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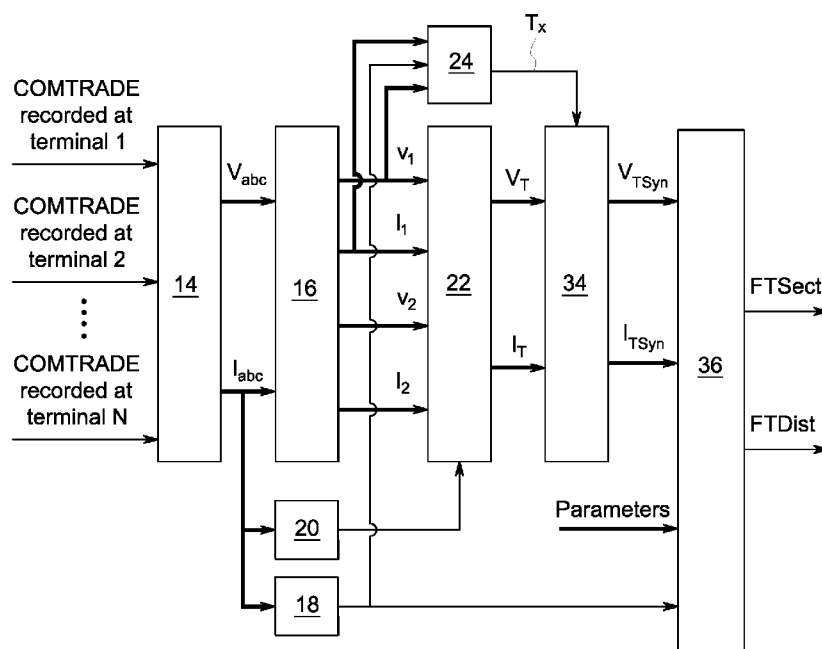


FIG. 2

(57) **Abstract:** In the field of power transmission schemes there is provided a method of locating a fault in a multi-terminal electrical power transmission scheme (10) in which each terminal (T1, T2, T3, T4, T5, T6) is connected with a junction (J1, J2, J3, J4) via a power transmission section (12) and the or each junction (J1, J2, J3, J4) interconnects a plurality of power transmission sections (12), the method comprising the steps of: (a) measuring the voltage and current at each terminal (T1, T2, T3, T4, T5, T6); (b) calculating from the measured voltage and current at each terminal (T1, T2, T3, T4, T5, T6) corresponding voltage and current phasors (V_1, I_1, V_2, I_2); (c) determining from the calculated voltage and current phasors (V_1, I_1) a synchronisation difference (Tp1, Tp2, Tp3, Tp4, Tp5) between the measured voltage and current at a designated terminal (T1) and the measured



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voltage and current at the or each other terminal (T2, T3, T4, T5, T6); (d) modifying the calculated voltage and current phasors (V_1 , I_1) to compensate for the or each synchronisation difference (Tp1, Tp2, Tp3, Tp4, Tp5); and (e) determining from the compensated voltage and current phasors (V_{TSyn} , I_{TSyn}) the location of the fault.

METHOD OF LOCATING A FAULT IN A POWER TRANSMISSION SCHEME

This invention relates to a method of locating a fault in a multi-terminal power transmission scheme.

5 According to an aspect of the invention there is provided a method of locating a fault in a multi-terminal electrical power transmission scheme in which each terminal is connected with a junction via a power transmission section and the or each junction interconnects a plurality of power transmission sections, the method comprising the steps of:

- 10 (a) measuring the voltage and current at each terminal;
- (b) calculating from the measured voltage and current at each terminal corresponding voltage and current phasors;
- (c) determining from the calculated voltage and current phasors a synchronisation difference between the measured voltage and current at a
15 designated terminal and the measured voltage and current at the or each other terminal;
- (d) modifying the calculated voltage and current phasors to compensate for the or each synchronisation difference; and
- (e) determining from the compensated voltage and current phasors
20 the location of the fault.

The voltage and current at each terminal are typically recorded, i.e. measured, by a disturbance recorder in a respective relay, i.e. a respective circuit breaker, which is operatively deployed with each terminal. More particularly the voltage and current values are usually recorded in a COMmon format of TRAnsient
25 Data Exchange (COMTRADE) format which provides for universal readability of the underlying data.

The method of the invention makes use of such readily available data to allow for the off-line determination of a fault location within an electrical power transmission scheme.

Preferably step (a) of measuring the voltage and current at each terminal
5 includes resampling the measured voltage and current from one or more terminals.

The voltage and current data, e.g. the COMTRADE data, from different terminals may have been obtained at different sampling rates, for example if the associated relays are produced by different manufacturers. Resampling the
10 measured voltage and current data from one or more terminals desirably permits all of the data to thereafter have the same equivalent sampling rate, and so facilitates subsequent use of all the data in the method of the invention.

Optionally the power transmission scheme is a multi-phase power transmission scheme, and

15 step (a) of measuring the voltage and current at each terminal includes measuring the voltage and current of each phase at each terminal, and

step (b) of calculating from the measured voltage and current at each terminal corresponding voltage and current phasors includes converting the measured phase voltages and phase currents into respective phase phasors
20 and then transforming the phase phasors into respective positive and negative sequence voltage phasors and positive and negative sequence current phasors.

The method may further include the step of determining from the measured phase currents whether a fault has occurred and if a fault has occurred whether it effects all phases.

25 In a preferred embodiment of the invention if the fault effects all phases then the positive sequence voltage and current phasors are used in subsequent steps of the invention, otherwise the negative sequence voltage and current phasors are used.

Positive sequence voltage and current phasors are always available, irrespective of the type of fault. Otherwise, so long as the fault does not effect all phases then the negative sequence voltage and current phasors are used in subsequent steps of the invention because they desirably omit load components and so are contaminated to a lesser extent under fault conditions.

Step (c) of determining from the calculated voltage and current phasors a synchronisation difference between the measured voltage and current at a designated terminal and the measured voltage and current at the or each other terminal may include:

- 10 - calculating, with respect to the designated terminal, an equivalent current flowing at the or each other terminal;
- equating, in respect of the or each other terminal, a sum of the measured current and the calculated equivalent current to zero according to Kirchhoff's first law; and
- 15 - extracting, in respect of the or each other terminal, a synchronisation difference between the measured voltage and current at the designated terminal and the measured voltage and current at the said respective other terminal from a corresponding equated sum of currents.

The calculation, with respect to the designated terminal, of an equivalent current flowing at the or each other terminal, provides the method of the invention with a desired degree of scalability and so permits its use with a wide range of different power transfer scheme configurations having, e.g. a significantly different number of terminals and/or junctions interconnecting those terminals

25 Meanwhile, equating, in respect of the or each other terminal, a sum of the measured current and the calculated equivalent current to zero according to Kirchhoff's first law readily and reliably permits the subsequent extraction of a corresponding synchronisation difference.

Preferably calculating, with respect to the designated terminal, an equivalent current flowing at the or each other terminal includes establishing an equivalent admittance matrix for the power transmission scheme.

5 The utilisation of an equivalent admittance matrix for the power transmission scheme to calculate an equivalent current flowing at the or each other terminal, has the benefit of removing from such a calculation any unknowns, e.g. regarding the status of current flow, in respect of the or each corresponding equivalent current, and so permits in a subsequent step the ready extraction of a corresponding synchronisation difference since the associated equated sum
10 of currents can be manipulated to include only one unknown, i.e. the required synchronisation difference.

In another preferred embodiment of the invention step (e) of determining from the compensated voltage and current phasors the location of the fault includes:

- designating a terminal at a first end of the power transmission
15 scheme as a first end terminal and a terminal at a second end of the power transmission scheme as a second end terminal;
- obtaining a first set of voltage phasors, wherein the first set of voltage phasors includes the compensated voltage phasor at the first end terminal and further includes respective voltage phasors at each of the second
20 end terminal and the or each junction that are determined based on the compensated first end terminal voltage phasor;
- obtaining a second set of voltage phasors, wherein the second set of voltage phasors includes the compensated voltage phasor at the second end terminal and further includes respective voltage phasors at each of the first
25 end terminal and the or each junction that are determined based on the compensated second end terminal voltage phasor; and
- comparing the first and second sets of voltage phasors to identify the power transmission section or junction corresponding to the location of the

fault, wherein each voltage phasor of the first set of voltage phasors is compared to the respective voltage phasor of the second set of voltage phasors that corresponds to the same end terminal or junction.

These steps not only result in efficient determination of the location of a fault in a power transmission scheme, but also are accurate due to the consideration of the distributed parameters of the power transmission scheme. In addition these steps are readily scalable to accommodate different topologies of power transmission scheme. The latter is particularly advantageous for use in a power transmission scheme with a complex layout, such as a multi-ended power transmission scheme.

These steps therefore permit quick determination of the location of a fault in a power transmission scheme, which reduces the time required to locate and repair the fault and thereby minimises the downtime of the power transmission scheme.

The method may further include the step, if a given power transmission section is identified as the location of the fault, of determining the distance of the fault along the power transmission section using corresponding voltages and currents of an equivalent two-ended system.

Such a step identifies with even more accuracy the location of the fault, and so reduces the time taken to find and deal with the said fault.

There now follows a brief description of preferred embodiments of the invention, by way of non-limiting example, with reference being made to the following figures in which:

Figure 1 shows a schematic representation of an example multi-terminal power transmission scheme;

Figure 2 shows a schematic view of an overall structure of a method according to a first embodiment of the invention;

Figure 3 shows various steps which take place within a second block shown in Figure 2;

Figure 4(a) shows various steps which take place within a fourth block shown in Figure 2;

5 Figure 4(b) shows a selection algorithm which forms one of the steps shown in Figure 4(a); and

Figure 5(a) shows an initial admittance representation of the power transmission scheme shown in Figure 1;

10 Figure 5(b) shows an equivalent admittance representation of the power transmission scheme shown in Figure 1;

Figure 6 shows various steps which take place within a seventh block shown in Figure 2; and

Figure 7 shows a schematic view of an implementation structure which lies within an eighth block shown in Figure 2.

15 An example multi-terminal electrical power transmission scheme is designated generally by reference numeral 10 and is shown schematically in Figure 1.

The power transmission scheme 10 includes first, second, third, fourth, fifth and sixth terminals T1, T2, T3, T4, T5, T6 and first, second, third and fourth junctions J1, J2, J3, J4. The terminals T1, T2, T3, T4, T5, T6 and junctions J1, J2, J3, J4
20 are interconnected with one another by respective power transmission sections 12, e.g. respective power transmission lines or other transmission conduits such as underground cables. The voltage and current at each terminal T1, T2, T3, T4, T5, T6 is measured and then recorded in the COMTRADE format.

Other multi-terminal power transmission schemes are also possible and the
25 method of the invention is equally capable of locating a fault in these other power transmission schemes.

Returning to the example power transmission scheme 10 shown, a method according to a first embodiment of the invention locates a fault with the transmission scheme 10.

The overall structure of the method is illustrated schematically in Figure 2 and
5 comprises the principle steps of:

(a) measuring the voltage and current at each terminal T1, T2, T3, T4, T5, T6;

(b) calculating from the measured voltage and current at each terminal T1, T2, T3, T4, T5, T6 corresponding voltage and current phasors V_1 ,
10 I_1 , V_2 , I_2 ;

(c) determining from the calculated voltage and current phasors V_1 , I_1 a synchronisation difference $Tp1$, $Tp2$, $Tp3$, $Tp4$, $Tp5$ between the measured voltage and current, i.e. the recorded COMTRADE data, at a designated terminal T1 and the measured voltage and current, i.e. the recorded
15 COMTRADE data, at each other terminal T2, T3, T4, T5, T6;

(d) modifying the calculated voltage and current phasors V_1 , I_1 , V_2 , I_2 to compensate for each synchronisation difference $Tp1$, $Tp2$, $Tp3$, $Tp4$, $Tp5$; and

(e) determining from the compensated voltage and current phasors
20 V_{TSyn} , I_{TSyn} the location of the fault.

More particularly, step (a) of measuring the voltage and current at each terminal T1, T2, T3, T4, T5, T6, i.e. reading the COMTRADE data recorded at each terminal T1, T2, T3, T4, T5, T6, additionally includes resampling the measured voltage and current from one or more of the terminals T1, T2, T3, T4, T5, T6.

25 By way of example, such resampling may include determining the minimum sampling rate of measured voltages and currents from all of the terminals T1,

T2, T3, T4, T5, T6 and down sampling, as needed, the other measured voltages and currents to the minimum sampling rate.

If the original sampling rate of one or more of the other measured voltages and currents is not an integer multiple of the minimum sampling rate then
 5 interpolation is needed. One possible interpolation algorithm (although others may be used) is

$$x_{resmp}(k) = x(n) + \Delta n[x(n+1) - x(n)]$$

where,

$x(n)$ is a sample series to be resampled;

10 x_{resmp} is the sample series after resampling;

n is $\text{floor}[kfs/f_{\min}]$;

Δn is $kfs/f_{\min} - n$;

fs is the original sampling rate; and

$f_{\min}$ is the minimum sampling rate

15 The example power transmission scheme 10 is a three-phase scheme (although the method of the invention is also applicable to schemes having fewer than or more than three phases), and so the aforementioned measuring and resampling steps are applied at each terminal T1, T2, T3, T4, T5, T6 to each phase a, b, c. The aforementioned measuring and resampling steps for
 20 each terminal T1, T2, T3, T4, T5, T6 take place inside a first block 14 within the overall structure shown in Figure 2.

Thereafter, step (b) of calculating from the measured voltage and current at each terminal corresponding voltage and current phasors takes place within a second block 16, and more particularly includes converting the measured
 25 phase voltages V_{abc} and phase currents I_{abc} into respective voltage phase

phasors V_a , V_b , V_c and current phase phasors I_a , I_b , I_c , and then transforming the voltage phase phasors V_a , V_b , V_c into respective positive and negative sequence voltage phasors V_1 , V_2 and the current phase phasors I_a , I_b , I_c into respective positive and negative sequence current phasors I_1 , I_2 .

- 5 One way of converting the measured phase voltages V_{abc} into respective voltage phase phasors V_a , V_b , V_c , and the measured phase currents I_{abc} into respective current phase phasors I_a , I_b , I_c , is to apply a Fourier transform of the type illustrated schematically in Figure 3.

More particularly, by way of example, the algorithm for the COS filter is

$$10 \quad X_{COS}(n) = \frac{2}{N} \sum_{k=1}^N x(n-N+k) \cos\left(\frac{2\pi k}{N} - \frac{\pi}{N}\right)$$

with the real and imaginary parts of each phasor V_a , V_b , V_c , I_a , I_b , I_c being

$$\begin{cases} X_{Re}(n) = X_{COS}(n-1) \\ X_{Im}(n) = [X_{COS}(n-2) - X_{COS}(n)] \cdot K \end{cases}$$

where,

K is $1/(2\sin(2\pi/N))$; and

- 15 N is the number of samples per cycle.

The three voltage phase phasors V_a , V_b , V_c can then be transformed into respective positive and negative sequence voltage phasors V_1 , V_2 according to

$$\begin{cases} V_1 = (V_a + aV_b + a^2V_c)/3 \\ V_2 = (V_a + a^2V_b + aV_c)/3 \end{cases}$$

- 20 and the current phase phasors I_a , I_b , I_c can be transformed into respective positive and negative sequence current phasors I_1 , I_2 according to

$$\begin{cases} I_1 = (I_a + aI_b + a^2I_c)/3 \\ I_2 = (I_a + a^2I_b + aI_c)/3 \end{cases}$$

In addition to the foregoing, the first embodiment method of the invention also includes the step of determining from the measured phase currents I_{abc} whether a fault has occurred and, if a fault has occurred, whether it effects all phases a, b, c.

Determining whether a fault has occurred, which takes place within a third block 18 shown in Figure 2, may be carried out according to any technique well known to a person skilled in the art, such as considering the sum of negative sequence current, zero sequence current and phase current, or by considering delta phase current.

Meanwhile, one way (if a fault is determined to have occurred) of determining whether the fault effects all phases a, b, c is to consider respective delta phase to phase currents Δi_{ab} , Δi_{bc} , Δi_{ca} in the manner illustrated schematically in Figures 4(a) and 4(b). Such consideration takes place within a fourth block 20 in Figure 2.

More particularly, once respective delta phase to phase currents Δi_{ab} , Δi_{bc} , Δi_{ca} have been calculated according to

$$\begin{cases} \Delta i_{ab}(n) = [i_a(n) - i_b(n)] - [i_a(n-N) - i_b(n-N)] \\ \Delta i_{bc}(n) = [i_b(n) - i_c(n)] - [i_b(n-N) - i_c(n-N)] \\ \Delta i_{ca}(n) = [i_c(n) - i_a(n)] - [i_c(n-N) - i_a(n-N)] \end{cases}$$

where N is the number of samples per cycle,

then Root Mean Squared (RMS) values of delta phase to phase currents ΔI_{ab} , ΔI_{bc} , ΔI_{ca} are calculated, e.g. using a half-cycle Fourier integral as shown below

$$X_{RMS}(n) = \frac{\pi}{\sqrt{2}N} \sum_{k=1}^N \left| x\left(n - \frac{N}{2} + k\right) \right|$$

where N is again the number of samples per cycle.

Other ways of calculating Root Mean Squared (RMS) values of delta phase to phase currents ΔI_{ab} , ΔI_{bc} , ΔI_{ca} are also possible, however, such as a one-cycle Fourier method or by a norm calculation.

Thereafter the or each faulty phase may be determined by applying the selection algorithm illustrated schematically in Figure 4(b), i.e. so as to identify a single phase fault to ground AG, BG, CG; a two-phase fault between two phases or between two phases and ground AB/ABG; BC/BCG, CA/CAG; or a three phase fault ABC.

If the fault effects all phases a, b, c then the first embodiment method of the invention determines that the positive sequence voltage and current phasors V_1 , I_1 are to be used in subsequent steps of the method. Otherwise, i.e. if some other fault of those identified above occurs, the method of the invention determines that the negative sequence voltage and current phasors V_2 , I_2 are to be used subsequently in the method. Such determination of whether to use positive or negative sequence phasors takes place within a fifth block 22 in the Figure 2 structure and leads to the use in some subsequent steps of the method of the invention of a selected voltage phasor V_T and a selected current phasor I_T corresponding to each terminal T1, T2, T3, T4, T5, T6.

Meanwhile step (c), i.e. determining from the calculated voltage and current phasors (e.g. the positive sequence voltage and current phasors V_1 , I_1) a synchronisation difference Tp1, Tp2, Tp3, Tp4, Tp5 between the measured voltage and current at a designated terminal T1 and the measured voltage and current at each other terminal T2, T3, T4, T5, T6, takes place within a sixth block 24 shown in Figure 2.

The main steps within step (c) are:

- calculating, with respect to the designated terminal T1, an equivalent current flowing at the or each other terminal T2, T3, T4, T5, T6;
- equating, in respect of the or each other terminal T2, T3, T4, T5, T6, a sum of the measured current i_{JR1} , i_{JR2} , i_{JR3} , i_{JR4} , i_{JR5} and the calculated equivalent current i_{JR1_L} , i_{JR2_L} , i_{JR3_L} , i_{JR4_L} , i_{JR5_L} to zero according to Kirchhoff's first law; and
- extracting, in respect of the or each other terminal T2, T3, T4, T5, T6, a synchronisation difference $Tp1$, $Tp2$, $Tp3$, $Tp4$, $Tp5$ between the measured voltage and current at the designated terminal T1 and the measured voltage and current at the said respective other terminal T2, T3, T4, T5, T6 from a corresponding equated sum of currents.

For the purpose of describing step (c) in more detail the additional nomenclature shown in Figure 1 is adopted with respect to the six terminals T1, T2, T3, T4, T5, T6. More particularly, the designated terminal T1, i.e. the first terminal T1, is referred to as a local terminal L and each of the other second, third, fourth, fifth and sixth terminals T2, T3, T4, T5, T6 is considered respectively as a first, second, third, fourth and fifth remote terminal R1, R2, R3, R4, R5.

It should be noted that the first terminal T1 need not necessarily be the designated terminal, i.e. need not necessarily be referred to as the local terminal L, and that in other embodiments of the method of the invention one of the other terminals T2, T3, T4, T5, T6 may instead be the designated terminal (and hence considered, for the purpose of identifying respective synchronisation differences, as the local terminal L).

Calculating, with respect to the designated terminal (T1), an equivalent current flowing at each other terminal T2, T3, T4, T5, T6, i.e. calculating respective first, second, third, fourth and fifth equivalent currents i_{JR1_L} , i_{JR2_L} , i_{JR3_L} , i_{JR4_L} , i_{JR5_L} at each of the first, second, third, fourth and fifth remote terminals R1, R2, R3, R4, R5, includes:

establishing an equivalent admittance y_{eR1} , y_{eR2} , y_{eR3} , y_{eR4} , y_{eR5} for each remote terminal R1, R2, R3, R4, R5;

establishing an initial admittance matrix Y_0 with respect to the or each junction, i.e. the first, second, third and fourth junctions J1, J2, J3, J4 in the particular example embodiment shown;

combining the equivalent admittance y_{eR1} , y_{eR2} , y_{eR3} , y_{eR4} , y_{eR5} for each remote terminal R1, R2, R3, R4, R5 with the initial admittance matrix Y_0 to establish an equivalent admittance matrix Y_{Mod} ;

obtaining a local equivalent current i_{JL} ; and

utilising the equivalent admittance matrix Y_{Mod} and the local equivalent current i_{JL} to calculate the corresponding equivalent current i_{JR1_L} , i_{JR2_L} , i_{JR3_L} , i_{JR4_L} , i_{JR5_L} for each remote terminal R1, R2, R3, R4, R5.

In terms of establishing an equivalent admittance y_{eR1} , y_{eR2} , y_{eR3} , y_{eR4} , y_{eR5} for each remote terminal R1, R2, R3, R4, R5, each of the currents i_{JR2} , i_{JR3} , i_{JR4} , i_{JR5} measured at the second, third, fourth and fifth remote terminals R2, R3, R4, R5 can be considered instead as a corresponding equivalent second, third, fourth and fifth admittance y_{eR2} , y_{eR3} , y_{eR4} , y_{eR5} .

The equivalent admittance y_{eR1} , y_{eR2} , y_{eR3} , y_{eR4} , y_{eR5} for each remote terminal R1, R2, R3, R4, R5 may be established by a sample based method or a Fourier based method.

By way of example, the method of the invention utilises a Fourier based method whereby

$$y_{eR1} = \frac{i_{JR1}}{\hat{V}_{JR1}}$$

$$y_{eR2} = \frac{i_{JR2}}{\hat{V}_{JR2}}$$

$$y_{eR3} = \frac{\dot{I}_{JR3}}{\dot{V}_{JR3}}$$

$$y_{eR4} = \frac{\dot{I}_{JR4}}{\dot{V}_{JR4}}$$

$$y_{eR5} = \frac{\dot{I}_{JR5}}{\dot{V}_{JR5}}$$

where,

5 $\dot{I}_{JR1}$ is the Fourier phasor of the measured current i_{JR1} at the first remote terminal R1, i.e. is the positive sequence current phasor I_1 corresponding to the first remote terminal R1, which embodies a first synchronisation difference, e.g. a first time difference $Tp1$, between the measured voltage and current at the first remote terminal R1 and the measured voltage and current at the local
10 terminal L;

$\dot{V}_{JR1}$ is the Fourier phasor of the measured voltage v_{JR1} at the first remote terminal R1, i.e. is the positive sequence voltage phasor V_1 corresponding to the first remote terminal R1 (which can be calculated from the COMTRADE data for the first remote terminal R1), and which again embodies a first
15 synchronisation difference $Tp1$;

$\dot{I}_{JR2}$ is the Fourier phasor of the measured current i_{JR2} at the second remote terminal R2, i.e. is the positive sequence current phasor I_1 corresponding to the second remote terminal R2, which embodies a second synchronisation difference, e.g. a second time difference $Tp2$, between the
20 measured voltage and current at the second remote terminal R2 and the measured voltage and current at the local terminal L;

$\dot{V}_{JR2}$ is the Fourier phasor of the measured voltage v_{JR2} at the second remote terminal R2, i.e. is the positive sequence voltage phasor V_1 corresponding to the second remote terminal R2 (which can be similarly

calculated from corresponding COMTRADE data), and which again embodies a second synchronisation difference $Tp2$;

$\dot{I}_{JR3}$ is the Fourier phasor of the measured current i_{JR3} at the third remote terminal R3, i.e. is the positive sequence current phasor I_1 corresponding to the third remote terminal R3, which embodies a third synchronisation difference, e.g. a third time difference $Tp3$, between the measured voltage and current at the third remote terminal R3 and the measured voltage and current at the local terminal L;

$\dot{V}_{JR3}$ is the Fourier phasor of the measured voltage v_{JR3} at the third remote terminal R3, i.e. is the positive sequence voltage phasor V_1 corresponding to the third remote terminal R3 (which can be similarly calculated from corresponding COMTRADE data), and which again embodies a third synchronisation difference $Tp3$;

$\dot{I}_{JR4}$ is the Fourier phasor of the measured current i_{JR4} at the fourth remote terminal R4, i.e. is the positive sequence current phasor I_1 corresponding to the fourth remote terminal R4, which embodies a fourth synchronisation difference, e.g. a fourth time difference $Tp4$, between the measured voltage and current at the fourth remote terminal R4 and the measured voltage and current at the local terminal L;

$\dot{V}_{JR4}$ is the Fourier phasor of the measured voltage v_{JR4} at the fourth remote terminal R4, i.e. is the positive sequence voltage phasor V_1 corresponding to the fourth remote terminal R4 (which can be similarly calculated from corresponding COMTRADE data), and which again embodies a fourth synchronisation difference $Tp4$;

$\dot{I}_{JR5}$ is the Fourier phasor of the measured current i_{JR5} at the fifth remote terminal R5, i.e. is the positive sequence current phasor I_1 corresponding to the fifth remote terminal R5, which embodies a fifth synchronisation difference, e.g. a fifth time difference $Tp5$, between the measured voltage and current at the

fifth remote terminal R5 and the measured voltage and current at the local terminal L; and

$\dot{V}_{JR5}$ is the Fourier phasor of the measured voltage v_{JR5} at the fifth remote terminal R5, i.e. is the positive sequence voltage phasor V_1 corresponding to the fifth remote terminal R5 (which can be similarly calculated from corresponding COMTRADE data), and which again embodies a fifth synchronisation difference $Tp5$.

Thereafter, an initial admittance matrix Y_0 is established with respect to the first, second, third and fourth junctions J1, J2, J3, J4, i.e. with respect only to the power transmission sections 12 between adjacent pairs of junctions J1-J2, J2-J3, J3-J4, in accordance with the initial admittance representation 44 of the power transmission scheme (10) shown in Figure 5(a), to give:

$$Y_0 = \begin{bmatrix} y_{12} + \frac{1}{z_{12}} & -\frac{1}{z_{12}} & 0 & 0 \\ -\frac{1}{z_{12}} & y_{12} + \frac{1}{z_{12}} + \frac{1}{z_{23}} + y_{23} & -\frac{1}{z_{23}} & 0 \\ 0 & -\frac{1}{z_{23}} & y_{23} + \frac{1}{z_{23}} + \frac{1}{z_{34}} + y_{34} & -\frac{1}{z_{34}} \\ 0 & 0 & -\frac{1}{z_{34}} & y_{34} + \frac{1}{z_{34}} \end{bmatrix}$$

Following such a step, the initial admittance matrix Y_0 is then combined with the equivalent admittance y_{eR1} , y_{eR2} , y_{eR3} , y_{eR4} , y_{eR5} for each remote terminal R1, R2, R3, R4, R5 to establish an equivalent admittance matrix Y_{Mod} in accordance with the equivalent admittance representation 46 of the power transmission scheme (10) shown in Figure 5(b), i.e.:

$$Y_{Mod} = \begin{bmatrix} y_{12} + \frac{1}{z_{12}} + y_{eR1} & -\frac{1}{z_{12}} & 0 & 0 \\ -\frac{1}{z_{12}} & y_{12} + \frac{1}{z_{12}} + \frac{1}{z_{23}} + y_{23} + y_{eR2} & -\frac{1}{z_{23}} & 0 \\ 0 & -\frac{1}{z_{23}} & y_{23} + \frac{1}{z_{23}} + \frac{1}{z_{34}} + y_{34} + y_{eR3} & -\frac{1}{z_{34}} \\ 0 & 0 & -\frac{1}{z_{34}} & y_{34} + \frac{1}{z_{34}} + y_{eR4} + y_{eR5} \end{bmatrix}$$

Meanwhile the local equivalent current i_{JL} , i.e. a designated equivalent current, is obtained from the measured current i_L at the local terminal L (available from corresponding COMTRADE data) by using the measured current i_L at the local terminal L to calculate the local equivalent current i_{JL} using a resistor-inductor model of the power transmission section 12 between the local terminal L and the first junction J1.

More particularly the power transmission section 12 between the local terminal L and the first junction J1 is regarded as a resistor-inductor series-connected circuit and, because the section is an overhead transmission line that is less than approximately 50km, the shunt admittance can be neglected such that the local equivalent current i_{JL} is given by

$$i_{JL} = i_L$$

A similar resistor-inductor model can be used in other embodiments of the method when applied to a network in which the corresponding section of transmission medium between the local terminal and the first junction J1 is defined by an underground cable that is less than approximately 3km.

In other embodiments of the method of invention, when applied to a network in which the power transmission section between the local terminal and the first junction is defined either by an overhead transmission line between approximately 50km and 150km in length, or by an underground cable that is between approximately 3km and 20km in length, the local equivalent current i_{JL} can be obtained using a linear resistor-inductor-capacitor model of the aforesaid section of transmission medium, i.e. the parameters of resistance, inductance (or reactance) and shunt capacitance (or admittance) are considered to vary linearly along the said section. Such a linear resistor-inductor-capacitor model may also be known as a pi-equivalent circuit.

In such embodiments the local equivalent current i_{JL} can be obtained by a sample based method or by a Fourier phase based method.

In terms of the Fourier phase based method, the local equivalent current i_{JL} is given by

$$i_{JL} = i_L - y_L \dot{V}_L / 2$$

where,

5 $\dot{I}_L$ is the Fourier phasor of measured current i_L at the local terminal L, i.e. is the positive sequence current phasor I_1 corresponding to the local terminal L ;

$\dot{V}_L$ is the Fourier phasor of measured voltage v_L at the local terminal L, i.e. is the positive sequence voltage phasor V_1 , corresponding to the local
10 terminal L;

$\dot{I}_{JL}$ is the Fourier phasor of the local equivalent current i_{JL} ; and

y_L is the shunt admittance of the power transmission section 12 between the local terminal L and the first junction J1.

With regards to the last parameter, i.e. the shunt admittance y_L , this can be
15 determined by multiplying the admittance per length (which can be obtained from the operator of the said power transmission section 12) by the total length of the section.

In still further embodiments of the method of invention, when applied to a network in which the power transmission section 12 between the local terminal
20 and the first junction is defined either by an overhead transmission line over approximately 150km in length, or by an underground cable that is over approximately 20km in length, the local equivalent current i_{JL} can be obtained using a distributed parameter model of the aforesaid power transmission section 12.

In such embodiments the local equivalent current i_{JL} can be obtained by a sample based method or by a Fourier phase based method, with the Fourier phase based method yielding the local node current i_{JL} according to

$$\dot{I}_{JL} = \cosh(\gamma D) \dot{I}_L - \sinh(\gamma D) \dot{V}_L / Z_C$$

5 where,

$\dot{I}_L$ is the Fourier phasor of measured current i_L at the local terminal L, i.e. is the positive sequence current phasor I_1 corresponding to the local terminal L;

$\dot{V}_L$ is the Fourier phasor of measured voltage v_L at the local terminal L, i.e. is the positive sequence voltage phasor V_1 , corresponding to the local
10 terminal L;

$\gamma = \sqrt{zy}$ is the propagation coefficient of the power transmission section 12, with z being the impedance per length and y being the shunt admittance per length of the power transmission section;

$Z_C = \sqrt{z/y}$ is the character impedance of the power transmission section,
15 with z again being the impedance per length and y being the shunt admittance per length of the power transmission section; and

D is the length of the power transmission section between the local terminal L and the calculation node, i.e. the first junction J1.

The equivalent admittance matrix Y_{Mod} and the local equivalent current i_{JL} are
20 then utilised to calculate the corresponding equivalent current i_{JR1_L} , i_{JR2_L} , i_{JR3_L} , i_{JR4_L} , i_{JR5_L} for each remote terminal R1, R2, R3, R4, R5 by, first of all determining an equivalent voltage $\dot{V}_{J1\_L}$, $\dot{V}_{J2\_L}$, $\dot{V}_{J3\_L}$, $\dot{V}_{J4\_L}$ at each junction J1, J2, J3, J4 according to:

$$\begin{bmatrix} \dot{V}_{J1\_L} \\ \dot{V}_{J2\_L} \\ \dot{V}_{J3\_L} \\ \dot{V}_{J4\_L} \end{bmatrix} = Y_{Mod} \begin{bmatrix} \dot{I}_{JL} \\ 0 \\ 0 \\ 0 \end{bmatrix}, \text{ and}$$

then determining each equivalent current i_{JR1_L} , i_{JR2_L} , i_{JR3_L} , i_{JR4_L} , i_{JR5_L} according to:

$$\begin{aligned} \dot{I}_{JR1\_L} &= y_{eR1} \dot{V}_{J1\_L} \\ 5 \quad \dot{I}_{JR2\_L} &= y_{eR2} \dot{V}_{J2\_L} \\ \dot{I}_{JR3\_L} &= y_{eR3} \dot{V}_{J3\_L} \\ \dot{I}_{JR4\_L} &= y_{eR4} \dot{V}_{J4\_L} \\ \dot{I}_{JR5\_L} &= y_{eR5} \dot{V}_{J4\_L} \end{aligned}$$

where,

$$\begin{aligned} 10 \quad \dot{I}_{JR1\_L} &\text{ is the Fourier phasor of the first equivalent current } i_{JR1\_L}; \\ \dot{I}_{JR2\_L} &\text{ is the Fourier phasor of the second equivalent current } i_{JR2\_L}; \\ \dot{I}_{JR3\_L} &\text{ is the Fourier phasor of the third equivalent current } i_{JR3\_L}; \\ \dot{I}_{JR4\_L} &\text{ is the Fourier phasor of the fourth equivalent current } i_{JR4\_L}; \\ \dot{I}_{JR5\_L} &\text{ is the Fourier phasor of the fifth equivalent current } i_{JR5\_L}; \text{ and} \\ 15 \quad \dot{I}_{JL} &\text{ is the Fourier phasor of the local equivalent current } i_{JL}. \end{aligned}$$

Thereafter, the step of equating, in respect of each remote terminal R1, R2, R3, R4, R5 a sum of the measured current i_{JR1} , i_{JR2} , i_{JR3} , i_{JR4} , i_{JR5} and the calculated

equivalent current i_{JR1_L} , i_{JR2_L} , i_{JR3_L} , i_{JR4_L} , i_{JR5_L} to zero according to Kirchhoff's first law, includes:

- for the first remote terminal R1, equating to zero the sum of the first calculated equivalent current i_{JR1_L} and the first measured current i_{JR1} ;
 - 5 – for the second remote terminal R2, equating to zero the sum of the second calculated equivalent current i_{JR2_L} and the second measured current i_{JR2} ;
 - for the third remote terminal R3, equating to zero the sum of the third calculated equivalent current i_{JR3_L} and the third measured current i_{JR3} ;
 - 10 – for the fourth remote terminal R4, equating to zero the sum of the fourth calculated equivalent current i_{JR4_L} and the fourth measured current i_{JR4} ;
and
 - for the fifth remote terminal R5, equating to zero the sum of the fifth calculated equivalent current i_{JR5_L} and the fifth measured current i_{JR5} .
- 15 In other words, according to Kirchhoff's first law the sum of all currents flowing into the same node, i.e. the corresponding remote terminal R1, R2, R3, R4, R5, must be zero such that in respect of the first remote terminal R1

$$i_{JR1L} + i_{JR1} = 0$$

in respect of the second remote terminal R2

$$20 \quad i_{JR2L} + i_{JR2} = 0$$

in respect of the third remote terminal R3

$$i_{JR3L} + i_{JR3} = 0$$

in respect of the fourth remote terminal R4

$$i_{JR4L} + i_{JR4} = 0$$

and in respect of the fifth remote terminal R5

$$i_{JR5\_L} + i_{JR5} = 0$$

Following the above, the step of extracting, in respect of each remote terminal R1, R2, R3, R4, R5 a corresponding synchronisation difference, which in the preferred embodiment described takes the form of a time difference Tp1, Tp2, Tp3, Tp4, Tp5 (although in other embodiments it may instead be a phase difference), between the measured voltage and current at the local terminal L and the measured voltage and current at the said respective remote terminal R1, R2, R3, R4, R5 from a corresponding equated sum of currents, i.e. from a corresponding one of the sums set out above, includes considering the phase of the said currents.

Accordingly, adopting a Fourier transform method to rewrite the sums set out above in a phasor form, and utilising respective phasors of the measured currents i_{JR1} , i_{JR2} , i_{JR3} , i_{JR4} , i_{JR5} at each remote terminal R1, R2, R3, R4, R5 to incorporate the corresponding synchronisation difference, i.e. corresponding time difference Tp1, Tp2, Tp3, Tp4, Tp5 gives, in respect of the first remote terminal R1

$$\dot{i}_{JR1\_L} + \dot{i}_{JR1} e^{j\omega_0 T_{p1}} = 0$$

where,

$\dot{i}_{JR1\_L}$ is the Fourier phasor of the first equivalent current i_{JR1_L} ;

$\dot{i}_{JR1}$ is the Fourier phasor of the first measured current i_{JR1} at the first remote terminal R1, i.e. is the positive sequence current phasor I_1 corresponding to the first remote terminal R1; and

f is frequency of the currents i_{JR1_L} , i_{JR1} ,

in respect of the second remote terminal R2

$$\dot{i}_{JR2\_L} + \dot{i}_{JR2} e^{j\omega_0 T_{p2}} = 0$$

where,

$\dot{I}_{JR2\_L}$ is the Fourier phasor of the second equivalent current i_{JR2_L} ;

$\dot{I}_{JR2}$ is the Fourier phasor of the second measured current i_{JR2} at the second remote terminal R2, i.e. is the positive sequence current phasor I_1 corresponding to the second remote terminal R2; and

f is frequency of the currents i_{JR2_L} , i_{JR2} ,

in respect of the third remote terminal R3

$$\dot{I}_{JR3\_L} + \dot{I}_{JR3} e^{j\omega_0 T_{p3}} = 0$$

where,

$\dot{I}_{JR3\_L}$ is the Fourier phasor of the third equivalent current i_{JR3_L} ;

$\dot{I}_{JR3}$ is the Fourier phasor of the third measured current i_{JR3} at the third remote terminal R3, i.e. is the positive sequence current phasor I_1 corresponding to the third remote terminal R3; and

f is frequency of the currents i_{JR3_L} , i_{JR3} ,

in respect of the fourth remote terminal R4

$$\dot{I}_{JR4\_L} + \dot{I}_{JR4} e^{j\omega_0 T_{p4}} = 0$$

where,

$\dot{I}_{JR4\_L}$ is the Fourier phasor of the fourth equivalent current i_{JR4_L} ;

$\dot{I}_{JR4}$ is the Fourier phasor of the fourth measured current i_{JR4} at the fourth remote terminal R4, i.e. is the positive sequence current phasor I_1 corresponding to the fourth remote terminal R4; and

f is frequency of the currents i_{JR4_L} , i_{JR4} , and

in respect of the fifth remote terminal R5

$$\dot{I}_{JR5\_L} + \dot{I}_{JR5} e^{j\omega_0 T_{p5}} = 0$$

where,

$\dot{I}_{JR5\_L}$ is the Fourier phasor of the fifth equivalent current i_{JR5_L} ;

- 5 $\dot{I}_{JR5}$ is the Fourier phasor of the fifth measured current i_{JR5} at the fifth remote terminal R5, i.e. is the positive sequence current phasor I_1 corresponding to the fifth remote terminal R5; and

f is frequency of the currents i_{JR5_L} , i_{JR5} .

- Each of the foregoing sums is then rearranged to give the corresponding time
10 difference T_{p1} , T_{p2} , T_{p3} , T_{p4} , T_{p5} , i.e. such that the first time difference T_{p1} is given by

$$T_{p1} = \frac{\arg(-\dot{I}_{JR1\_L}/\dot{I}_{JR1})}{2\pi f}$$

where $\arg$ gives the angle of the aforementioned Fourier phasors,

the second time difference T_{p2} is given by

15
$$T_{p2} = \frac{\arg(-\dot{I}_{JR2\_L}/\dot{I}_{JR2})}{2\pi f}$$

the third initial time difference T_{p3} is given by

$$T_{p3} = \frac{\arg(-\dot{I}_{JR3\_L}/\dot{I}_{JR3})}{2\pi f}$$

the fourth time difference T_{p4} is given by

$$T_{p4} = \frac{\arg(-\dot{I}_{JR4\_L}/\dot{I}_{JR4})}{2\pi f}$$

and such that the fifth time difference T_{p5} is given by

$$T_{p5} = \frac{\arg(-\dot{I}_{JR5\_L}/\dot{I}_{JR5})}{2\pi f}$$

Following the determination of the synchronisation difference, i.e. the time difference T_{p1} , T_{p2} , T_{p3} , T_{p4} , T_{p5} between the voltage and current measured
 5 at the local terminal L, i.e. the designated first terminal T1, and the voltage and current measured at each remote terminal R1, R2, R3, R4, R5, i.e. each other terminal T2, T3, T4, T5, T6, the method of the invention carries out principle step (d) of modifying the calculated voltage and current phasors, i.e. modifying the selected voltage and current phasors V_T , I_T for each terminal T1, T2, T3, T4,
 10 T5, T6, to compensate for the synchronisation differences, i.e. the time differences T_{p1} , T_{p2} , T_{p3} , T_{p4} , T_{p5} .

Such compensation takes place within a seventh block 34 shown in Figure 2, and may be carried out by applying a compensation factor to the selected voltage and current phasors V_T , I_T for each terminal T1, T2, T3, T4, T5, T6 (i.e.
 15 $V_{T(T1)}$, $I_{T(T1)}$ for the first terminal T1; $V_{T(T2)}$, $I_{T(T2)}$ for the second terminal T2; $V_{T(T3)}$, $I_{T(T3)}$ for the third terminal T3; $V_{T(T4)}$, $I_{T(T4)}$ for the fourth terminal T4; $V_{T(T5)}$, $I_{T(T5)}$ for the fifth terminal T5; and $V_{T(T6)}$, $I_{T(T6)}$ for the sixth terminal T6), as illustrated schematically in Figure 6, to give rise to corresponding compensated voltage and current phasors V_{TSyn} , I_{TSyn} (i.e. $V_{TSyn(T1)}$, $I_{TSyn(T1)}$ for the first terminal T1;
 20 $V_{TSyn(T2)}$, $I_{TSyn(T2)}$ for the second terminal T2; $V_{TSyn(T3)}$, $I_{TSyn(T3)}$ for the third terminal T3; $V_{TSyn(T4)}$, $I_{TSyn(T4)}$ for the fourth terminal T4; $V_{TSyn(T5)}$, $I_{TSyn(T5)}$ for the fifth terminal T5; and $V_{TSyn(T6)}$, $I_{TSyn(T6)}$ for the sixth terminal T6).

The compensation factor preferably takes the form

$$\exp(j\omega_0 T_x)$$

25 where,

ω_0 is the fundamental angular frequency of the power transmission scheme 10; and

T_x is the corresponding time difference, i.e. Tp1 for second terminal T2 (i.e. the first remote terminal R1), Tp2 for the third terminal T3 (i.e. the second remote terminal R2), Tp3 for the fourth terminal T4 (i.e. the third remote terminal R3), Tp4 for the fifth terminal T5 (i.e. the fourth remote terminal R4), and Tp5
 5 for the sixth terminal T6 (i.e. the fifth remote terminal R5).

Thereafter the method of the invention carries out, within an eighth block 36 of Figure 2, further principle step (e) of determining from the compensated voltage and current phasors V_{TSyn} , I_{TSyn} the location of the fault.

Such a determination includes the main steps of:

- 10 - designating a terminal, e.g. the first terminal T1, at a first end 40 of the power transmission scheme 10 as a first end terminal and a terminal, e.g. the sixth terminal T6, at a second end 42 of the power transmission scheme 10 as a second end terminal;
- obtaining a first set of voltage phasors V_{JL} , wherein the first set of
 15 voltage phasors V_{JL} includes the compensated voltage phasor at the first end terminal, i.e. the compensated voltage phasor $V_{TSyn(T1)}$ at the first terminal T1, and further includes respective voltage phasors at each of the second end terminal, i.e. the sixth terminal T6, and each junction J1, J2, J3, J4 that are determined based on the compensated first end terminal voltage phasor
 20 $V_{TSyn(T1)}$;
- obtaining a second set of voltage phasors V_{JR} , wherein the second set of voltage phasors V_{JR} includes the compensated voltage phasor at the second end terminal, i.e. the compensated voltage phasor $V_{TSyn(T6)}$ at the sixth terminal T6, and further includes respective voltage phasors at each of the
 25 first end terminal, i.e. the first terminal T1, and each junction J1, J2, J3, J4 that are determined based on the compensated second end terminal voltage phasor $V_{TSyn(T6)}$; and

- comparing the first and second sets of voltage phasors V_{JL} , V_{JR} to identify the power transmission section 12 or junction J1, J2, J3, J4 corresponding to the location of the fault, wherein each voltage phasor of the first set of voltage phasors V_{JL} is compared to the respective voltage phasor of the second set of voltage phasors V_{JR} that corresponds to the same end terminal T1, T6 or junction J1, J2, J3, J4.

A schematic view of a second implementation structure 38 which lies within the eighth block 36 and determines the location of the fault, including identifying the power transmission section 12 (or junction J1, J2, J3, J4) corresponding to the location of the fault and (in the embodiment method described) the distance of the fault along the given power transmission section 12, is illustrated schematically in Figure 7.

More particularly, determining the location of the fault includes feeding the compensated voltage and current phasors V_{TSyn} , I_{TSyn} for each terminal T1, T2, T3, T4, T5, T6 (i.e. $V_{TSyn(T1)}$, $I_{TSyn(T1)}$ for the first terminal T1; $V_{TSyn(T2)}$, $I_{TSyn(T2)}$ for the second terminal T2; $V_{TSyn(T3)}$, $I_{TSyn(T3)}$ for the third terminal T3; $V_{TSyn(T4)}$, $I_{TSyn(T4)}$ for the fourth terminal T4; $V_{TSyn(T5)}$, $I_{TSyn(T5)}$ for the fifth terminal T5; and $V_{TSyn(T6)}$, $I_{TSyn(T6)}$ for the sixth terminal T6) into a Block A within the second implementation structure 38 to calculate, i.e. to obtain: first and second sets of voltage phasors V_{JL} , V_{JR} ; first and second sets of current phasors I_{JL} , I_{JR} ; and further voltage phasors V_{JT} .

Moving from the first terminal T1 to the sixth terminal T6 (i.e. left to right in Figure 1), the first sets of voltage and current phasors V_{JL} , I_{JL} are determined as follows.

In the first set of voltage phasors V_{JL} , for the purposes of the description below, the voltage phasor at the first terminal T1 (which for the purposes of simplification can temporarily be considered a zero junction J_0) is identified as V_{J0L} , the voltage phasor at junction J1 is identified as V_{J1L} , the voltage phasor at junction J2 is identified as V_{J2L} , the voltage phasor at junction J3 is identified as V_{J3L} , the voltage phasor at junction J4 is identified as V_{J4L} , and the voltage

phasor at the sixth terminal T6 (which for the purposes of simplification can temporarily be considered a fifth junction J₅) is identified as V_{J5L}.

The first set of current phasors I_{JL} includes the following current phasors (which are identified as indicated for the purposes of the description below): a current
 5 phasor in the power transmission section between the first terminal T1 and the first junction J₁ which is identified as I_{J0_J1L}, a current phasor in the power transmission section between junctions J₁ and J₂ which is identified as I_{J1_J2L}, a current phasor in the power transmission section between junctions J₂ and J₃ which is identified as I_{J2_J3L}, a current phasor in the power transmission section
 10 between junctions J₃ and J₄ which is identified as I_{J3_J4L}, and a current phasor in the power transmission section between junctions J₄ and J₅ which is identified as I_{J4_J5L}.

The voltage phasor V_{J0L} at the first terminal T1 is, as indicated above the compensated voltage phasor V_{TSyn(T1)} for the first terminal T1, and similarly the
 15 current phasor I_{J0_J1L} in the power transmission section between the first terminal T1 and the first junction J₁ is the compensated current phasor I_{TSyn(T1)} for the first terminal T1, i.e.

$$V_{J0L} = V_{TSyn(T1)} \quad I_{J0\_J1L} = I_{TSyn(T1)}$$

Each of the other voltage phasors V_{J1L}, V_{J2L}, V_{J3L}, V_{J4L}, V_{J5L} at the respective
 20 junctions J₁, J₂, J₃, J₄ and the second end terminal, i.e. the sixth terminal T6 (which for purposes of simplification can, as indicated above, temporarily be considered a fifth junction J₅) is calculated based on the voltage phasor of the preceding junction and the current phasor of the preceding power transmission section. Each of the other current phasors I_{J1_J2L}, I_{J2_J3L}, I_{J3_J4L}, I_{J4_J5L} in the
 25 respective power transmission sections are based on the voltage phasor of the preceding junction, the current phasor of the preceding power transmission section, and the current phasor in a further power transmission section connected to the preceding junction.

Accordingly, the foregoing are given by:

$$V_{JkL} = A_{Jk-1Jk} V_{Jk-1L} + B_{Jk-1Jk} I_{Jk-1\_JkL} ;$$

$$I_{Jk\_Jk+1L} = C_{Jk-1Jk} V_{Jk-1L} + D_{Jk-1Jk} I_{Jk-1\_JkL} + \sum_{n \in J_k} I_{Jk\_Tn} ;$$

where k ranges from 1 to 5;

$$A_{Jk-1Jk} = D_{Jk-1Jk} = \cosh(\gamma_{Jk-1Jk} l_{Jk-1Jk}) ;$$

$$5 \quad B_{Jk-1Jk} = -Z_{CJk-1Jk} \sinh(\gamma_{Jk-1Jk} l_{Jk-1Jk}) ;$$

$$C_{Jk-1Jk} = -\sinh(\gamma_{Jk-1Jk} l_{Jk-1Jk}) / Z_{CJk-1Jk} ;$$

$$\gamma_{Jk-1Jk} = \sqrt{Z_{Jk-1Jk} y_{Jk-1Jk}} ;$$

$$Z_{CJk-1Jk} = \sqrt{Z_{Jk-1Jk} / y_{Jk-1Jk}} ;$$

Z_{Jk-1Jk} is the impedance per length of the power transmission section
10 interconnecting the k-1th junction to the kth junction;

y_{Jk-1Jk} is the admittance per length of the power transmission section
interconnecting the k-1th junction to the kth junction;

l_{Jk-1Jk} is the line length of the power transmission section
interconnecting the k-1th junction to kth the junction;

15 I_{Jk_Tn} is the nth-terminal-to-kth-junction current flowing in the further
power transmission medium connected to the kth junction.

Moving from the sixth terminal T6, to the first terminal T1 (i.e. right to left in
Figure 1), the second sets of voltage and current phasors V_{JR} , I_{JR} are
determined as follows.

- In the second set of voltage phasors V_{JR} , for the purposes of the description below, the voltage phasor at the first terminal T1 (which for the purposes of simplification can, as indicated above, temporarily be considered a zero junction J_0) is identified as V_{J0R} , the voltage phasor at junction J_1 is identified as V_{J1R} , the voltage phasor at junction J_2 is identified as V_{J2R} , the voltage phasor at junction J_3 is identified as V_{J3R} , the voltage phasor at junction J_4 is identified as V_{J4R} , and the voltage phasor at the sixth terminal T6 (which, for the purposes of simplification can, as indicated above, temporarily be considered a fifth junction J_5) is identified as V_{J5R} .
- The second set of current phasors I_{JR} includes the following current phasors (which are identified as indicated for the purposes of the description below): a current phasor in the power transmission section between the sixth terminal T6 and the fourth junction J_4 which is identified as I_{J5_J4R} , a current phasor in the power transmission section between junctions J_4 and J_3 which is identified as I_{J4_J3R} , a current phasor in the power transmission section between junctions J_3 and J_2 which is identified as I_{J3_J2R} , a current phasor in the power transmission section between junctions J_2 and J_1 which is identified as I_{J2_J1R} , and a current phasor in the power transmission section between junction J_1 and the first terminal T1 which is identified as I_{J1_J0R} .
- The voltage phasor V_{J5R} at the sixth terminal T6 is, as indicated above, the compensated voltage phasor $V_{TSyn(T6)}$ for the sixth terminal T6, and similarly the current phasor I_{J4_J5L} in the power transmission section between junction J_4 and the sixth terminal T6 is the compensated current phasor $I_{TSyn(T6)}$ for the sixth terminal T6, i.e.

$$V_{J5R} = V_{TSyn(T6)} \quad I_{J5\_J4R} = I_{TSyn(T6)}$$

Each of the other voltage phasors $V_{J0R}, V_{J1R}, V_{J2R}, V_{J3R}, V_{J4R}$ at the respective junctions J_1, J_2, J_3, J_4 and the first end terminal, i.e. the first terminal T1 (which for purposes of simplification can, as indicated above, temporarily be considered a zero junction J_0) is calculated based on the voltage phasor of the

preceding junction and the current phasor of the preceding power transmission section. Each of the other current phasors $I_{J1\_J0R}, I_{J2\_J1R}, I_{J3\_J2R}, I_{J4\_J3R}$ in the respective power transmission sections are based on the voltage phasor of the preceding junction, the current phasor of the preceding power transmission section, and the current phasor in a further power transmission section connected to the preceding junction.

Accordingly the foregoing are given by:

$$V_{JkR} = A_{Jk+1Jk} V_{Jk+1R} + B_{Jk+1Jk} I_{Jk+1\_JkR} ;$$

$$I_{Jk\_Jk-1L} = C_{Jk+1Jk} V_{Jk+1R} + D_{Jk+1Jk} I_{Jk+1\_JkR} + \sum_{n \in J_k} I_{Jk\_Tn} ;$$

where k ranges from 0 to 4,;

$$A_{Jk+1Jk} = D_{Jk+1Jk} = \cosh(\gamma_{Jk+1Jk} l_{Jk+1Jk}) ;$$

$$B_{Jk+1Jk} = -Z_{CJk+1Jk} \sinh(\gamma_{Jk+1Jk} l_{Jk+1Jk}) ;$$

$$C_{Jk+1Jk} = -\sinh(\gamma_{Jk+1Jk} l_{Jk+1Jk}) / Z_{CJk+1Jk} ;$$

$$\gamma_{Jk+1Jk} = \sqrt{Z_{Jk+1Jk} y_{Jk+1Jk}} ;$$

$$Z_{CJk+1Jk} = \sqrt{Z_{Jk+1Jk} / y_{Jk+1Jk}} ;$$

Z_{Jk+1Jk} is the impedance per length of the power transmission section interconnecting the k+1th junction to kth junction;

y_{Jk+1Jk} is the admittance per length of the power transmission section interconnecting the k+1th junction to the kth junction;

$l_{Jk+1,Jk}$ is the line length of the power transmission section interconnecting the k+1th junction to the kth junction;

I_{Jk_Tn} is the nth-terminal-to-kth-junction current flowing in the further power transmission medium connected to the kth junction.

- 5 The further voltage phasors V_{JT} , include the following further voltage phasors (which are identified as indicated for the purposes of the description below): a further voltage phasor at junction J_1 which is identified as V_{J1_T2} , a further voltage phasor at junction J_2 which is identified as V_{J2_T3} , a further voltage phasor at junction J_3 which is identified as V_{J3_T4} , and a further voltage phasor
10 at junction J_4 which is identified as V_{J4_T5} .

Further current phasors in respective further power transmissions sections are also calculated. These further current phasors I_{JT} include the following current phasors (which are identified as indicated for the purposes of the description below): a further current phasor in the further power transmission section
15 between junction J_1 and terminal T2 which is identified as I_{J1_T2} , a further current phasor in the further power transmission section between junction J_2 and terminal T3 which is identified as I_{J2_T3} , a further current phasor in the further power transmission section between junction J_3 and terminal T4 which is identified as I_{J3_T4} , and a further current phasor in the further power
20 transmission section between junction J_4 and terminal T5 which is identified as I_{J4_T5} .

The further voltage and current phasors for junction J_1 with respect to terminal T2 are calculated by the following equations:

$$\begin{cases} V_{J1\_T2} = A_2 V_{TSyn(T2)} + B_2 I_{TSyn(T2)} \\ I_{J1\_T2} = C_2 V_{TSyn(T2)} + D_2 I_{TSyn(T2)} \end{cases}$$

25 where,

$$A_2 = D_2 = \cosh(\gamma_2 l_{T2}) ;$$

$$B_2 = -Z_{C2} \sinh(\gamma_2 l_{T2}) ;$$

$$C_2 = -\sinh(\gamma_2 l_{T2}) / Z_{C2} ;$$

$$\gamma_2 = \sqrt{z_2 y_2} ;$$

$$5 \quad Z_{C2} = \sqrt{z_2 / y_2} ;$$

z_2 is the impedance per length of the further power transmission section interconnecting junction J₁ to terminal T2;

y_2 is the admittance per length of the further power transmission section interconnecting junction J₁ to terminal T2;

10 l_{T2} is the line length of the further power transmission section interconnecting junction J₁ to terminal T2.

The further voltage and current phasors for junction J₂ with respect to terminal T3 are calculated by the following equations:

$$\begin{cases} V_{J2\_T3} = A_3 V_{TSyn(T3)} + B_3 I_{TSyn(T3)} \\ I_{J2\_T3} = C_3 V_{TSyn(T3)} + D_3 I_{TSyn(T3)} \end{cases}$$

15 where,

$$A_3 = D_3 = \cosh(\gamma_3 l_{T3}) ;$$

$$B_3 = -Z_{C3} \sinh(\gamma_3 l_{T3}) ;$$

$$C_3 = -\sinh(\gamma_3 l_{T3}) / Z_{C3} ;$$

$$\gamma_3 = \sqrt{z_3 y_3} ;$$

$$Z_{C3} = \sqrt{z_3 / y_3} ;$$

z_3 is the impedance per length of the further power transmission section interconnecting junction J₂ to terminal T3;

- 5 y_3 is the admittance per length of the further power transmission section interconnecting junction J₂ to terminal T3;

l_{T3} is the line length of the further power transmission section interconnecting junction J₂ to terminal T3.

- The further voltage and current phasors for junction J₃ with respect to terminal
10 T4 are calculated by the following equations:

$$\begin{cases} V_{J3\_T4} = A_4 V_{TSyn(T4)} + B_4 I_{TSyn(T4)} \\ I_{J3\_T4} = C_4 V_{TSyn(T4)} + D_4 I_{TSyn(T4)} \end{cases}$$

where,

$$A_4 = D_4 = \cosh(\gamma_4 l_{T4});$$

$$B_4 = -Z_{C4} \sinh(\gamma_4 l_{T4});$$

- 15 $C_4 = -\sinh(\gamma_4 l_{T4}) / Z_{C4};$

$$\gamma_4 = \sqrt{z_4 y_4} ;$$

$$Z_{C4} = \sqrt{z_4 / y_4} ;$$

z_4 is the impedance per length of the further power transmission section interconnecting junction J₃ to terminal T4;

y_4 is the admittance per length of the further power transmission section interconnecting junction J₃ to terminal T4;

5 l_{T4} is the line length of the further power transmission section interconnecting junction J₃ to terminal T4.

The further voltage and current phasors for junction J₄ with respect to terminal T5 are calculated by the following equations:

$$\begin{cases} V_{J4\_T5} = A_5 V_{TSyn(T5)} + B_5 I_{TSyn(T5)} \\ I_{J4\_T5} = C_5 V_{TSyn(T5)} + D_5 I_{TSyn(T5)} \end{cases}$$

10 where,

$$A_5 = D_5 = \cosh(\gamma_5 l_{T5});$$

$$B_5 = -Z_{C5} \sinh(\gamma_5 l_{T5});$$

$$C_5 = -\sinh(\gamma_5 l_{T5}) / Z_{C5};$$

$$\gamma_5 = \sqrt{z_5 y_5};$$

15 $Z_{C5} = \sqrt{z_5 / y_5};$

z_5 is the impedance per length of the further power transmission section interconnecting junction J₄ to terminal T5;

y_5 is the admittance of the further power transmission section interconnecting junction J₄ to terminal T5;

l_{T5} is the line length of the further power transmission section interconnecting junction J₄ to terminal T5).

The first and second sets of voltage phasors V_{JL}, V_{JR} and the further voltage phasors V_{JT} are then fed into a Block B within the second implementation structure 38 to compare the voltage phasors to identify the power transmission section or junction corresponding to the location of the fault, as follows.

A subtraction voltage phasor for each junction is obtained. In this regard the subtraction voltage phasor of each junction is equal to the difference between the corresponding voltage phasors of the first and second sets of voltage phasors V_{JL}, V_{JR} , as shown in the following equation.

$$\Delta V_J = \begin{bmatrix} \Delta V_{J0} \\ \Delta V_{J1} \\ \Delta V_{J2} \\ \Delta V_{J3} \\ \Delta V_{J4} \\ \Delta V_{J5} \end{bmatrix} = \begin{bmatrix} V_{J0L} - V_{J0R} \\ V_{J1L} - V_{J1R} \\ V_{J2L} - V_{J2R} \\ V_{J3L} - V_{J3R} \\ V_{J4L} - V_{J4R} \\ V_{J5L} - V_{J5R} \end{bmatrix}$$

Then the minimum amplitude value (modular) $\Delta V_{\min}$ of the plurality of subtraction voltage phasors ΔV_J is determined using the equation: $\Delta V_{\min} = \min\{|\Delta V_{Jk}|, k = 0,1,2,3,4,5\}$.

The minimum amplitude value $\Delta V_{\min}$ is subsequently compared with a predefined voltage threshold V_{thres1} to determine whether $\Delta V_{\min}$ is less than V_{thres1} . V_{thres1} is exemplarily set at 0.02 times of the rated voltage of the power transmission scheme 10 so that, for example, if the rated voltage is 110 V, then V_{thres1} is 2.2 V.

If the minimum amplitude value $\Delta V_{\min}$ is less than the predefined voltage threshold V_{thres1} , it indicates that the fault is either on the junction corresponding to the minimum amplitude value $\Delta V_{\min}$ or in the further power transmission section connected to this junction. For example, if $|\Delta V_{J3}| = \Delta V_{\min}$,

it indicates that the fault is either on the junction J_3 or in the further power transmission section interconnecting the junction J_3 and the terminal T_4 .

Subsequently the location of the fault is more accurately determined by using the discriminative criterion of $|V_{JkL}-V_{Jk\_Tn}| > V_{thres2}$, where $\Delta V_{min} = V_{JkL}$.

- 5 Therefore, for example, if $|\Delta V_{J3}|=\Delta V_{min}$, the discriminative criterion is $|V_{J3L}-V_{J3\_T4}| > V_{thres2}$. V_{thres1} is exemplarily set at 0.05 times of the rated voltage of the power transmission scheme so that, for example, if the rated voltage is 110 V, then V_{thres1} is 5.5 V.

- 10 If $|V_{JkL}-V_{Jk\_Tn}| > V_{thres2}$, then the fault is located in the further power transmission section interconnecting the k th junction and the n th terminal. If $|V_{JkL}-V_{Jk\_Tn}| \leq V_{thres2}$, then the fault is located on the k th junction. If there are multiple terminals connected to the junction in question, the discriminative criterion is applied to each terminal in turn.

- 15 If the minimum amplitude value ΔV_{min} is more than the predefined voltage threshold V_{thres1} , it indicates that the fault is in the power transmission section interconnecting the k th junction and the $k+1$ th junction. For example, if $|\Delta V_{J3}|=\Delta V_{min}$, it indicates that the fault is in the power transmission sections interconnecting the junctions $J_0, J_1, J_2, J_3, J_4, J_5$.

- 20 Subsequently the location of the fault is more accurately determined by comparing the voltage phasor of a given junction with the voltage phasor of a neighbouring junction to identify the power transmission section corresponding to the location of the fault. Different criterion may be applied to determine the power transmission section in which the fault is located.

- 25 In a first exemplary criterion, the power transmission section in which the fault is located is determined by comparing the phases of the subtraction voltage phasor ΔV_{Jk} of a given junction and the subtraction voltage phasor ΔV_{Jk+1} of a neighbouring junction to check whether the comparison meets the following criterion:

$$90^0 < \arg \frac{\Delta V_{J_k}}{\Delta V_{J_{k+1}}} < 270^0$$

If the criterion is met, then the fault is located in the power transmission section interconnecting junctions J_k and J_{k+1} .

In a second exemplary criterion, the power transmission section in which the fault is located is determined by comparing the amplitudes of the subtraction voltage phasor ΔV_{J_k} of a given junction and the subtraction voltage phasor $\Delta V_{J_{k+1}}$ of a neighbouring junction to check whether an amplitude comparison meets the following criterion:

$$\text{imag}\left(\frac{\Delta V_{J_k} \text{conj}(\Delta V_{J_{k+1}})}{|\Delta V_{J_k}| |\Delta V_{J_{k+1}}|}\right) < \varepsilon_1$$

where ε_1 is the threshold with per-unit value. For example, $\varepsilon_1 = -0.01$.

If the criterion is met, then the fault is located in the power transmission section interconnecting junctions J_k and J_{k+1} .

In a third exemplary criterion, the power transmission section in which the fault is located is determined by comparing the subtraction voltage phasor ΔV_{J_k} of a given junction and the subtraction voltage phasor $\Delta V_{J_{k+1}}$ of a neighbouring junction to check whether the comparison meets the following criterion.

$$|\Delta V_{J_k} + \Delta V_{J_{k+1}}| < |\Delta V_{J_k} - \Delta V_{J_{k+1}}|$$

If the criterion is met, then the fault is located in the power transmission section interconnecting junctions J_k and J_{k+1} .

If a given power transmission section is identified as the location of the fault, a Block C within the second implementation structure then selects the appropriate voltage and current phasors from the first and second sets of voltage and current phasors V_{JL} , V_{JR} , I_{JL} and I_{JR} and forms a two-ended system equivalent

of the power transmission section identified as the location of the fault with voltages and currents V_M , V_N , I_M , I_N .

If the relevant power transmission section is connected between junctions J_k and J_{k+1} , the voltage and current phasors V_{JkL} , I_{Jk_k+1L} , V_{Jk+1R} , $I_{Jk+1,kR}$ are selected to form the two-ended system equivalent such that: $V_M = V_{JkL}$; $I_M = I_{Jk\_k+1L}$; $V_N = V_{Jk+1R}$; and $I_N = I_{Jk+1\_kR}$. That is, junction J_k is the equivalent end M of the two-ended system equivalent, and junction J_{k+1} is the equivalent N of the two-ended system equivalent.

If the relevant power transmission section is a further power transmission section interconnecting a junction J_k and a terminal T_n , Block C then selects the voltage and current phasors at the terminal T_n , the voltage phasor V_{JkL} , V_{JkR} at the junction to which the terminal T_n is connected, and the negative summation of the corresponding current phasors of the first and second sets of current phasors $-(I_{Jk, k+1L} + I_{Jk, k-1R})$, such that: $V_M = V_{Tn}$; $I_M = I_{Tn}$; $V_N = V_{JkL}$; $I_N = -(I_{Jk, k+1L} + I_{Jk, k-1R})$. That is, terminal T_n is the equivalent end M of the two-ended system equivalent, and junction J_k is the equivalent end N of the two-ended system equivalent.

Based on the two-ended system equivalent the distance of the fault along the power transmission section is determined on the basis of the voltage and currents V_M, V_N, I_M, I_N of the two-ended system equivalent. In the second implementation structure 38, Block C feeds the voltage and currents V_M, V_N, I_M, I_N of the two-ended system equivalent to a Block D, which determines the fault distance using the following equation:

$$V_M \cosh(\gamma x) - Z_C I_M \sinh(\gamma x) = V_N \cosh(\gamma(l-x)) - Z_C I_N \sinh(\gamma(l-x))$$

where

x is the distance to the end M of the two-system equivalent;

$$\gamma = \sqrt{zy} ;$$

$$Z_C = \sqrt{z/y};$$

z is the impedance per length of corresponding section, which is settable by customer;

y is the admittance per length of corresponding section, which is
5 settable by customer;

l is the line length of corresponding section.

The above equation can be simplified as:

$$V_M - zxI_M = V_N - z(l-x)I_N$$

CLAIMS:

1. A method of locating a fault in a multi-terminal electrical power transmission scheme (10) in which each terminal (T1, T2, T3, T4, T5, T6) is connected with a junction (J1, J2, J3, J4) via a power transmission section (12) and the or each junction (J1, J2, J3, J4) interconnects a plurality of power transmission sections (12), the method comprising the steps of:

(a) measuring the voltage and current at each terminal (T1, T2, T3, T4, T5, T6);

(b) calculating from the measured voltage and current at each terminal corresponding voltage and current phasors (V_1, I_1, V_2, I_2);

(c) determining from the calculated voltage and current phasors (V_1, I_1) a synchronisation difference (Tp1, Tp2, Tp3, Tp4, Tp5) between the measured voltage and current at a designated terminal (T1) and the measured voltage and current at the or each other terminal (T2, T3, T4, T5, T6);

(d) modifying the calculated voltage and current phasors (V_1, I_1) to compensate for the or each synchronisation difference (Tp1, Tp2, Tp3, Tp4, Tp5); and

(e) determining from the compensated voltage and current phasors (V_{TSyn}, I_{TSyn}) the location of the fault.

2. A method according to Claim 1 wherein step (a) of measuring the voltage and current at each terminal (T1, T2, T3, T4, T5, T6) includes resampling the measured voltage and current from one or more terminals (T1, T2, T3, T4, T5, T6).

3. A method according to Claim 1 or Claim 2 wherein the power transmission scheme (10) is a multi-phase (a, b, c) power transmission scheme,

step (a) of measuring the voltage and current at each terminal (T1, T2, T3, T4, T5, T6) includes measuring the voltage and current of each phase (a, b, c) at each terminal (T1, T2, T3, T4, T5, T6), and

step (b) of calculating from the measured voltage and current at each terminal (T1, T2, T3, T4, T5, T6) corresponding voltage and current phasors (V_1 , I_1 , V_2 , I_2) includes converting the measured phase voltages (V_{abc}) and phase currents (I_{abc}) into respective phase phasors (V_a , V_b , V_c , I_a , I_b , I_c) and then transforming the phase phasors (V_a , V_b , V_c , I_a , I_b , I_c) into respective positive and negative sequence voltage phasors (V_1 , V_2) and positive and negative sequence current phasors (I_1 , I_2).

4. A method according to Claim 3 further including the step of determining from the measured phase currents (I_{abc}) whether a fault has occurred and if a fault has occurred whether it effects all phases (a, b, c).

5. A method according to Claim 4 wherein if the fault effects all phases (a, b, c) then the positive sequence voltage and current phasors (V_1 , I_1) are used in subsequent steps of the invention, otherwise the negative sequence voltage and current phasors (V_2 , I_2) are used.

6. A method according to any preceding claim wherein step (c) of determining from the calculated voltage and current phasors (V_1 , I_1) a synchronisation difference (Tp1, Tp2, Tp3, Tp4, Tp5) between the measured voltage and current at a designated terminal (T1) and the measured voltage and current at the or each other terminal (T2, T3, T4, T5, T6) includes:

- calculating, with respect to the designated terminal (T1), an equivalent current flowing at the or each other terminal (T2, T3, T4, T5, T6);

- equating, in respect of the or each other terminal (T2, T3, T4, T5, T6), a sum of the measured current (i_{JR1} , i_{JR2} , i_{JR3} , i_{JR4} , i_{JR5}) and the calculated equivalent current (i_{JR1_L} , i_{JR2_L} , i_{JR3_L} , i_{JR4_L} , i_{JR5_L}) to zero according to Kirchhoff's first law; and

- extracting, in respect of the or each other terminal (T2, T3, T4, T5, T6), a synchronisation difference (Tp1, Tp2, Tp3, Tp4, Tp5) between the measured voltage and current at the designated terminal (T1) and the measured voltage and current at the said respective other terminal (T2, T3, T4, T5, T6) from a corresponding equated sum of currents.

7. A method according to Claim 6 wherein calculating, with respect to the designated terminal (T1), an equivalent current flowing at the or each other terminal (T2, T3, T4, T5, T6) includes establishing an equivalent admittance matrix (Y_{Mod}) for the power transmission scheme (10).

8. A method according to any preceding claim wherein step (e) of determining from the compensated voltage and current phasors (V_{TSyn} , I_{TSyn}) the location of the fault includes:

- designating a terminal (T1) at a first end (40) of the power transmission scheme (10) as a first end terminal and a terminal (T6) at a second end (42) of the power transmission scheme (10) as a second end terminal;

- obtaining a first set of voltage phasors (V_{JL}), wherein the first set of voltage phasors (V_{JL}) includes the compensated voltage phasor ($V_{TSyn(T1)}$) at the first end terminal (T1) and further includes respective voltage phasors at each of the second end terminal (T6) and the or each junction (J1, J2, J3, J4) that are determined based on the compensated first end terminal voltage phasor ($V_{TSyn(T1)}$);

- obtaining a second set of voltage phasors (V_{JR}), wherein the second set of voltage phasors (V_{JR}) includes the compensated voltage phasor ($V_{TSyn(T6)}$) at the second end terminal (T6) and further includes respective voltage phasors at each of the first end terminal (T1) and the or each junction (J1, J2, J3, J4) that are determined based on the compensated second end terminal voltage phasor ($V_{TSyn(T6)}$); and

- comparing the first and second sets of voltage phasors (V_{JL} , V_{JR}) to identify the power transmission section (12) or junction (J1, J2, J3, J4) corresponding to the location of the fault, wherein each voltage phasor of the first set of voltage phasors (V_{JL}) is compared to the respective voltage phasor of the second set of voltage phasors (V_{JR}) that corresponds to the same end terminal (T1, T6) or junction (J1, J2, J3, J4).

9. A method according to Claim 8 further including the step, if a given power transmission section (12) is identified as the location of the fault, of determining the distance (x) of the fault along the power transmission section (12) using corresponding voltages and currents (V_M, V_N, I_M, I_N) of an equivalent two-ended system.

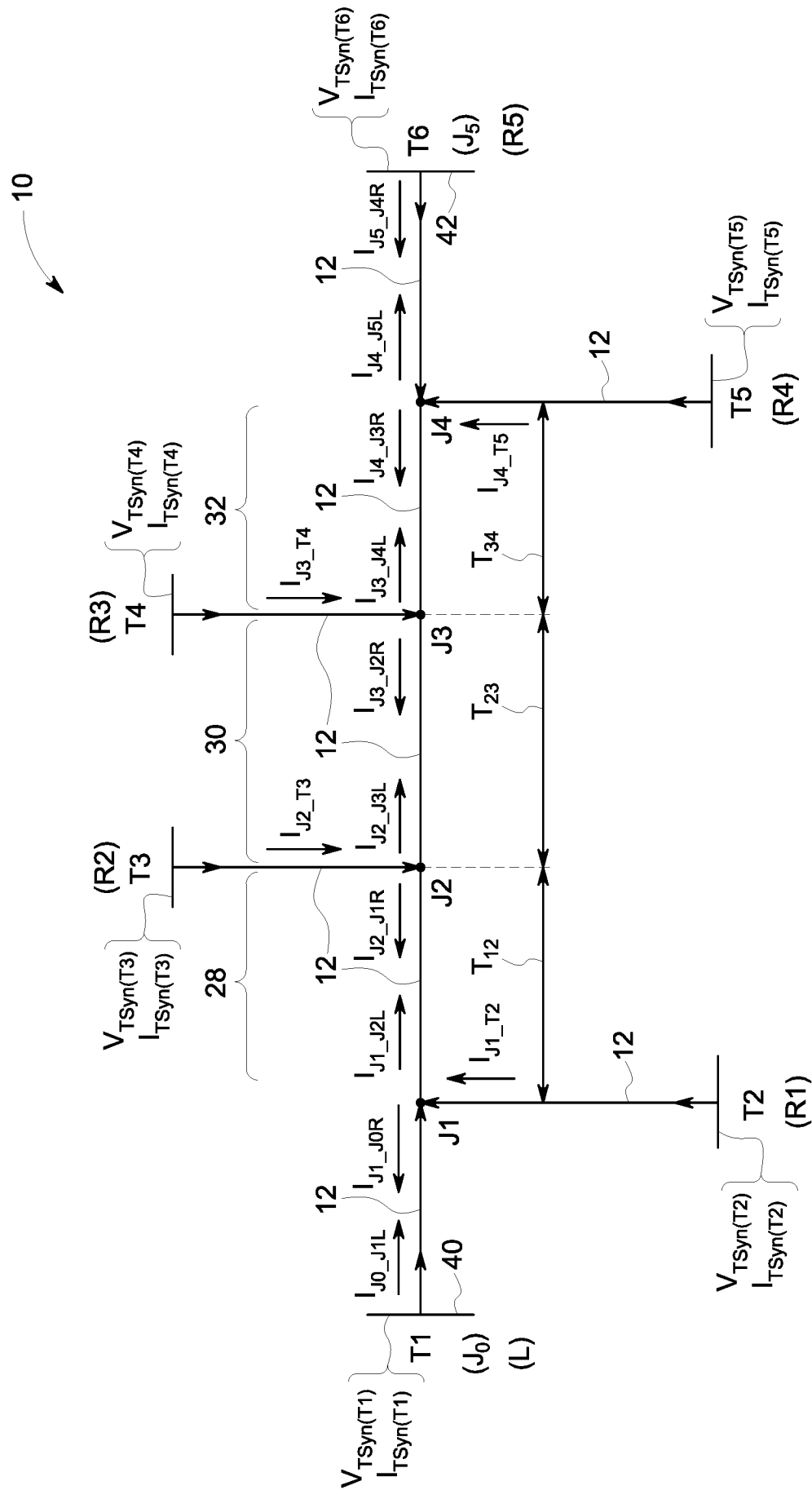


FIG. 1

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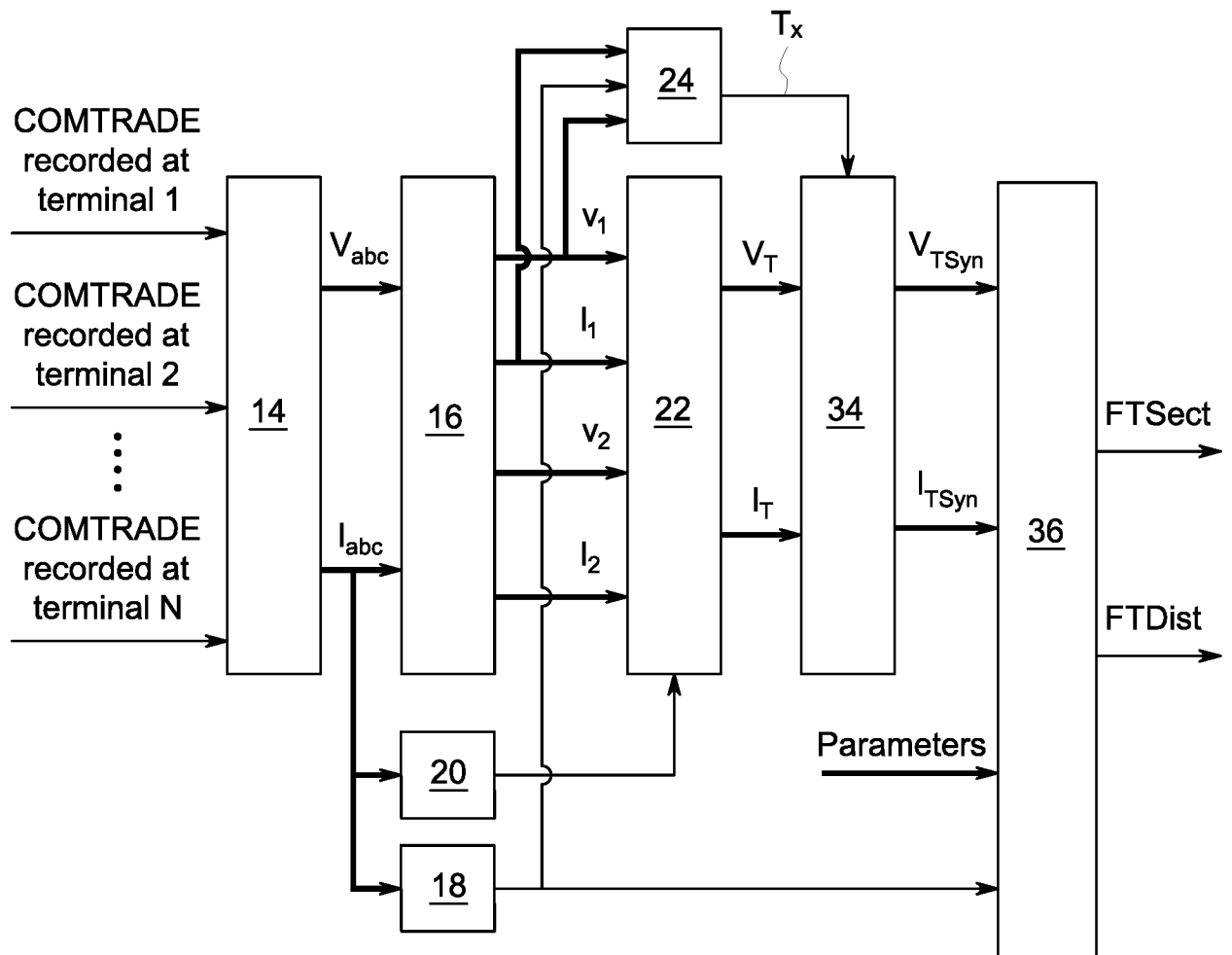


FIG. 2

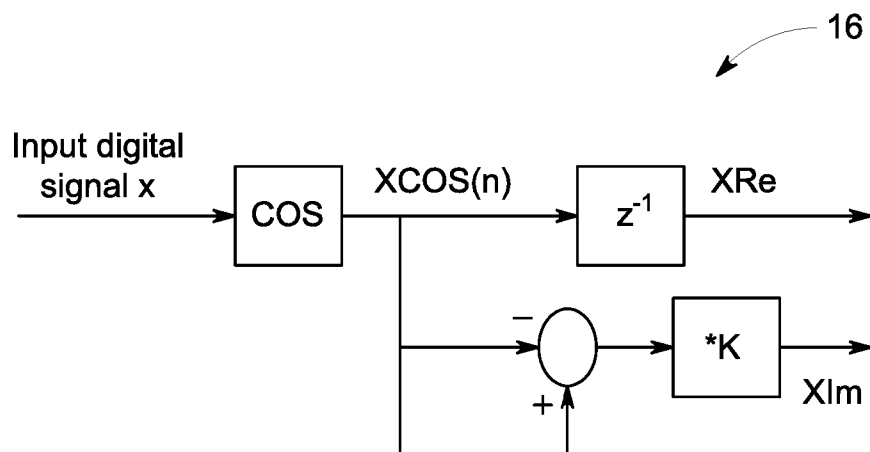


FIG. 3

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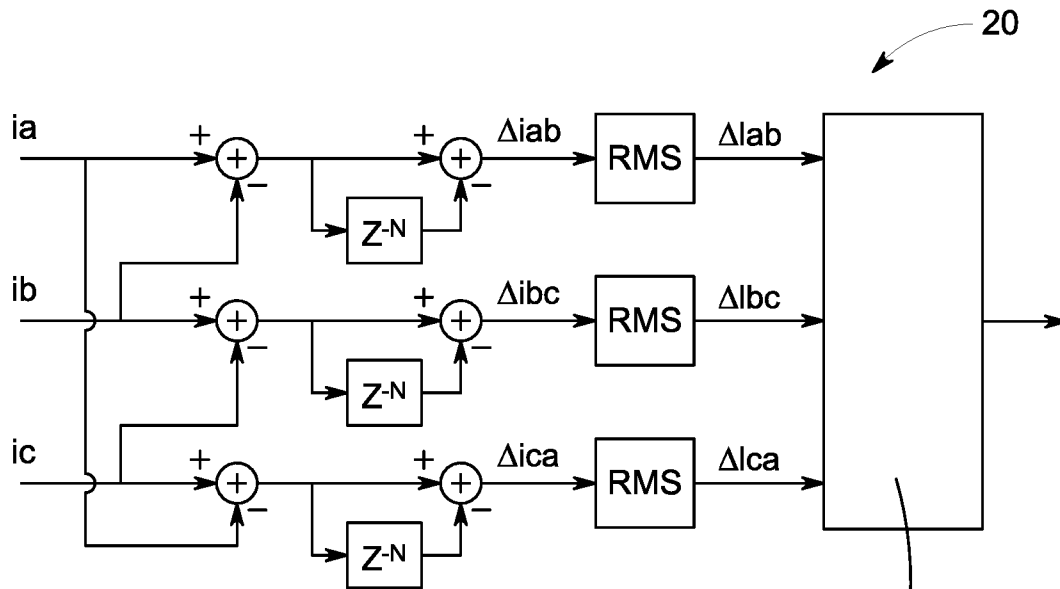


FIG. 4(a)

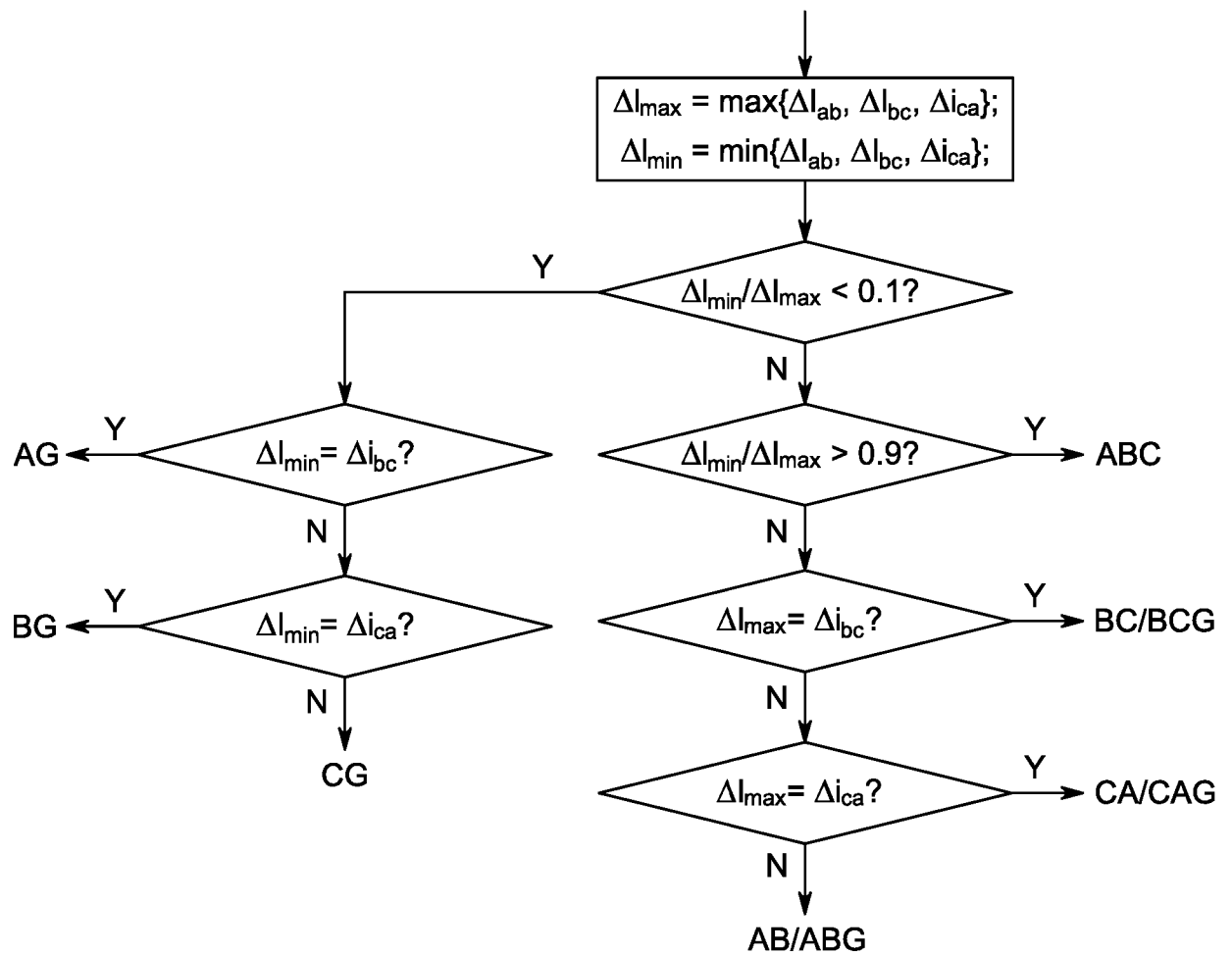


FIG. 4(b)

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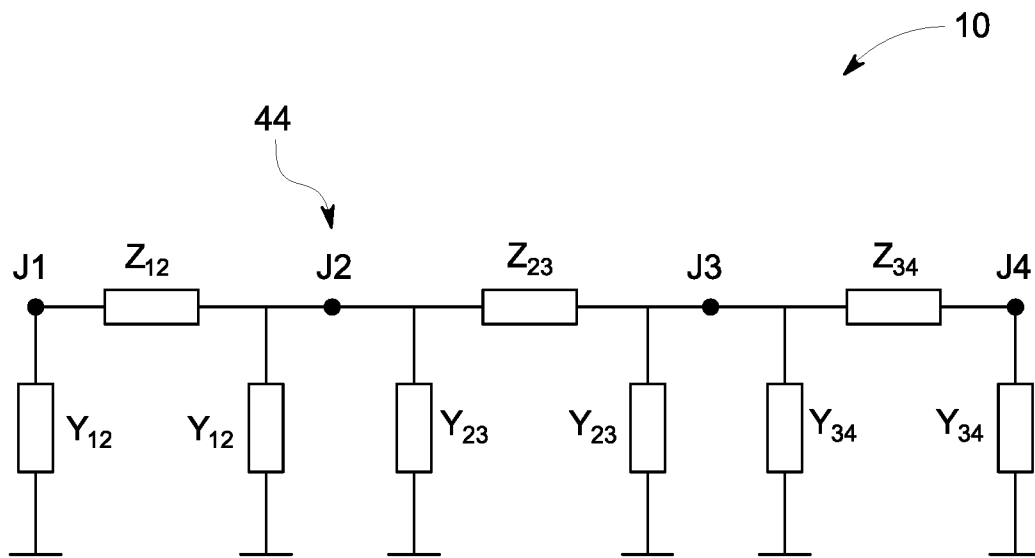


FIG. 5(a)

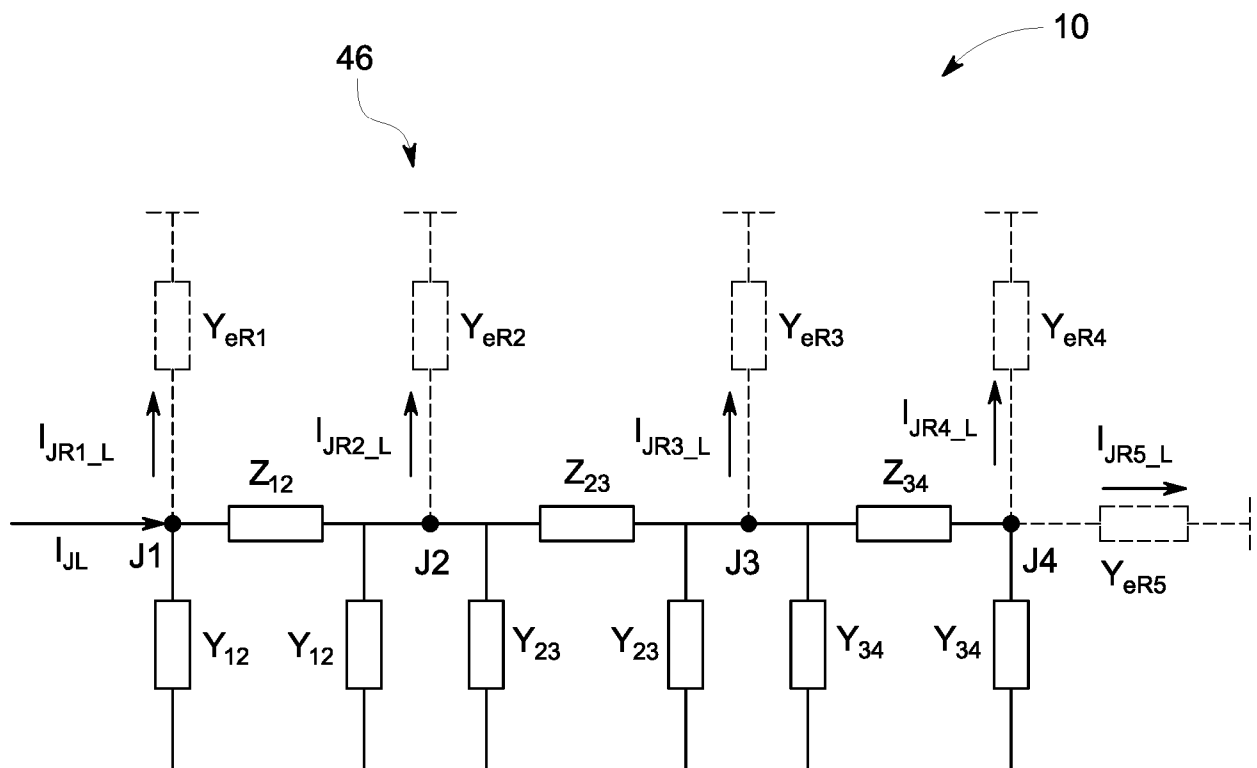


FIG. 5(b)

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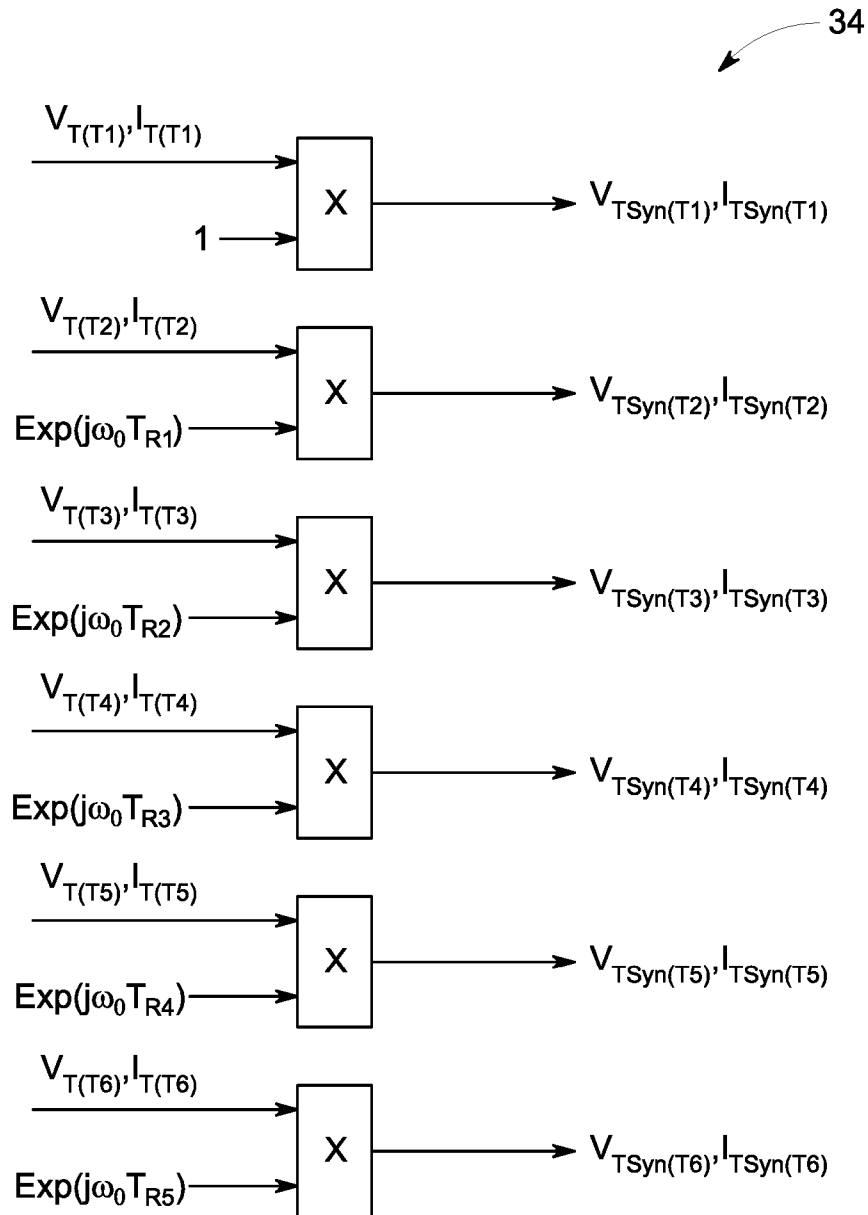


FIG. 6

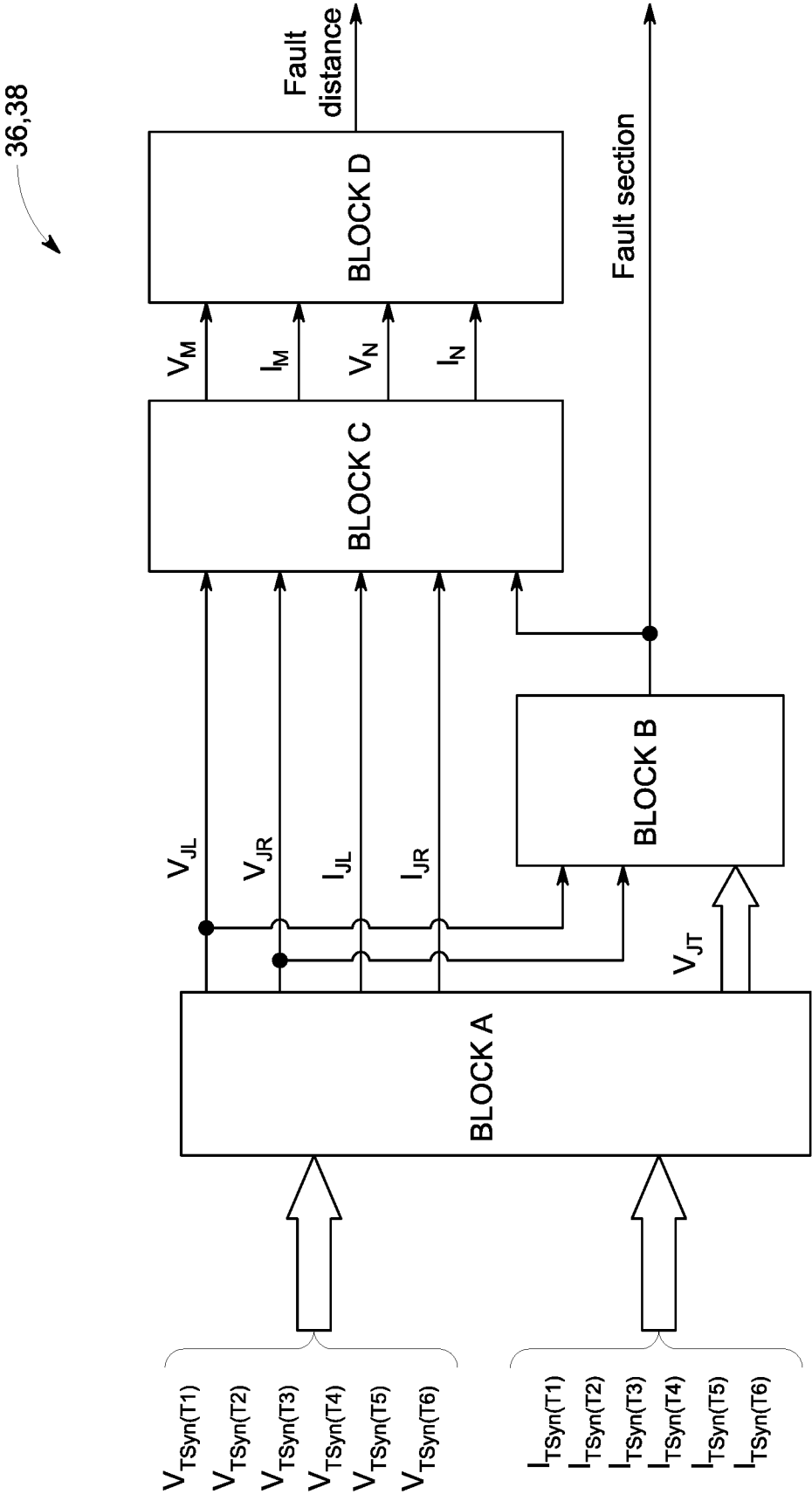


FIG. 7

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2017/078152A. CLASSIFICATION OF SUBJECT MATTER
INV. G01R31/08
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
G01R

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	ABE M ET AL: "DEVELOPMENT OF A NEW FAULT LOCATION SYSTEM FOR MULTI-TERMINAL SINGLE TRANSMISSION LINES", IEEE TRANSACTIONS ON POWER DELIVERY, IEEE SERVICE CENTER, NEW YORK, NY, US, vol. 10, no. 1, 31 January 1995 (1995-01-31), pages 159-167, XP000513164, ISSN: 0885-8977, DOI: 10.1109/61.368402 abstract; figures 1-2,5-7 paragraph [0002] - paragraph [0005] ----- -/--	1-9



Further documents are listed in the continuation of Box C.



See patent family annex.

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"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

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"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

22 December 2017

Date of mailing of the international search report

05/01/2018

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Authorized officer

Maric, Viktor

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2017/078152

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

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