the primary wellbore 10, but with a new milling bit 72' disposed at its end. In addition, a watermelon mill 75 is optionally placed along the working string 70 above the second milling bit 72'. Thus, a fuller window 18 may be formed. The milling bits 72', 76 are rotated until a window 18 is fully formed in the surrounding casing 12 of the primary wellbore 10. The formed window 18 is commonly elliptical, and is dimensioned to allow a drill bit 78 (seen in Figure 1D) to then be run through the formed window 18 and engaged with the formation 30. In this way, a new lateral wellbore 20 may be formed.

After the window 18 has been formed, the working string 70 and connected mill 72 are pulled from the primary wellbore 10. Thereafter, the working string 70 is again run into the wellbore 100, but with a drilling assembly. The drilling assembly includes a formation drill bit 78. The drill bit 78 is run into the lateral wellbore 20 for drilling of the formation. **Figure 1D** shows this next sequential step in the formation of a lateral wellbore **20**.

When the desired length of the lateral wellbore **20** is achieved, a generally tubular liner **28** (seen in **Figure 1G**) is inserted into the casing **12**. The liner **28** is lowered through the parent wellbore **10**, deflected radially outward through the window **18**, and positioned appropriately within the lateral wellbore **20**. A curvature **45** is formed in the liner **28** at the intersection of the primary wellbore **10** and the lateral wellbore **20**.

In one procedure, deflection of the liner **28** into the lateral wellbore **20** is by means of the whipstock **20**. This procedure is demonstrated in U.S. Patent No. 5,803,176, entitled "Sidetracking Operations," issued in 1998 to William A. Blizzard, Jr. *et al.* The '176 patent was a continuation-in-part of Ser. No. 642,118 dated May 2, 1996, which in turn was a continuation-in-part of Ser. No. 590,747 dated January 24, 1996. Ser. No. 590,747 issued on March 17, 1998 as U.S. Patent No. 5,727,629, also to William A. Blizzard, Jr. *et al.* The '629 patent is entitled "Wellbore Milling Guide and Method." A softer central core material (not shown) may fill the tubular body of the whipstock **40**. In this way, the central core of the whipstock may be drilled out for access to the primary wellbore **10** below the window **18**.

In an alternate procedure, a bent joint or hydraulic kick-over joint (not shown) is placed at the bottom of the liner string **28**. The joint is biased to exit the window **18** upon reaching the depth of the window **18**. This allows the liner **28** to be placed in the wellbore **100** without need of the whipstock **20** (or other deflector). Thus, in more recent procedures the whipstock **20** is pulled before the liner **28** is run into the wellbore **100**.

Figure 1E shows the working string **70** having been pulled from the wellbore **100**. A new working string **80** is being lowered into the primary wellbore **10**. The working string **80** may be coiled tubing, wireline, or other known string. A fishing hook **82** is disposed at an end of the working string **80**. The purpose of the fishing hook **82** is to retrieve the whipstock **40** from the primary wellbore.

Figure 1F shows the fishing hook **82** engaging the whipstock **40**. The whipstock **40** is now being pulled from the packer **50** and attached orientation member **52**.

In **Figure 1G** it can be seen that the whipstock **40** has been removed from the parent wellbore **10**. Where a whipstock is not maintained in the primary wellbore **10**, a kick-out sub or other tool (not shown) may be used to urge the liner **28** through the window **18**. The liner **28** is placed at the intersection of the parent wellbore **10** and the lateral wellbore **20**. The liner **28** may be secured against displacement relative to the casing **12** by a conventional liner hanger, shown at **16**. The liner hanger **16** is attached to the liner **28** and grippingly engages the casing **12** of the parent wellbore **10** above the window **18**. In the completion of **Figure 1G**, the liner **28** is not cemented into place. However, it is understood that the liner **28** may be sealed within the casing **12** of the parent wellbore **10**, the earth formation **30**, and the lateral wellbore **20** by injecting cement **25** into the liner **28**, and then squeezing the cement back upwards into the annular areas surrounding the liner **28**. In this way, a cement column is formed around the liner **28**.

It may be readily seen that an upper portion of the liner **28** overlaps the casing **12** above the window **18**. In this manner, fluid, tools, tubing, and other equipment (not shown) may be conveyed downward from the earth's surface, through an upper portion **6** of the parent wellbore **10**, into an upper portion **4** of the liner **28**, and thence through the window **18** and into the lateral wellbore **20**. The lateral wellbore **20** portion of the subterranean well **100** may, thus, be completed (i.e., perforated, stimulated, gravel packed, etc.).

In the completion of **Figure 1G**, the liner **28** includes a slotted liner **27**. However, this is purely for purposes of illustration. A solid tubular for later perforation could alternatively be employed. In addition, the liner **28** is preferably cemented into the lateral wellbore **20** by a column of cement. In addition, it is understood that other methods of milling a window and forming a lateral wellbore are known. The steps of **FIGS. 1A-1G** are illustrative, and the methods of the present invention are not limited by the steps taken to form the lateral wellbore or to install a liner **28**.

It is known to re-enter the primary wellbore **10** below the window **18** by milling out a portion of the liner **28**. U.S. Patent No. 6,202,752 entitled "Wellbore Milling Methods" discloses one such method. The '752 patent issued to Kuck, et al., in 2001, applies weight to the drill string to cause axial movement during milling. Before that, U.S. Patent No. 5,803,176 entitled "Sidetracking Operations" was issued. That patent issued to Blizzard, Jr., et al., in 1998. Blizzard, Jr. employed various versions of a mill guide during milling. However, a need yet exists for an improved method that allows the operator to re-enter the primary wellbore from the lateral wellbore. In addition, a need exists for a bottom hole assembly that facilitates re-entry into the primary wellbore.

SUMMARY OF THE INVENTION

The present invention generally provides a method that allows the operator to re-enter a primary wellbore after a lateral wellbore has been completed. In addition, the present invention provides for a bottom hole assembly that facilitates re-entry into the primary wellbore from a lateral wellbore.

In one embodiment, the method generally comprises the steps of locating a cutting device such as a milling bit adjacent a tubular such as a liner within a wellbore, rotating the milling bit while maintaining an axial position of the milling bit relative to the liner to initiate an opening, and then rotating and axially advancing the milling bit to complete the opening. In one embodiment of the method, the milling bit is used to form an opening within a liner at the intersection between a primary wellbore and a lateral wellbore. The milling bit is run into the primary wellbore at the end of a working string, and is located at a point along the curvature of the liner. The milling bit may then be rotated until the liner is entirely breached, thereby forming a lip. Thereafter, the milling bit is axially advanced and rotated to form the re-entry path the in the primary wellbore.

In one arrangement, the method further comprises the step of applying a lateral pressure through the milling bit against the curvature of the liner while rotating the milling bit to initiate the opening. This lateral pressure is directed through the milling bit against the curvature of the liner by a moment force generated by stiffness within the bottom hole assembly. A hydraulically actuated centralizing mechanism may also be used to provide lateral pressure.

In another embodiment of the method, an additional step of reciprocating the milling bit along a length of the curvature of the liner while rotating the milling bit is provided. This step is practiced prior to the step of rotating the cutting device while maintaining an axial position of the cutting device relative to the wall, thereby shaving an inner portion of the liner.

In addition, a bottom hole assembly that facilitates re-entry into the primary wellbore from a lateral wellbore is provided. The bottom hole assembly generally includes a drill collar, a sub connected to the drill collar, and a lead mill. The lead mill has a body connected to the sub, and blades. The blades are dimensioned to increase lateral contact pressure between the blades and the surrounding tubular.

In one arrangement, the sub has an outer diameter that is smaller than the outer diameter of cutting blades along the lead mill. The outer diameter of the sub is preferably tapered to become smaller from the drill collar to the lead mill.

In one arrangement, the bottom hole assembly includes an angled tool joint to create additional deflection of the mill against the liner. The angled tool joint may be a bent sub, a bent extension sub, or a bent upper mill. Alternatively, the lead mill may have a cutting structure that is eccentrically arranged. The eccentric arrangement will increase the lateral load on the surrounding liner by amplifying the deflection of the mill against the liner during rotation.

BRIEF DESCRIPTION OF THE DRAWINGS

So that the manner in which the above recited features of the present invention can be understood in detail, a more particular description of the invention, briefly summarized above, may be had by reference to embodiments, some of which are illustrated in the appended drawings. It is to be noted, however, that the appended drawings illustrate only typical embodiments of this invention and are therefore not to be considered limiting of its scope, for the invention may admit to other equally effective embodiments.

Figures 1A-1G present sequential steps of one known method for forming a lateral wellbore.

Figure 1A presents a partial cross-sectional view of a wellbore. The wellbore in this initial step comprises only a primary wellbore. The primary wellbore is an essentially vertically formed wellbore extending downward through the earth formation.

Figure 1B shows the next sequential step in the formation of a lateral wellbore, in one embodiment. Here, a milling bit is being urged against the concave face of a whipstock so as to frictionally engage the surrounding casing.

Figure 1C demonstrates that the original milling bit has been removed from the wellbore, and a working string has been run into the primary wellbore with a new milling bit. In addition, a watermelon mill is placed along the working string above the second milling bit.

Figure 1D again shows a cross-sectional view of the wellbore of Figure 1A. Here, a drilling assembly including a formation drill bit has been run into the lateral wellbore.

Figure 1E shows the working string having been pulled from the wellbore of Figure 1D. A new working string is being lowered into the primary wellbore, with a fishing hook disposed on the working string.

Figure 1F shows the fishing hook from Figure 1E engaging the whipstock. The whipstock is now being pulled from the wellbore.

Figure 1G shows yet a next progressive step in the formation of a lateral wellbore and the completion of the well. Here, the whipstock of Figure 1F has been removed from the parent wellbore. A liner has been positioned at the intersection between the parent wellbore and the lateral wellbore, and has been directed through the window and into the lateral wellbore.

Figure 2A is a cross-sectional view of a wellbore. The wellbore has both a primary wellbore and a lateral wellbore having been drilled off of the primary wellbore. A liner is visible providing access to the lateral wellbore through a window. A bottom hole assembly is being moved into the primary wellbore.

Figure 2B provides another cross-sectional view of the wellbore of Figure 2A. This view represents a next step in the creation of a re-entry path through the liner in the primary wellbore. In this step, the bottom hole assembly has milled through the liner, forming the re-entry path.

Figure 2C shows the wellbore of Figure 2B, with the bottom hole assembly having been removed. The packer remains in the primary wellbore, waiting to be milled out or otherwise removed for final access to the primary wellbore below the window.

Figure 3 provides a perspective view of a bottom hole assembly for forming a re-entry path through a tubular such as a lateral wellbore liner, in one embodiment. The bottom hole assembly includes a lead mill.

Figure 4 presents a cross-sectional view of the bottom hole assembly of Figure 3.

Figure 5 presents a perspective view of the lead mill of Figure 3.

Figure 6 shows an enlarged, side cross-sectional view of the lead mill of Figure 3.

Figure 7 presents a plan view of a bottom hole assembly, in an alternate arrangement. In this arrangement, the assembly includes an angled tool joint to deflect the lead mill.

Figure 8 provides a plan view of a bottom hole assembly in yet an additional alternate embodiment. In this embodiment, the assembly includes a mill with an eccentrically arranged cutting structure.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

Figure 2A is a cross-sectional view of a wellbore **100**. The wellbore **100** has both a primary wellbore **10**, and a lateral wellbore **20** having been drilled off of the primary wellbore **10**. A liner **28** is visible, providing access to the lateral wellbore **20** through a window **18**. The liner **28** includes a curved portion **45**, or "curvature," that substantially blocks passage through the primary wellbore **10** at the point of intersection with the lateral wellbore **20**.

In **Figure 2A**, a bottom hole assembly **200** is being moved into the primary wellbore **10**. The bottom hole assembly **200** is not completely visible, but is just beginning to enter the liner **28**. It is understood, of course, that the features of **Figure 2A** are not to scale, and that the liner **28** may extend from 100 to 500 feet, depending upon desired build-rate.

Figure 3 provides a perspective view of a bottom hole assembly **200** for forming an entry path through a tubular body, in one embodiment. In this arrangement, the bottom hole assembly **200** includes various components, including an elongated, heavy pipe structure **230**, a pair of extension subs **220**, **220'** connected to the pipe structure **230**, an upper mill **240**, and a lead mill **210**. The bottom hole assembly **200** is configured to be run into a wellbore **100** on working string (not shown). Non-limiting examples of a working string include a string of drill pipe, and coiled tubing. In the event of coiled-tubing, a downhole rotary motor (not shown) would be needed to impart rotation to the bottom hole assembly **200**.

Figure 4 shows the bottom hole assembly **200** in cross-section. First, the bottom hole assembly **200** includes an elongated, heavy pipe structure **230**. This pipe structure **230** is preferably defined by one or more drill collars, as shown in **Figure 3**. The drill collars **230** are fabricated from a sturdy metal to imbue substantial stiffness to the bottom hole assembly **200**. The drill collars **230** also have an outer diameter that provides close tolerance within the inner diameter of the surrounding liner **28**. For example, 7 5/8" liner has an inner diameter of 6 3/8". Drill collars **230** having an outer diameter of 6 1/8" would then be preferred. The drill collars **230** also include a bore **235** along the longitudinal axis.

Fluids are circulated through an inner bore (not shown) of the drill collars **230**. The fluid circulation serves to remove metal shavings and cuttings during the tubular milling process. Fluid circulation also serves to cool the milling bit **210** during milling. Milling fluids are circulated through the bore of the drill collars **230**, through the milling bit **210**, and back up an annular region between the assembly **200** and the surrounding liner **28**. Because of the close annular tolerance of the heavy pipe structure **230**, helical grooves are preferably formed around the pipe structure **230**, e.g., drill collars.

During run-in for the bottom hole assembly **200**, the drill collars **230** are connected to the working string. Preferably, a threaded connection is provided for connecting the one or more drill collars **230** to a working string. A fishing neck **232** is also seen on the drill collars **230**.

As noted, the bottom hole assembly **200** also includes at least one sub. In the arrangement of **Figure 3**, two extension subs **220, 220'** are shown connected below the drill collars **230**. The subs **220, 220'** are preferably undersized, meaning that they provide an outer diameter that is smaller than lateral cutting structures of the lead mill **210** (to be discussed further, below). Sub **220** is shown as having a tapered outer diameter such that the outer diameter becomes smaller from the drill collars **230** as the sub approaches the lead mill **210**.

The bottom hole assembly **200** may also include an upper mill. In the arrangement of **Figure 3**, an upper mill is shown at **240**. The upper mill **240** is preferably configured as a watermelon mill. However, the upper mill **240** is optional, as it is preferred that the lead mill **210** be sized to provide a full-bore access into the primary wellbore **10**.

As noted, the bottom hole assembly **200** also includes a cutting device such as a lead mill **210**. **Figure 5** presents a perspective view of the lead mill of **Figure 3**, in one embodiment. **Figure 6** provides an enlarged cross-sectional view of the lead mill **210**, amplifying certain features of the lead mill **210**. The lead mill **210** first includes a body **212**. A bore **205** runs through the body **212**. The body **212** has an outer diameter, shown in **Figure 6** as "d_1." Connected to the body **212** are cutting structures **214**. In the arrangement of **Figure 6**, the cutting structures **214** represent radially arranged blades. Hardened material (not shown) is imbedded into the cutting structures **214**. A non-limiting example of such a hardened material is the welding of carbide onto the blades **214**.

The one or more blades **214** form a second outer diameter "d_2" for the lead mill **210**. In addition, the one or more blades **214** define a length "**h**". The preferred dimensions for d_1 and d_2 are relative to the thickness of the tubular being breached, e.g., liner **28**. The wall **28** has a thickness "**t**" (see **Figure 2A**), and preferably:

$$1 \leq [(d_2 - d_1) \div 2t] \leq 2.5.$$

In addition, preferably:

$$(d_2 \div h) \geq 2.0.$$

Referring again to **Figure 5**, **Figure 5** presents a perspective view of the lead mill of **Figure 4**. This perspective view allows for a view of the bottom of the lead mill **210**. More specifically, the face **216** of the mill **210** is visible. It can be seen that the face **216** of the mill **210** is tapered. As will become more apparent herein, the preferred tapered aspect of the face **216** enables the lead mill **210** to continue to act against the liner **28** during a mill-through operation after initial breakthrough in the curvature **45**, and to resist "kicking out" into the lateral wellbore **20**.

To aid in the milling operation, the bottom hole assembly **200** is configured to apply a lateral pressure against the liner **28**. In this respect, the elongated heavy pipe structure **230** creates stiffness in the bottom hole assembly **200**. This, in turn, creates resistance to deflection in the sub **220** and lead mill **210** as it encounters the curvature **45** of the liner **28**. The bottom hole assembly **200** employs simultaneous rotational and lateral force to totally breach the adjacent liner **28**, thereby forming the lip. Stated another way, the bottom hole assembly **200** provides lateral forces to provide load on the cutting structure in order to complete wall penetration through the adjacent liner prior to axial movement of the rotated milling assembly **200**.

For some pipe, a contact pressure greater than 115 psi is required to mill through its thickness. Therefore, in one embodiment, the bottom hole assembly **200** is configured to generate lateral force sufficient to provide a cutting surface contact pressure greater than 115 psi at any cutting depth through the casing wall "**t**". Specifically,

$$115 \text{ psi} \leq \frac{6EI\delta}{L^3 \phi \pi h}$$

δ = deflection of mill head in liner curvature from the intended straight path at contact point (in inches);

L= length of milling assembly to a second point of contact with the liner, where an opposing lateral force is supplied (in inches);

E= modulus of elasticity (psi);

I= moment of inertia of the milling assembly between the contact points (in inches^4);

Ø= milling head diameter (in inches) (referred to as "$\mathbf{d_2}$," above); and

h= cutting structure length (in inches).

In addition to the stiffness of the bottom hole assembly **200** as provided by (1) the length of the drill collars **230**; (2) the stiffness of the drill collars **230**; and (3) the tight tolerance of the drill collars **230** within the surrounding liner **28**, other features of the bottom hole assembly **200** aid in generating the desired lateral force against the surrounding liner **28**. For example, the limited blade length "**h**" serves to direct pressure against the liner **28** at a more precise point by reducing the milling contact area. Also, the tapered configuration of the lower sub **220** avoids interference of pipe structure with the lateral cutting function of the lead mill **210** during milling. In addition, the ratio of plunge-through depth [($d_2 - d_1$) / 2] to liner wall thickness "**t**" is between 1 to 1 and 2.5 to 1 (inclusive). This configuration uniquely allows the mill **210** to relieve the bending loads, e.g. cut through the liner **28**, without supporting the mill **210** with additional contact area.

The step of applying the lateral pressure through the milling bit against the curvature of the liner is provided at least in part by the moment force applied by stiffness within the drill collar **230** and connected sub **220**. The milling bit **210** is lowered to a first desired depth in the primary wellbore **10** so that an outer edge of the milling bit cutting structure **214** is in contact with the wall **45**. The operator may be observing weight indicators, first movements, and/or monitoring depth to position the milling bit **210** below the beginning of the liner curvature **45**. The milling bit **210** is then rotated until the wall "**t**" is entirely breached at a point, thereby forming the lip.

Turning now to **Figure 2B**, **Figure 2B** provides another cross-sectional view of the wellbore **100** of **Figure 2A**. This view represents a next step in the creation of a re-entry path through the liner **28** in the primary wellbore **10**. In this step, the bottom hole assembly **200** has milled through the liner **28**, forming the re-entry path into the primary wellbore **10**. After forming the lip through the liner wall **45**, the working string and attached milling bit are advanced axially so that a first re-entry path is formed in the primary wellbore **10**. These steps may be repeated for additional lateral junctions.

Figure 2C shows the wellbore of **Figure 2B**, with the bottom hole assembly having been removed. The packer **50** remains in the primary wellbore **10**. The packer **50** and supported orientation anchor remain in the primary wellbore **10**. Where desired for additional completion operations for the lateral wellbore **20**, a re-entry guide (not shown) may be landed on the anchor **50** to aid in directing tools into the lateral wellbore **20**. Where the liner **28** has been cemented in place, an under-gauge rock bit (not shown) with near-gauge smooth outer diameter stabilizer may be used to form a bore through the packer **50**. The packer **50** may later be completely milled out for final access to the primary wellbore **10** below the window **18**. Where the liner **28** has not been cemented into the primary wellbore **10**, the packer **50** may be released and pulled out of the hole after lateral completion operations are performed.

By way of example, a 7-inch liner may be hung within a size 9-5/8-inch casing. The 7-inch liner has a 6.184 inch i.d., and receives a 6.125-inch diameter spiraled drill collar. In this way, minimal flexure and maximum stabilization of the drill collar is obtained. The special collar incorporates a non-flat surface, e.g., outer spirals, in order to expand the return flow area. The large collar diameter yields a significant "bending" force, or moment, that permits a substantial lateral cutting force to be applied against the liner.

In one test, it was found that in a liner curvature formed from a 15° per hundred-build rate, with a mill being run to a depth of 1 foot below the top of the beginning of the liner radius, a side force of about 8900-lbs was created. In previous tests, the mill breakthrough was achieved upon rotation within 15 minutes. In a 25° per hundred-build rate, and a distance of 1 foot below the top of the liner curvature, a side force of 5,650-lbs may be created. In previous tests, the mill breakthrough in this instance was achieved within 44 minutes after beginning rotation. These test results were achieved without the installation of centralizers to align milling centerlines.

Alternate bottom hole assembly configurations may be employed with the above-described methods to provide additional deflection force. **Figure 7** presents a plan view of a bottom hole assembly **700** in an alternate arrangement. The assembly **700** may generally include the tools from the assembly **200** of **Figure 4**. These include a heavy pipe structure **730** such as drill collars, a fishing neck **732**, a pair of extension subs **720**, **720'** connected to the drill collars **730**, an upper mill **740**, and a lead mill **710**. The bottom hole assembly **700** is again configured to be run into a wellbore **100** on working string (not shown). However, in this arrangement, one of the tools is bent in order to produce a slightly eccentric rotation of the lead mill **710** during rotation of the bottom hole assembly **700**. By bending the tool, an angled tool joint along the assembly **700** is produced. The angled tool joint may be the upper mill **740** or one of the subs **720, 720'**. In the arrangement of **Figure 7**, the angled tool joint is the sub **720**. The bent sub **720** provides additional deflection force for the mill **710** against the liner curvature **45** when the assembly **700** is rotated.

Figure 8 provides a plan view of a bottom hole assembly **800** in yet an additional alternate embodiment. The assembly **800** may again include tools from the assembly **200** of **Figure 4**. These include a heavy pipe structure **830** such as drill collars, a fishing neck **832**, a pair of extension subs **820, 820'** connected to the drill collars **830**, an upper mill **840**, and a lead mill **810**. However, in this arrangement, the lead mill **810** has an eccentrically arranged cutting structure **814** relative to a longitudinal axis of the mill **810**. The offset cutting structure **814** in **Figure 8** will increase the lateral load on the cutting structure **814** by amplifying the deflection of the mill **810** against the curvature **45.**

In another embodiment of a method for forming a re-entry path, an additional step of applying a lateral pressure through the milling bit **210** against the curvature **45** of the liner **28** while rotating the milling bit **210** is provided. This may be accomplished through a centralizing mechanism, such as a hydraulically activated directional drilling tool. Once a lip is formed, weight and rotation are used to fully develop a re-entry path of some desired length. This path may be fully produced in either one or multiple trips. The use of a large diameter mill helps avoid the requirement of additional trips and/or mills to enlarge pilot openings.

In another embodiment, the method further comprises the step reciprocating the milling bit along a length of the curvature of the liner while rotating the milling bit. The reciprocating action may be conducted prior to the step of rotating the cutting device while maintaining an axial position of the cutting device relative to the wall. Alternatively, the reciprocating action may be conducted after the lip in the wall has been formed. In this respect, testing has demonstrated that it is possible to "skip over" the lip by adding weight and slowly rotating. Alternatively, more than one lip may be formed along the curvature before or after shaving. Continued lowering and reciprocation of the assembly **200**, with or without rotation, against the inside tubular curvature utilizes the stored energy of the milling assembly **200** to create a side force to reduce the wall thickness. In this manner, an inner portion of the liner is “pre-shaved,” thereby assisting the milling process. Where the lip has already been formed prior to shaving, the milling assembly **200** would have to be raised back to the point of the initial breach for complete milling.

Various methods of removing lateral material for creating access to a main wellbore below a lateral wellbore are provided. Generally, the steps include locating a cutting device adjacent a portion of the wall within the wellbore. The cutting device is rotated while its axial position is maintained relative to the wall. Lateral force from the cutting device is used to initiate an opening in the wall. Thereafter, the cutting device is rotated and advanced axially within the primary wellbore to complete the opening. This method, in one embodiment, is used to provide access to the primary wellbore after a plurality of lateral wellbores has been formed, with each lateral wellbore having a tubular passing from the primary wellbore into respective lateral wellbores. The cutting device in this instance removes material from the curvature of a liner at the intersection of the primary wellbore and the lateral wellbores. Preferably, the cutting device is a milling bit that is introduced into the primary wellbore at the end of a working string. The milling bit may be a part of the bottom hole assembly **200** as described above, such as the assembly **200** shown in **Figure 3.**

As can be seen, the present invention provides a method by which complete re-entry or access into a parent wellbore below the intersection of the parent wellbore with a lateral wellbore may be accomplished. A "re-entry path" is formed to provide access for the passage of tools as well as the flow of fluids between an upper portion and a lower portion of the parent wellbore. Preferably, the re-entry path has an inner diameter that approaches the drift diameter of the liner of the lateral wellbore located above the intersection of the parent and lateral wellbores. In this way, the diameter of the re-entry path is large enough to allow the passage of tools into the parent wellbore below the intersection, including, but not limited to, monitoring, pressure control, reworking, and stimulating tools. Thus, upon completion of the re-entry path at the intersection of the parent wellbore and a lateral wellbore, the parent wellbore and that lateral wellbore have "equivalent" inner diameters for full-bore access of downhole tools.

The milling assembly configurations described above require no hydraulics for centralization nor other extraneous mechanisms to urge a lateral cutting action. The above-described milling assembly configuration **200** simulates the radius of liner at its juncture achieving minimum flexure while operational in a curved tubular and allowing the mill to breach this liner. At the same time, additional lateral forces may optionally be generated through the use of a biasing mechanism or directional drilling device.

The above described methods may be used with known mills and liner materials. The above described methods may eliminate the need for expensive junction equipment and the associated complex cementing procedures used in many "ML Level 4" systems.

The methods also allow for stacked ML systems, without the continual reduction of the mainbore diameter. In this respect, more than one lateral wellbore can be directed from a portion of the parent wellbore having a particular diameter casing, each lateral wellbore being cased by an internal liner having the same inner diameter. The lateral wellbores are generally, successively completed starting from the downhole side of the portion of the parent wellbore. After a particular lateral wellbore is completed, as described above, then a new lateral wellbore can be extended from the parent wellbore at a location above the previously-completed wellbore. Once each lateral wellbore extending from the parent wellbore is completed, the operator would have full-bore access for the passage of the same-sized downhole tools to any equivalent-bore lateral wellbore or the parent wellbore.

While the foregoing is directed to embodiments of the present invention, other and further embodiments of the invention may be devised without departing from the basic scope thereof, and the scope thereof is determined by the claims that follow.

Claims:

1. A method of creating an opening in a wall of a tubular within a wellbore, comprising:

connecting a milling bit proximate to a lower end of a working string;

running the milling bit and connected working string to a desired depth within the wellbore and adjacent a portion of the well;

rotating the milling bit while maintaining an axial position of the milling bit relative to the wall to initiate the opening; and

rotating and axially advancing the milling bit to complete the opening.

2. The method of claim 1, wherein:

the wall has a curvature;

the milling bit is located along the curvature;

the milling bit is part of a bottom hole assembly; and

a stiffness of the bottom hole assembly, a contact area of the milling bit, and the location of the milling bit along the curvature are selected so that a contact pressure of greater than or equal to 115 psi is maintained while initiating the opening.

3. The method of claim 1, wherein the step of rotating the milling bit while maintaining an axial position of the milling bit relative to the wall to initiate the opening is continued until the wall is breached.

4. The method of claim 1, wherein:

the tubular is a liner secured at the intersection of a primary wellbore and a lateral wellbore, the wall having a curvature;

the milling bit is part of a bottom hole assembly; and

the opening is initiated by a lateral pressure exerted by the milling bit against the wall, the lateral pressure generated by a stiffness of the bottom hole assembly.

5. The method of claim 4, wherein the step of rotating the milling bit while maintaining an axial position of the milling bit relative to the wall to initiate the opening is continued until the liner is breached, thereby forming a lip.

6. The method of claim 5, wherein the step of rotating and axially advancing the milling bit to complete the opening comprises rotating and axially advancing the milling bit along a desired length of the liner to form a re-entry path in a primary wellbore.

7. The method of claim 4, further comprising the step of:

actuating a biasing mechanism to apply additional lateral pressure against the curvature of the liner while rotating the milling bit to initiate the opening.

8. The method of claim 7, further comprising the step:

reciprocating the milling bit along a length of the curvature of the liner while rotating the milling bit prior to the step of rotating the milling bit while maintaining an axial position of the milling bit relative to the wall, thereby shaving an inner portion of the liner.

9. The method of claim 7, wherein:

the step of running the milling bit and connected working string to a desired depth within the wellbore and adjacent a portion of the wall comprises locating the milling bit at a first point along the curvature of the liner; and

the step of rotating the milling bit while maintaining an axial position of the milling bit relative to the wall to initiate the opening comprises forming a first lip at the first point along the curvature of the liner;

and wherein the method further comprises:

locating the milling bit adjacent a second point along the curvature of the liner after forming the first lip; and

rotating the milling bit while maintaining an axial position of the milling bit relative to the liner to initiate an opening, thereby forming a second lip at a second point along the curvature of the liner.

10. The method of claim 1, wherein:

the milling bit is connected to a bottom hole assembly, the bottom hole assembly comprising:

an elongated, heavy pipe structure connected proximate an end of a working string; and

a sub connected to the heavy pipe structure at an end opposite the working string, the sub also being connected to the milling bit at an end opposite the heavy pipe structure; and

wherein the opening is initiated by a lateral pressure exerted by the milling bit against the wall, the lateral pressure generated by a stiffness of the heavy pipe structure and connected sub.

11. The method of claim 10, wherein the sub has an outer diameter that is smaller than the outer diameter of cutting blades along the milling bit.

12. The method of claim 11, wherein the outer diameter of the sub is generally tapered to become smaller from the heavy pipe structure to the milling bit.

13. The method of claim 11, wherein the sub is bent to produce an eccentric rotation of the milling bit when the bottom hole assembly is rotated.

14. The method of claim 11, wherein the milling bit has eccentrically arranged cutting structures to provide an additional moment force against the wall when the bottom hole assembly is rotated.

15. The method of claim 10, wherein the heavy pipe structure is one or more drill collars.

16. The method of claim 10, wherein:

the bottom hole assembly further comprises a hydraulically actuated centralizing mechanism; and lateral pressure exerted by the milling bit against the wall is further generated by actuating the centralizing mechanism.

17. The method of claim 10, wherein:

the bottom hole assembly further comprises a biasing means; and

lateral pressure exerted by the milling bit against the wall is further generated by actuating the biasing means.

18. The method of claim 1, wherein the milling bit comprises a lead mill, the lead mill comprising:

a body having an inner bore and a first outer diameter "d_1"; and

one or more blades at a point along the outer diameter of the body, the blades forming a second outer diameter "d_2"; and having a length "h".

19. The method of claim 18, wherein:

the wall has a thickness "t"; and

$1 \le [(d_2 - d_1) \div 2t] \le 2.5$.

20. The method of claim 18, wherein:

$(d_2 \div h) \ge 2.0$.

21. The method of claim 18, wherein the blades are eccentrically arranged relative to a longitudinal axis of the body.

22. A method of removing a portion of a liner at the intersection of a lateral wellbore and a primary wellbore in order to permit access to the primary wellbore below the lateral wellbore, the method comprising the steps of:

running a milling assembly into the primary wellbore, the milling assembly having a lead mill comprising:

a body having an inner bore and a first outer diameter "d_1";

one or more blades at a point along the outer diameter of the body, the blades forming a second outer diameter "d_2" and having a length "h";

engaging the milling assembly to a portion of the liner obstructing the primary wellbore;

rotating the milling assembly at a point along the curvature;

using lateral forces created by the milling assembly contacting the liner to provide load on the cutting structure in order to complete wall penetration through the liner prior to axial movement of the milling assembly;

axially moving downward and further rotating the milling assembly to mill through the liner and to form a re-entry into the primary wellbore.

23. The method of claim 22, wherein:

the wall has a thickness "t"; and

$1 \leq [(d_2 - d_1) \div 2t] \leq 2.5$.

24. The method of claim 22, wherein:

$(d_2 \div h) \geq 2.0$.

25. The method of claim 22, wherein the lead mill further comprises a concave inner face.

26. The method of claim 22, wherein the milling assembly further comprises a drill collar, and an extension sub connected to the drill collar.

27. The method of claim 26, wherein the milling assembly further comprises an upper mill intermediate the drill collar and the extension sub.

28. A bottom hole assembly for laterally milling a lip in a tubular body having a wall, the bottom hole assembly comprising:

a drill collar;

a sub connected to the drill collar; and

a lead mill, the lead mill comprising:

a body connected to the sub, and having an inner bore and a first outer diameter "d_1"; and one or more cutting surfaces at a point along the outer diameter of the body, the cutting surfaces forming a second outer diameter "d_2" and having a length "h".

29. The bottom hole assembly of claim 28, wherein:

the wall has a thickness "t"; and

$1 \leq [(d_2 - d_1) \div 2t] \leq 2.5$.

30. The bottom hole assembly of claim 29, wherein:

$(d_2 \div h) \geq 2.0$.

31. The bottom hole assembly of claim 28, wherein the lead mill further comprises a concave inner face.

32. The bottom hole assembly of claim 28, wherein the sub has an outer diameter that is smaller than the outer diameter of the cutting surfaces along the lead mill.

33. The bottom hole assembly of claim 32, wherein the outer diameter of the sub is generally tapered to become smaller from the drill collar to the lead mill.

34. The bottom hole assembly of claim 32, wherein the sub is bent.

35. The bottom hole assembly of claim 28, wherein:

the drill collars and connected sub form a longitudinal axis of the bottom hole assembly; and

the cutting surfaces of the lead mill are eccentrically arranged relative to the longitudinal axis.

36. The bottom hole assembly of claim 28, further comprising:

an upper mill disposed between the sub and the drill collars.

37. The method of claim 4, wherein the lateral pressure is determined using the formula $\frac{6EI\delta}{L^3\phi\pi h}$, where: δ is a deflection of a head of the milling bit in the curvature from an intended straight path at a contact point (in inches), L is a length of the bottom hole assembly to a second contact point with the liner where an opposing lateral force is supplied (in inches); E is a modulus of elasticity (psi) of the bottom hole assembly, I is a moment of inertia of the bottom hole assembly to the contact point (in inches^4), Ø is an outside diameter of the head of the milling bit (in inches); and h is a cutting structure length of the milling bit (in inches).

38. The method of claim 4, wherein an outside diameter of at least a portion of the bottom hole assembly is slightly less than an inside diameter of the liner.

39. The method of claim 38, wherein slightly is less than or equal to one-quarter inch.

40. The method of claim 39, wherein slightly is less than or equal to 0.059 inch.

41. A method of creating an opening in a wall of a wellbore tubular, comprising:

locating a cutting device adjacent a portion of the wall within the wellbore;

rotating the cutting device while maintaining an axial position of the cutting device relative to the wall to initiate the opening; and

rotating an axially advancing the cutting device to complete the opening wherein:

the wall has a curvature;

the cutting device is located along the curvature of the wall;

the cutting device is part of a bottom hole assembly; and

a stiffness of the bottom hole assembly, a contact area of the cutting device, and the location of the cutting device along the curvature are selected so that a contact pressure of greater than or equal to 115 psi is maintained while initiating the opening.

42. A method of creating an opening in a wall of a wellbore tubular, comprising:

locating a milling bit adjacent a portion of the wall within the wellbore;

rotating the milling bit while maintaining an axial position of the milling bit relative to the wall to initiate the opening; and

rotating and axially advancing the miling bit to complete the opening;

wherein:

the wall within the wellbore is the wall of a liner secured at the intersection of a primary wellbore and a lateral wellbore, the wall having a curvature;

the milling bit is part of a bottom hole assembly; and

the opening is initiated by a lateral pressure exerted by the milling bit against the wall, the lateral pressure generated by a stiffness of the bottom hole assembly.

43. A method of creating an opening in a wall of a wellbore tubular, comprising:

locating a milling bit adjacent a portion of the wall within the wellbore;

rotating the milling bit while maintaining an axial position of the cutting device relative to the wall to initiate the opening; and

rotating and axially advancing the milling bit to complete the opening,

wherein:

the milling bit is connected to a bottom home assembly, the bottom hole assembly comprising:

an elongated, heavy pipe structure connected proximate an end of a working string; and

a sub connected to the heavy pipe structure at an end opposite the working string, the sub also being connected to the milling bit at an end opposite the heavy pipe structure; and

the opening is initiated by a lateral pressure exerted by the milling bit against the wall, the lateral pressure generated by a stiffness of the heavy structure and connected sub.

44. A method of creating an opening in a wall of a wellbore tubular, comprising:

locating a lead mill adjacent a portion of the wall within the wellbore;

rotating the lead mill while maintaining an axial position of the lead mill relative to the wall to initiate the opening; and

rotating and axially advancing the lead mill to complete the opening,

wherein the lead mill comprises:

a body having an inner bore and a first outer diameter "d_1"; and

one or more blades at a point along the outer diameter of the body, the blades forming a second outer diameter "d_2" and having a length "h".

45. The method of claim 44, wherein:

the wall has a thickness "t"; and

$1 \leq [(d_2 - d_1) \div 2t] \leq 2.5$.

46. The method of claim 44 wherein:

$(d_2 \div h) \geq 2.0$.

47. The bottom hole assembly of claim 44, wherein the lead mill further comprises a concave inner face.

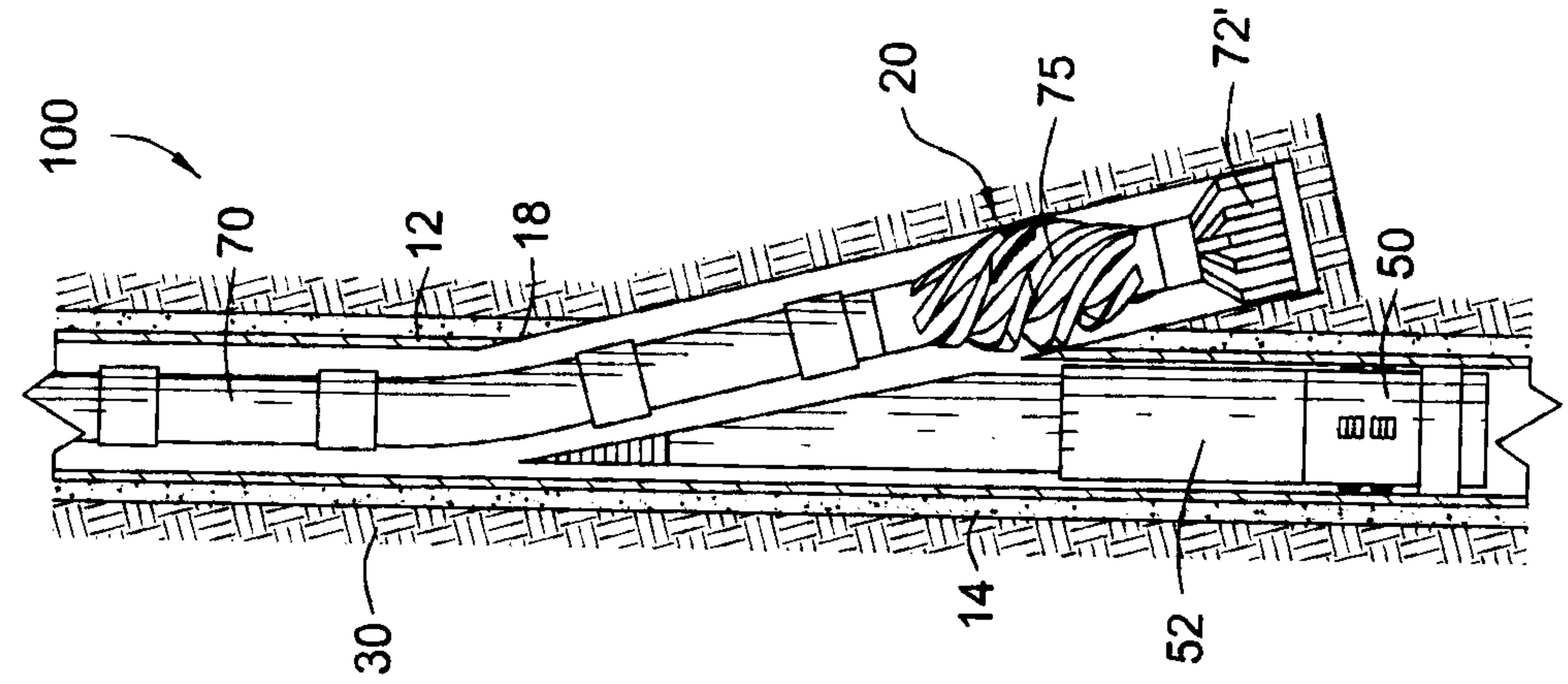


FIG. 1C
(PRIOR ART)

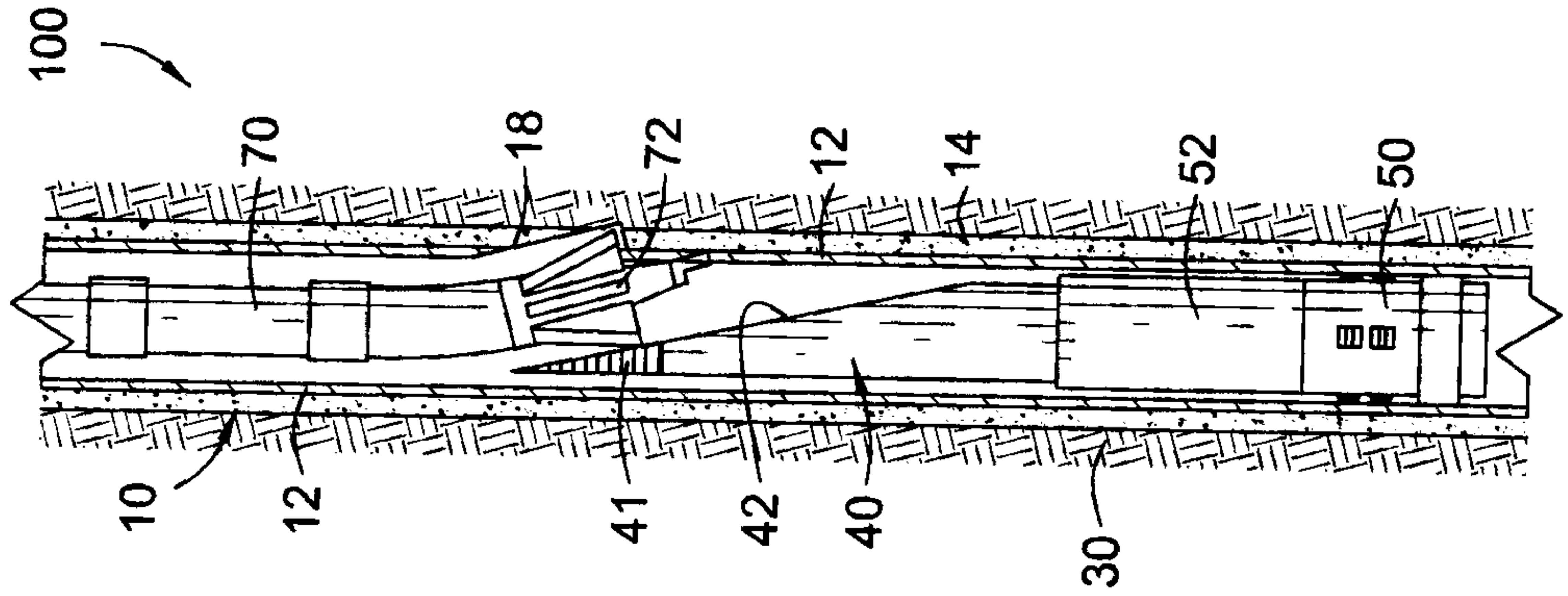


FIG. 1B
(PRIOR ART)

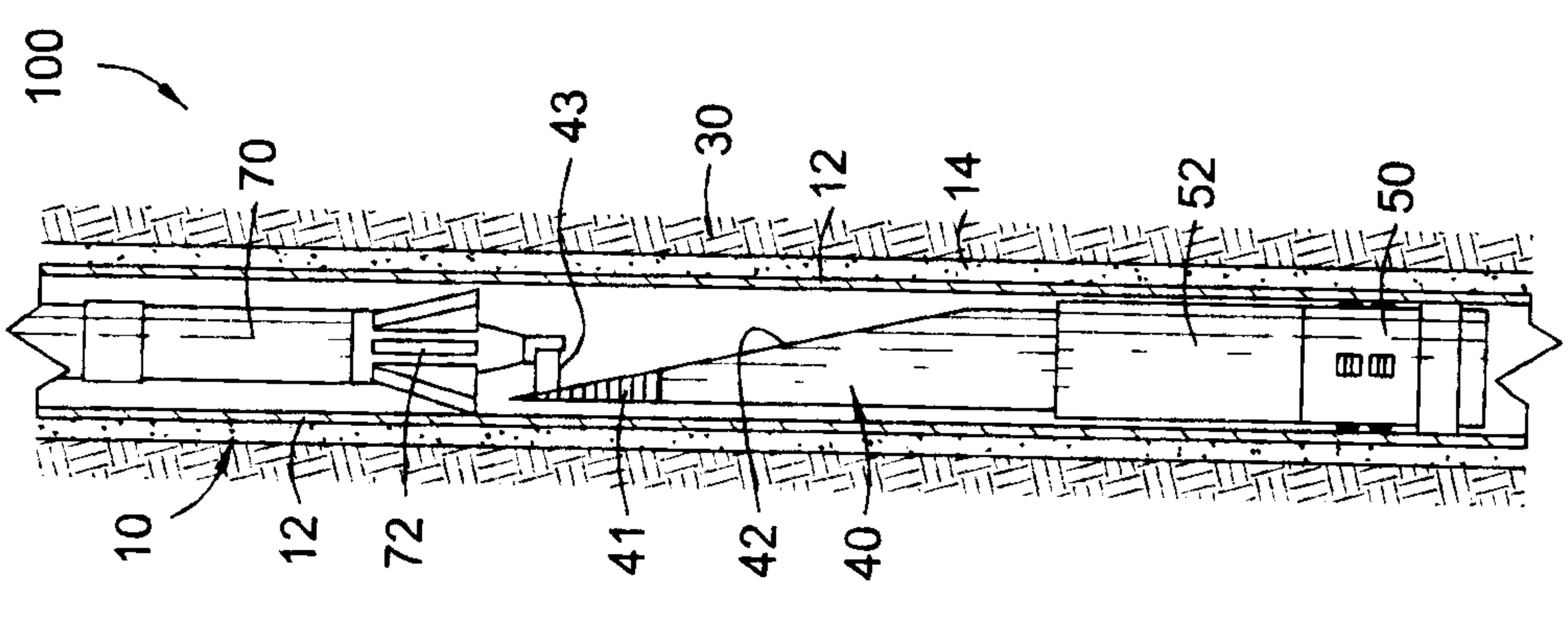


FIG. 1A
(PRIOR ART)

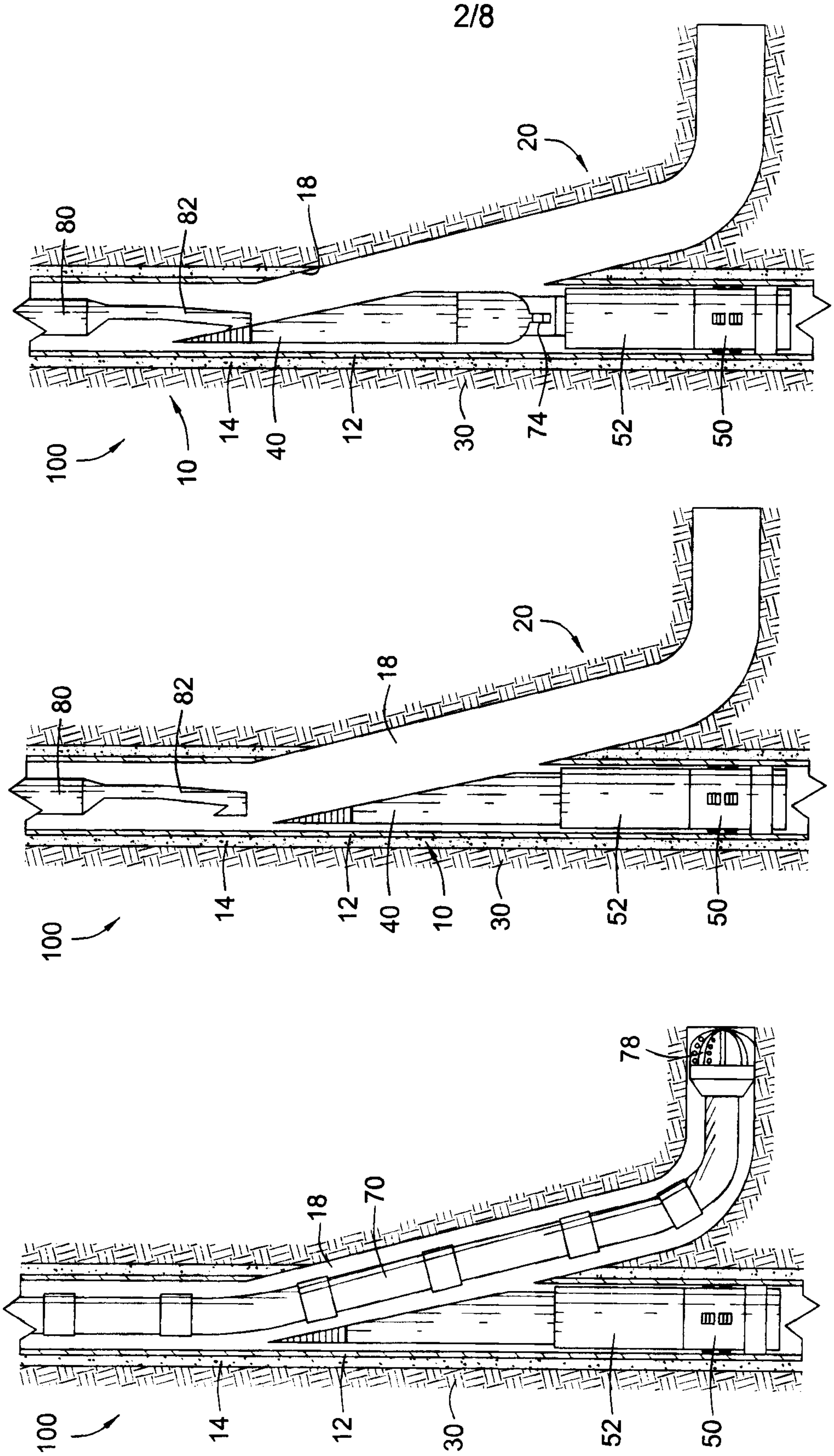


FIG. 1D (PRIOR ART)

FIG. 1E (PRIOR ART)

FIG. 1F (PRIOR ART)

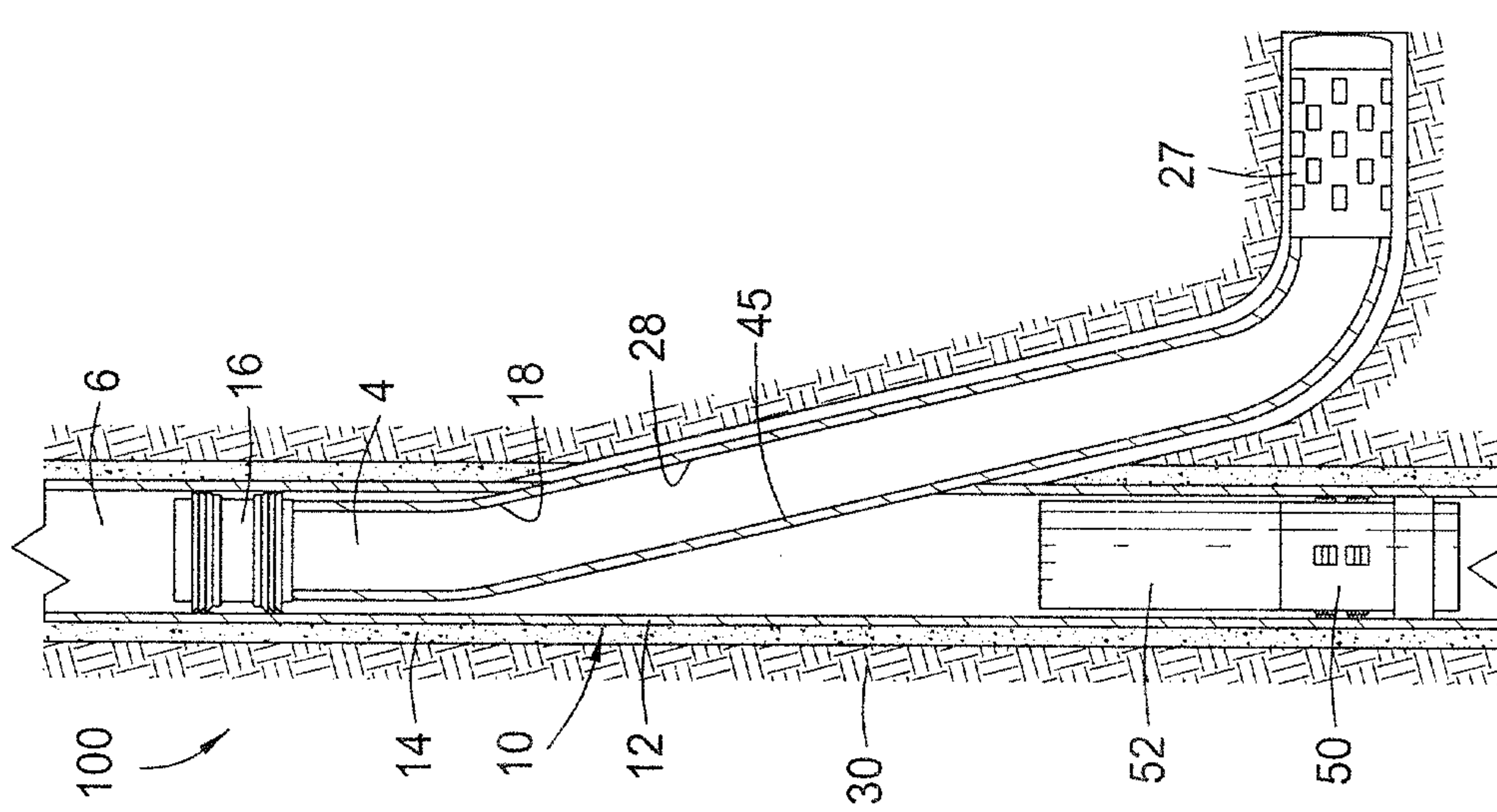


FIG. 1G
(PRIOR ART)

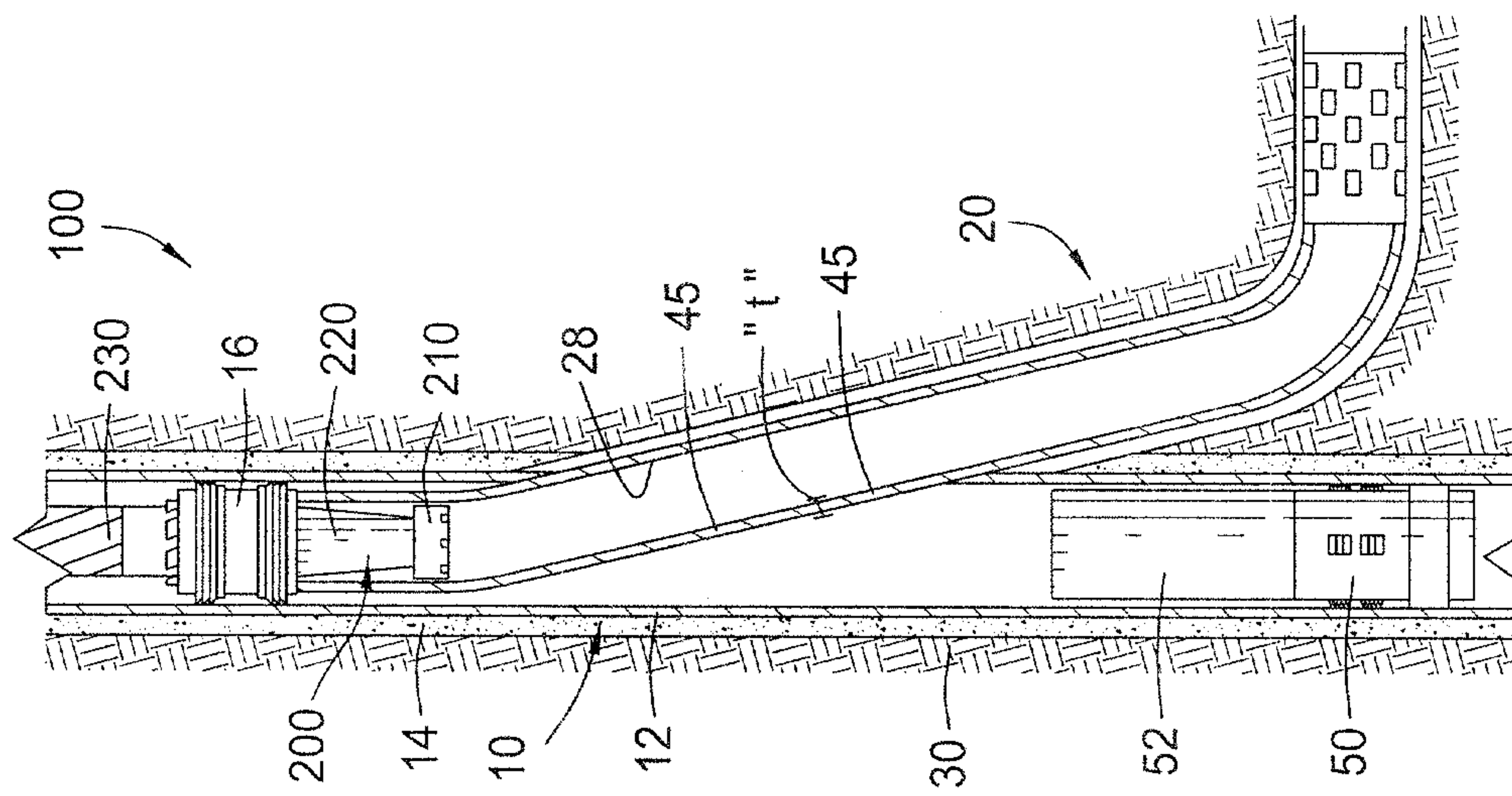
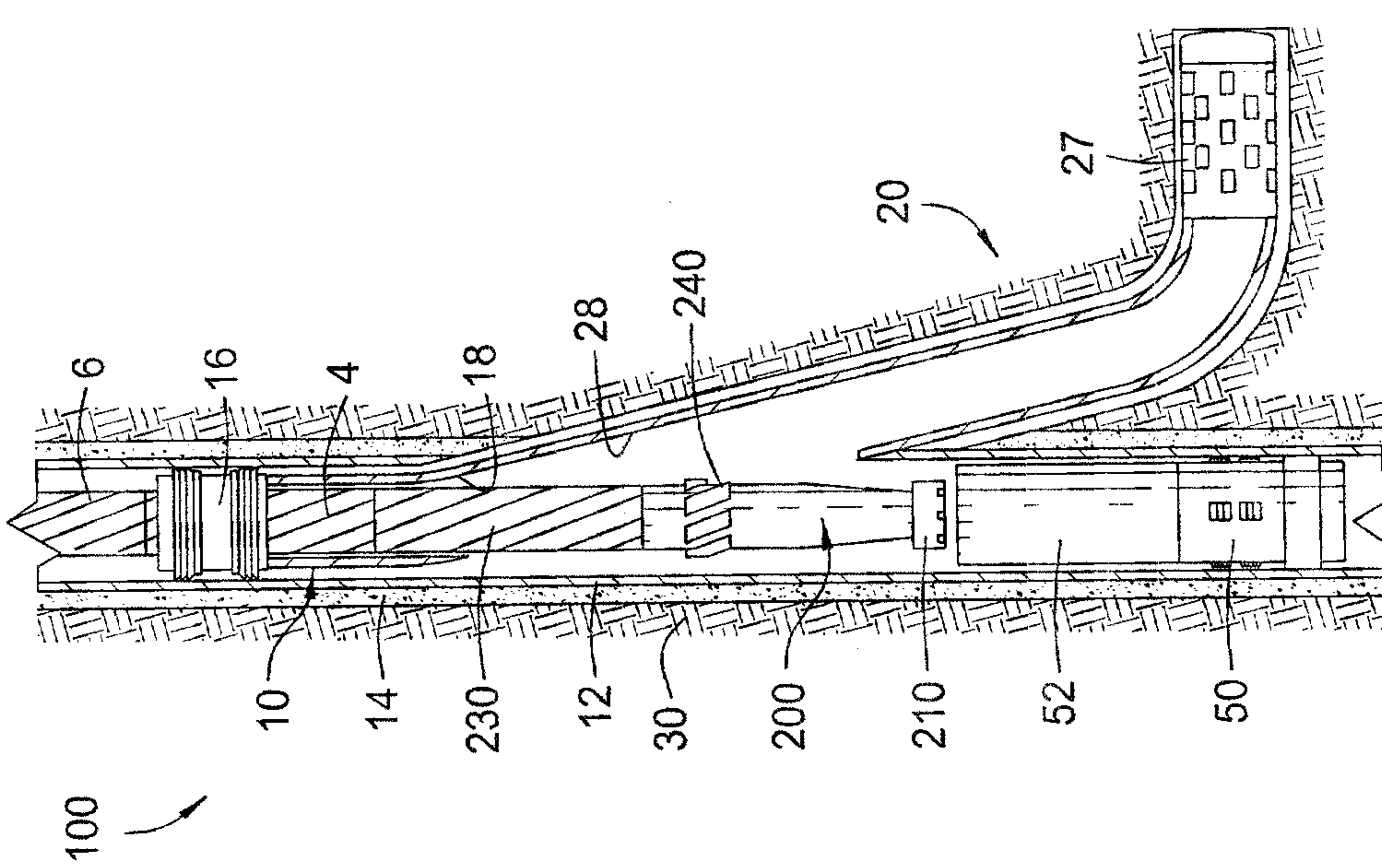


FIG. 2A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6
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200
210
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50

FIG. 2B

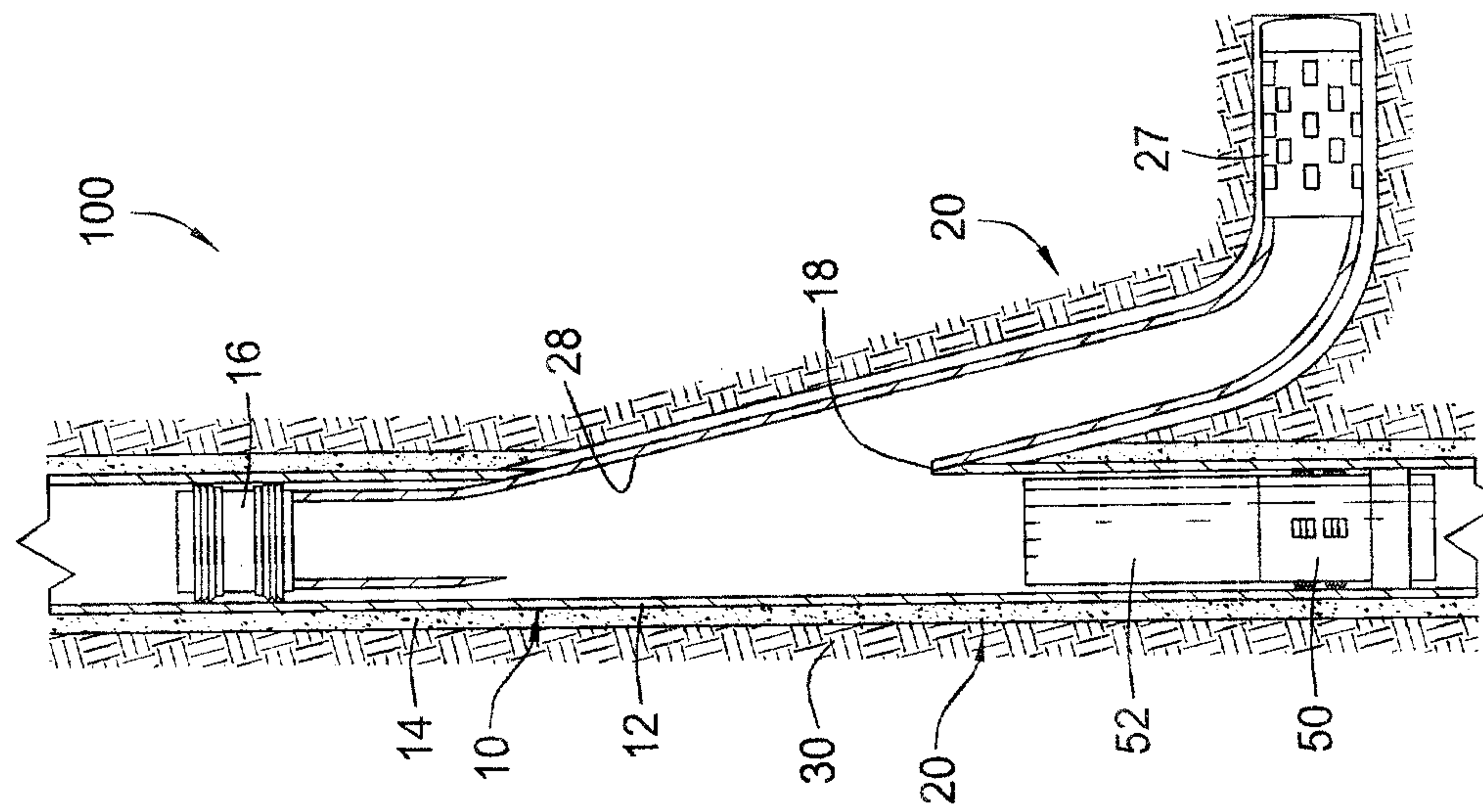
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FIG. 2C

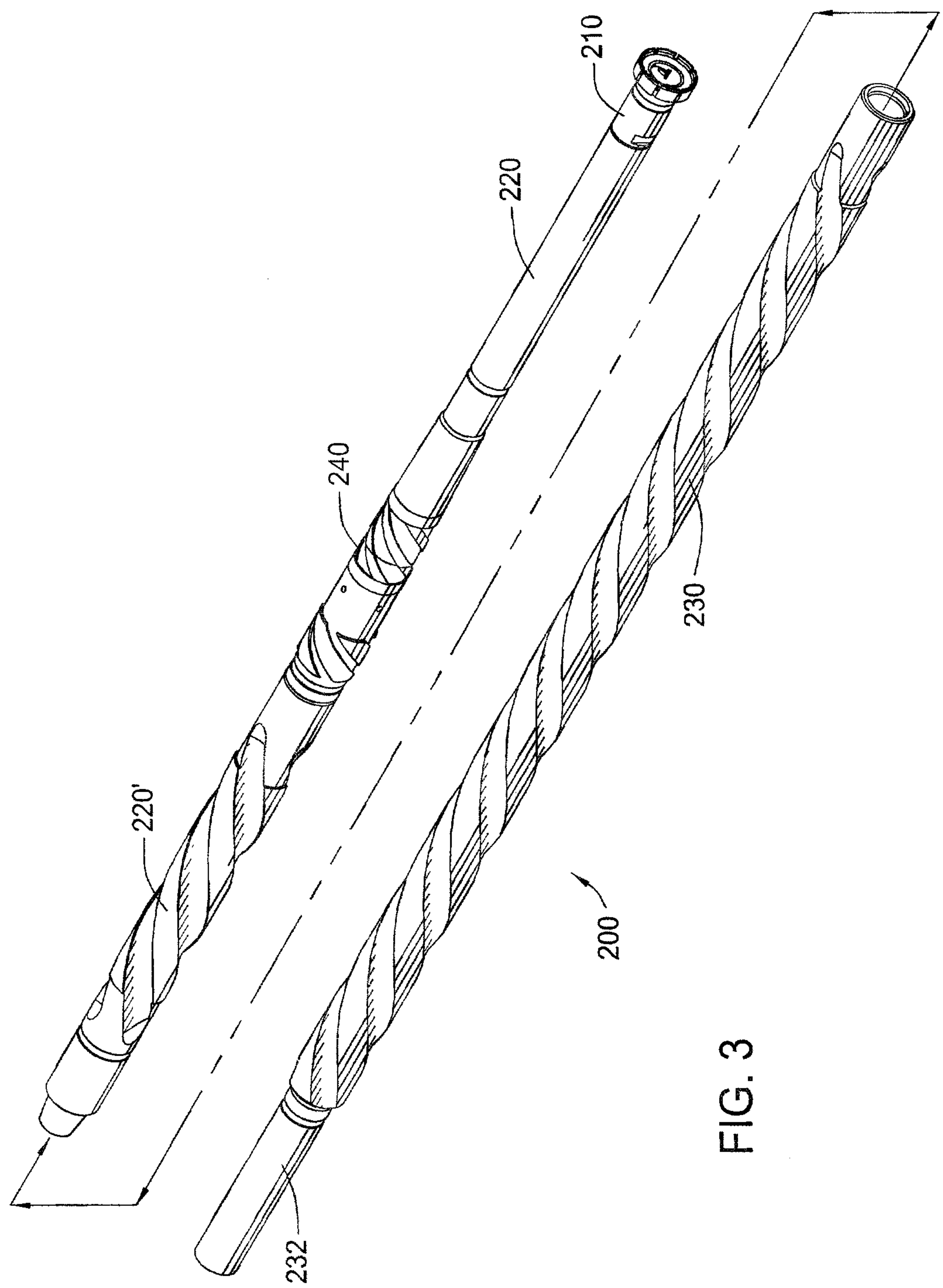


FIG. 3

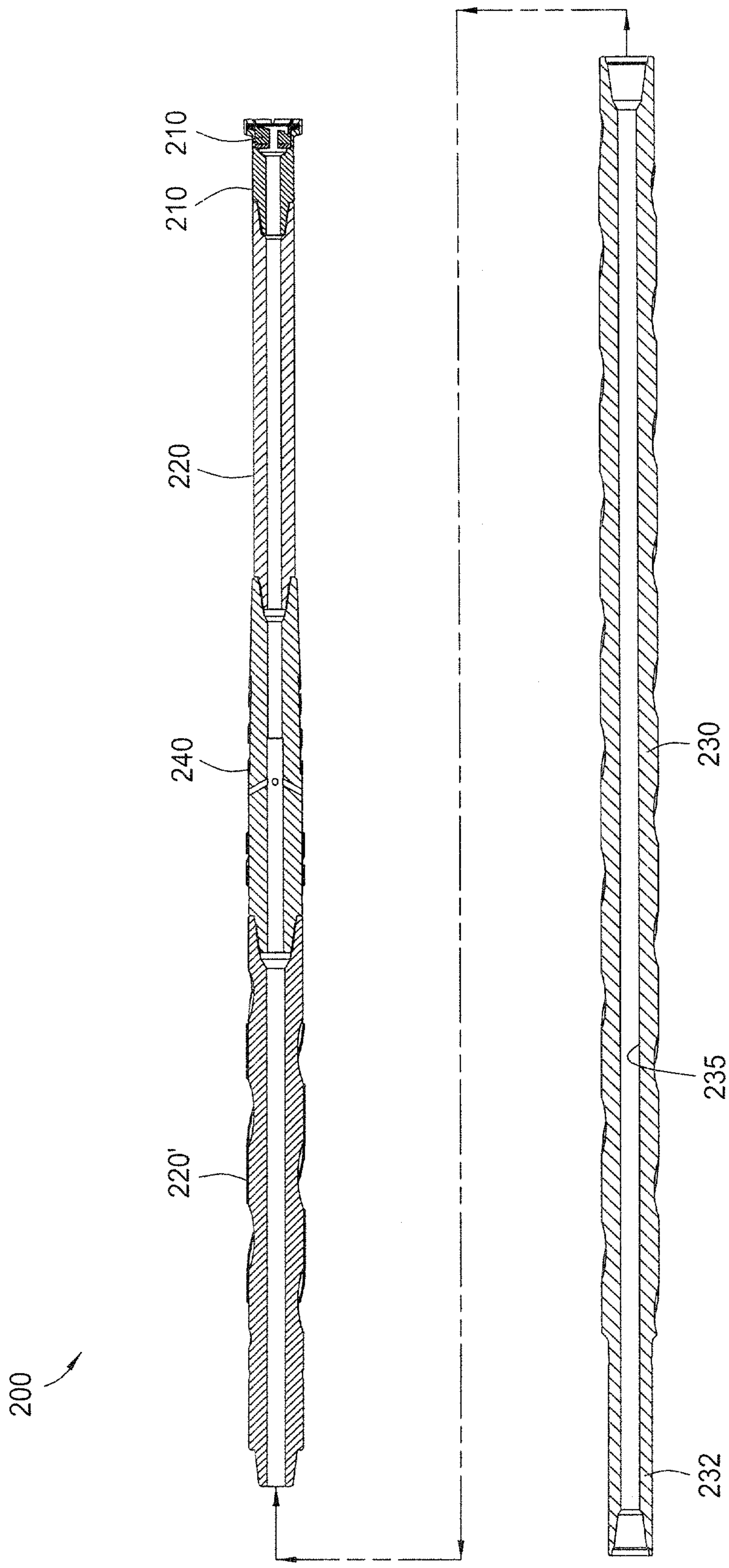


FIG. 4

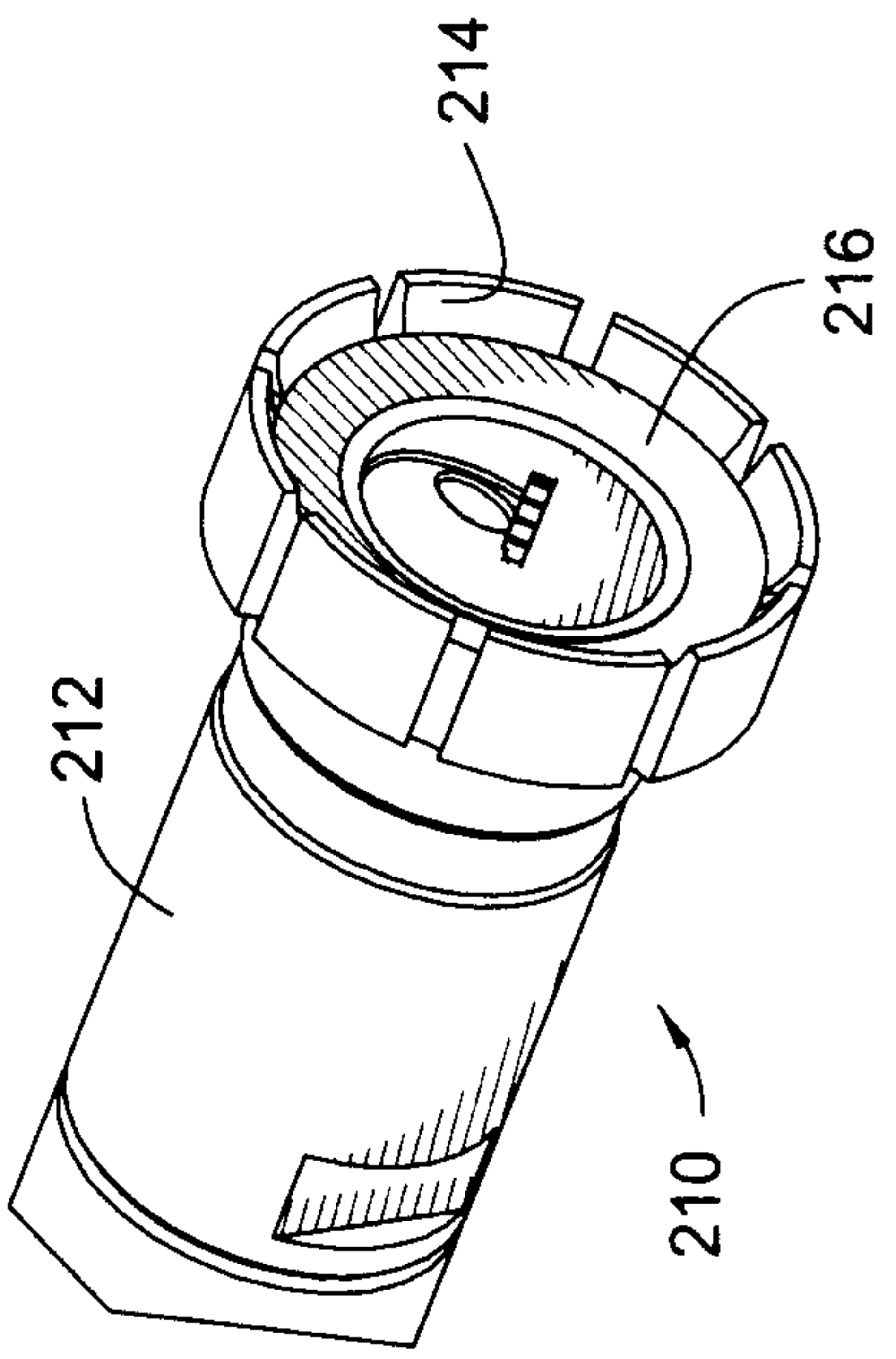


FIG. 5

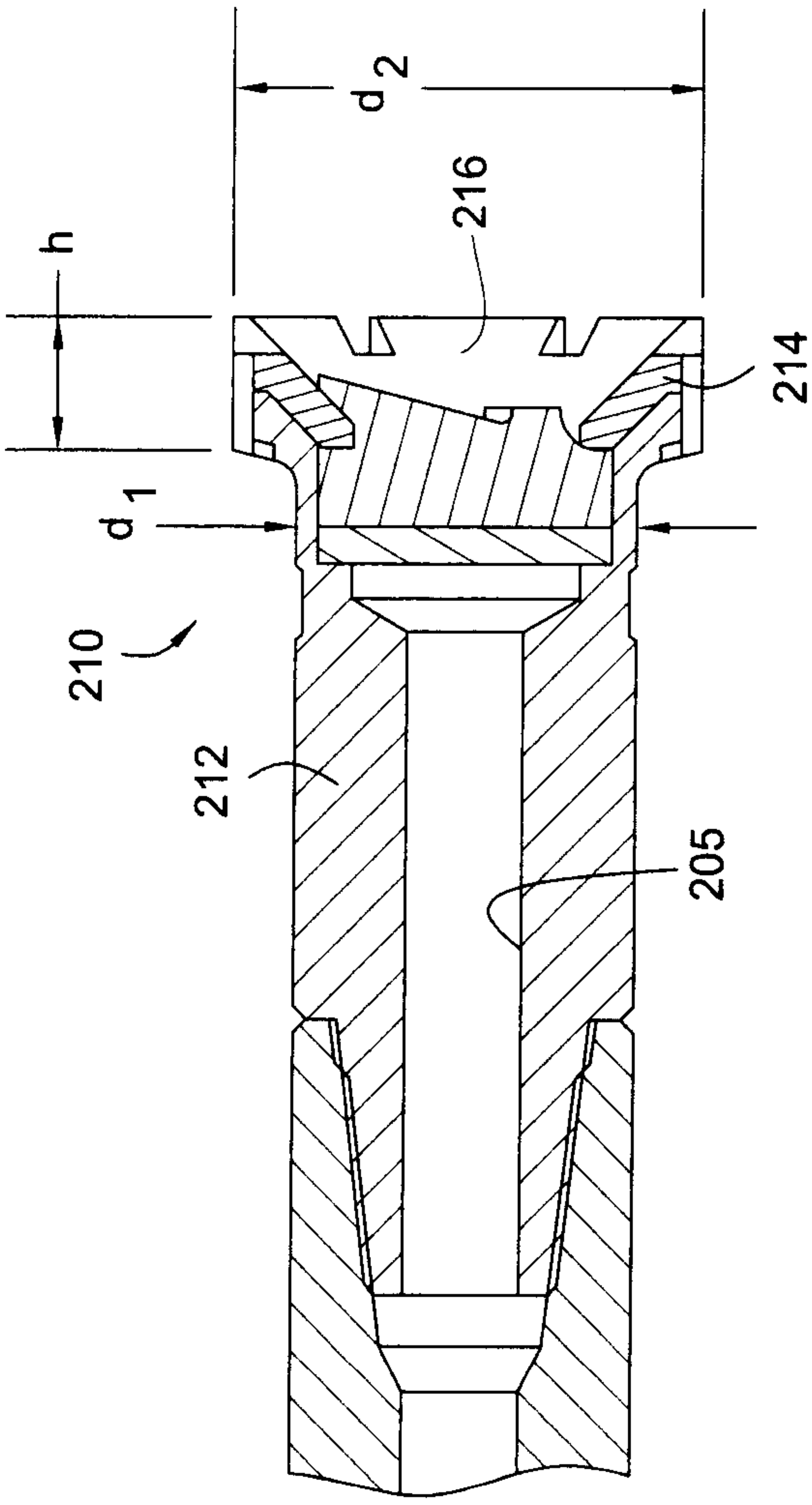


FIG. 6

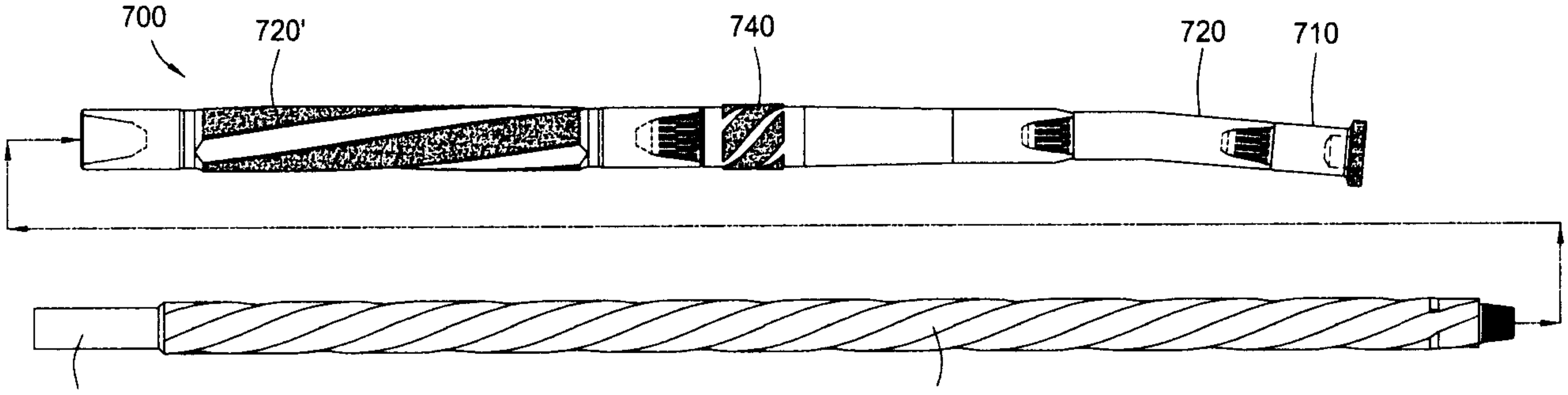


FIG. 7

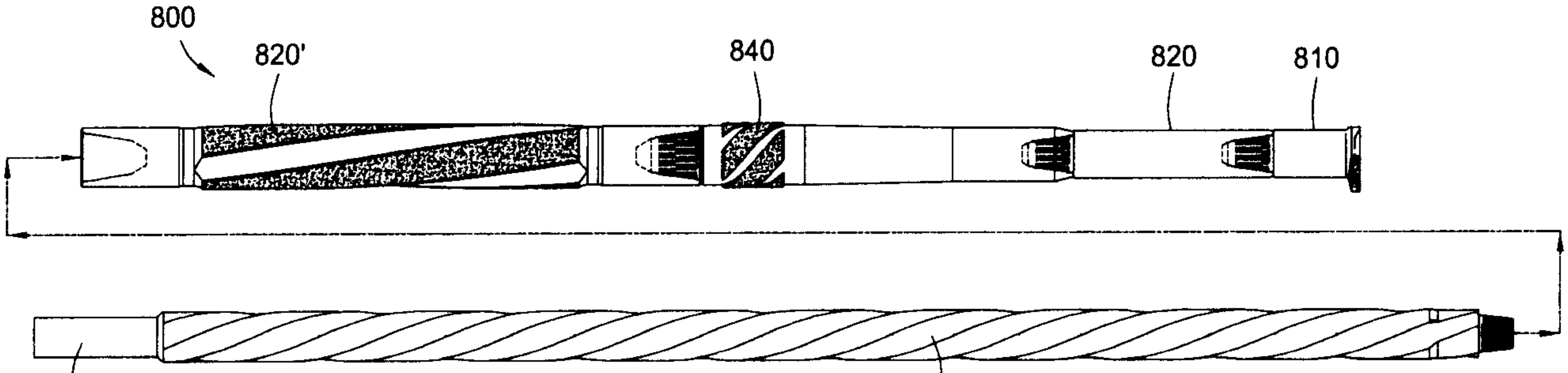
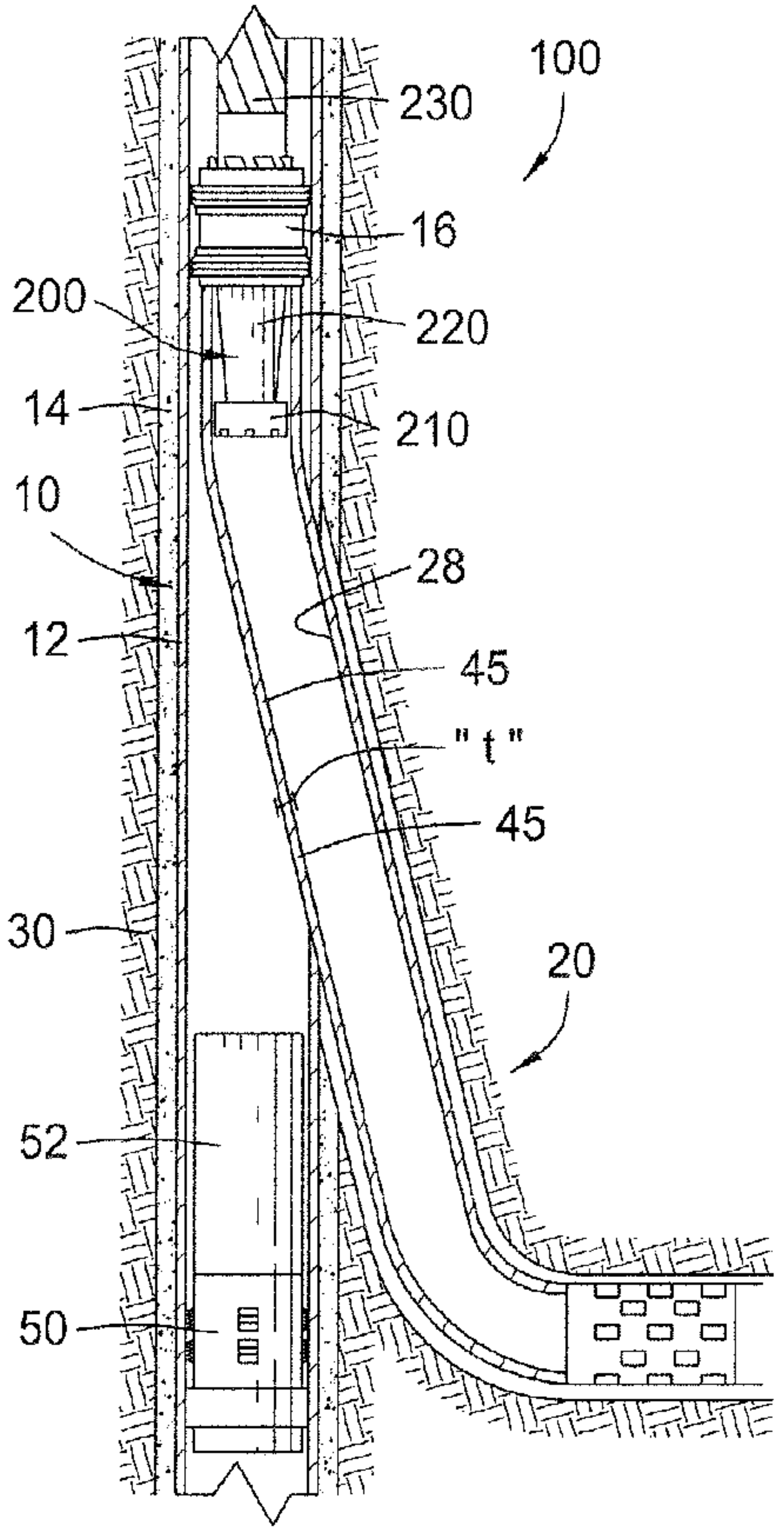


FIG. 8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