

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
11 October 2007 (11.10.2007)

PCT

(10) International Publication Number
WO 2007/114620 A1

(51) International Patent Classification:
H01Q 1/38 (2006.01)

(74) Agent: LEE, Du-Han; 3F, Yongma B/D., #668-2 Yeok-sam-dong, Gangnam-gu, Seoul 135-080 (KR).

(21) International Application Number:
PCT/KR2007/001597

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(22) International Filing Date: 2 April 2007 (02.04.2007)

(25) Filing Language: Korean

(26) Publication Language: English

(30) Priority Data:
10-2006-0030232 3 April 2006 (03.04.2006) KR
10-2007-0025085 14 March 2007 (14.03.2007) KR

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IS, IT, LT, LU, LV, MC, MT, NL, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

(71) Applicant (for all designated States except US): ACE ANTENNA CORP. [KR/KR]; 724-4 Gojan-dong, Nam-dong-gu, Incheon-shi 405-822 (KR).

(72) Inventors; and

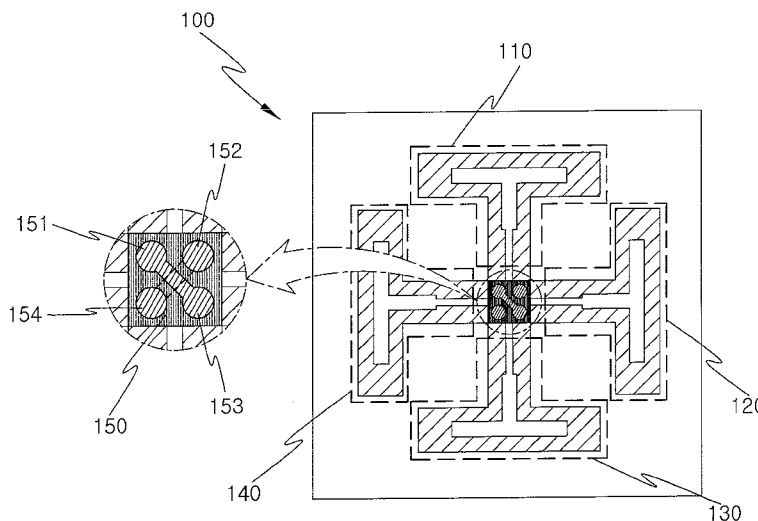
(75) Inventors/Applicants (for US only): PARK, Joo Sung [KR/KR]; Woosung 2nd Apt. 217-1207, Yeonsu-dong, Yeonsu-gu, Incheon-shi 406-110 (KR). JIN, Jae Sun [KR/KR]; Hyoja Villa 301, 724-16 Bupyeong-gu, Incheon-shi 403-010 (KR).

Published:

— with international search report

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: DUAL POLARIZATION BROADBAND ANTENNA HAVING WITH SINGLE PATTERN



(57) Abstract: The present invention relates to a dual polarization broadband antenna having a single pattern, which is provide with a radiation device having a square structure, in which a plurality of folded dipole elements are formed in a single continuously-connected pattern, and a feeding portion for feeding signals to the plurality of folded dipole elements is formed on the radiation device. Accordingly, the plurality of folded dipole elements formed on the radiation device are connected in a single square and rectangular pattern, so that the structure thereof is simplified, with the result that the cost can be reduced. Furthermore, the feeding portion, that dually feeds signals, and the plurality of folded dipole elements, connected in a single pattern, are coupled, so that the dual polarization characteristic can be easily acquired. Furthermore, currents input to the feeding points of the feeding portion are induced only to the folded dipole elements without having to flow into other feeding points, so that excellent isolation can be achieved.

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[DESCRIPTION]**[Invention Title]**

**DUAL POLARIZATION BROADBAND ANTENNA HAVING WITH SINGLE
PATTERN**

5 **[Technical Field]**

The present invention relates to a dual polarization
broadband antenna having a single pattern and, more particularly,
to a dual polarization broadband antenna, which has both a dual
polarization characteristic and a broadband characteristic
10 because it uses a structure in which a plurality of folded dipole
elements are formed in a single continuous pattern on a radiation
device, which is coupled to a dual feeding portion.

[Background Art]

As an example of a conventional dual polarization dipole
15 antenna, the dual polarization dipole antenna disclosed in Korean
Unexamined Patent Publication No. 2001-0040623 transmits
polarized electrical radiation at an angle of $+45^\circ$ or -45° in
relation to a predetermined arrangement of dipoles. The ends of
the symmetrical or approximately symmetrical lines, which lead to
20 respective dipole halves, are interconnected in such a way that
the corresponding line halves of adjacent dipole halves, which
are perpendicular to each other, are electrically connected, and
the supply of electrical power to the diametrically opposite
dipole halves results in a first polarization, and decouples a

second polarization which is orthogonal thereto.

However, the conventional technology has a structure in which four dipoles are uniformly separated from each other, so that there is a problem in that the structure of the antenna is complicated.

Furthermore, the four uniformly-separated dipoles and two pairs of symmetrical feeding portions are made of a metal material and are coupled to each other on a radiation substrate, so there are problems, not only in that impedance matching is difficult to achieve, but also in that the broadband characteristic and the antenna gain are lowered.

[Disclosure]

[Technical Problem]

Accordingly, the present invention has been made keeping in mind the above problems occurring in the prior art, and an object of the present invention is to provide an antenna having a simple structure, in which a plurality of folded dipole elements formed on a radiation device are connected in a single square and rectangular pattern.

Another object of the present invention is to form the plurality of folded dipole elements on the radiation device in a single pattern, thus not only facilitating impedance matching but also further improving the broadband characteristic and the antenna gain.

A further object of the present invention is to decrease squint error by forming the plurality of folded dipole elements

at different lengths, thus decreasing signal noise occurring at the time of transmission and reception.

[Technical Solution]

In order to accomplish the above objects, the present invention provides a dual polarization broadband antenna having a single pattern, including a radiation device having a square structure, in which a plurality of folded dipole elements are formed in a single continuous pattern; and a feeding portion for feeding signals to the plurality of folded dipole elements formed on the radiation device.

In accordance with an embodiment of the present invention, each of the plurality of folded dipole elements comprises a feeding line portion and a radiation portion.

In accordance with an embodiment of the present invention, the feeding portion includes four feeding points, the four feeding points being formed to cross each other and configured to feed the signals.

In accordance with an embodiment of the present invention, the plurality of folded dipole elements causes polarization through the vector addition of electrical fields formed by the flow of a current fed to the feeding portion.

In accordance with an embodiment of the present invention, the plurality of folded dipole elements forms dual polarizations using a single pattern in response to the signals that are dually fed to the feeding portion single pattern.

In accordance with an embodiment of the present invention,

the plurality of folded dipole elements causes a polarization direction to be formed at an angle of $+45^\circ$ or -45° in response to the signals that are dually fed to the feeding portion.

In addition, the present invention provides a dual
5 polarization broadband antenna having a single pattern, including a radiation device having a rectangular structure, in which a plurality of folded dipole elements are formed in a single continuous pattern; and a feeding portion for feeding signals to the plurality of folded dipole elements formed on the radiation
10 device.

In accordance with another embodiment of the present invention, each of the plurality of folded dipole elements comprises a feeding line portion and a radiation portion.

In accordance with another embodiment of the present
15 invention, the feeding portion comprises four feeding points, the four feeding points being formed to cross each other and configured to feed the signals.

In accordance with another embodiment of the present invention, the plurality of folded dipole elements are formed at
20 different lengths.

In accordance with another embodiment of the present invention, the plurality of folded dipole elements decreases squint error.

In accordance with another embodiment of the present
25 invention, the plurality of folded dipole elements causes polarization through the vector addition of electrical fields formed by the flow of a current fed to the feeding portion.

In accordance with another embodiment of the present invention, the plurality of folded dipole elements forms dual polarizations using a single pattern in response to the signals that are dually fed to the feeding portion single pattern.

5 In accordance with another embodiment of the present invention, the plurality of folded dipole elements causes a polarization direction to be formed at an angle of $+45^\circ$ or -45° in response to the signals that are dually fed to the feeding portion.

10 **[Advantageous Effects]**

According to the present invention, the plurality of folded dipole elements formed on the radiation device are connected in a single square and rectangular pattern, so that the structure thereof is simplified and the manufacturing thereof is
15 convenient, with the result that the cost can be reduced. Furthermore, the feeding portion dually feeds signals to the plurality of folded dipole elements, so that the dual polarization characteristic can be acquired using the single pattern. Furthermore, the plurality of folded dipole elements
20 formed on the radiation device is elaborately and conveniently formed using the single pattern, so that the impedance matching can be easily achieved and the broadband characteristic and the antenna gain can be improved. Furthermore, currents input to the feeding points of the feeding portion are induced to the folded
25 dipole elements without having to flow into other feeding points, so that excellent isolation characteristics can be achieved.

Furthermore, the plurality of folded dipole elements are formed at different lengths, so that the squint error can be decreased. Accordingly, the signal noise occurring at the time of transmission and reception can be decreased.

5 **[Description of Drawings]**

FIG. 1 is a front view of a dual polarization broadband antenna having a single pattern according to an embodiment of the present invention;

10 FIG. 2 is a diagram showing the construction of a folded dipole antenna having a single pattern according to FIG. 1 of the present invention;

FIG. 3 is a diagram showing polarization caused by a first current flow according to FIG. 1 of the present invention;

15 FIG. 4 is a diagram showing polarization caused by a second current flow according to FIG. 1 of the present invention;

FIG. 5 is a characteristic diagram showing a standing-wave ratio according to FIG. 1 of the present invention;

20 FIG. 6 is a front view of a dual polarization broadband antenna having a single pattern according to another embodiment of the present invention;

FIG. 7 is a diagram showing the construction of a folded dipole antenna having a single pattern according to FIG. 6 of the present invention;

25 FIG. 8 is a diagram showing polarization caused by a first current flow according to FIG. 6 of the present invention;

FIG. 9 is a diagram showing polarization caused by a

second current flow according to FIG. 6 of the present invention;
and

FIG. 10 is a diagram indicating whether squint error occurs according to FIG. 6 of the present invention.

- 5 *Description of reference numerals of principal elements*
- 100, 500: radiation devices
- 110, 510: first folded dipole elements
- 111, 511: first feeding line portions
- 112, 512: first radiation portions
- 10 120, 520: second folded dipole elements
- 121, 521: second feeding line portions
- 122, 522: second radiation portions
- 130, 530: third folded dipole elements
- 131, 531: third feeding line portions
- 15 132, 532: third radiation portions
- 140, 540: fourth folded dipole elements
- 141, 541: fourth feeding line portions
- 142, 542: fourth radiation portions
- 150, 550: feeding portions
- 20 151, 551: first feeding points
- 152, 552: second feeding points
- 153, 553: third feeding points
- 154, 554: fourth feeding points
- 200, 600: direction of current
- 25 300, 700: direction of electric field
- 400, 800: direction of polarization

[Mode for Invention]

FIG. 1 is a front view of a dual polarization broadband antenna having a single pattern according to an embodiment of the present invention. The dual polarization broadband antenna includes a radiation device 100a having a square structure, in which a plurality of folded dipole elements 110, 120, 130 and 140 are formed in a single continuously-connected pattern, and a feeding portion 150 for feeding signals to the plurality of folded dipole elements 110, 120, 130 and 140 formed on the radiation device 100.

In greater detail, the radiation device 100 is configured such that the first to fourth folded dipole elements 110, 120, 130 and 140 are formed thereon and are coupled to the feeding portion 150 in order to feed signals, thus radiating a signal formed using vector addition for the first to fourth folded dipole elements 110, 120, 130 and 140.

The feeding portion 150 is configured such that first to fourth feeding points 151, 152, 153 and 154 are formed in respective locations, in which the first to fourth feeding line portions 111, 121, 131 and 141 of the first to fourth folded dipole elements 110, 120, 130 and 140 are interconnected, the first feeding point 151 and the third feeding point 153 are connected to each other, the second feeding point 152 and the fourth feeding point 154 are connected to each other, and the connected first and third feeding points 151 and 153 and the connected second and fourth feeding points 152 and 154 are formed to cross each other, thus causing dual polarization by enabling

signals, which are supplied from the outside, to be dually fed to the first to fourth folded dipole elements 110, 120, 130 and 140.

Furthermore, the current flowing into the feeding portion 150 is induced only by the first to fourth folded dipole elements 110, 120, 130 and 140, so that excellent isolation characteristics can be achieved.

The first folded dipole element 110, as shown in FIG. 2, is provided with the first radiation portion 112 and the first feeding line portion 111. In this case, current supplied from the outside to the feeding portion 150 flows into the first feeding line portion 111, and the current flowing into the first feeding line portion 111 is induced to the first radiation portion 112.

Furthermore, the second, third and fourth folded dipole elements 120, 130 and 140 are respectively provided with the second feeding line portion 121 and a second radiation portion 122, the third feeding line portion 131 and a third radiation portion 132, and the fourth feeding line portion 141 and a fourth radiation portion 142. In this case, current is induced to each of the second, third and fourth radiation portions 122, 132 and 142 in response to the signals that flow into the feeding portion 150.

FIG. 3 is a diagram showing polarization caused by a first current flow according to FIG. 1 of the present invention, in which one of the dual polarizations, obtained through the vector addition of an electric field generated by the first current flow, is shown. FIG. 4 is a diagram showing polarization caused by a second current flow according to FIG. 1 of the present

invention, in which the other polarization, which is obtained through the vector addition of an electrical field generated by the second current flow, is shown.

In greater detail, as shown in FIG. 3, a positive (+) current is applied to the first feeding point 151 and a negative (-) current is applied to the third feeding point 153, so that current directions 200 are respectively formed along the first to fourth folded dipole elements 110, 120, 130 and 140 by the applied currents, the directions 300 of respective electric fields are formed to correspond to the first to fourth folded dipole elements 110, 120, 130 and 140 by the flow of the currents, and a polarization direction 400 is formed at an angle of $+45^\circ$ by the vector addition of the formed electric fields.

In FIG. 4, a positive (+) current is applied to the fourth feeding point 154 and a negative (-) current is applied to the second feeding point 152, so that the directions 300 of electric fields are determined by the current directions 200 of the first to fourth folded dipole elements 110, 120, 130 and 140, and a polarization direction 400 is formed at an angle of -45° by the vector addition of the formed electric fields.

Accordingly, as shown in FIGS. 3 and 4, the directions 300 of electric fields are determined by the current directions 200, and the polarization direction 400 is formed at an angle of $+45^\circ$ or -45° by the vector addition of the formed electric fields, and thus the dual polarization characteristic for the polarization direction 400 can be achieved.

FIG. 5 is a characteristic diagram showing a standing-wave

ratio according to FIG. 1 of the present invention. When a standing wave ratio is 2 : 1, an efficiency of about 90% is exhibited. In the proposed antenna, the range of a frequency band in which an efficiency of more than 90% is exhibited is around 800 MHz. Accordingly, the broadband characteristic can be achieved.

In particular, the present invention may be used to achieve a high gain characteristic in both a frequency range (2.3 GHz ~ 2.39 GHz) for Wibro, which is a wireless Internet service, and a frequency range (2.63 GHz ~ 2.655 GHz) for Digital Multimedia Broadcasting (DMB), because it has a broadband antenna characteristic.

FIG. 6 is a front view of a dual polarization broadband antenna having a single pattern according to another embodiment of the present invention. The dual polarization broadband antenna includes a radiation device 500a having a rectangular structure, in which a plurality of folded dipole elements 510, 520, 530 and 540 are formed thereon in a single continuously-connected pattern, and a feeding portion 550 configured to feed signals to the plurality of folded dipole elements 510, 520, 530 and 540 is formed on the radiation device 500.

In greater detail, the radiation device 500 is configured such that the first to fourth folded dipole elements 510, 520, 530 and 540 are formed thereon and are coupled to the feeding portion 550 to feed signals, thus radiating a signal formed using vector addition for the first to fourth folded dipole elements 510, 520, 530 and 540.

The plurality of folded dipole elements 510, 520, 530 and 540 are formed at different lengths, so that squint error can be decreased.

The feeding portion 550 is configured such that first to fourth feeding points 551, 552, 553 and 554 are formed in respective locations, in which the first to fourth feeding line portions 511, 521, 531 and 541 of the first to fourth folded dipole elements 510, 520, 530 and 540 are interconnected, the first feeding point 551 and the third feeding point 553 are connected to each other, the second feeding point 552 and the fourth feeding point 554 are connected to each other, and the connected first and third feeding points 551 and 553 and the connected second and fourth feeding points 552 and 554 are formed to cross each other, thus causing dual polarization by enabling signals, which are supplied from the outside, to be dually fed to the first to fourth folded dipole elements 510, 520, 530 and 540.

Furthermore, the current flowing into the feeding portion 550 is induced only by the first to fourth folded dipole elements 510, 520, 530 and 540, so that excellent isolation characteristics can be achieved.

The first folded dipole element 510, as shown in FIG. 7, is provided with the first radiation portion 512 and the first feeding line portion 511. In this case, current supplied from the outside to the feeding portion 550 flows into the first feeding line portion 511 and the current flowing to the first feeding line portion 511 is induced to the first radiation portion 512.

Furthermore, the second, third and fourth folded dipole

elements 520, 530 and 540 are respectively provided with the second feeding line portion 521 and a second radiation portion 522, the third feeding line portion 531 and a third radiation portion 532, and the fourth feeding line portion 541 and a fourth radiation portion 542. In this case, current is induced to each of the second, third and fourth radiation portions 522, 532 and 542 in response to the signals that flow into the feeding portion 150.

In particular, it can be seen that the plurality of folded dipole elements 510, 520, 530 and 540 is set such that the second and fourth folded dipole elements 520 and 540 have the same length, the first folded dipole element 510 is relatively long, and the third folded dipole element 530 is relatively short, and thus the folded dipole elements 510, 520, 530 and 540 are formed at different lengths, with the result that the squint error is decreased.

In addition, when the plurality of folded dipole elements 510, 520, 530 and 540 are formed at different lengths, the magnitude and phase of each of the currents varies arbitrarily. In this case, the magnitude and phase of the positive (+) current and the magnitude and phase of the negative (-) current differ from each other, and the magnitudes and phases of the electric fields also differ from each other, so that the electric field obtained through the vector addition varies, and the beam orientation of the plurality of folded dipole elements 510, 520, 530 and 540 varies. Therefore, the squint error can be decreased.

FIG. 8 is a diagram showing polarization caused by a first current flow according to FIG. 6 of the present invention, in which one of the dual polarizations, obtained through the vector addition of an electric field generated by the first current flow, is shown. FIG. 9 is a diagram showing a polarization caused by a second current flow according to FIG. 6 of the present invention, in which the other polarization, which is obtained through the vector addition of an electric field generated by the second current flow, is shown.

In greater detail, as shown in FIG. 8, a positive (+) current is applied to the first feeding point 551 and a negative (-) current is applied to the third feeding point 553, so that current directions 600 are respectively formed along the first to fourth folded dipole elements 510, 520, 530 and 540 by the applied currents, the directions 700 of respective electric fields are formed to correspond to the first to fourth folded dipole elements 510, 520, 530 and 540 by the flow of the currents, and a polarization direction 800 is formed at an angle of $+45^\circ$ by the vector addition of the formed electric fields.

In FIG. 9, a positive (+) current is applied to the fourth feeding point 554 and a negative (-) current is applied to the second feeding point 552, so that the directions 700 of electric fields are determined by the current directions 600 of the first to fourth folded dipole elements 510, 520, 530 and 540, and a polarization direction 800 is formed at an angle of -45° by the vector addition of the formed electric fields.

Accordingly, in FIGS. 8 and 9, the directions 700 of

electric fields are determined by the current directions 600, and the polarization direction 800 is formed at an angle of $+45^\circ$ or -45° by the vector addition of the formed electric fields, and thus the dual polarization characteristic for the polarization direction 800 can be achieved.

FIG. 10 is a diagram showing whether squint error occurs according to FIG. 6 of the present invention. FIG. 10 (a) shows that the forward direction of the antenna is 0° and the radiation direction of the antenna varies from 0° to θ° . In this case, such variation is called squint error. In contrast, FIG. 10 (b) shows that the forward direction of the antenna is 0° and the radiation direction of the antenna is 0° , and thus there is no squint error. Accordingly, it can be seen that an adjustment is made such that the folded dipole elements have different lengths, so that the radiation direction deviated by a specific angle in the forward direction is compensated for, therefore the squint error can be decreased.

Although the present invention has been described above in detail, it should be understood that the embodiments mentioned in the process are only illustrative and not restrictive. Furthermore, modifications in the elements of the present invention within the extent that they represent equal replacements in a range that does not depart from the technical spirit of the present invention, defined by the following claims, should be considered as being included in the scope of the present invention.

【CLAIMS】**【Claim 1】**

A dual polarization broadband antenna having a single pattern, comprising:

5 a radiation device having a square structure, in which a plurality of folded dipole elements are formed in a single continuous pattern; and

10 a feeding portion configured to feed signals to the plurality of folded dipole elements formed on the radiation device.

【Claim 2】

The dual polarization broadband antenna according to claim 1, wherein each of the plurality of folded dipole elements comprises a feeding line portion and a radiation portion.

15 【Claim 3】

The dual polarization broadband antenna according to claim 1, wherein the feeding portion comprises four feeding points, the four feeding points being formed to cross each other and configured to feed the signals.

20 【Claim 4】

The dual polarization broadband antenna according to claim 1, wherein the plurality of folded dipole elements causes polarization through vector addition of electrical fields formed by the flow of a current fed to the feeding portion.

【Claim 5】

The dual polarization broadband antenna according to claim 4, wherein the plurality of folded dipole elements forms dual polarizations using a single pattern in response to the signals that are dually fed to the feeding portion single pattern.

【Claim 6】

The dual polarization broadband antenna according to claim 5, wherein the plurality of folded dipole elements causes a polarization direction to be formed at an angle of $+45^\circ$ or -45° in response to the signals that are dually fed to the feeding portion.

【Claim 7】

A dual polarization broadband antenna having a single pattern, comprising:

a radiation device having a rectangular structure, in which a plurality of folded dipole elements are formed in a single continuous pattern; and

a feeding portion configured to feed signals to the plurality of folded dipole elements formed on the radiation device.

【Claim 8】

The dual polarization broadband antenna according to claim 7, wherein each of the plurality of folded dipole elements

comprises a feeding line portion and a radiation portion.

【Claim 9】

The dual polarization broadband antenna according to claim 7, wherein the feeding portion comprises four feeding points, the
5 four feeding points being formed to cross each other and configured to feed the signals.

【Claim 10】

The dual polarization broadband antenna according to claim 7, wherein the plurality of folded dipole elements are formed at
10 different lengths.

【Claim 11】

The dual polarization broadband antenna according to claim 10, wherein the plurality of folded dipole elements decreases
squint error.

15 **【Claim 12】**

The dual polarization broadband antenna according to claim 11, wherein the plurality of folded dipole elements causes
polarization through vector addition of electrical fields formed by the flow of a current fed to the feeding portion.

20 **【Claim 13】**

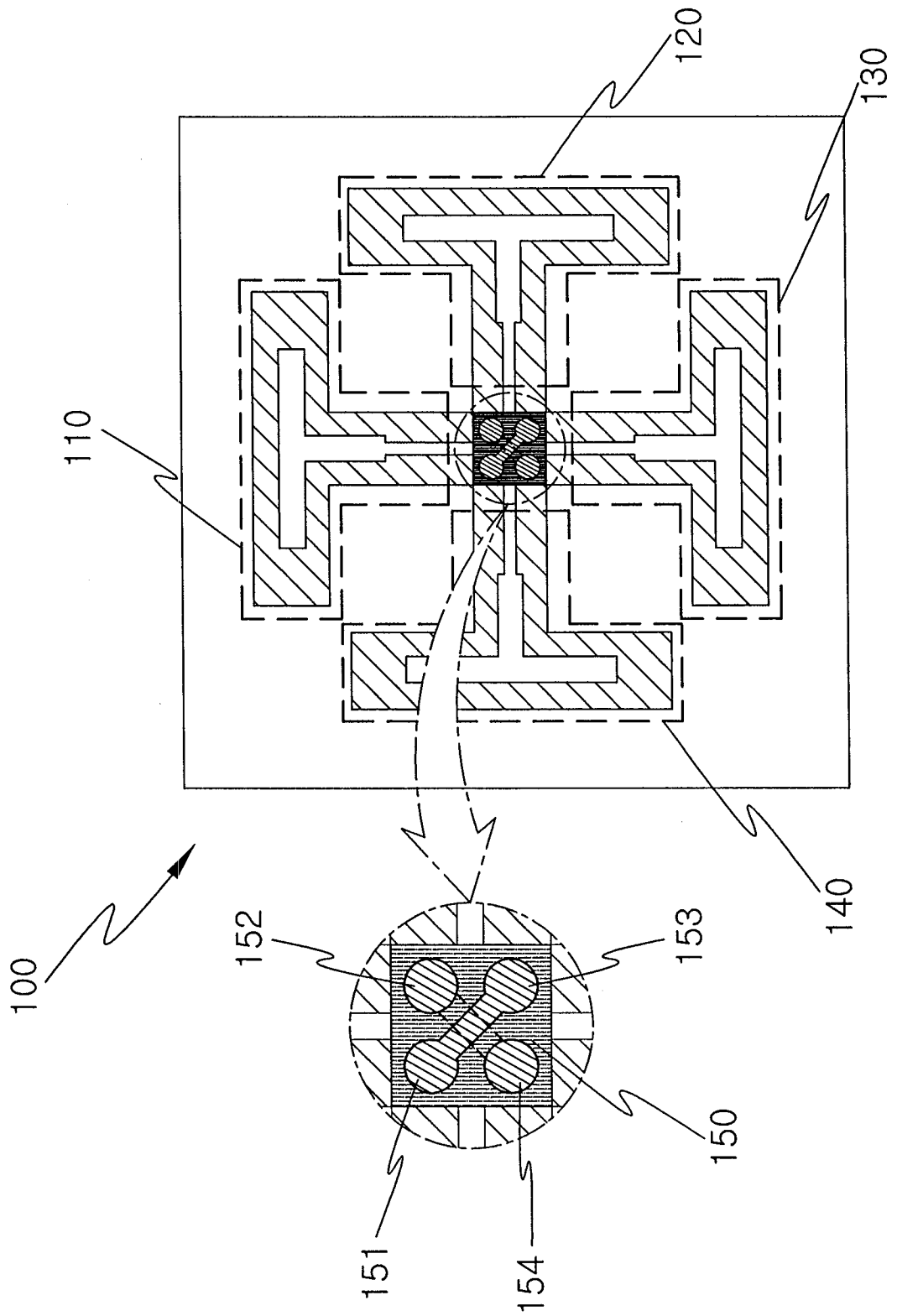
The dual polarization broadband antenna according to claim 12, wherein the plurality of folded dipole elements forms dual

polarizations using a single pattern in response to the signals that are dually fed to the feeding portion single pattern.

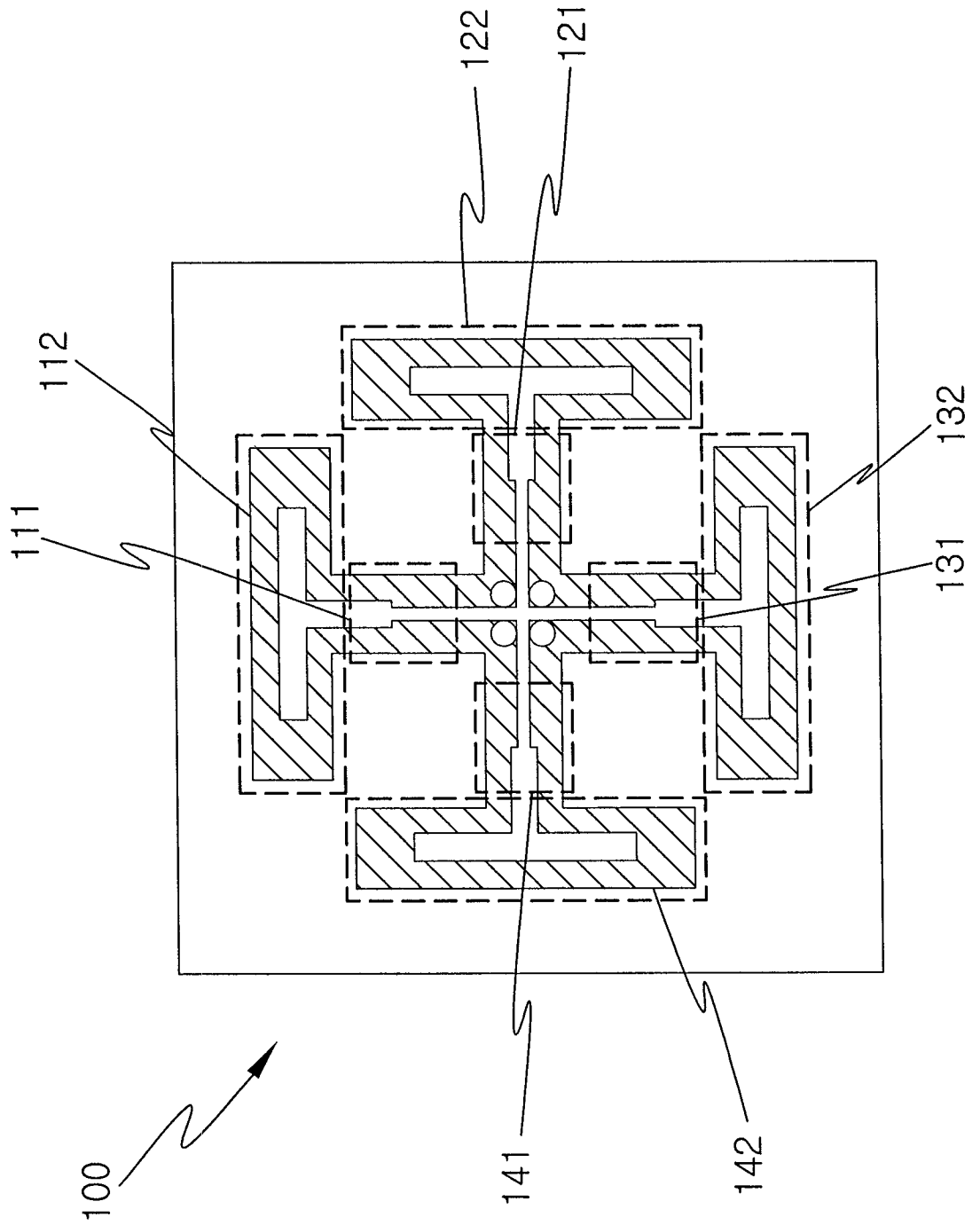
【Claim 14】

5 The dual polarization broadband antenna according to claim 13, wherein the plurality of folded dipole elements causes a polarization direction to be formed at an angle of $+45^\circ$ or -45° in response to the signals that are dually fed to the feeding portion.

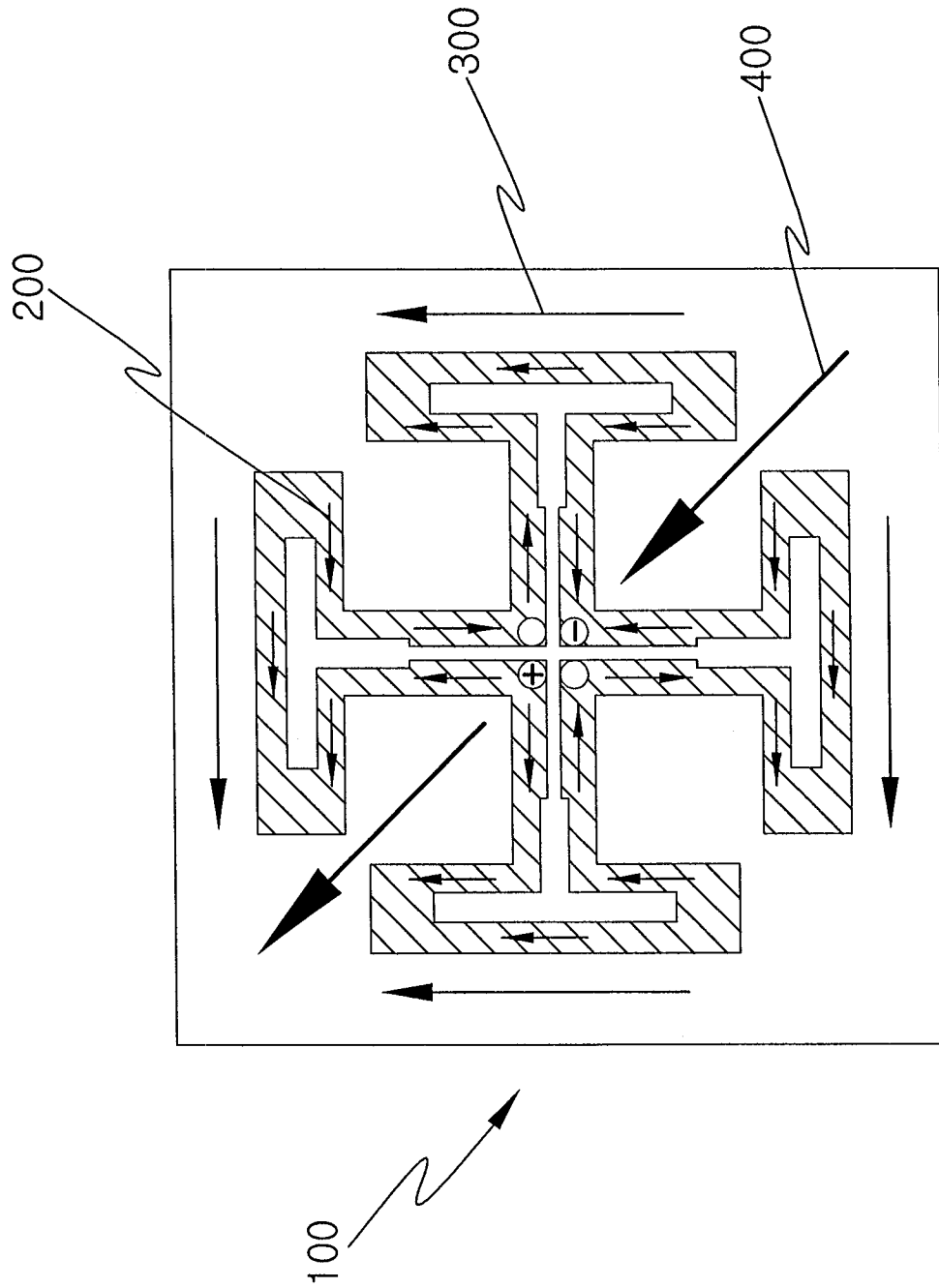
[Fig 1]



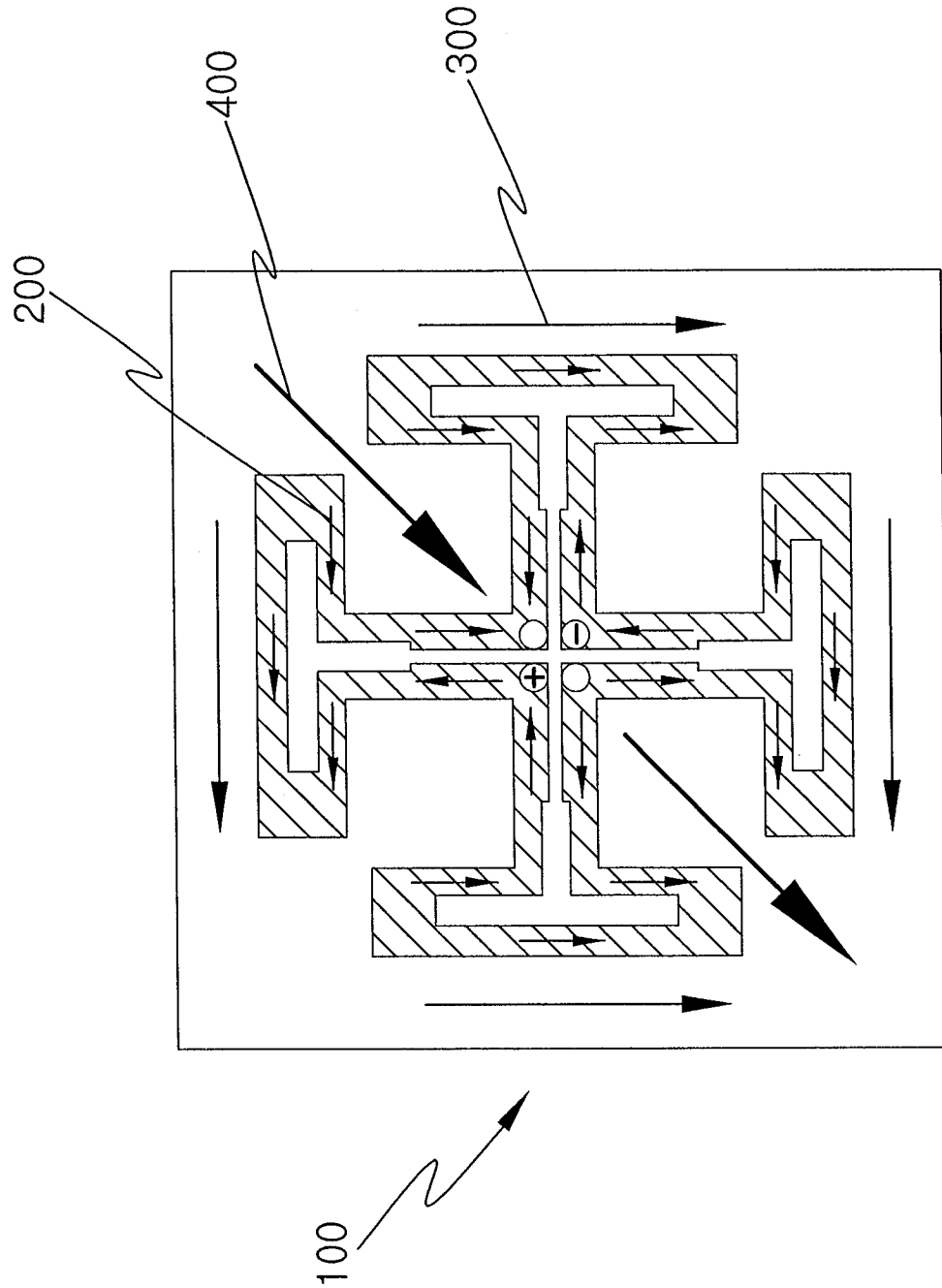
[Fig 2]



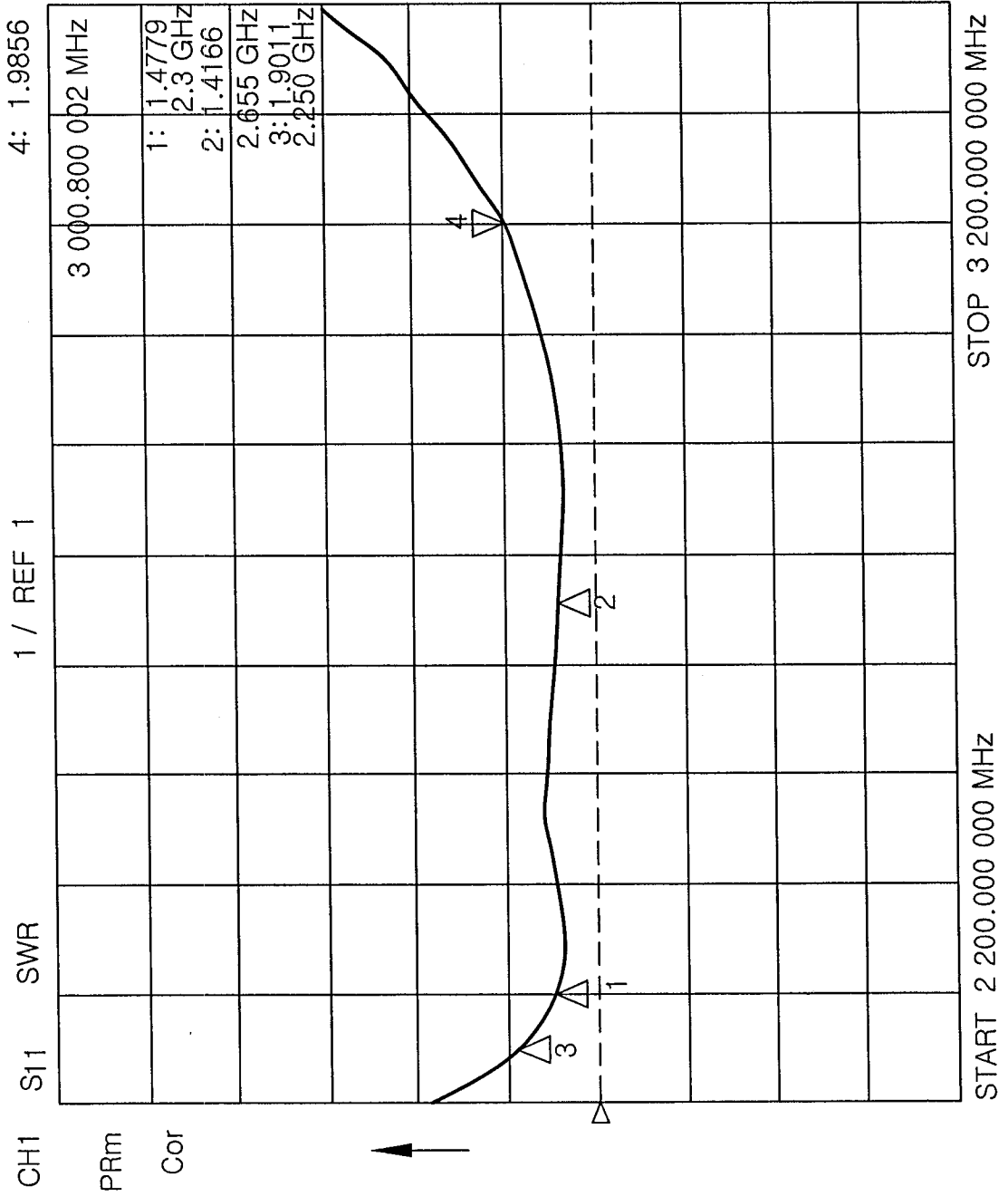
[Fig 3]



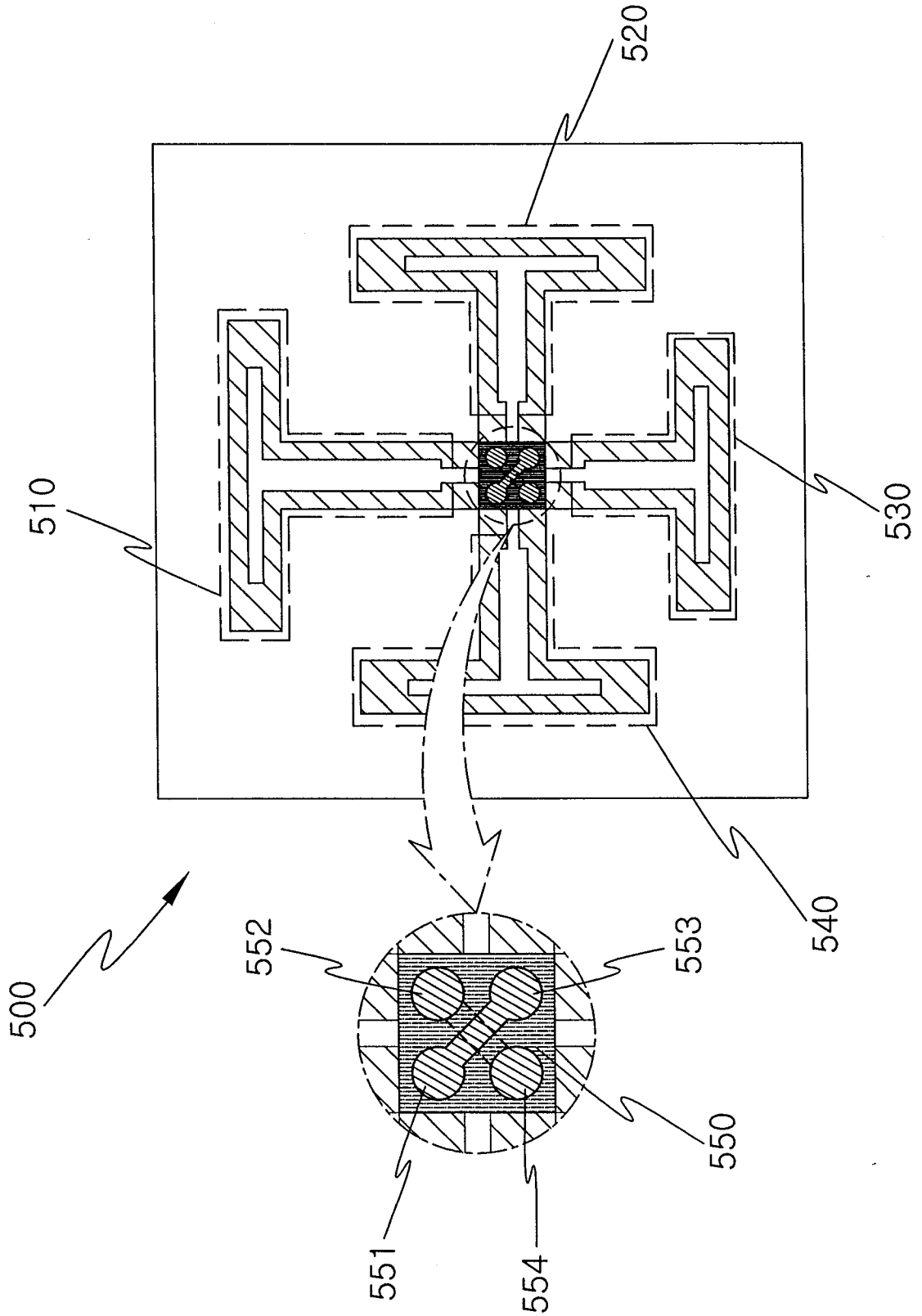
[Fig 4]



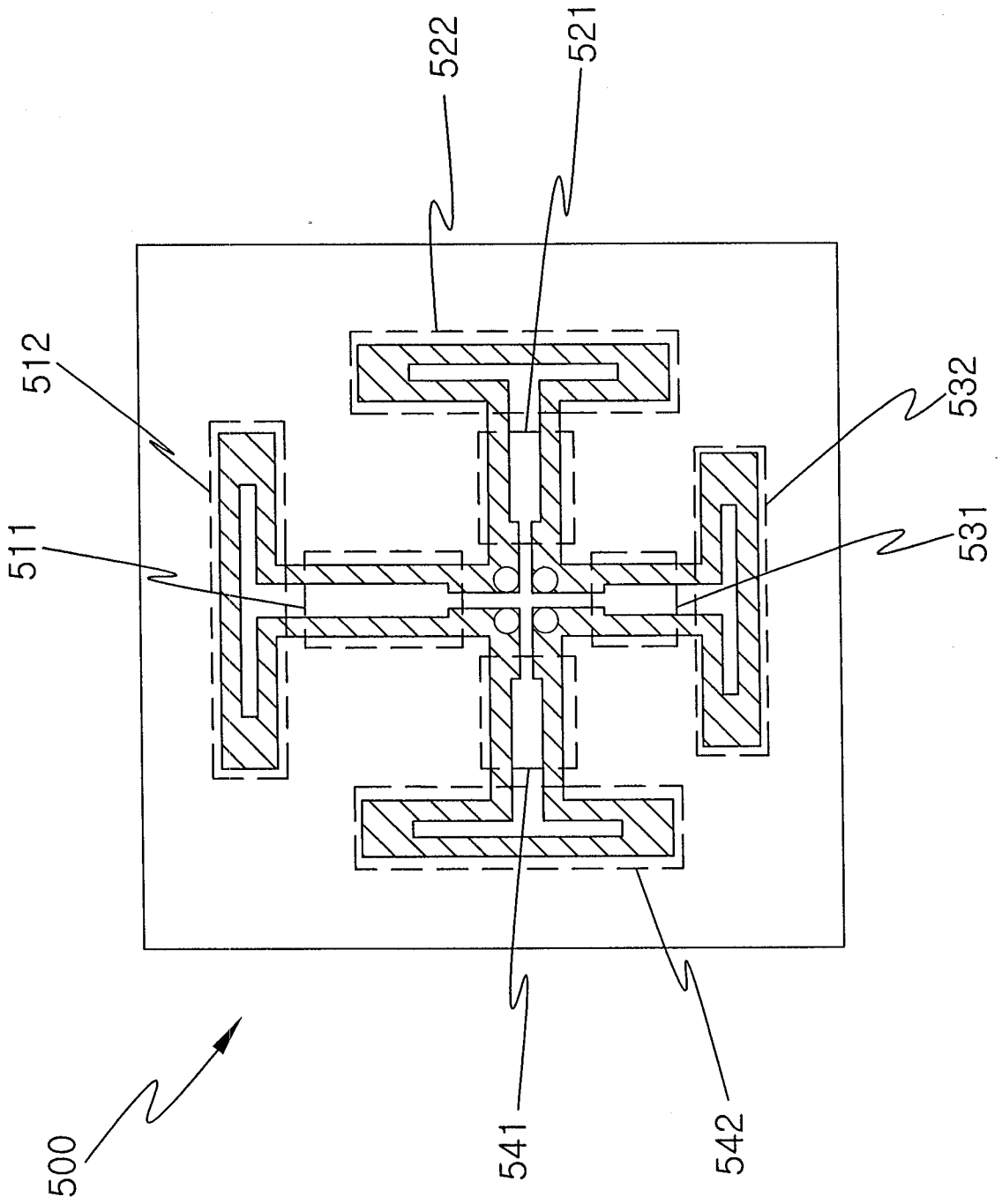
[Fig 5]



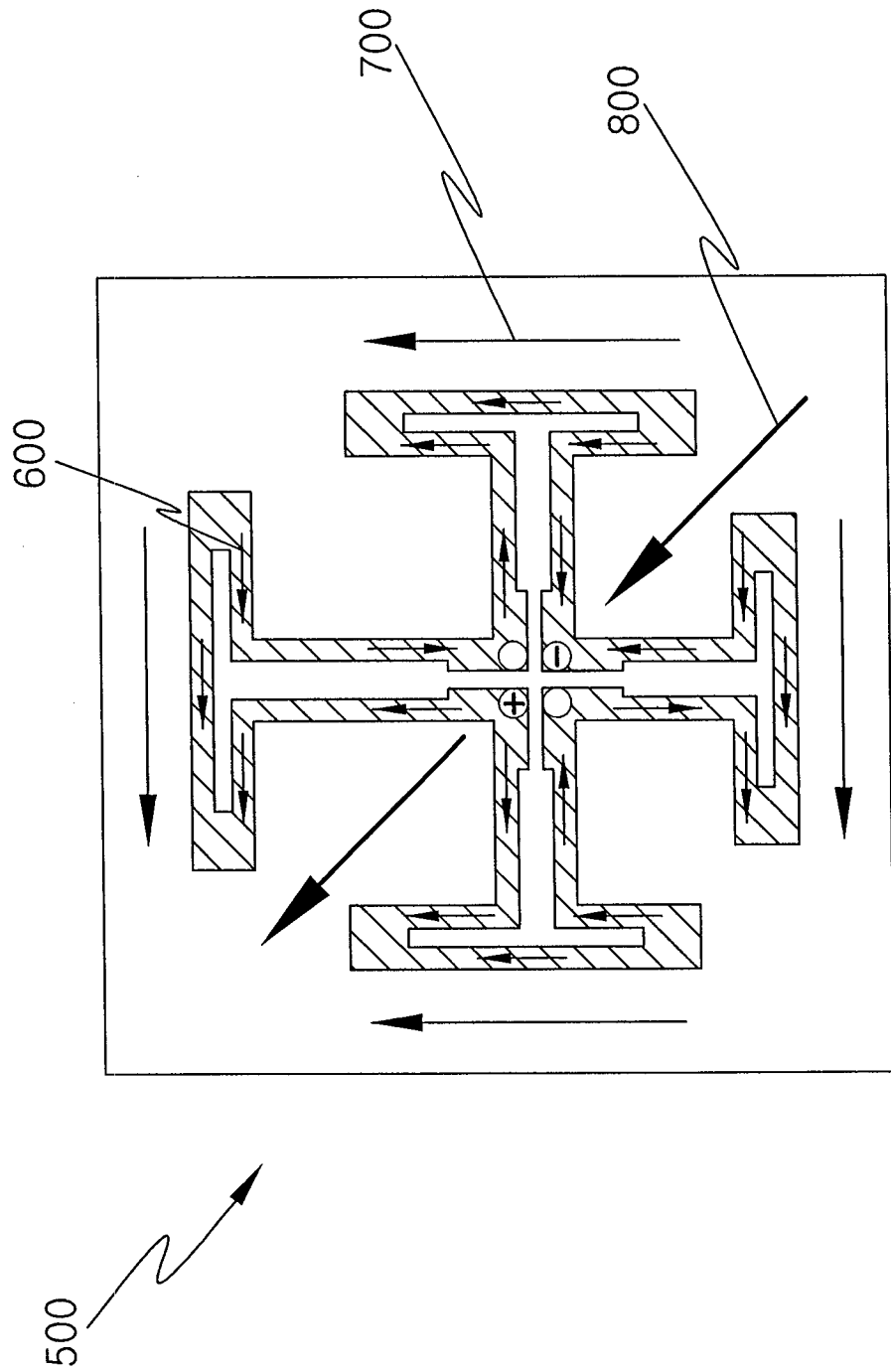
[Fig 6]



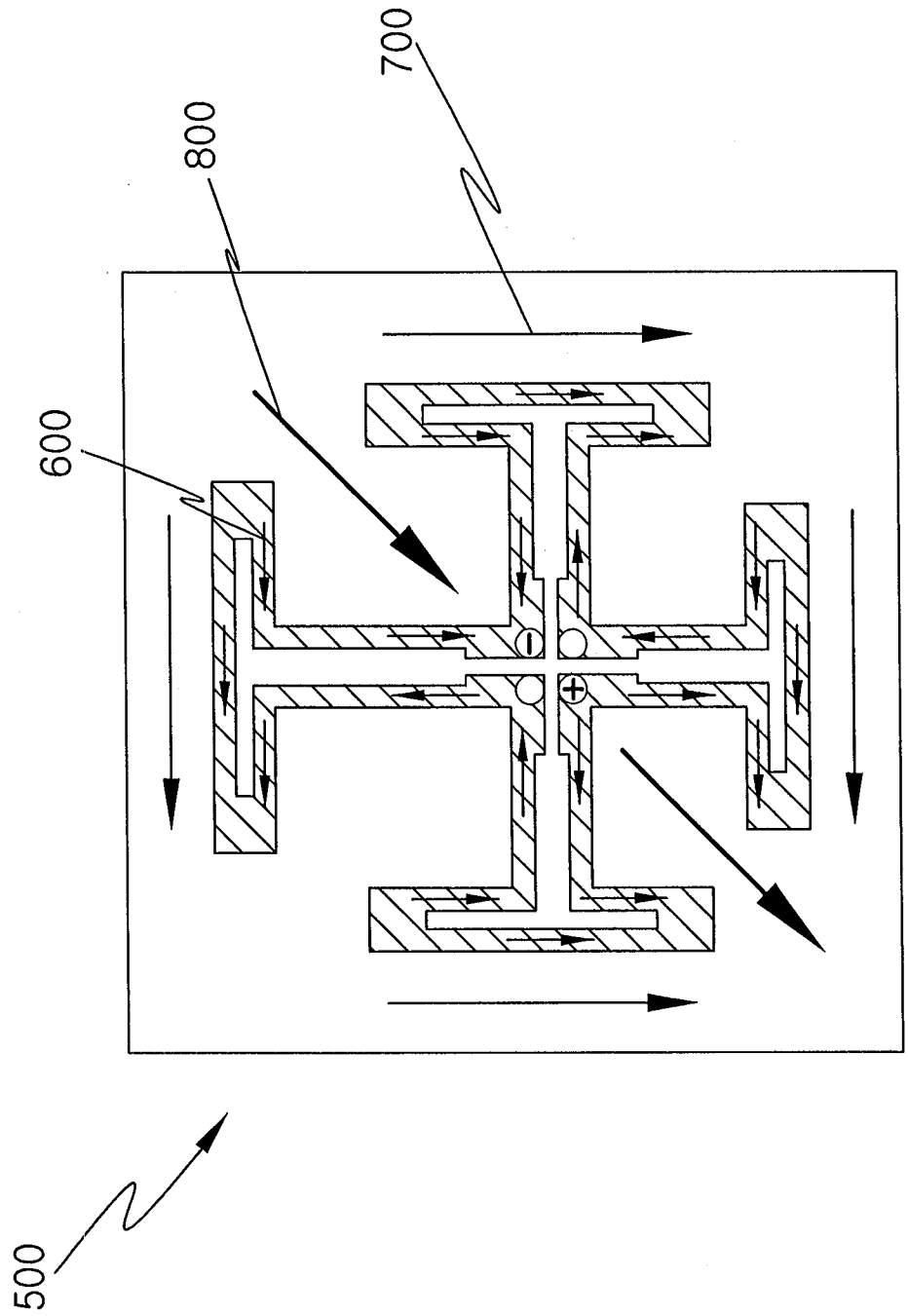
[Fig 7]



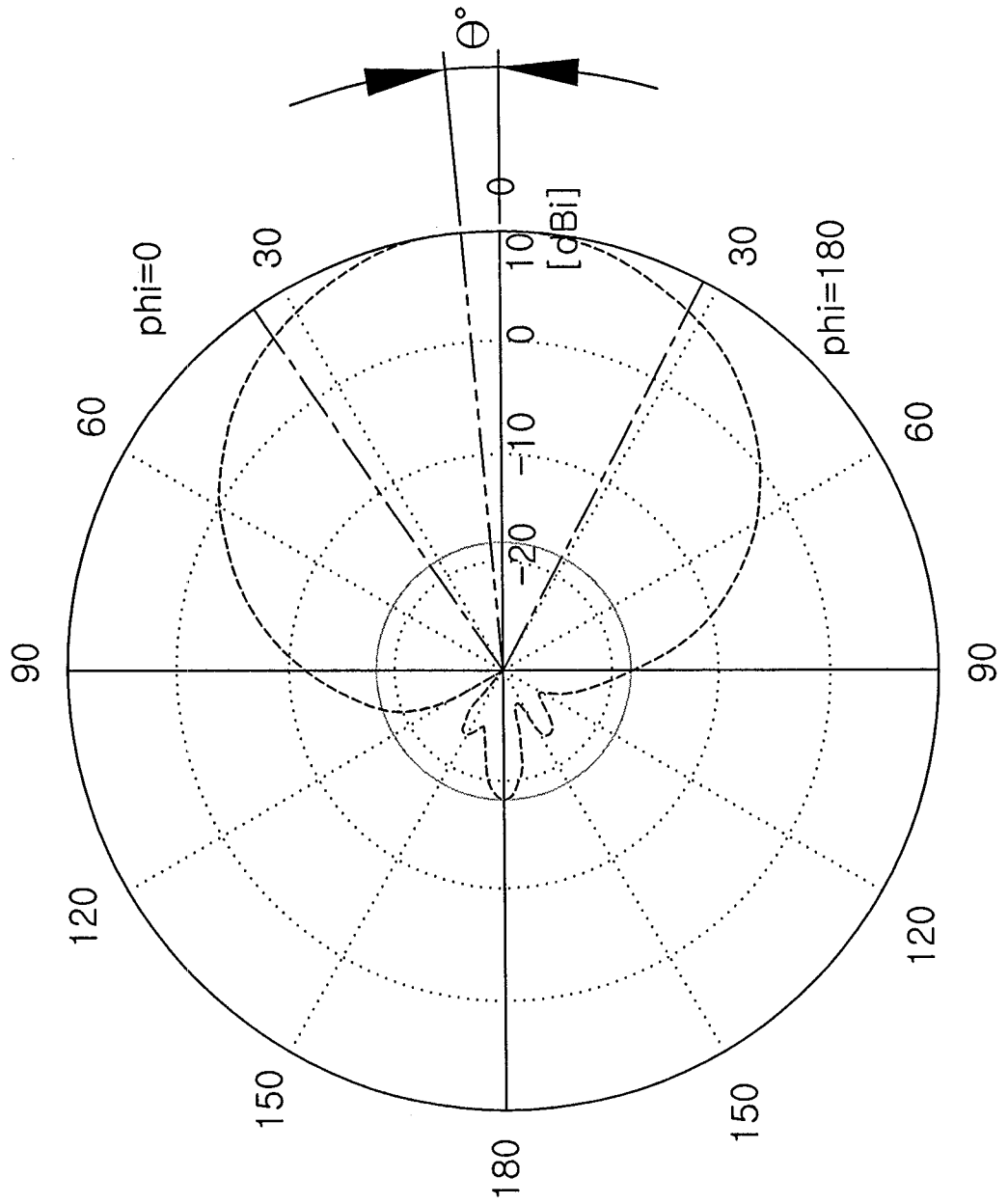
[Fig 8]



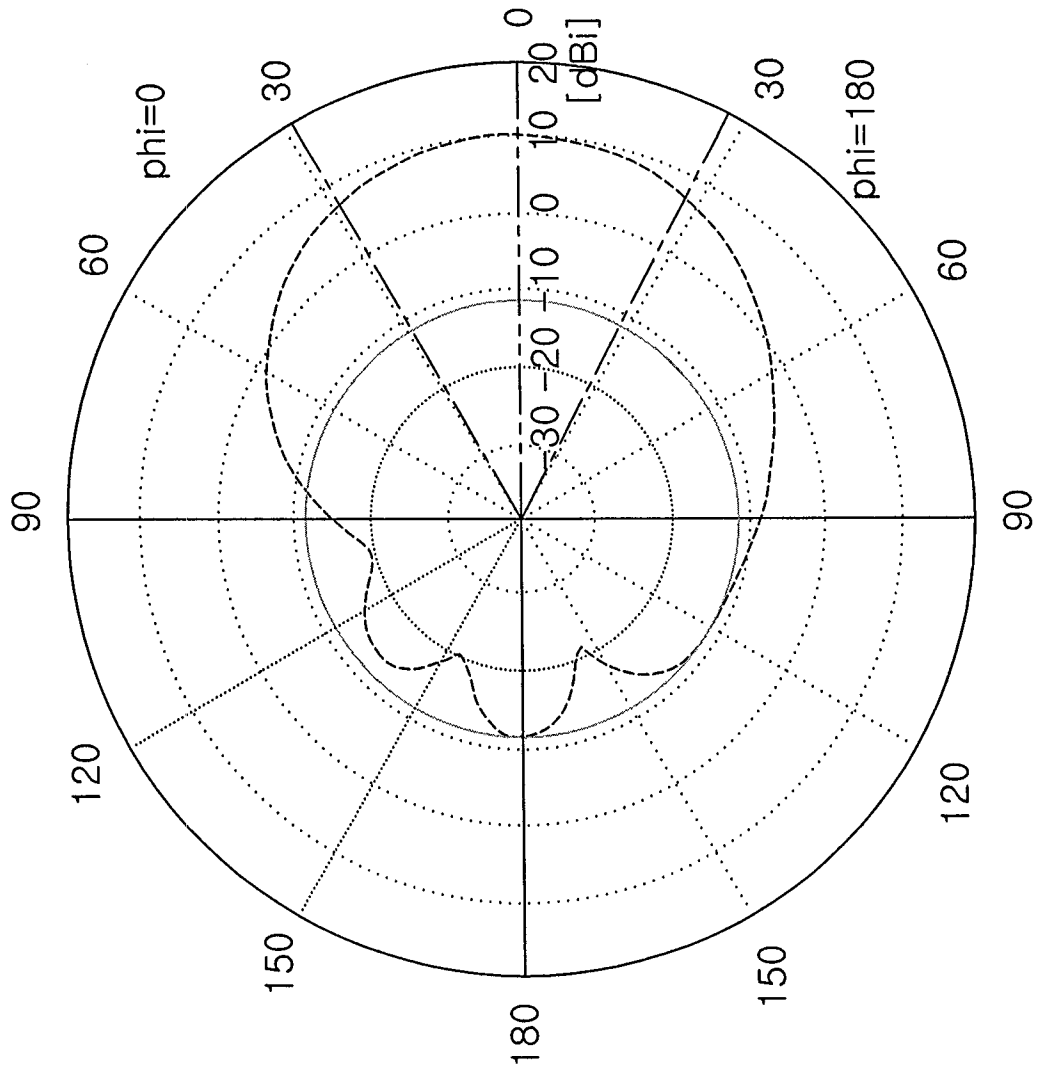
[Fig 9]



[Fig 10]



[Fig 11]



INTERNATIONAL SEARCH REPORT

International application No.
PCT/KR2007/001597**A. CLASSIFICATION OF SUBJECT MATTER****H01Q 1/38(2006.01)i**

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC8 H01Q

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Korean Utility models and applications for Utility models since 1975
Japanese Utility models and applications for utility models since 1975

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

eKIPASS (KIPO internal) "antenna", "radiation", "pattern", "dual", "polarization", "folded"

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	KR 10-2001-0040623 A (KATHREIN-WERKE KG) 15 May 2001 See abstract, claims 1-24, figures 1-5.	1-14
A	JP 06-177635 A (MITSUBISHI ELECTRIC CORP.) 24 June 1994 See abstract, claims 1-3, figures 1- 5.	1-14
A	JP 2003-535541 A (BAE SYSTEMS INFORMATION AND ELECTRONIC SYSTEMS INTEGRATION INC.) 25 November 2003 See abstract, claims 1-19, figures 1-7.	1-14

 Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents:

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23 JULY 2007 (23.07.2007)

Date of mailing of the international search report

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/KR2007/001597

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