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(71) Applicant (for all designated States except US): **ST-ER-ICSSON SA** [CH/CH]; 39 Chemin du Champ-des-Filles, CH-1228 Plan-Les-Ouates (CH).

(72) Inventors; and

(75) Inventors/Applicants (for US only): **WAGNER, Grégory** [FR/FR]; 10, avenue Dugueyt Jouvin, F-38500 Voiron (FR). **MINA, Rayan** [LB/FR]; 49 Bd Joseph Vallier, F-38100 Grenoble (FR).(74) Agents: **LABAUNE, Anne-Lise** et al.; Cabinet Plasseraud, 52 rue de la Victoire, F-75440 Paris Cedex 09 (FR).

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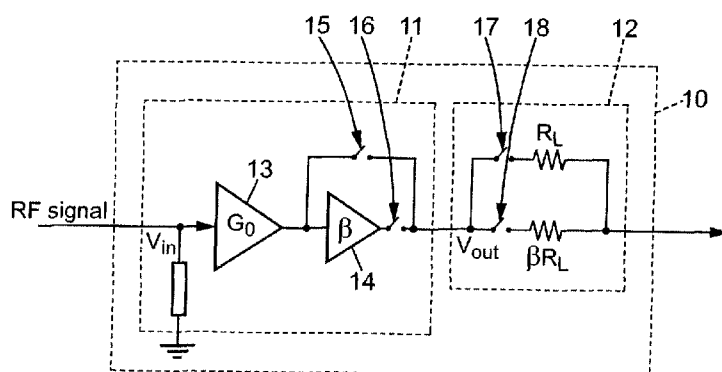


FIG. 2

(57) Abstract: Amplifier (6) for a wireless receiver, the amplifier comprising a voltage amplifier module having a voltage gain switchable between a first voltage gain value and a second voltage gain value higher than the first gain value, and a resistance module having a resistance switchable between a first resistance value and a second resistance value higher than the first resistance value, an output of the voltage amplifier module being connected to an input of the resistance module, the amplifier further comprising a set of switches configured to set the voltage gain value and the resistance value, the amplifier being operable in: - a nominal mode of operation in which the voltage gain value is set to the second voltage gain value, the resistance value being set to the second resistance value, and - a high linearity mode of operation in which the voltage gain value is set to the first voltage gain value to improve linearity of the amplifier, the resistance value being set to the first resistance value to have the same ratio of the voltage gain value to the resistance value as in the nominal mode of operation.



AMPLIFIER FOR A WIRELESS RECEIVER

TECHNICAL FIELD

The present invention generally relates to communication systems and more specifically to RF amplifier in wireless receivers.

5

BACKGROUND

The approaches described in this section could be pursued, but are not necessarily approaches that have been previously conceived or pursued. Therefore, unless otherwise indicated herein, the approaches described in this section are not prior art to the claims in this application and are not admitted to be prior art by inclusion in this section. Furthermore, all embodiments are not necessarily intended to solve all or even any of the problems brought forward in this section.

Radio Frequency (RF) systems generally comprise an antenna, connected to a RF receiver and to a RF transmitter via a Front-End Module (FEM). For example, the RF receiver may comprise a Low Noise Amplifier (LNA) and the RF transmitter may comprise a Power Amplifier (PA).

RF receivers have to maintain their performance even when receiving high-power blocking signals at the antenna. This is generally the case in Frequency Division Duplex (FDD) systems where the RF transmitter sends a high-level signal while the RF receiver receives a low-level signal. Usually the blocking signals are filtered prior to the Low Noise Amplifier (LNA) of the RF receiver, and sometimes after the LNA.

In some cases, an intermodulation product between an incoming blocking signal and the own transmission signal leakage (due to finite isolation between amplifiers PA and LNA) may fall into the frequency bandwidth of the low-level

reception signal. In such cases, the RF receiver sensitivity is jeopardized and the performance is below requirements.

These scenarios may be very frequent depending on the transmission-reception frequency separation and on the blocking signal spectral position. The levels of the blocking signal are specified by the standardization organization of the targeted RF communication system.

Moreover, in most modern mobile communication devices, the RF system, i.e. the cellular Radio Frequency Integrated Circuit (RF-IC), is coexisting with other radio engines, e.g. Bluetooth and Wireless LAN. In this case, the blocking signal is coming from a transmitter exhibiting thereby very high power levels. Even with good antenna isolation between radio engines and good RF filtering performance between the cellular antenna and the input of the reception path, intermodulation products may completely desensitize the receiver.

To overcome this coexistence issue a highly linear RF front-end (LNA and mixer) must be designed.

At the present time, existing RF CMOS front-end solutions are using inductors for output load and for feedback loops to achieve a high linearity in LNA circuits. Such components require large areas to be integrated properly with good quality factors.

Other solutions use thick oxide MOS devices along with above nominal process supply voltage. Such devices require an additional process mask during fabrication which significantly increases the cost of the overall processing in mass production. Also they slightly increase the overall power consumption of the RF front-end.

Other solutions comprise passive transferred impedance filtering at the LNA output. Such technique cannot work efficiently with feedback LNA as input impedance at blocker frequency will increase and voltage swing at the amplifier input accordingly. Besides, such filter requires large capacitor area to work properly along with additional RF phase generation.

US 6,288,609 describes a 2-stage LNA with an Automatic Gain Control (AGC) system that commands the gain of the 2nd stage (VGA) and the bias of the 1st stage (amplifier feedback stage) to achieve gain control and linearity

enhancement respectively. The total LNA gain does not remain constant when linearity enhancement is activated, and, as a consequence, noise performance is decreased.

US 7,746,169 describes a LNA with two possible modes of operation: a distortion cancellation mode (PDC) for linearity improvement and a high-gain mode for sensitivity case. To improve LNA linearity, additional active devices are used to cancel 3rd order intermodulation products generated by the main active device. Moreover, the gain is decreased and as a consequence the power consumption will increase. The PDC has a gate-to-source voltage dependency and is sensitive to device mismatch. Therefore, it requires a proper calibration method to achieve the linearity improvement.

US 7,266,360 describes an RF amplifier that includes a parasitic capacitor cancellation system, an image frequency filtering section and a gain controllable section. As in the systems described above, the total LNA gain does not remain constant, and, as a consequence, noise performance is decreased.

There is a need for improved methods and devices for enhancing linearity of an amplifier while maintaining the overall gain and power consumption of the amplifier constant.

SUMMARY

To address these needs, a first aspect of the present invention relates to an amplifier for a wireless receiver, the amplifier comprising a voltage amplifier module having a voltage gain switchable between a first voltage gain value and a second voltage gain value higher than the first gain value, and a resistance module having a resistance switchable between a first resistance value and a second resistance value higher than the first resistance value, an output of the voltage amplifier module being connected to an input of the resistance module, the amplifier further comprising a set of switches configured to set the voltage gain value and the resistance value, the amplifier being operable in:

- a nominal mode of operation in which the voltage gain value is set to the second voltage gain value, the resistance value being set to the second resistance value, and

- a high linearity mode of operation in which the voltage gain value is set to the first voltage gain value to improve linearity of the amplifier, the resistance value being set to the first resistance value to have a similar ratio of the voltage gain value to the resistance value as in the nominal mode of operation.

5 The word “similar” means that the ratio of the voltage gain value to the resistance value is the same in the two modes of operation, or at least that the ratio has close values in the two modes of operation. For example, the ratio is similar with less than 5% difference.

 The present invention aims to enhance the linearity of an amplifier for a
10 wireless receiver while maintaining the overall gain and power consumption of the amplifier constant. This permits to obtain a constant Signal to Noise Ratio (SNR) by keeping constant all the noise contributions of the succeeding stages.

 According to embodiments of the invention, the amplifier comprising a detection circuit configured to detect a risky intermodulation scenario in which the
15 wireless receiver may be desensitized, the high linearity mode of operation being activated when a risky intermodulation scenario is detected.

 According to other embodiments of the invention, the amplifier is configured to be connected to a detection circuit configured to detect a risky intermodulation scenario in which the wireless receiver may be desensitized, the
20 high linearity mode of operation being activated when a risky intermodulation scenario is detected.

 The voltage amplifier module may comprise a fixed gain part with a fixed voltage gain and a commutable gain part with a commutable voltage gain, the resistance module comprising a first resistance in parallel with a second
25 resistance, the set of switches comprising a first switch disposed in parallel with the commutable gain part, a second switch disposed between the output of the commutable gain part and the input of the resistance module, and a third switch disposed between the input of the resistance module and the first resistance, the first and third switches being open in the nominal mode of operation and closed in
30 the high linearity mode of operation, the second switch being closed in nominal mode of operation and open in high linearity mode of operation.

The set of switches may further comprise a fourth switch disposed between the input of the resistance module and the second resistance, the fourth switch being closed in nominal mode of operation and open in high linearity mode of operation.

5 According to some embodiments of the invention, the voltage amplifier module comprises a first fixed resistance in parallel with a first commutable resistance, the resistance module comprising a second fixed resistance in parallel with a second commutable resistance, the set of switches comprising a first switch disposed between an input of the voltage amplifier module and the first
10 commutable resistance, and a second switch disposed between the input of the resistance module and the second commutable resistance, the first and second switches being open in nominal mode of operation and closed in high linearity mode of operation.

A second aspect of the present invention relates to a method for
15 controlling an amplifier of a wireless receiver, the amplifier comprising a voltage amplifier module having a voltage gain switchable between a first voltage gain value and a second voltage gain value higher than the first gain value, and a resistance module having a resistance switchable between a first resistance value and a second resistance value higher than the first resistance value, an output of
20 the voltage amplifier module being connected to an input of the resistance module, the amplifier further comprising a set of switches configured to set the voltage gain value and the resistance value, the method comprising steps of:

- testing whether a risky intermodulation scenario, in which the wireless receiver may be desensitized, is detected,
- 25 - if no risky intermodulation scenario is detected, activating a nominal mode of operation by setting the voltage gain value to the second voltage gain value, and by setting the resistance value to the second resistance value, and
- if a risky intermodulation scenario is detected, activating a high linearity mode of operation by setting the voltage gain value to the first voltage gain value to
30 improve linearity of the amplifier, and by setting the resistance value to the first

resistance value to have a similar ratio of the voltage gain value to the resistance value as in the nominal mode of operation.

In some embodiments of the invention, the voltage amplifier module comprises a fixed gain part with a fixed voltage gain and a commutable gain part with a commutable voltage gain, the resistance module comprising a first resistance in parallel with a second resistance, the set of switches comprising a first switch disposed in parallel with the commutable gain part, a second switch disposed between the output of the commutable gain part and the input of the resistance module, and a third switch disposed between the input of the resistance module and the first resistance. The step of activating the nominal mode of operation then comprises opening the first and third switches and closing the second switch, and the step of activating the high linearity mode of operation comprises closing the first and third switches and opening the second switch.

When the set of switches further comprises a fourth switch disposed between the input of the resistance module and the second resistance, the step of activating the nominal mode of operation comprises closing the fourth switch, and the step of activating the high linearity mode of operation comprises opening the fourth switch.

In some embodiments of the invention, the voltage amplifier module comprises a first fixed resistance in parallel with a first commutable resistance, the resistance module comprising a second fixed resistance in parallel with a second commutable resistance, the set of switches comprising a first switch disposed between an input of the voltage amplifier module and the first commutable resistance, and a second switch disposed between the input of the resistance module and the second commutable resistance, the step of activating the nominal mode of operation comprising opening the first and second switches, the step of activating the high linearity mode of operation comprising closing the first and second switches.

The wireless receiver may be part of a RF transmission-reception system of a user equipment, the user equipment further comprising a radio engine. The

step of testing whether a risky intermodulation scenario is detected may then comprise:

- testing whether a risky RF band is selected, and, if a risky RF band is selected,
- testing whether the radio engine is activated.

5 The step of testing whether a risky intermodulation scenario is detected may further comprise testing whether the transmission signal power is above a predetermined threshold.

 A third aspect of the present invention relates to a computer program product comprising a computer readable medium, having thereon a computer
10 program comprising program instructions, the computer program being loadable into a data-processing unit and adapted to cause the data-processing unit to carry out the steps of the method according to the second aspect when the computer program is run by the data-processing unit.

 A fourth aspect of the present invention relates to a method for controlling
15 an amplifier of a wireless receiver, the method comprising steps of:

- testing whether a risky intermodulation scenario, in which the wireless receiver may be desensitized, is detected,
- if no risky intermodulation scenario is detected, activating a nominal mode of operation, and
- 20 - if a risky intermodulation scenario is detected, activating a high linearity mode of operation, the step of testing whether a risky intermodulation scenario is detected comprises:
 - testing whether a risky RF band is selected, and, if a risky RF band is selected,
 - testing whether the radio engine is activated.

25 In some embodiments, the step of testing whether a risky intermodulation scenario is detected further comprises testing whether the transmission signal power is above a predetermined threshold.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention is illustrated by way of example, and not by way of limitation, in the figures of the accompanying drawings, in which like reference numerals refer to similar elements and in which:

- 5 - Fig.1 is a schematic block diagram of a user equipment according to some embodiments of the invention;
- Fig.2 is a schematic block diagram of an amplifier of a wireless RF receiver according to some embodiments;
- Fig.3 is a schematic block diagram of an amplifier of a wireless RF receiver according to other embodiments;
- 10 - Fig.4 is a diagram of an amplifier implementation according to some embodiments; and
- Fig.5 is a flow chart showing steps of a method for controlling an amplifier according to embodiments of the invention.

15

DESCRIPTION OF EMBODIMENTS

Embodiments of the invention deal with the problem of enhancing the linearity of a RF amplifier of a wireless receiver while maintaining a constant overall gain.

20

Fig.1 shows a user equipment (UE) 1, for example a mobile device, comprising a cellular RF transmission-reception system 2 and a connectivity radio engine 3, for example a WiFi or a Bluetooth or a WiMAX radio engine.

The RF transmission-reception system 2 comprises an antenna 4, a duplexer 5, a RF receiver and a RF transmitter. The RF receiver comprises a Low Noise Amplifier (LNA) 6 and other processing blocks not represented. The RF transmitter comprises a Power Amplifier (PA) 7 and other processing blocks not represented. The antenna 4 is connected to the duplexer 5. The duplexer 5 is connected to the LNA 6 and to the PA 7.

25

The WiFi/Bluetooth/WiMAX radio engine 3 comprises an antenna 8 and a processing unit 9, connected to each other.

When a RF signal is received at the antenna 4, it is transmitted to the LNA 6, via the duplexer 5, as symbolized by arrow A1. The RF signal is
 5 processed by the LNA 6, and then transmitted by the LNA 6 to another block of the RF receiver for further processing, as symbolized by arrow A2.

When a RF signal has to be transmitted by the antenna 4, it is transmitted to the PA 7, as symbolized by arrow A3, processed by the PA 7, and then transmitted from the PA 7 to the antenna 4, via the duplexer 5, as symbolized by
 10 arrow A4. Such a transmission generates a transmission leakage signal symbolized by arrow A5.

In the same way, when a blocker signal is transmitted by the antenna 8, it generates a blocker leakage signal, as symbolized by arrow A6.

These leakage signals may desensitize the RF receiver when they
 15 create third order intermodulation product (IM_3) falling into the reception channel bandwidth. However, the blocker and transmission signal leakages can create IM_3 falling into the reception channel bandwidth only if the following condition between their frequencies is met:

$$\text{Equation 1: } F_{\text{Blocker}} = 2F_{TX} + F_{RX}$$

20

where F_{blocker} represents the blocker signal frequency, F_{TX} represents the transmission signal frequency and F_{RX} represents the reception signal frequency.

The scenarios that satisfy the condition stated in Equation 1 are called risky scenarios as they can desensitize the RF receiver. In the same way, the
 25 specific RF bands in which these scenarios occur are called risky bands.

A risky scenario may arise, for example, when a mobile terminal user connects his Bluetooth kit while being far away from the cellular base station with which a communication is established in a risky RF band. In this case, the power of the reception signal is low, the transmission signal is at maximum output power

and, as a consequence, the intermodulation between Bluetooth blocker leakage and own cellular transmission leakage may cut-off the communication.

Depending on the bandwidth of the modulations and their carrier frequencies, there is a mitigation factor M_f resulting from the intermodulation process that may reduce the IM_3 power, the latter can be calculated as follows:

$$\text{Equation 2: } IM_3 = (2P_{TX,leakage} + P_{blocker,leakage}) - 2IIP_3 - M_f$$

Where $P_{TX,leakage}$ is the transmission leakage signal power, $P_{blocker,leakage}$ is the blocker leakage signal power, and IIP_3 is the third order input intercept point of the RF receiver.

The IIP_3 performance needed when Wide-band Code Division Multiple Access (WCDMA) or Evolved Universal Terrestrial Radio Access (E-UTRA) must coexist with WiFi/Bluetooth/WiMAX may be estimated from Equation 2, by taking into account duplexer transmission-reception isolation, reception out-of-band attenuation and mitigation factor M_f value (coming from proper electrical simulations).

For example, the IIP_3 needed can be as high as +8dBm to keep RF receiver performance at nominal values when a risky scenario occurs. From this estimation we may deduce that at least 6dB of linearity enhancement is required from already highly-linear state-of-the-art LNAs.

An objective of the invention is to enhance linearity while maintaining the overall gain and power consumption of the LNA constant. This feature permits to obtain a constant Signal to Noise Ratio (SNR) needed for a proper demodulation of the communication channel.

On the contrary, with current state-of-the-art LNA, if the before-mentioned risky scenarios occur the SNR obtained at the Digital Base Band Integrated Circuit (DBB-IC) stage may be several dB below requirement, meaning that the communication channel is completely cut.

Fig.2 represents an amplifier 10 of a wireless RF receiver, for example a LNA, according to embodiments of the invention. The amplifier 10 comprises a voltage amplifier module 11 and a resistance module 12. The input of the voltage amplifier module 11 is configured to receive a RF signal from an antenna

connected to the RF receiver via a FEM. The output of the voltage amplifier module 11 is connected to the input of the resistance module 12. The output of the resistance module 12 is for example connected to a mixer of the RF receiver.

The voltage amplifier module 11 comprises a fixed gain part 13 with a
5 fixed gain G_0 and a commutable gain part 14 with a commutable gain β .

The resistance module 12 comprises a resistance R_L in parallel with a resistance βR_L .

A first switch 15 is disposed in parallel with the commutable gain part 14, that is to say between the input of the commutable gain part 14 and the output of
10 the commutable gain part 14. A second switch 16 is disposed between the output of the commutable gain part 14, that is to say the output of the voltage amplifier module 11, and the input of the resistance module 12. A third switch 17 is disposed between the input of the resistance module 12 and the resistance R_L . A fourth switch 18 is disposed between the input of the resistance module 12 and
15 the resistance βR_L .

The first and third switches 15, 17 are controlled to be open simultaneously and to be close simultaneously. The second and fourth switches 16, 18 are controlled to be open simultaneously and to be close simultaneously. The switches are further controlled such that the first and third switches 15, 17 are
20 open when the second and fourth switches 16, 18 are close, and the first and third switches 15, 17 are close when the second and fourth switches 16, 18 are open.

In variant, the switch 17 may be disposed between the resistance R_L and the output of the resistance module 12. In the same way, the switch 18 may be disposed between the resistance βR_L and the output of the resistance module 12.
25 The linearity of the amplifier can thus be further improved because the switches are at the output.

Fig.3 represents an amplifier 20 of a wireless RF receiver according to other embodiments of the invention. As described above, the amplifier 20 comprises a voltage amplifier module 21 and a resistance module 22.

The voltage amplifier module 21 comprises a fixed gain part 23 with a fixed gain G_0 and a commutable gain part 24 with a commutable gain βG_0 .

The resistance module 22 comprises a fixed resistance R_L in parallel with a commutable resistance αR_L .

5 A first switch 25 is disposed in parallel with the commutable gain part 24, that is to say between the input of the commutable gain part 24 and the output of the commutable gain part 24. A second switch 26 is disposed between the output of the commutable gain part 24 and the input of the resistance module 22. A third switch 27 is disposed between the input of the resistance module 22 and the
10 commutable resistance αR_L .

In this embodiment, there is no switch disposed between the input of the resistance module 22 and the fixed resistance R_L .

The first and third switches 25, 27 are controlled to be open simultaneously and to be close simultaneously. The switches are further
15 controlled such that the first and third switches 25, 27 are open when the second switch 26 is close, and the first and third switches 25, 27 are close when the second switch 26 is open.

In variant, the switch 27 may be disposed between the resistance αR_L and the output of the resistance module 22.

20 **Fig.4** represents an example of implementation of an amplifier 30 of a wireless RF receiver according to embodiments of the invention. As described above, the amplifier 30 comprises a voltage amplifier module 31 and a resistance module 32.

The resistance module 32 comprises a fixed resistance R_L in parallel with
25 a commutable resistance αR_L .

The voltage amplifier module 31 is a wide-band inductor-less resistive-feedback voltage amplifier. The voltage amplifier module 31 comprises a fixed resistance R_{Feed} in parallel with a commutable resistance δR_{Feed} . The voltage amplifier module 31 further comprises four transistors M_1 , M_2 , M_3 and M_4 .

30 A first switch 35 is disposed between the input of the voltage amplifier module 31 and the commutable resistance δR_{Feed} . A second switch 36 is

disposed between the input of the resistance module 32 and the commutable resistance αR_L .

The first and second switches 35, 36 are controlled to be open simultaneously and to be close simultaneously. The switches 35, 36 permit to
5 choose between two possible values for resistances R_L and R_{feed} , that is to say to choose between R_L and αR_L , and to choose between R_{feed} and δR_{Feed} . Both switches 35, 36 are commanded with the same control signal. Therefore whenever resistance R_L is changed, resistance R_{feed} is changed accordingly. In this way, input impedance matching is preserved from any change during High
10 Linearity Mode (HLM) operation, which is described below.

A RF signal received in the input of the voltage amplifier module 31, for example from an antenna connected to the RF receiver via a FEM, is injected into the gates of transistors M1 and M4 which works in parallel to amplify the input signal. Cascode transistors M2 and M3 insure high output impedance with respect
15 to resistance R_L to maximize voltage gain.

A feedback by means of resistance R_{feed} is used to achieve impedance matching at the amplifier input node.

The amplifier 30 may further comprise two capacitors C_{HPF} , which are used as DC blocks at the output and in the feedback paths to allow different DC
20 operating points.

In variant, the switch 36 may be disposed between the resistance αR_L and the output of the resistance module 32.

This linearization system is very well adapted to CMOS single-chip solutions for mobile platforms and to low-voltage operation. Only switches are
25 required to work properly and activate dynamically the dual-mode of operation. It ensures a high flexibility in the implementation of the linearization technique. It does not require any additional component thus saving a lot of area compared to other linearization techniques in the state-of-the-art.

As voltage gain is reduced and gain steadiness is insured by load
30 variation, the power consumption of the RF amplifier cannot increase in any way.

Amplifier 6, 10, 20, 30 of the RF receiver is configured to implement a method for controlling the amplifier, in particular for performing a dynamic

linearization, for example in the presence of the previously described risky scenarios. Referring to **Fig.5** we are describing below the method according to embodiment of the invention.

In step S1, the user equipment containing the amplifier 6, 10, 20, 30 is
5 powered up.

In step S2, the amplifier 6, 10, 20, 30 writes a first value, called value '0', in a HLM register.

In step S3, the amplifier 6, 10, 20, 30 tests whether any risky RF band is selected. If a risky RF band is selected, the method goes to step S4. If not the
10 method goes to step S3a.

In step S3a, the amplifier 6, 10, 20, 30 tests whether the HLM register contains a second value, called value '1'. If the HLM register contains value '1', the method goes to step S3b. If not, the method returns to step S3.

In step S3b, the amplifier 6, 10, 20, 30 deactivates HLM commands. The
15 amplifier 6, 10, 20, 30 is thus set in nominal mode.

To set the nominal mode in embodiment shown in Fig.2, the first and third switches 15, 17 are opened and the second and fourth switches 16, 18 are closed. In embodiment shown in Fig.3, the first and third switches 25, 27 are opened and the second switch 26 is closed. In embodiment shown in Fig.4, the
20 first and second switches 35, 36 are opened.

In a general way, to set the nominal mode, the commutable gain part is activated to increase the overall voltage gain. Accordingly, the resistance is set to increase the overall impedance value.

In the embodiment represented in Fig.3, the gain and load of the amplifier
25 20 in normal linearity mode may be calculated as follows:

$$\text{Equation 3: } G_m = \frac{\beta \times G_0^2}{R_{Load}} \quad G_v = \beta \times G_0^2 \quad R_{Load} = R_L$$

In step S3c, the amplifier 6, 10, 20, 30 writes value '0' in HLM register. Then the method returns to step S3.

In step S4, the amplifier 6, 10, 20, 30 tests whether any radio engine 3 is activated. If a radio engine 3 is activated, the method goes to step S5. If not, the method returns to step S3a.

5 In step S5, the amplifier 6, 10, 20, 30 tests whether the transmission signal power is above a predetermined threshold. If the transmission signal power is above the predetermined threshold, the method goes to step S6. If not, the method returns to step S3a.

Steps S3, S4 and S5 permit to detect a risky intermodulation scenario. These steps are performed by a detection circuit, which may be integrated in the
10 amplifier 6, 10, 20, 30 or connected to the amplifier.

In step S6, the amplifier 6, 10, 20, 30 tests whether the HLM register contains value '1'. If the HLM register contains value '1', the method returns to step S3. If not, the method goes to step S7.

15 In step S7, the amplifier 6, 10, 20, 30 activates HLM commands. The amplifier 6, 10, 20, 30 is thus set in high linearity mode.

To set the high linearity mode in embodiment shown in Fig.2, the first and third switches 15, 17 are closed and the second and fourth switches 16, 18 are opened. In embodiment shown in Fig.3, the first and third switches 25, 27 are closed and the second switch 26 is opened. In embodiment shown in Fig.4, the
20 first and second switches 35, 36 are closed.

In a general way, to set the high linearity mode, the commutable gain part of the voltage amplifier module of the amplifier is shut down to reduce the overall voltage gain and consequently the voltage swing V_{out} that limits the amplifier linearity.

25 Accordingly, the resistance value of the resistance module is set to reduce the overall impedance value and thus guarantee an unchanged transconductance gain that can be defined as the ratio of the voltage gain to the load resistance. The amplifier intrinsic linearity is enhanced as voltage gain has been reduced.

In the embodiment represented in Fig.3, the gain and load of the amplifier 20 in high linearity mode may be calculated as follows:

$$\text{Equation 4: } G_m = \frac{G_0}{R_{Load}} \quad G_v = G_0 \quad R_{Load} = \frac{\alpha}{(\alpha + 1)} \times R_L$$

5

In step S8, the amplifier 6, 10, 20, 30 writes value '1' in HLM register. Then the methods returns to step S3.

In some embodiments of the invention, the detection of the risky intermodulation scenarios may imply operation of communication between the RF transmitter and the RF receiver, between cellular Digital Base Band Integrated Circuit (DBB-IC) and Radio Frequency Integrated Circuit (RF-IC) of the wireless RF transmission-reception system and finally between connectivity and cellular radio engine.

A measurement receiver of the cellular RF-IC may be used to estimate the transmission signal power at the antenna 4. This information may be directly used to detect a risky scenario.

The cellular DBB-IC is capable of identifying the selected RF band. This information may also be directly used to detect a risky scenario.

An application processor of the mobile equipment is informed when the connectivity radio engine is powered-up and ready to work. This signal and its corresponding information may also be used to detect a risky scenario.

Embodiments of the invention enable a dynamic mode of operation for the amplifier 6, 10, 20, 30 by switching between nominal and HLM modes quickly and efficiently, based on the status of the three internal signals described above. As soon as one of them is off the amplifier switches back to its nominal mode of operation.

For example, when the mobile network requests a handover on another non-risky RF band during a communication or in idle mode, the DBB-IC signal permits to deactivate the HLM mode. Same procedure applies if connectivity radio engine is turned off or if own cellular transmitter signal is below maximum output power.

In this way, the mode of operation of the amplifier is modified only when needed. This improves the efficiency.

In addition, the amplifier according to some embodiments of the invention is built in a way that it exploits the ratio of circuit components making it insensitive
5 to device mismatch.

Another advantage is that the system part of the invention which relates to the scenario detection method uses only valid internal signals coming from the same RF-IC or a neighbor circuit inside the same mobile platform. Therefore, no specific processing is required and consequently there is no latency in deciding
10 which mode to use when needed.

While there has been illustrated and described what are presently considered to be the preferred embodiments of the present invention, it will be understood by those skilled in the art that various other modifications may be made, and equivalents may be substituted, without departing from the true scope
15 of the present invention. Additionally, many modifications may be made to adapt a particular situation to the teachings of the present invention without departing from the central inventive concept described herein. Furthermore, an embodiment of the present invention may not include all of the features described above. Therefore, it is intended that the present invention not be limited to the particular
20 embodiments disclosed, but that the invention include all embodiments falling within the scope of the invention as broadly defined above.

For example, the invention includes embodiments where a cellular engine interferes with a connectivity engine or with different types of engine.

Expressions such as "comprise", "include", "incorporate", "contain", "is" and "have" are to be construed in a non-exclusive manner when interpreting the
25 description and its associated claims, namely construed to allow for other items or components which are not explicitly defined also to be present. Reference to the singular is also to be construed in a reference to the plural and vice versa.

A person skilled in the art will readily appreciate that various parameters
30 disclosed in the description may be modified and that various embodiments disclosed may be combined without departing from the scope of the invention.

CLAIMS

1. Amplifier (6, 10, 20, 30) for a wireless receiver, the amplifier comprising a voltage amplifier module (11, 21, 31) having a voltage gain switchable between a first voltage gain value and a second voltage gain value higher than the first gain value, and a resistance module (12, 22) having a resistance switchable between a first resistance value and a second resistance value higher than the first resistance value, an output of the voltage amplifier module being connected to an input of the resistance module, the amplifier further comprising a set of switches (15, 16, 17, 18, 25, 26, 27, 35, 36) configured to set the voltage gain value and the resistance value, the amplifier (6, 10, 20, 30) being operable in:
- a nominal mode of operation in which the voltage gain value is set to the second voltage gain value, the resistance value being set to the second resistance value, and
 - a high linearity mode of operation in which the voltage gain value is set to the first voltage gain value to improve linearity of the amplifier, the resistance value being set to the first resistance value to have a similar ratio of the voltage gain value to the resistance value as in the nominal mode of operation.
2. Amplifier according to claim 1, comprising a detection circuit configured to detect a risky intermodulation scenario in which the wireless receiver may be desensitized, the high linearity mode of operation being activated when a risky intermodulation scenario is detected.
3. Amplifier according to claim 1, configured to be connected to a detection circuit configured to detect a risky intermodulation scenario

in which the wireless receiver may be desensitized, the high linearity mode of operation being activated when a risky intermodulation scenario is detected.

- 5 4. Amplifier (10, 20) according to one of claims 1 to 3, wherein the voltage amplifier module (11, 21) comprises a fixed gain part (13, 23) with a fixed voltage gain (G_0) and a commutable gain part (14, 24) with a commutable voltage gain (β , βG_0), the resistance module (12, 22) comprising a first resistance (R_L , αR_L) in parallel with a second resistance (βR_L , R_L), the set of switches comprising a first switch (15, 25) disposed in parallel with the commutable gain part (14, 24), a second switch (16, 26) disposed between the output of the commutable gain part (14, 24) and the input of the resistance module (12, 22), and a third switch (17, 27) disposed between the input of the resistance module (12, 22) and the first resistance (R_L , αR_L), the first and third switches (15, 17, 25, 27) being open in the nominal mode of operation and closed in the high linearity mode of operation, the second switch (16, 26) being closed in nominal mode of operation and open in high linearity mode of operation.
- 20 5. Amplifier (10) according to claim 4, wherein the set of switches comprises a fourth switch (18) disposed between the input of the resistance module (12) and the second resistance (βR_L), the fourth switch (18) being closed in nominal mode of operation and open in high linearity mode of operation.
- 25 6. Amplifier (30) according to one of claims 1 to 3, wherein the voltage amplifier module (31) comprises a first fixed resistance (R_{Feed}) in parallel with a first commutable resistance (δR_{Feed}), the resistance module (32) comprising a second fixed resistance (R_L) in parallel with
- 30

5 a second commutable resistance (αR_L), the set of switches comprising a first switch (35) disposed between an input of the voltage amplifier module (31) and the first commutable resistance (δR_{Feed}), and a second switch (36) disposed between the input of the resistance module (32) and the second commutable resistance (αR_L), the first and second switches (35, 36) being open in nominal mode of operation and closed in high linearity mode of operation.

- 10 7. Method for controlling an amplifier (6, 10, 20, 30) of a wireless receiver, the amplifier comprising a voltage amplifier module (11, 21, 31) having a voltage gain switchable between a first voltage gain value and a second voltage gain value higher than the first gain value, and a resistance module (12, 22, 32) having a resistance switchable between a first resistance value and a second resistance value higher than the first resistance value, an output of the voltage amplifier module being connected to an input of the resistance module, the amplifier further comprising a set of switches (15, 16, 17, 18, 25, 26, 27, 35, 36) configured to set the voltage gain value and the resistance value, the method comprising steps of:
- 15
- 20 - testing whether a risky intermodulation scenario, in which the wireless receiver may be desensitized, is detected,
- 25 - if no risky intermodulation scenario is detected, activating a nominal mode of operation by setting the voltage gain value to the second voltage gain value, and by setting the resistance value to the second resistance value, and
- 30 - if a risky intermodulation scenario is detected, activating a high linearity mode of operation by setting the voltage gain value to the first voltage gain value to improve linearity of the amplifier, and by setting the resistance value to the first resistance value to have a similar ratio of the voltage gain value to the resistance value as in the nominal mode of operation.

- 5 8. Method according to claim 7, wherein the voltage amplifier module (11, 21) comprises a fixed gain part (13, 23) with a fixed voltage gain (G_0) and a commutable gain part (14, 24) with a commutable voltage gain (β , βG_0), the resistance module (12, 22) comprising a first resistance (R_L , αR_L) in parallel with a second resistance (βR_L , R_L), the set of switches comprising a first switch (15, 25) disposed in parallel with the commutable gain part (14, 24), a second switch (16, 26) disposed between the output of the commutable gain part (14, 24) and the input of the resistance module (12, 22), and a third switch (17, 27) disposed between the input of the resistance module (12, 22) and the first resistance (R_L , αR_L), the step of activating the nominal mode of operation comprising opening the first and third switches (15, 17, 25, 27) and closing the second switch (16, 26), the step of activating the high linearity mode of operation comprising closing the first and third switches (15, 17, 25, 27) and opening the second switch (16, 26).
- 10 9. Method according to claim 8, wherein the set of switches comprises a fourth switch (18) disposed between the input of the resistance module (12) and the second resistance (βR_L), the step of activating the nominal mode of operation comprising closing the fourth switch (18), the step of activating the high linearity mode of operation comprising opening the fourth switch (18).
- 15 20 10. Method according to claim 7, wherein the voltage amplifier module (31) comprises a first fixed resistance (R_{Feed}) in parallel with a first commutable resistance (δR_{Feed}), the resistance module (32) comprising a second fixed resistance (R_L) in parallel with a second commutable resistance (αR_L), the set of switches comprising a first switch (35) disposed between an input of the voltage amplifier module (31) and the first commutable resistance (δR_{Feed}), and a second switch
- 25 30

(36) disposed between the input of the resistance module (32) and the second commutable resistance (αR_L), the step of activating the nominal mode of operation comprising opening the first and second switches (35, 36), the step of activating the high linearity mode of operation comprising closing the first and second switches (35, 36).

11. Method according to one of the claims 7 to 10, wherein the wireless receiver is part of a RF transmission-reception system of a user equipment, the user equipment further comprising a radio engine, the step of testing whether a risky intermodulation scenario is detected comprises:

- testing whether a risky RF band is selected, and, if a risky RF band is selected,
- testing whether the radio engine is activated.

12. Method according to claim 11, wherein the step of testing whether a risky intermodulation scenario is detected further comprises testing whether the transmission signal power is above a predetermined threshold.

13. Computer program product comprising a computer readable medium, having thereon a computer program comprising program instructions, the computer program being loadable into a data-processing unit and adapted to cause the data-processing unit to carry out the steps of any of claims 7 to 12 when the computer program is run by the data-processing unit.

14. Method for controlling an amplifier (6, 10, 20, 30) of a wireless receiver, the method comprising steps of:

- testing whether a risky intermodulation scenario, in which the wireless receiver may be desensitized, is detected,
 - if no risky intermodulation scenario is detected, activating a nominal mode of operation, and
 - 5 - if a risky intermodulation scenario is detected, activating a high linearity mode of operation, the step of testing whether a risky intermodulation scenario is detected comprises:
 - testing whether a risky RF band is selected, and, if a risky RF band is selected,
 - 10 - testing whether the radio engine is activated.
15. Method according to claim 14, wherein the step of testing whether a risky intermodulation scenario is detected further comprises testing whether the transmission signal power is above a predetermined threshold.
- 15

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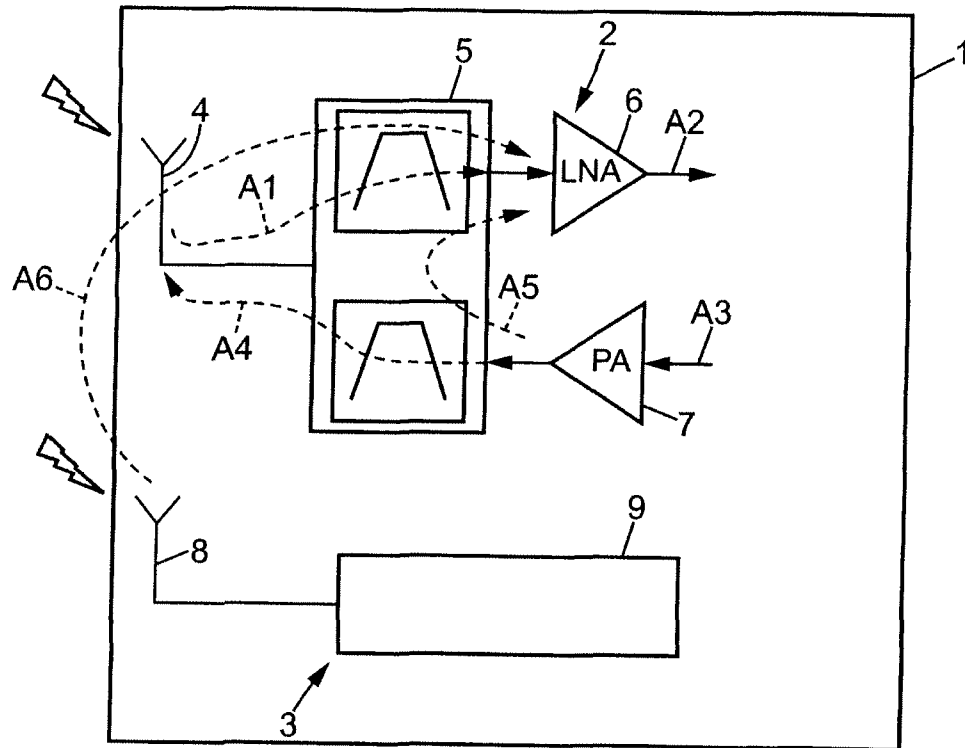


FIG. 1

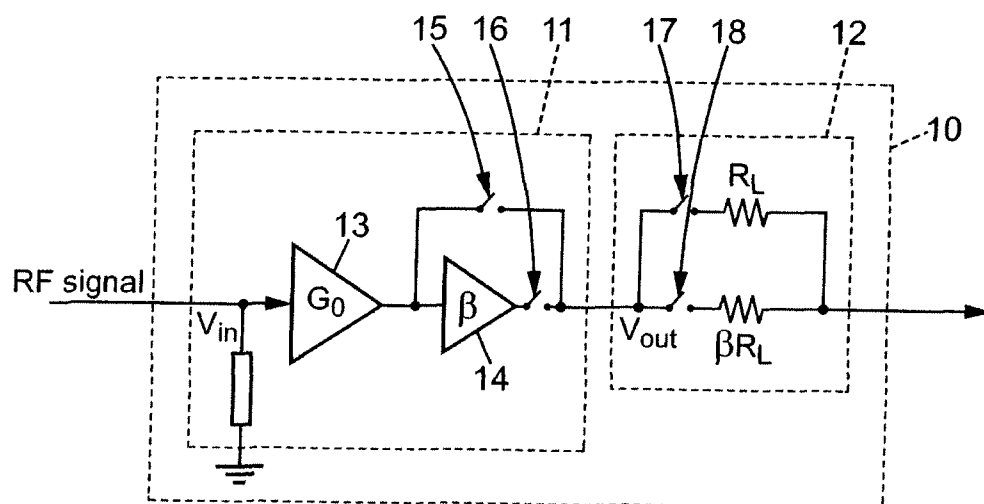


FIG. 2

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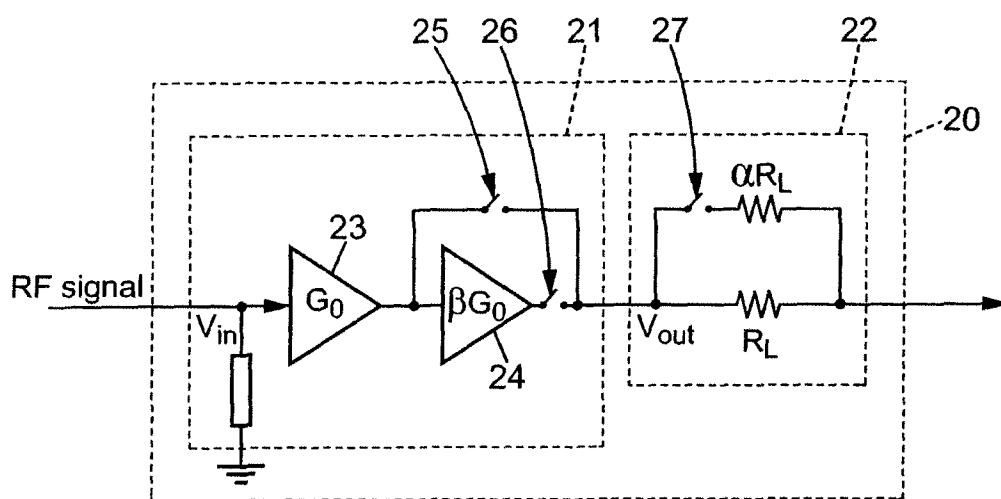


FIG. 3

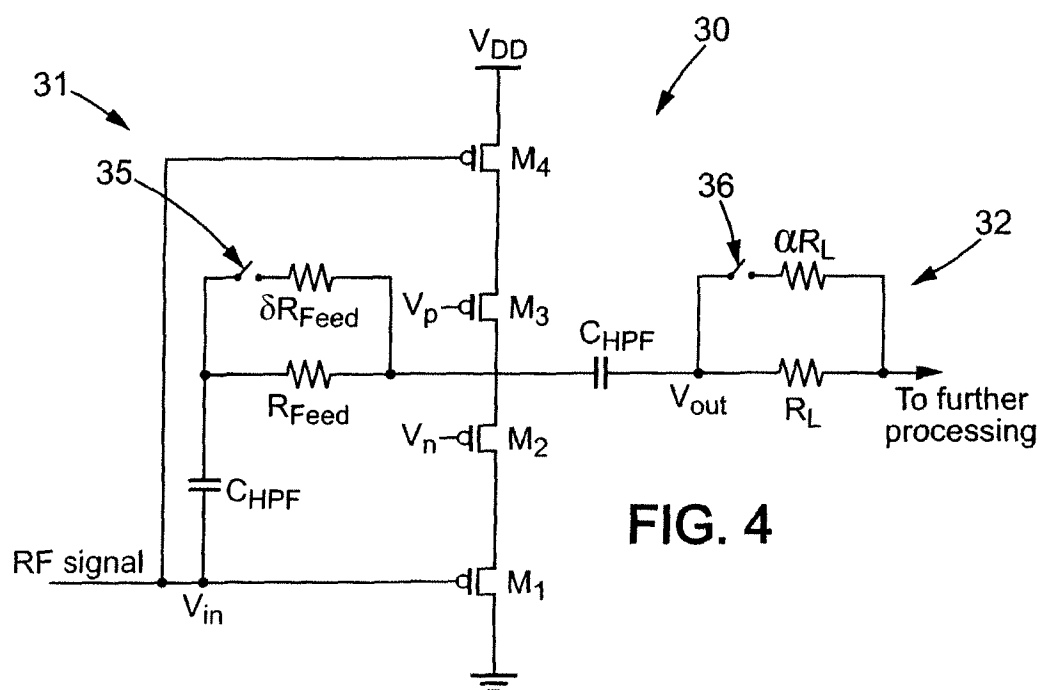
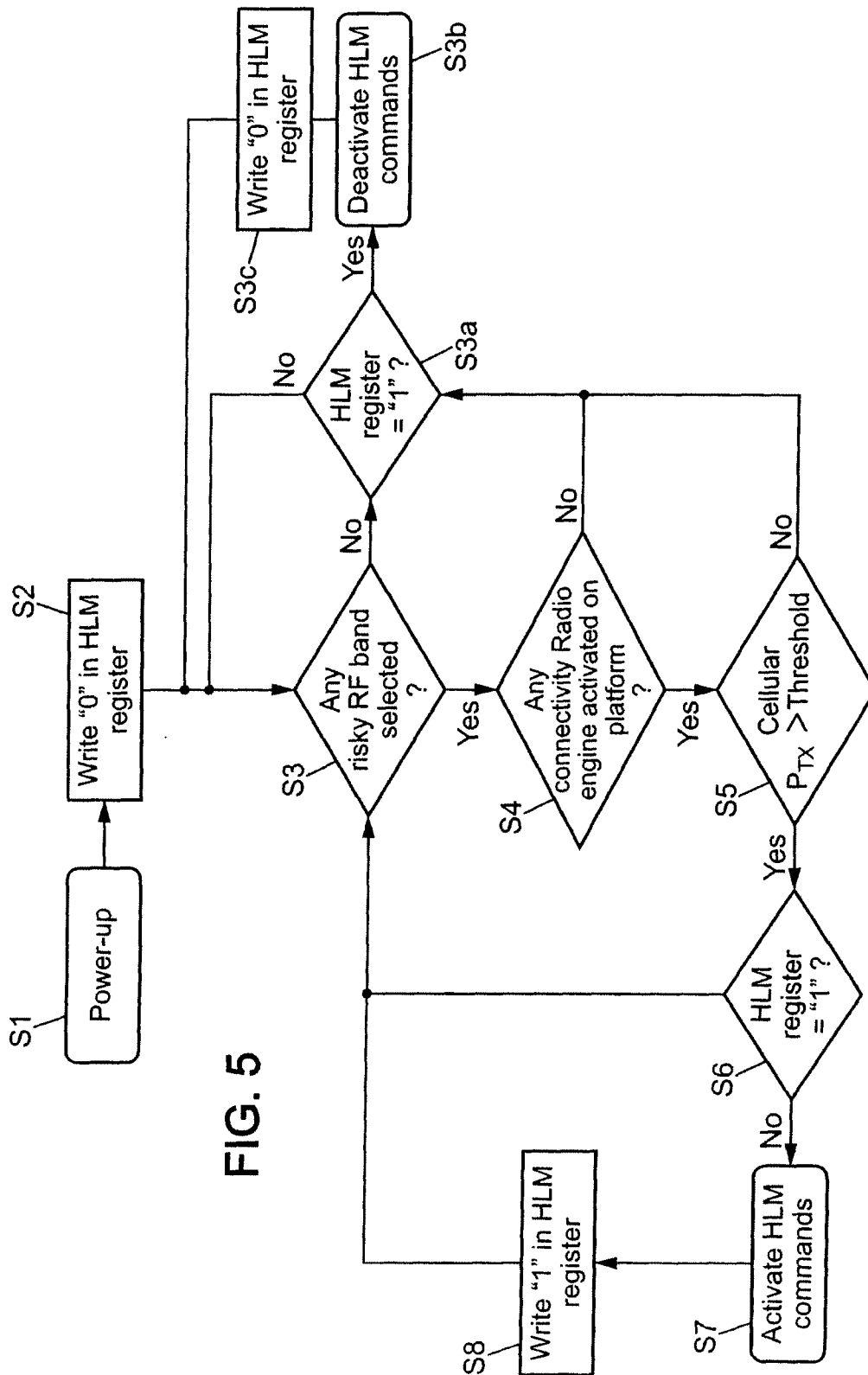


FIG. 4

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INTERNATIONAL SEARCH REPORT

WO 2012/107452

International application No

PCT/EPCT/EP2012/052063

A. CLASSIFICATION OF SUBJECT MATTER
 INV. H03G1/00 H03G3/30 H04B1/10
 ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

H03G H04B H03F G01S H04L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 2010/014806 A1 (QUALCOMM INC [US]; WEISSMAN HAIM [IL]; JANOSEVIC ZORAN [GB]; BRILLANT) 4 February 2010 (2010-02-04) abstract; figures 3,9,9a,9b,9c,12 paragraphs [0001] - [0006], [0027] - [0030], [0032], [0046] - [0051] -----	1-13
A	JP 2008 028908 A (JAPAN RADIO CO LTD) 7 February 2008 (2008-02-07) abstract; figures 1-4 paragraphs [0001], [0020] - [0022], [0029] - [0038] -----	1-13
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Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier application or patent but published on or after the international filing date

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"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

27 June 2012

Date of mailing of the international search report

05/07/2012

Name and mailing address of the ISA/

European Patent Office, P.B. 5818 Patentlaan 2
 NL - 2280 HV Rijswijk
 Tel. (+31-70) 340-2040,
 Fax: (+31-70) 340-3016

Authorized officer

Wichert, Beate

INTERNATIONAL SEARCH REPORT

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PCT/EPCT/EP2012/052063

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2005/075077 A1 (MACH RICHARD [US] ET AL) 7 April 2005 (2005-04-07) abstract; claim 8; figures 1,2 paragraphs [0005], [0013], [0023] - [0038] -----	14,15
X	US 2004/152429 A1 (HAUB DAVID [US] ET AL) 5 August 2004 (2004-08-05) abstract; figures 1, 2 paragraphs [0010], [0019] - [0027], [0030], [0032] -----	14,15
X	WO 2007/014982 A1 (NOKIA CORP [FI]; KIUKKONEN NIKO [FI]; PIIPPONEN ANTTI [FI]) 8 February 2007 (2007-02-08) abstract; figures 3-5	14
A	paragraphs [0006], [0007], [0027], [0031] - [0034] -----	15

INTERNATIONAL SEARCH REPORT

International application No.
PCT/EP2012/052063

Box No. II Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☐ Claims Nos.:
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. ☐ Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box No. III Observations where unity of invention is lacking (Continuation of item 3 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

see additional sheet

1. ☒ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fees, this Authority did not invite payment of additional fees.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest and, where applicable, the payment of a protest fee.
- ☐ The additional search fees were accompanied by the applicant's protest but the applicable protest fee was not paid within the time limit specified in the invitation.
- ☒ No protest accompanied the payment of additional search fees.

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

This International Searching Authority found multiple (groups of) inventions in this international application, as follows:

1. claims: 1-13

Invention 1 as defined in claim 1 refers to an amplifier comprising a voltage amplifier module followed by a resistance module whereby amplifier and resistance module each can be switched between two values to provide a nominal mode and a high linearity mode with the ratio of gain value of the amplifier module to resistance value of the resistance module being similar for both modes.

2. claims: 14, 15

Invention 2 as defined in claim 14 refers to a method for controlling an amplifier comprising testing whether a risky intermodulation scenario is detected, and if yes, activating a high linearity mode of operation, otherwise a nominal mode.

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/EP2012/052063

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