REducing Leukocyte interference in non-competitive immunoassays

Abstract: The invention is directed to methods and devices for reducing interference from leukocytes in an analyte immunoassay, and in particular in non-competitive immunoassays. In one embodiment, the invention is to a method comprising the steps of (a) amending a biological sample such as a whole blood sample with sacrificial beads; and (b) performing a non-competitive immunoassay on the amended sample to determine the concentration of said analyte in said sample. Preferably, the sample is amended with IgG-coated sacrificial beads.
REDUCING LEUKOCYTE INTERFERENCE IN NON-COMPETITIVE IMMUNOASSAYS

CROSS REFERENCE TO RELATED APPLICATION

The present application claims priority to U.S. Patent Application No. 12/620,179, filed on November 17, 2009, which is incorporated herein by reference.

FIELD OF THE INVENTION

The present invention relates to reducing or eliminating interference from buffy coat components, notably leukocytes, in devices and methods for determining the presence or concentration of an analyte in a blood sample by non-competitive immunoassay. In particular, the invention relates to reducing or eliminating leukocyte immunosensor interference by amending a blood sample with opsonized sacrificial beads and similarly opsonized elements.

BACKGROUND OF THE INVENTION

A multitude of laboratory immunoassay tests for analytes of interest are performed on biological samples for diagnosis, screening, disease staging, forensic analysis, pregnancy testing, drug testing, and other reasons. While a few qualitative tests, such as pregnancy tests, have been reduced to simple kits for the patient's home use, the majority of quantitative tests still require the expertise of trained technicians in a laboratory setting using sophisticated instruments. Laboratory testing increases the cost of analysis and delays the results. In many circumstances, delay can be detrimental to a patient's condition or prognosis, such as for example the analysis of markers indicating myocardial infarction and heart failure. In these and similar critical situations, it is advantageous to perform such analyses at the point-of-care, accurately, inexpensively, and with a minimum of delay.

Many types of immunoassay devices and processes have been described. One disposable sensing device for successfully measuring analytes in a sample of blood is
disclosed by Lauks in U.S. Pat. No. 5,096,669. Other devices are disclosed by Davis et al. in U.S. Pat. Nos. 5,628,961 and 5,447,440 for a clotting time. These devices employ a reading apparatus and a cartridge that fits into the reading apparatus for the purpose of measuring analyte concentrations and viscosity changes in a sample of blood as a function of time. U.S. Pat. Nos. 5,096,669; 5,628,961 and 5,447,440 are hereby incorporated herein by reference in their entirities. US 20060160164 describes an immunoassay device with an immuno-reference electrode, US 20050054078 describes an immunoassay device with improved sample closure, US 20040018577 describes a multiple hybrid immunoassay, and US 20030170881 (issued as US 7,419,821) describes an apparatus and methods for analyte measurement and immunoassay, all of which are jointly owned and are incorporated here by reference.

Non-competitive two-site immunoassays, also called sandwich-type immunoassays, are often employed for determining analyte concentration in biological test samples, and are used, for example, in the point-of-care analyte detection system developed by Abbott Point of Care Inc. as the i-Stat® system. In a typical two-site enzyme-linked immunosorbent assay (ELISA), one antibody is bound to a solid support to form an immobilized or capture antibody and a second antibody is conjugated or bound to a signal-generating reagent such as an enzyme to form a signal or labeled antibody. Upon reaction with a sample containing the analyte to be measured, the analyte becomes "sandwiched" between the immobilized antibody and the signal antibody. After washing away the sample and any non-specifically bound reagents, the amount of signal antibody remaining on the solid support is measured and should be proportional to the amount of analyte in the sample.

Electrochemical detection, in which binding of an analyte directly or indirectly causes a change in the activity of an electroactive species adjacent to an electrode, has also been applied to immunoassays. For a review of electrochemical immunoassays, see Laurell et al., Methods in Enzymology, vol. 73, "Electroimmunoassay", Academic Press, New York, 339, 340, 346-348 (1981).
In an electrochemical immnosensor, the binding of an analyte to its cognate antibody produces a change in the activity of an electroactive species at an electrode that is poised at a suitable electrochemical potential to cause oxidation or reduction of the electroactive species. There are many arrangements for meeting these conditions. For example, electroactive species may be attached directly to an analyte, or the antibody may be covalently attached to an enzyme that either produces an electroactive species from an electroinactive substrate or destroys an electroactive substrate. See, M. J. Green (1987) Philos. Trans. R. Soc. Lond. B. Biol. Sci. 316:135-142, for a review of electrochemical immnosensors.

The concept of differential amperometric measurement is well known in the electrochemical art. See, for example, jointly owned Cozzette, U.S. Pat. No. 5,12,455, incorporated herein by reference in its entirety. In addition, a version of a differential amperometric sensor combination is disclosed in jointly owned Cozzette, U.S. Pat. No. 5,063,081. This patent also discloses the use of permselective layers for electrochemical sensors and the use of film-forming latexes for immobilization of bioactive molecules, incorporated here by reference. The use of poly(vinyl alcohol) (PVA) in sensor manufacture is described in U.S. Pat. No. 6,030,827 incorporated here by reference. Vikholm (U.S. 2003/0059954A1) teaches antibodies directly attached to a surface with a biomolecule repellant coating, e.g. PVA, the surface in the gaps between antibodies, and Johansson (U.S. Pat. No. 5,656,504) teaches a solid phase, e.g. PVA, with antibodies immobilized thereon. U.S. Pat. Nos. 6,030,827 and 6,379,883 teach methods for patterning poly(vinylalcohol) layers and are incorporated by reference in their entirety.

As is well known in the art immunoassays are susceptible to various forms of interferences. Jointly owned pending US application 12/41 1,325, for example, addresses ameliorating interferences from heterophile antibodies by the inclusion IgM into an IgG reagent cocktail. The '325 application is incorporated herein by reference in its entirety.

As immunoassay technology has increasingly been adapted to enter the point of care testing market, the use of whole blood as the test medium has increased relative to plasma and serum, which are generally used in central laboratory testing. This obviously
means that erythrocytes, and buffy coat components, e.g., leukocytes and platelets, are present in the assay medium. It has been found that in certain assays, various assay components, e.g., beads and electrode surfaces, can effectively be opsonized with respect to leukocytes. Note that with respect to an electrode surface, Hill et al. (FEBS 191, 257-263, 1985) opsonized a microvoltammetric electrode with human IgG for the purpose of observing the respiratory burst of a human neutrophil based on electrochemical detection of the superoxide ion.

Previously mentioned US 20060160164 (the ‘164 application) discusses electrochemical immunoassays and bias between whole-blood and plasma and that immunoassays for markers such as troponin and the like are generally measured and reported as plasma or serum values. It mentions that when these immunoassays are used for analysis of whole-blood, either a correction factor or a means for eliminating the bias needs to be employed. It states that certain aspects of this bias can be eliminated, including a bias in whole-blood electrochemical immunoassays associated with components of the buffy coat (which consists of white blood cells and platelets), and also a bias associated with hematocrit variations between samples. Those skilled in the art recognize that the buffy coat is a layer of leukocytes and platelets that forms above the erythrocytes when blood is centrifuged.

In the ‘164 application it was further observed that white cell (or leukocyte) interference occurs on immunoassays having beads coated with an analyte antibody, e.g., troponin antibody. Control experiments showed that this positive bias is absent in plasma samples and in blood samples where the buffy coat has been removed. Thus, it appears that leukocytes are able to stick to the immunoassay and promote non-specific binding of the enzyme-labeled antibodies, which remain bound even after a washing step. In this disclosure it was shown that this bias could be partially eliminated by adding a small amount of an antibody to human serum albumin during bead preparation. Consequently, when a sample contacts the modified beads, albumin from the sample rapidly coats the beads and once they are coated with a layer of native albumin the leukocytes should not recognize the beads as an opsonized surface.
The ‘164 application also described another solution to the leukocyte interference problem where this bias is eliminated by increasing the salt concentration of the blood sample from a normal sodium ion concentration of about 140 mM to above about 200 mM, preferably to about 230 mM. It is believed that the mechanism that accounts for reduced interference may be that the salt causes osmotic shrinkage of the leukocytes. This interpretation is consistent with the leukocytes' impaired ability to interact with the disclosed immunosensor.

However, it is apparent that the need remains for improved processes for ameliorating additional subtle effects of leukocyte activity in immunoassays in at least the following areas: (i) immunosensor interference, most notably in the context of point-of-care testing, (ii) electrochemical immunoassays, (iii) the use of an immunosensor in conjunction with an immuno-reference sensor, (iv) whole blood immunoassays, (v) single-use cartridge based immunoassays, (vi) non-sequential immunoassays with only a single wash step, and (vii) dry reagent coatings.

**SUMMARY OF THE INVENTION**

The invention is directed to kits, cartridges and methods for reducing or eliminating leukocyte interference, particularly in non-competitive immunoassays. According to the various embodiments of the invention, leukocyte interference may be reduced or eliminated by employing sacrificial beads opsonized for leukocytes. The leukocytes preferentially phagocytose the sacrificial beads thereby reducing leukocyte interference.

In one embodiment, for example, the invention is to a kit for performing a sandwich immunoassay for an analyte suspected of being present in a blood sample, comprising sacrificial beads opsonized to leukocytes, an immobilized first antibody to the analyte and a labeled second antibody to the analyte.

In another embodiment, the invention is to a cartridge for performing a sandwich immunoassay for an analyte suspected of being present in a blood sample, the cartridge comprising: (a) a sample inlet for receiving the blood sample; (b) a metering chamber for
metering the blood sample to form a metered sample; (c) one or more dry reagent coating layers comprising sacrificial beads opsonized to leukocytes and a labeled antibody to the analyte; (d) an electrode comprising an immobilized antibody to the analyte; and (e) one or more pumping elements for moving a metered sample, fluidized sacrificial beads, and the labeled antibody to the electrode.

In another embodiment, the invention is to a method of performing a sandwich immunoassay for an analyte suspected of being present in a blood sample comprising: (a) exposing a blood sample suspected of containing the analyte to sacrificial beads opsonized to leukocytes; an immobilized first antibody to the analyte; and a labeled second antibody to form a complex comprising said first antibody, said analyte and said second antibody; and (b) determining the amount of complexed label. In one aspect, the blood sample is mixed with the sacrificial beads, then mixed with the immobilized first antibody, and then mixed with the labeled second antibody. In another aspect, the blood sample is mixed with the sacrificial beads, the immobilized first antibody, and the labeled second antibody at substantially the same time. In another aspect, the blood sample is mixed with the immobilized first antibody and the labeled second antibody at substantially the same time. In still another aspect, the blood sample is mixed with the sacrificial beads and the labeled second antibody at substantially the same time, and before the blood sample is mixed with the immobilized first antibody.

In another embodiment, the invention is to a method of substantially ameliorating white blood cell accumulation on an analyte immunosensor comprising antibody-coated beads to the analyte immobilized on an electrode comprising, the method comprising the steps of: (a) mixing a sample suspected of containing an analyte with sacrificial beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads, and (b) contacting the amended sample with an immunosensor.

In another embodiment, the invention is to a method of performing an immunoassay for an analyte suspected of being present in a blood sample comprising: (a) mixing a blood sample suspected of containing an analyte with an excess of sacrificial
beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads; (b) contacting the amended sample with an immunosensor comprising antibody-coated beads to the analyte immobilized on an electrode forming a sandwich between said antibody-coated bead, said analyte and a second labeled antibody; (c) washing said blood sample from said immunosensor; and (d) determining the amount of said sandwiched label with said immunosensor and relating the amount of said label to the concentration of the analyte in the sample.

In another embodiment, the invention is to a method of performing a sandwich immunoassay for an analyte suspected of being present in a blood sample, comprising: (a) mixing a blood sample suspected of containing an analyte with an excess of opsonized sacrificial beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads; (b) contacting the amended sample with antibody-coated beads to the analyte under conditions effective to form a sandwich between said antibody-coated bead, said analyte and a second labeled antibody; (c) washing said blood sample from said antibody-coated beads; and (d) determining the amount of said sandwiched label and relating the amount of said label to the concentration of the analyte in the sample.

A test cartridge for performing an immunoassay for an analyte suspected of being present in a blood sample, the test cartridge comprising an immunosensor in a conduit, said immunosensor having an immobilized first antibody to the analyte, and said conduit having a dry reagent coating disposed therein, the dry reagent coating comprising sacrificial beads and a second labeled antibody to said analyte and being configured to dissolve into said blood sample.

In the above embodiments, the blood sample preferably is a whole blood sample, optionally amended with an anticoagulant. The analyte preferably is selected from the group consisting of BNP, proBNP, NTproBNP, cTnl, TnT, HCG, TSH, PSA, D-dimer, CRP, myoglobin, NGAL, CKMB and myeloperoxidase. The sacrificial beads, for example, may comprise substrate beads coated with non-human IgG or fragments thereof. The substrate beads may be formed of a material selected from the group
consisting of polystyrene, polyacrylic acid, and dextran. In some other aspects, the sacrificial beads comprise substrate beads coated with a material or fragment thereof selected from the group consisting of a protein, a bacterium, a virus and a xenobiotic. In another embodiment, the sacrificial beads are stabilized bacterium or bacterial spores.

The sacrificial beads preferably have an average particle size of from 0.01 µm to 20 µm, e.g., from 0.1 µm to 5 µm, and ideally are present in an amount sufficient to provide a dissolved sacrificial bead concentration of at least 10^4 beads per microliter of sample. The sacrificial beads and the second labeled antibody may be in one or more dissolvable dry reagent coatings, which, for example, may be disposed within the metering chamber.

The immobilized first antibody that is employed preferably is attached to a sensor selected from the group consisting of an amperometric electrode, a potentiometric electrode, a conductimetric electrode, an optical wave guide, a surface plasmon resonance sensor, an acoustic wave sensor and a piezoelectric sensor. For example, the immobilized first antibody may be attached to an assay bead, and the assay bead may be attached to an amperometric electrode.

The labeled second antibody optionally is labeled with a label selected from the group consisting of a radiolabel, an enzyme, a chromophore, a fluorophore and a chemiluminescent species. Where the labeled second antibody is labeled with an enzyme, the enzyme preferably is selected from the group consisting of alkaline phosphatase, glucosidase, diaphorase, horse radish peroxidase and glucose oxidase.

**BRIEF DESCRIPTION OF THE DRAWINGS**

These and other objectives, features and advantages of the present invention are described in the following detailed description of the specific embodiments and are illustrated in the following Figures, in which:

- FIG. 1 is an isometric top view of an immunosensor cartridge cover;
- FIG. 2 is an isometric bottom view of an immunosensor cartridge cover;
FIG. 3 is a top view of the layout of a tape gasket for an immunosensor cartridge;

FIG. 4 is an isometric top view of an immunosensor cartridge base;

FIG. 5 is a schematic view of the layout of an immunosensor cartridge;

FIG. 6 is a schematic view of the fluid and air paths within an immunosensor cartridge, including sites for amending fluids with dry reagents;

FIG. 7 illustrates the principle of operation of an electrochemical immunosensor with the inclusion of IgM;

FIG. 8 is a side view of the construction of an electrochemical immunosensor with antibody-labeled particles not drawn to scale;

FIG. 9 is a top view of the mask design for the conductimetric and immunosensor electrodes for an immunosensor cartridge;

FIG. 10 illustrates the principle of operation of an electrochemical immunosensor with the inclusion of sacrificial beads opsonized for leukocytes;

FIG 11(a) shows an unexpected waveform for a BNP cartridge with a positively sloping output signal, and FIG 11(b) shows an unexpected waveform for a BNP cartridge with a negatively sloping output signal. FIG 11(c) shows a normal response which has a near-zero slope for a low analyte concentrations, and FIG 11(d) shows that negative slopes are expected only at high analyte concentrations where the measurement can become substrate-limited rather than enzyme limited.

FIG 12 shows the effect of oxidative electrode pulsing during the wash step on (a) a normal sample, and (b) an aberrant buffy sample.

FIG. 13 is a schematic illustration of enzymatic regeneration of an electroactive species;

FIG. 14 illustrates segment forming means;
FIG. 15 is a top view of the preferred embodiment of an immunosensor cartridge;

FIG. 16 is a schematic view of the fluidics of a preferred embodiment of an immunosensor cartridge;

FIG. 17(a) and (b) show micrographs of immunosensors after assay of BNP in a high buffy sample in (a) absence and (b) presence of sacrificial beads in the sample;

FIG. 18 illustrates the cartridge device with a slidable sealing element for closing the sample entry port in the closed position;

FIG. 19 illustrates the cartridge device with a slidable sealing element for closing the sample entry port in the open position;

FIG. 20 illustrates the signal generating reactions occurring during the analysis: (a) cleavage of substrate by alkaline phosphatase to generate electroactive p-aminophenol and (b) oxidation of p-aminophenol;

FIG. 21 shows graphical data for the effect on immunosensor slope in high buffy (left panel) and normal whole blood (right panel) samples with (sublots 2 and 3) and without (sublot 1) sacrificial microparticles incorporated in the reagent;

FIG. 22(a) and (b) show analyzer waveforms for the associated immunosensor micrographs in FIG 17(a) and (b); and

FIG. 23 illustrates the effect of poor washing (inability to replace sample fluid within sensor structure with analysis fluid) on amperometric waveforms.

DETAILED DESCRIPTION OF THE INVENTION

The present invention relates to enhanced ways of reducing or eliminating interference caused by the presence of leukocytes. In preferred embodiments, the present invention may be employed in one or more of the following areas: (i) immunosensors, most notably in the context of point-of-care testing, (ii) electrochemical immunoassays, (iii) the use of an immunosensor in conjunction with an immuno-reference sensor, (iv)
whole blood immunoassays, (v) single-use cartridge based immunoassays, (vi) non-sequential immunoassays with only a single wash step, and (vii) dry reagent coatings. Notably, while US 20060160164, discussed above, addresses certain interferences associated with leukocytes based on the addition of an anti-human serum albumin antibody coating on an immunosensor and the addition of salts to the assay medium, the present specification discloses additional sources of bias associated with leukocytes and provides a novel solution for reducing same. As will be appreciated by those skilled in the art, the general concept disclosed here is applicable to many immunoassay methods and platforms.

The present invention permits rapid in situ determinations of analytes using a cartridge having an array of analyte sensors and means for sequentially presenting an amended sample to an immunosensor or analyte array. In preferred embodiments, the invention is employed in cartridges that are designed to be operated with a reading device, such as that disclosed in U.S. Pat. No. 5,096,669 to Lauks et al., issued Mar. 17, 1992, or U.S. Pat. No. 7,419,821, issued Sept. 2, 2008, both of which are incorporated by reference herein in their entireties. The invention is best understood in this context. Consequently, a suitable device and method of operation for a point-of-care immunoassay system is first described, followed by how the system may be best adapted to further reduce or eliminate leukocyte interference in whole blood immunoassays.

The sacrificial beads for use with the present invention may be employed in either heterogeneous or a homogeneous bead-based assays, as well as in non-competitive (sandwich) immunoassays or competitive immunoassays. In a preferred embodiment, the invention is employed in a heterogeneous electrochemical immunoassay based on the formation of a sandwich at or near the electrode surface. In another embodiment, the invention is employed in a homogeneous sandwich immunoassay, that is, within the fluid medium. Thus, in this context, the terms "heterogeneous" and "homogeneous" refer to the capture step. Hence, for homogeneous assays, the capture step occurs in the fluid medium while in a heterogeneous assays, the capture step occurs on a macroscopic surface, e.g., sensor surface (in either a competitive or non-competitive manner). In each of these examples, the immobilized assay beads will be susceptible to attack by
leukocytes when the assay is performed in a blood sample. In competitive and non-competitive assays, this effect can be reduced by the addition of sacrificial beads, preferably in excess, that are opsonized to leukocytes.

In one embodiment, the invention relates to cartridges and methods for processing liquid samples to determine the presence or amount of an analyte in the sample. The cartridges preferably contain a metering means, which permits an unmetered volume of sample to be introduced, from which a metered amount is processed by the cartridge and its associated reading apparatus. Thus, the physician or operator is relieved of manually measuring the volume of the sample prior to measurement saving time, effort, and increasing accuracy and reproducibility. The metering means, in one embodiment, comprises an elongated sample chamber bounded by a capillary stop and having along its length an air entry point. Air pressure exerted at the air entry point drives a metered volume of the sample past the capillary stop. The metered volume is predetermined by the volume of the sample chamber between the air entry point and the capillary stop.

The cartridge may have a closure device for sealing the sample port in an air-tight manner. This closure device is preferably slidable with respect to the body of the cartridge and provides a shearing action that displaces any excess sample located in the region of the port, reliably sealing a portion of the sample in the holding chamber between the entry port and the capillary stop. See, for example, Published US patent application US2005/0054078 Al, the entirety of which is incorporated herein by reference. The cartridge may be sealed, for example, by slidably moving a sealing element over the surface of the cartridge in a manner that displaces excess fluid sample away from the sample orifice, seals a volume of the fluid sample within the internal fluid sample holding chamber, and inhibits fluid sample from prematurely breaking through the internal capillary stop. The seal obtained by this slidable closure device is preferably irreversible and prevents excess blood from being trapped in the cartridge because the closure device moves in the plane of the orifice through which blood enters the cartridge and provides a shearing action that seals blood below the plane of the entry port, thereby moving excess blood, i.e., blood above the plane of the orifice, away from the entry port and optionally to a waste chamber.
One exemplary closure device is shown in FIG. 1 and comprises integrated elements 2, 3, 4 and 9 of cover 1. In this embodiment, closure device 2 rotates about a hinge until hook 3 snaps shut blocking sample entry port 4. An alternative to the closure device comprising integrated elements 2, 3, 4 and 9 of cover 1 in FIG. 1 is shown as a separate slidable element 200 in FIGS. 18 and 19. FIGS. 18 and 19 show a cartridge device comprising a modified version of the cover of FIG. 1 attached to a base similar to the base in FIG. 4 with intervening adhesive layer 21 shown in FIG. 3 along with the separate slidable closure element 200. FIG. 19 shows the closure device 200 in the open position, where the sample entry port 4 can receive a sample, e.g., blood. FIG. 18 shows the closure device 200 in the closed position where it seals the sample entry port in an air-tight manner. In operation, element 200 is manually actuated from the open to the closed position after the sample, e.g., blood, has been added to the entry port and it enters the holding chamber 34. In the embodiment shown, any excess blood in the region of the entry port is moved into an overflow chamber 201 or an adjacent retaining region or cavity. This chamber or region may include a fluid-absorbing pad or material to retain the excess sample, e.g., blood.

The sample entry port 4 may be an orifice that is circular, as shown in FIG. 19, or oval and the diameter of the orifice is generally in the range 0.2-5 mm, preferably 1-2 mm, or having a perimeter of 1-15 mm for an oval. The region around the orifice may be selected to be hydrophobic or hydrophilic to control the drop-shape of the applied sample to promote entry into the entry port. One advantage of the closure device shown in FIGS. 18 and 19 is that it prevents the sample from being pushed beyond the capillary stop element 25 at the end of the holding chamber 34. The presence of a small amount of sample, e.g., blood, beyond the capillary stop is not significant for tests that measure bulk concentration of an analyte and thus do not depend on sample volume. However, for immunoassay applications where metering of the sample is generally advantageous the sealing element improves metering accuracy of the device and assures the assayed segment of sample is appropriately positioned with respect to the immunosensor when the analyzer actuates the sample within the cartridge conduits.
In operation, when the sample, e.g., blood, is added to the cartridge it moves to the capillary stop. Thus sufficient sample for the assay is present when the region from the capillary stop to the sample entry port, i.e., the holding chamber 34, contains the sample. During the process of filling the holding chamber some sample may remain above the plane of the orifice of the entry port. When the sealing element is moved from the opened to closed position, any sample that is above the entry port is sheared away without trapping additional sample in the act of closure, thus ensuring that the sample does not move beyond capillary stop 25. In a preferred embodiment, sealing element 200 is positioned within a few thousandths of an inch above the surface of the tape gasket 211 of FIG. 3. The entry port is sealed by the subsequent lowering of the surface of 200 to the adhesive tape gasket when it engages locking features 212 and 213. Since the tape is essentially incompressible and the orifice has a small diameter, any inadvertent pressure applied to the sealing element by the user will not cause the sample to move beyond the capillary stop.

In certain cartridge embodiments that use several drops of sample, it is desirable that no bubbles form in the holding chamber as this can affect the assay. Accordingly, a reliable means for introducing more than one drop of sample, e.g., blood, into the holding chamber 34 without entraining bubbles has been developed. The sample entry port can be designed to receive multiple drops of sample without successive drops causing trapped bubbles to form in the holding chamber 34 by first treating the holding chamber with a Corona and/or a reagent cocktail.

The use of Corona treatments on disposable medical devices is well known in the art and is an effective way to increase the surface activity of virtually any material, e.g., metallized surfaces, foils, paper, paperboard stock, or plastics such as polyethylene, polypropylene, nylon, vinyl, PVC, and PET. This treatment makes them more receptive to inks, coatings, and adhesives. In practice the material being treated is exposed to an electrical discharge, or "corona." Oxygen molecules in the discharge area break into atoms and bond to molecules in the material being treated, resulting in a chemically activated surface. Suitable equipment for corona treatments is commercially available (e.g. Corotec Corp., Farmington, Conn.). The process variables include the amount of
power required to treat the material, the material speed, the width, the number of sides to be treated, and the responsiveness of a particular material to corona treatment, which variables can be determined by a skilled operator. The typical place to install a corona treatment is in-line with the printing, coating, or laminating process. Another common installation is directly on a blown film or cast film extruder since fresh material is more receptive to corona treatment.

As described above, the non-competitive (sandwich) immunoassay format is the most widely used immunoassay method and it is also a preferred format in the analysis device, e.g., cartridge, discussed herein. In this embodiment, one antibody (the immobilized antibody) is bound to a solid support or immunosensor, and a second antibody (the signal antibody) is conjugated/bound to a signal-generating reagent such as an enzyme, e.g., alkaline phosphatase.

Briefly, FIG. 20 illustrates the signal generating reactions occurring during the analysis with FIG. 20(a) showing the cleavage of substrate by alkaline phosphatase to generate electroactive p-aminophenol and FIG. 20(b) showing oxidation of p-aminophenol. The reaction in FIG. 20(a) occurs in the upper layer of the sensor structure while that in FIG. 20(b) occurs at the gold electrode surface. The inset in FIG. 20(a) illustrates the pH-dependence of the alkaline phosphatase catalyzed hydrolysis. The central illustration depicts the gross features of the immunosensor structure prior to exposure to sample.

The signal-generating reagent (e.g., signal antibody) may be part of a dry reagent coating in the analysis device, as described below, and preferably dissolves into the biological sample before the sample reaches the immunosensor. After washing away the sample and non-specifically bound reagents, the amount of signal-generating reagent (e.g., signal antibody) remaining on the solid support should in principle be proportional to the amount of analyte in the sample. However, one limitation of the assay configuration is the susceptibility to interference(s) caused by leukocytes present in the blood sample.
While leukocyte interferences are mitigated by the means disclosed in jointly owned US 20060160164, it has now been discovered that for certain blood samples the effect surprisingly can be substantially reduced or eliminated by the addition of sacrificial beads that are homogeneously mixed with the sample, and where the beads are specifically opsonized with respect to leukocytes.

The sacrificial beads preferably are coated with a non-human IgG (IgG class immunoglobulins) or fragments thereof isolated from animal species. As used herein, the term "fragment" refers to any epitope-bearing fragment derived from the specified molecule. Thus, an IgG fragment may comprise, for example, epitope bearing F(ab')2 or Fab fragments or an Fc fragment. Further, by "IgG or fragments thereof" it is meant IgG alone, IgG fragments alone (i.e., one or more of F(ab')2 fragments, Fab fragments and/or Fc fragments of IgG), or a combination of IgG and IgG fragments. The desired effect may be achieved with a variety of surface coatings, so long as the surface coating is opsonized or opsonizable upon exposure to a sample to be assayed.

In a preferred embodiment, the sacrificial beads are incorporated into a dry reagent coating, which in some embodiments may be the same dry reagent coating that contains the signal-generating reagent (e.g., signal antibody). Thus, in one embodiment, the analysis device includes a dry reagent coating that comprises either or both: (a) a component suitable for ameliorating the effect of leukocytes, e.g., beads coated with IgG or fragments thereof, and/or (b) a signal antibody. The dry reagent coating may be formed from a reagent cocktail, which also preferably comprises either or both: (a) a component suitable for ameliorating the effect of leukocytes, e.g., beads coated with IgG or fragments thereof, and/or (b) a signal antibody. In one aspect, the reagent coating and/or cocktail further comprises IgM or fragments thereof for ameliorating interference caused by heterophile antibodies, as disclosed in co-pending US application 12/41 1,325. The surface on which the reagent cocktail is to be deposited preferably is first Corona treated to provide charged surface groups that will promote spreading of the printed cocktail.
In general, the reagent cocktail used to form the dry reagent coating may further comprise a water-soluble protein, an amino acid, a polyether, a polymer containing hydroxyl groups, a sugar or carbohydrate, a salt and optionally a dye molecule. One or more of each component can be used. In one embodiment, the cocktail contains bovine serum albumin (BSA), glycine, salt, methoxypolyethylene glycol, sucrose and optionally bromophenol blue to provide color that aids visualizing the printing process. In one embodiment, from 1 to 20 µL of cocktail is printed onto the desired surface, e.g., within the holding chamber or other conduit, of the analysis device and allowed to air dry (with or without heating) before being assembled with its cover. In a preferred aspect, the reagent cocktail and the dry reagent coating formed therefrom comprise lactitol, DEAE-dextran, salts such as magnesium and sodium chloride, IgG/IgM, heparin, surfactant(s) and rhodamine.

The reagent cocktail preferably is formulated as a printable aqueous solution containing the sacrificial beads and optionally other interference-reducing reagents. Upon introduction of a biological sample, e.g., blood, the sample preferably mixes with the reagent in a first step of the assay. The reagent may also include inorganic salts and surfactants to optimize assay performance with respect to chemical and fluidic attributes. Other optional additives may include heparin to ensure adequate anticoagulation and dyes for visualization of the location of the reagent after printing. Also optionally present are stabilizers such as sodium azide for inhibition of microbial growth and a mixture of lactitol and diethylaminoethyl-dextran (Applied Enzyme Technologies Ltd., Monmouth House, Mamhilad Park, Pontypool, NP4 0HZ UK) for stabilization of proteins. Once deposited in the device, the deposited reagent may, for example, be dried for 30 to 60 minutes in a stream of warm air. In one embodiment, the reagent is printed in the sample inlet of the device using an automated printing instrument and dried to form a sacrificial bead containing reagent coating layer.

In addition to the inclusion of sacrificial beads, other optional additives may be included in the cartridge or used in conjunction with the assay. The anticoagulant heparin can be added, as discussed above, to improve performance in cases where the sample was not collected in a heparinized tube or was not properly mixed in a heparinized tube.
Enough heparin is added so that fresh unheparinized blood will remain uncoagulated during the assay cycle of the cartridge, typically in the range of 2 to 20 minutes. Goat and mouse IgG can by added to combat heterophile antibody problems well known in the immunoassay art. Proclín, DEAE dextran, Tris buffer and lactitol can be added as reagent stabilizers. Tween 20 can be added to reduce binding of proteins to the plastic, which is the preferred material for the cartridge. It also allows the reagents to coat the plastic surface more evenly and acts as an impurity that minimizes the crystallization of sugars, such as lactitol, so that they remain a glass. Sodium azide may be added to inhibit bacterial growth.

In a preferred embodiment, the base print cocktail is prepared as follows for a 1 liter (L) batch: Protein stabilization solution (PSS, AET Ltd., 50% solids, 100.0 g) is added to 200-250 mL of an aqueous solution of sodium chloride (8.00 g) and sodium azide (0.500 g) and the resulting solution is transferred to a 1L volumetric flask. A solution of murine IgG is prepared by adding murine IgG (0.9 g) to 75 mL of deionized water and stirred for 15-60 minutes until dissolution is complete. An equally concentrated solution of caprine IgG is prepared in an identical manner and both solutions are filtered through a 1.2 μM filter. Murine IgM is acquired as a liquid from the supplier (for example, Sigma-Aldrich). The protein concentrations of each of the three immunoglobulin (Ig) stock solutions are measured spectrophotometrically at 280 nm. The masses of these Ig solutions required to provide murine IgG (0.75 g), caprine IgG (0.75 g) and murine IgM (25 mg) are calculated and these amounts are added to the printing solution. A solution of diethylaminoethyl-dextran (DEAE-dextran) is prepared by adding DEAE-dextran (2.5 g) to 50-100 mL of deionized water and stirred for 30 minutes. The DEAE-dextran solution is added to the printing solution. To this is added sodium heparin (10,000 IU/mL, 3.00 mL), Tween-20 (3.00 g) and a 5% (w/v) aqueous solution of Rhodamine (200 μL). The resulting solution is diluted to 1.000 L with deionized water and stored in a freezer or refrigerator until use. When included, IgG-coated microparticles for leukocyte interference mitigation can be added before this final dilution.
Printing of these and similar fluids to form a dry reagent coating on the cartridge component is preferably automated and based on a microdispensing system, including a camera and computer system to align components, as disclosed in U.S. Pat. No. 5,554,339, incorporated herein by reference in its entirety. In this patent, the wafer chuck is replaced by a track for feeding the plastic cartridge bases to the dispensing head. The track presents the bases to the head in a predetermined orientation to ensure consistent positional dispensing.

In another embodiment, the test cartridge may comprise a plurality of dry reagent coatings (in which case the coatings may be respectively referred to as a first reagent coating, a second reagent coating, etc., in order to distinguish them). For example, the sacrificial beads may be included in a first reagent coating, which, for example, may be adjacent to a second reagent coating that contains the signal generating element, e.g., signal antibody. In this aspect, the second reagent coating may be located upstream or downstream of the first reagent coating, although it is preferable for the reagent coating that contains the signal antibody to be located downstream of the reagent coating that contains the sacrificial beads. In a preferred embodiment, the holding chamber is coated with a first reagent coating that comprises sacrificial beads and optionally other reagents that ameliorate various forms of interference. In this aspect, a second reagent coating comprising the signal antibody preferably is located downstream of the holding chamber, e.g., immediately upstream of the immunosensor.

In still other embodiments, the sacrificial beads may not be part of the analysis device, e.g., cartridge. For example, the sacrificial beads may be incorporated in a sample collection device, e.g., capillary, Vacutainer™ or syringe. For example, the sacrificial bead coating may be formed on an interior wall of the collection device. Thus, in one embodiment, the invention is to a kit for performing an immunoassay that comprises the sacrificial beads which are first used to amend the blood sample in a first container or location, and then the sample is passed to a second container or location which has the capture and signal antibodies.
In another embodiment, the component(s) for ameliorating leukocyte interference may be contained in solution and mixed with the biological sample, e.g., blood, and the resulting amended sample is introduced into the analysis device, e.g., cartridge. In one embodiment, for example, a blood sample may be mixed with the sacrificial beads to form an amended sample, which is then introduced into the analysis device, e.g., cartridge. In another aspect, the device includes a pouch therein that contains a liquid comprising sacrificial beads, which is mixed with a blood sample in the device and then processed substantially as described herein to form an assay, e.g., sandwich assay, for analyte detection.

In another embodiment, electrowetting is employed to mix a first liquid comprising sacrificial beads with a liquid biological sample such as blood. In this embodiment, an apparatus may be provided for manipulating droplets. The apparatus, for example, may have a single-sided electrode design in which all conductive elements are contained on one surface on which droplets are manipulated. An additional surface can be provided parallel with the first surface for the purpose of containing the droplets to be manipulated. Droplets are manipulated by performing electrowetting-based techniques in which electrodes contained on or embedded in the first surface are sequentially energized and de-energized in a controlled manner. The apparatus may allow for a number of droplet manipulation processes, including merging and mixing two droplets together, splitting a droplet into two or more droplets, sampling a continuous liquid flow by forming from the flow individually controllable droplets, and iterative binary or digital mixing of droplets to obtain a desired mixing ratio. In this manner, droplets of the first liquid comprising sacrificial beads and other reagents may be carefully and controllably merged and mixed with the liquid biological sample, e.g., blood. See, e.g., U.S. Pat. No. 6,911,132, the entirety of which is incorporated herein by reference.

While the present invention is broadly applicable to immunoassay systems, it is best understood in the context of the i-STAT™ immunoassay system (Abbott Point of Care Inc., Princeton, N.J.), as described in jointly owned pending and issued patents cited above. In some embodiments, the system employs an immuno-reference sensor (See US 2006/0160164 Al, incorporated herein by reference in its entirety) for purposes of
assessing the degree of non-specific binding (NSB) occurring during an assay. NSB may arise due to inadequate washing or due to the presence of interferences. The net signal from the assay is comprised of the specific signal arising from the analyte immunosensor corrected by subtracting the non-specific signal arising from the immuno-reference sensor. The amount of signal at the immuno-reference sensor is subject to limits defined by a quality control algorithm.

In one embodiment, the present invention improves the resistance of the i-STAT immunoassay format to interference caused by leukocytes; however, it is equally applicable to the standard ELISA format, where these cells are present in the analysis medium. Specifically, the invention involves the use of coated sacrificial beads which have been found to substantially reduce the interference caused by leukocytes in certain test specimens.

As indicated above, it has now been discovered that amending a sample with sacrificial beads preferably in combination with other reagents (as disclosed, for example, in the ‘164 and ‘325 applications) results in reduced or eliminated leukocyte interference. In experiments, non-human IgG-labeled microparticle beads were added to the sample conditioning dry reagent print cocktail used in the i-STAT™ immunoassay format. Then known samples that could not previously be reliably analyzed due to interference from leukocytes were tested. It is notable that while traditional sandwich assays yield erroneous results in these cases, prior i-STAT system assays did not previously report inaccurate results for these samples, as the system includes an algorithm that detects spurious signals, alerts the user with an error code, and suppresses the result from being displayed. This is an example of one part of a quality system required for reliable point-of-care testing. In this way the quality and integrity of the analytical system is maintained.

Surprisingly, when modified cartridges containing sacrificial beads were tested and the results compared with conventional cartridges lacking sacrificial beads, the results demonstrated that blood samples exhibiting leukocyte interference in the
conventional cartridges, could be analyzed accurately when the sacrificial beads were employed.

With regard to the subject matter of the present invention, it was discovered that certain immunoassay test cartridges, notably BNP cartridges, exhibited unexpected positively and negatively sloping waveforms arising from a previously unknown interference mechanism. See, for example, FIG 11(a) and (b), respectively. This led to a hypothesis concerning the mechanism of the interference based on experiments on the effect of pulsing the electrode to positive potentials during the wash step.

Note that the normal immunosensor response, expected on a theoretical basis, has a near-zero slope at low analyte concentrations, and negative slopes are expected only at high analyte concentrations where the measurement can become substrate-limited rather than enzyme limited. These two cases are shown in FIGS. 11(c) and (d), respectively.

There are several potential mechanisms causing dynamic (non-steady state) amperometric signals. Dynamic electrode activity (changing effective electrode area) is unlikely since the electrode is sequestered from formed elements owing to the presence of immobilized assay beads (microparticles) on a polyvinyl alcohol (PVA) layer, neither of which exhibit this effect in plasma samples. Dynamic layer thickness, e.g., swelling or shrinking of the components above, depending on fluid contact, is unlikely as there is no driving force for such a phenomenon that would elicit both positive and negative slopes. Dynamic coverage of the enzyme (e.g., ALP, changing surface concentration of enzyme) is ruled out because in the thin-layer format, diffusion of enzyme (e.g., ALP) from the sensor over the time-scale of the measurement is not possible. Dynamic transport of the enzyme substrate, e.g., para-aminophenol phosphate (p-APP), to the electrode surface is unlikely given the size of the molecule, which is relatively small and has a relatively facile diffusion (D $\sim 5 \times 10^{-9}$ cm$^2$/s). Thus, by the process of elimination, dynamic ALP activity was considered the most likely cause of dynamic sensor signals. Further, investigation was made to assess the mechanism. It is noted that the hydrolysis of p-aminophenyl phosphate by ALP is pH-dependent with an optimum near pH 10. In the cartridge, a working pH of 9.2 is used as this slightly lower pH ensures stability of
immunocomplexes. In addition, the oxidation of para-aminophenol (p-AP) at the electrode is pH dependent and is expected to shift by about +59 mV per decade decrease in pH, i.e., at lower pH the reaction must be driven harder, i.e., an increased applied potential is required.

If the microparticle print layer were to become less permeable due to interaction with the interfering components to the extent that sample fluid (pH 7.4) within the sensor structure could not be fully replaced with analysis fluid (pH 9.2) during the wash step, this would result in suboptimal detection step pH, particularly for the electrode reaction which occurs at a region farthest from the point of entry of the analysis fluid. More importantly, this impaired fluid replacement would necessarily create a pH gradient that would undergo relaxation with time. As the relative rates of the enzyme and electrode reactions change, so will the observed signal. This technical evaluation has the considerable advantage that it offers an explanation for both positive and negatively sloping signals. See, e.g., FIGS. 11(a) and (b).

The conception that the observed interference is associated with an incomplete wash step due to "plugging" or "fouling" of the microparticle layer was assessed further by applying a pulse to extreme potentials, e.g., applying a pulse to an oxidizing potential, during the wash step. It was anticipated that positively sloping waveforms might be caused by an inactive blocked sensor and that pulsing might be employed to clean the electrode prior to the analysis step. It was observed that applying an oxidizing pulse during the wash step in a normal sample had no effect on observed signal and in the subsequent analysis. See FIG. 12(a). However, in the case of aberrant high buffy samples the effect of pulsing was large and dynamic signals and further, these signals were greater than expected given the concentration of analyte. See FIG. 12(b).

The difference in the response to an oxidizing potential pulse in these two cases demonstrated that the fluids within the sensor structure were indeed different. As anticipated, the correct response resulted from the presence of desired analysis fluid over the sensor, whereas the abnormal response arose because the fluid over the sensor structure was plasma, or a combination of plasma and analysis fluid. The difference in
response can be understood as follows: the oxidizing pulse results in the evolution of oxygen and a decrease in pH according to: \( \text{H}_2\text{O} \rightarrow \frac{1}{2} \text{O}_2 + 2\text{H}^+ + 2\text{e}^- \).

In the case of the sensor structure containing analysis fluid buffered to pH 9.2, protons evolved at the electrode were rapidly consumed in the presence of the buffer (100 mM carbonate in analysis fluid). However, in the absence of the buffering afforded by the analysis fluid, protons persisted in the region of the electrode resulting in a plume of acidic fluid. This acidic plume resulted in the acid-catalyzed hydrolysis of pAPP to pAP generating a larger signal than anticipated. Specifically, the aberrant waveform arose from pAP generated by the enzymatic action of the enzyme, e.g., ALP, on pAPP and also non-enzymatic acid-catalyzed hydrolysis.

It is noted that the acid-catalyzed hydrolysis reaction does not occur significantly for p-aminophenyl phosphate unless the amino group is protonated as it is at low pH. This is because the reaction requires a strongly electron-withdrawing substituent in the para position (Barnard et al. J. Chem. Soc. (1966), 227-235). As is known in the art, an -NH\(_2\) substituent is significantly electron-donating, whereas upon protonation the -NH\(_3^+\) substituent becomes highly electron-withdrawing (more so even than -NO\(_2\)); for example the Hammett para-rho values are -0.66 for -N\(_3^+\) and 1.70 for -NH\(_3^+\).

These experiments associated the observed interference with "high buffy" samples and could intentionally be elicited by running whole blood samples with an enriched buffy coat. Note that this term is given to the layer of white blood cells and platelets that form at the plasma-red cell boundary when a blood sample is centrifuged. Further evidence implicating leukocytes and potentially platelets as fouling agents is shown in the micrographs FIGS. 17(a) (assay without use of sacrificial beads) and 17(b) (assay after using sacrificial beads). For comparison, a pristine immunosensor prior to contact with a blood sample is illustrated in FIG. 20.

FIG. 17(a) shows a sensor that was exposed to a high buffy sample (~10\(^5\) leukocytes per \(\mu\text{L}\)) using the standard measurement cycle with a sensor incubation time of 10 minutes. The sample was not exposed to opsonized sacrificial beads. It is clear
that a portion of the assay bead-coated sensor surface is covered with an adhered layer of cells that were not easily removed by the wash step.

By contrast, FIG 17(b) shows a sensor that was exposed to a high buffy sample (-105 leukocytes per µL) using the standard measurement cycle with a sensor incubation time of 10 minutes. However, in contrast to the assay shown in FIG. 17(a), the sample shown in FIG. 17(b) was exposed to opsonized (IgG coated) sacrificial beads according to one embodiment of the present invention. It is clear that the portion of the assay bead-coated sensor surface has significantly less adhered cells when compared to FIG. 17(a) after the wash step.

IgG acts as an opsonin, which is a substance capable of marking a pathogen for phagocytosis, for example, by leukocytes. IgGs are generally added to immunoassays to manage heterophile antibody interference as described in co-pending US application 12/41 1,325, and are present on assay beads in the BNP cartridge described herein. Consequently, it is likely that either this source of IgG (when present in an immunoassay device) or IgG naturally present in the blood sample may act to undesirably opsonize the sensor surface to leukocytes. In addition, as the assay beads are similar in size to biological cells (bacteria), which are the natural target of phagocytosis, it is probable that IgG accumulation on the assay beads is undesirably promoting accumulation of leukocytes on these beads. This is consistent with the observed interference in samples with high white cell counts, and possibly those with an activated immune status. The present invention provides a solution to this leukocyte interference whereby the inclusion of sacrificial IgG-coated microparticles into the sample affords a decoy target for leukocyte activity so as to divert them from the primary immune reagents on the sensor.

Preparation of IgG-coated microparticles was effected using methods analogous to those employed for preparation of the assay beads. This method involved adsorption of IgG onto carboxylated polystyrene microparticles in MES buffer (2-(N-morpholino)ethanesulfonic acid) followed by cross-linking in the presence of EDAC (1-ethyl-3-(3-dimethylaminopropyl)carbodiimide).
One non-limiting method for forming the sacrificial beads is now described. In a preferred procedure, raw microparticles are pelleted by centrifugation at 18,000 RCF (relative centrifugal force) for 20 minutes from their matrix (10% microparticles in water, Seradyn) and re-suspended in 25 mM MES buffer to a concentration of 100-200 mg/mL microparticles. IgG dissolved in 25 mM MES buffer is then added in a quantity equal to about 1 to 5% of the weight of the microparticles. After a 15-20 minutes nutation in a refrigerator, the microparticles are pelleted by centrifugation for 20 minutes at 1300 RCF and re-suspended in fresh MES buffer to a concentration of 75 mg/mL. The supernatant from centrifugation is assayed for protein content by measuring absorbance at 280 nm (effective extinction coefficient of 1.4 AU/mg/mL protein) to confirm the IgG has absorbed onto the microparticles. Freshly prepared EDAC cross-linking agent (10 mM in MES buffer) is added to the re-suspended microparticles to a final concentration of about 2-4 mM. The mixture is then stirred by nutation in a refrigerator for 120 ± 15 minutes. The microparticles may then again be pelleted by centrifugation at 1300 RCF for 20 minutes and re-suspended in 1/5 PPS (phosphate buffered saline) and nutated in the refrigerator for 15-30 minutes. Upon final centrifugation, the microparticles can be re-suspended in PBS + 0.05% Sodium Azide or in 1:1 1/5 PPB:PSS (1/5 PPB is PBS diluted with 4 parts water, PSS = protein stabilization solution, Applied Enzyme Technologies, Pontypool, UK) to a concentration of 10% solids. The resulting preparation may be aliquoted and stored frozen, preferably at -60°C. Microparticles suspended in PBS formed by this process were employed in the experiments described herein and were dosed directly into blood samples.

Preparation of an enriched or high buffy whole blood sample, as described for use in the experiments described herein was as follows. Fresh whole blood was drawn from a donor into two 6 mL EDTA-anticoagulated Vacutainers™ and was centrifuged for 10 minutes at 2000 RCF (standard rotor). Where BNP "positive" samples were desired, the tubes were spiked with the BNP antigen prior to centrifugation. All of the plasma except the last millimeter above the plasma / buffy coat / red blood cell interface was withdrawn and set aside. The interfacial region was then withdrawn using a pipettor (with the intention of removing as much of the buffy coat layer as possible) and was set aside. The red blood cells were then removed and set aside. By recombining the buffy coat
materials with lesser portions of the plasma and red cell fractions, it was possible to create high buffy blood samples while retaining a normal sample hematocrit, e.g., 35-55 wt.%. Similarly, samples with a low or essentially no buffy material (leukocytes and platelets) present can be created.

In experiments, BNP test cartridges were tested with: (i) high buffy samples, (ii) high buffy samples treated with a 10 percent volume a suspension of 10 weight percent microparticles coated with IgG (μP-IgG) in PBS immediately before running, (iii) high hematocrit leukocyte-free samples, and (iv) low hematocrit leukocyte-free samples.

FIG. 21 contains graphical data illustrating the effect of leukocyte interference on electrochemical immunosensor signal slopes and the effect of sacrificial microparticle treatment on the slopes. Illustrated in the right and left panels are Sensor.

Slopes (y-axis) plotted as a function of Net Signal (x-axis) for normal whole blood sample (right panel) and high buffy blood sample (enriched leukocyte, high buffy, left panel). The left panel illustrates the considerable variability of signal slopes observed in high buffy samples in the absence of sacrificial microparticles (Sublot 1). This variability was substantially ameliorated in the presence of sacrificial microparticles (Sublots 2 and 3). Note that minimal signal slope variability was observed in the normal whole blood samples (right panel) both with and without sacrificial microparticles.

Microscopic inspection of sensors following the assay revealed the presence of a thick deposit on chips run in high buffy (HB) and the absence of a deposit on samples run in HB/μP-IgG. Micrographs of the immunosensors are shown in FIGS. 17(a) and 17(b) and their associated analyzer waveforms are illustrated in FIGS. 22(a) and (b), respectively. It is clear from a comparison of a pristine immunosensor prior to contact with a blood sample as illustrated in FIG. 20 with the immunosensor after contact with blood treated with the preferred formulation of sacrificial beads (FIG. 17(b)) that visually there is a significant improvement, i.e., a reduction in adhered leukocytes compared to FIG. 17(a). Based on many observations, this visual improvement correlates directly with an actual improvement in immunosensor performance.
Additional experiments showed that the interference phenomenon does not occur in plasma alone or in samples containing platelets but not leukocytes, but only in samples containing a high buffy level. In addition, smaller microparticles, e.g., those having an average particle size less than 0.2 \( \mu \text{m} \), coated with IgG do not have the same interference mitigating effect on sensor slopes as do larger particles. Preferably, the average particle size of the IgG-coated microparticles (sacrificial beads) is from 0.01 to 20 \( \mu \text{m} \), e.g., from 0.1 to 20 \( \mu \text{m} \), from 1 to 10 \( \mu \text{m} \), from 0.1 to 5 \( \mu \text{m} \), or from 2 to 5 \( \mu \text{m} \). The particle size distribution of the sacrificial microparticles preferably is unimodal, although polymodal distributions are also possible. In principal, any particles of the correct size and capable of being opsonized may be used; however, polystyrene beads are preferred. In preferred aspects, goat or sheep IgG coated particles are employed, although other IgG sources may be employed such as, for example, mouse or rabbit IgG. In general, it was found that the size of the microparticles is important but not its composition or the source of the IgG. With regard to the sacrificial beads, they preferably comprise substrate beads formed of a material selected from the group consisting of polystyrene, polyacrylic acid and dextran, and can have an average particle size in the range of about 0.01 \( \mu \text{m} \) to about 20 \( \mu \text{m} \), more preferably an average particle size in the range of from 0.1 \( \mu \text{m} \) to 5 \( \mu \text{m} \) or from about 2 \( \mu \text{m} \) to about 5 \( \mu \text{m} \). Note that while use of a spherical bead is preferred, other bead structures, e.g., ovals and other irregular shaped particles, are within the meaning of the terms beads and microparticles as used here. In this case the average particle size refers to the average longest dimension of the particles, for example diameter for spherical particles, as determined by methods well-known in the art.

Collectively, the experimental data support the conclusion that leukocytes are primarily responsible for a phenomenon in which the sensor becomes less permeable in the wash cycle and that this immunoassay interference can be ameliorated by addition of sacrificial IgG coated particles to the assay medium.

Wafer-level microfabrication of a preferred embodiment of the immunosensor is as follows. The base electrode (94 of FIG. 9) comprises a square array of 7 \( \mu \text{m} \) gold disks on 15 \( \mu \text{m} \) centers. The array covers a circular region approximately 600 \( \mu \text{m} \) in diameter, and is achieved by photo-patterning a thin layer of polyimide of thickness 0.35 \( \mu \text{m} \) over a
substrate made from a series of layers comprising Si/SiO₂/TiW/Au. The array of 7 µm microelectrodes affords high collection efficiency of electroactive species with a reduced contribution from any electrochemical background current associated with the capacitance of the exposed metal. The inclusion of a PVA layer over the metal significantly enhances the reduction of background currents.

The porous PVA layer is prepared by spin-coating an aqueous mixture of PVA plus a stilbizonium photoactive, cross-linking agent over the microelectrodes on the wafer. The spin-coating mixture optionally includes bovine serum albumin (BSA). It is then photo-patterned to cover only the region above and around the arrays and preferably has a thickness of about 0.6 µm.

The general concept of differential measurement is known in the electrochemical and sensing arts. A novel means for reducing interfering signals in an electrochemical immunosensing systems is now described. However, while it is described for pairs of amperometric electrochemical sensors it is of equal utility in other electrochemical sensing systems including potentiometric sensors, field effect transistor sensors and conductimetric sensors. It is also applicable to optical sensors, e.g., evanescent wave sensors and optical wave guides, and also other types of sensing including acoustic wave and thermometric sensing and the like. Thus, the immobilized antibody may be attached to a sensor selected from the group consisting of an amperometric electrode, a potentiometric electrode, a conductimetric electrode, an optical wave guide, a surface plasmon resonance sensor, an acoustic wave sensor and a piezoelectric sensor. Ideally, in the non-competitive assay embodiments, the signal from an immunosensor (IS) is derived solely from the formation of a sandwich comprising an immobilized antibody (Abl), the analyte, and a signal antibody (Ab2) that is labeled, wherein the label (e.g., an enzyme) reacts with a substrate (S) to form a detectable product (P) as shown below in scheme (1).

\[
\text{Surface-Ab1-analyte-Ab2-enzyme; enzyme + S} \rightarrow P \quad (1)
\]
It is known that some of the signal antibody (Ab2) may bind non-specifically to
the surface, as shown below in schemes (2) and (3), and might not be washed away
completely from the region of the immunosensor (up to approx. 100 microns away)
during the washing step giving rise to a portion of the total detected product that is not a
function of the surface-Abl-analyte-Ab2-enzyme immunoassay sandwich structure,
thereby creating an interfering signal.

Surface-Ab2-enzyme; enzyme + S → P  (2)

Surface-analyte-Ab2-enzyme; enzyme + S → P  (3)

As indicated above, a second immunosensor optionally may be placed in the
cartridge that acts as an immuno-reference sensor (IRS) and gives the same (or a
predictably related) degree of NSB as occurs on the primary immunosensor. Interference
can be reduced by subtracting the signal of this immuno-reference sensor from that of the
primary immunosensor, i.e., the NSB component of the signal is removed, improving the
performance of the assay, as shown in scheme (4) below. This correction may optionally
include the subtraction or addition of an additional offset value.

Corrected signal = IS - IRS  (4)

The immuno-reference sensor is preferably the same in all significant respects
(e.g., dimensions, porous screening layer, latex particle coating, and metal electrode
composition) as the primary immunosensor except that the capture antibody for the
analyte (for instance, cTnI) is replaced by an antibody to a plasma protein that naturally
occurs in samples (both normal and pathological) at a high concentration. The
immunosensor and reference immunosensor may be fabricated as adjacent structures 94
and 96, respectively, on a silicon chip as shown in FIG. 9. While the preferred
embodiment is described for troponin I and BNP assays, this structure is also useful for
other cardiac marker assays including, for example, troponin T, creatine kinase MB, procalcitonin, proBNP, NTproBNP, myoglobin and the like, plus other sandwich assays used in clinical diagnostics, e.g., PSA, D-dimer, CRP, HCG, NGAL, myeloperoxidase and TSH.

Examples of suitable antibodies that bind to plasma proteins include antibodies to human serum albumin, fibrinogen and IgG Fc region, with albumin being preferred. However, any native protein or blood component that occurs at a concentration of greater than about 100 ng/mL can be used if an appropriate antibody is available. The protein should, however, be present in sufficient amounts to coat the sensor quickly compared to the time needed to perform the analyte assay. In a preferred embodiment, the protein is present in a blood sample at a concentration sufficient to bind more than 50% of the available antibody on the reference immunosensor within about 100 seconds of contacting a blood sample. In general the second immobilized antibody has an affinity constant of about $1 \times 10^{-7}$ to about $1 \times 10^{-15}$ M. For example, an antibody to albumin having an affinity constant of about $1 \times 10^{-10}$ M is preferred, due to the high molar concentration of albumin in blood samples, which is about $1 \times 10^{-3}$ M.

It has been found that providing a surface that is covered by native albumin derived from the sample significantly reduces the binding of other proteins and cellular materials that may be present. This method is generally superior to conventional immunoassays that use conventional blocking agents to minimize NSB because these agents must typically be dried down and remain stable for months or years before use, during which time they may degrade, creating a stickier surface than desired and resulting in NSB that rises with age. In contrast, the method described here provides a fresh surface at the time of use.

An immunosensor for cardiac brain natriuretic peptide (BNP) with a reference-immunosensor for performing differential measurement to reduce the effect of NSB is described next. Carboxylate-modified latex microparticles (supplied by Bangs Laboratories Inc. or Seradyn Microparticles Inc.) coated with anti-BNP and anti-HSA are both prepared by the same method. The particles are first buffer exchanged by
centrifugation, followed by addition of the antibody, which is allowed to passively adsorb onto the particles. The carboxyl groups on the particles are then activated with EDAC in MES buffer at pH 6.2, to form amide bonds to the antibodies. Any bead aggregates are removed by centrifugation and the finished beads are stored frozen.

It was found that for the anti-human serum albumin (HSA) antibody, saturation coverage of the latex beads results in about a 7% increase in bead mass. Coated beads were prepared using covalent attachment from a mixture comprising 7 mg of anti-HSA and 100 mg of beads. Using this preparation a droplet of about 0.4 nL, comprising about 1% solids in deionized water, was microdispensed (using the method and apparatus of U.S. Pat. No. 5,554,339, incorporated herein by reference in its entirety) onto a photo-patterned porous polyvinyl alcohol permselective layer covering sensor 96, and allowed to dry. The dried particles adhered to the porous layer and substantially prevented their dissolution in the blood sample or the washing fluid.

For the BNP antibody, saturation coverage of the latex bead surface resulted in a mass increase in the beads of about 10%. Thus by adding 10 mg of anti-BNP to 100 mg of beads along with the coupling reagent, saturation coverage was achieved. These beads were then microdispensed onto sensor 94.

In another embodiment, immunosensor 94 is coated with beads having both a plasma protein antibody, e.g., anti-HSA, and the analyte antibody, e.g., anti-BNP. Latex beads made with the about 2 mg or less of anti-HSA per 100 mg of beads and then saturation-coated with anti-BNP provide superior NSB properties at the immunosensor. It has been found that the slope (signal versus analyte concentration) of the troponin assay is not materially affected because there is sufficient anti-BNP on the bead to capture the available analyte (antigen). By determining the bead saturation concentration for different antibodies, and the slope of an immunosensor having beads with only the antibody to the target analyte, appropriate ratios of antibody combinations can be determined for beads having antibodies to both a given analyte and a plasma protein.

An important aspect of immunosensors having a reference immunosensor is the "humanizing" of the surface created by a layer of plasma protein, preferably the
HSA/anti-HSA combination. This appears to make the beads less prone to NSB of the antibody-enzyme conjugate. It also seems to reduce bead variability. Without being bound by theory, it appears that as the sensors are covered by the sample they are rapidly coated with native albumin due to the anti-HSA surface. This gives superior results compared to conventional blocking materials, which are dried down in manufacturing and re-hydrated typically after a long period in storage. Another advantage to "humanizing" the sensor surface is that it provides an extra mode of resistance to human anti-mouse antibodies (HAMA) and other heterophile antibody interferences. The effects of HAMA on immunoassays are well known.

Another use of the immuno-reference sensor, which may be employed in the devices and methods of the invention, is to monitor the wash efficiency obtained during the analytical cycle. As stated above, one source of background noise is the small amount of enzyme conjugate still in solution, or non-specifically absorbed on the sensor and not removed by the washing step. This aspect of the invention relates to performing an efficient washing step using a small volume of washing fluid, by introducing air segments as mentioned in Example 2.

In operation of the preferred embodiment, which is an amperometric electrochemical system, the currents associated with oxidation of p-aminophenol at immunosensor 94 and immuno-reference sensor 96 arising from the activity of ALP, are recorded by the analyzer. The potentials at the immunosensor and immuno-reference sensor are poised at the same value with respect to a silver-silver chloride reference electrode. To remove the effect of interference, the analyzer subtracts the signal of the immuno-reference sensor from that of the immunosensor according to equation (4) above. Where there is a characteristic constant offset between the two sensors, this also is subtracted. It will be recognized that it is not necessary for the immuno-reference sensor to have all the same non-specific properties as the immunosensor, only that it be consistently proportional in both the wash and NSB parts of the assay. An algorithm embedded in the analyzer can account for any other essentially constant difference between the two sensors.
Use of a differential combination of immunosensor and immuno-reference sensor, rather than an immunosensor alone, provides the following improvement to the assay. In a preferred embodiment the cartridge design provides dry reagent that yields about 4-5 billion enzyme conjugate molecules dissolved into about a 10 μL blood sample. At the end of the binding and wash steps the number of enzyme molecules at the sensor is about 70,000. In experiments with the preferred embodiment there were, on average, about 200,000 (± about 150,000) enzyme molecules on the immunosensor and the reference immunosensor as non-specifically bound background. Using a differential measurement with the immuno-reference sensor, about 65% of the uncertainty was removed, significantly improving the performance of the assay. While other embodiments may have other degrees of improvement, the basis for the overall improvement in assay performance remains.

An additional use of the optional immuno-reference sensor is to detect anomalous sample conditions, such as improperly anti-coagulated samples which deposit material throughout the conduits and cause increased currents to be measured at both the immunosensor and the immuno-reference sensor. This effect is associated with both non-specifically adsorbed enzyme and enzyme remaining in the thin layer of wash fluid over the sensor during the measurement step.

Another use of the optional immuno-reference sensor is to correct signals for washing efficiency. In certain embodiments the level of signal at an immunosensor depends on the extent of washing. For example, longer washing with more fluid/air segment transitions can give a lower signal level due to a portion of the specifically bound conjugate being washed away. While this may be a relatively small effect, e.g., less than 5%, correction can improve the overall performance of the assay. Correction may be achieved based on the relative signals at the sensors, or in conjunction with a conductivity sensor located in the conduit adjacent to the sensors, acting as a sensor for detecting and counting the number of air segment/fluid transitions. This provides the input for an algorithmic correction means embedded in the analyzer.
In another embodiment of the reference immunosensor with an endogenous protein, e.g., HSA, it is possible to achieve the same goal by having an immuno-reference sensor coated with antibody to an exogenous protein, e.g., bovine serum albumin (BSA). In this case the step of dissolving a portion of the BSA in the sample, provided as an additional reagent, prior to contacting the sensors is needed. This dissolution step can be done with BSA as a dry reagent in the sample holding chamber of the cartridge, or in an external collection device, e.g., a BSA-coated syringe. This approach offers certain advantages, for example the protein may be selected for surface charge, specific surface groups, degree of glycosylation and the like. These properties may not necessarily be present in the available selection of endogenous proteins.

In addition to salts, other reagents can improve whole-blood precision in an immunoassay. These reagents should be presented to the blood sample in a way that promotes rapid dissolution. Support matrices including cellulose, polyvinyl alcohol and gelatin (or mixtures thereof) that are coated on to the wall of the blood-holding chamber (or another conduit) promote rapid dissolution, e.g., greater than 90% complete in less than 15 seconds.

A cartridge of the present invention has the advantage that the sample and a second fluid can contact the sensor array at different times during an assay sequence. The sample and the second fluid also may be independently amended with other reagents or compounds present initially as dry coatings within the respective conduits. Controlled motion of the liquids within the cartridge further permits more than one substance to be amended into each liquid whenever the sample or fluid is moved to a new region of the conduit. In this way, provision is made for multiple amendments to each fluid, greatly extending the complexity of automated assays that can be performed, and therefore enhancing the utility of the present invention.

In a disposable cartridge, the amount of liquid contained is preferably kept small to minimize cost and size. Therefore, in the present invention, segments within the conduits may also be used to assist in cleaning and rinsing the conduits by passing the air-liquid interface of a segment over the sensor array or other region to be rinsed at least
once. It has been found that more efficient rinsing, using less fluid, is achieved by this method compared to continuous rinsing by a larger volume of fluid.

Restrictions within the conduits serve several purposes in the present invention. A capillary stop located between the sample holding chamber and first conduit is used to facilitate sample metering in the holding chamber by preventing displacement of the sample in the holding chamber until sufficient pressure is applied to overcome the resistance of the capillary stop. A restriction within the second conduit is used to divert wash fluid along an alternative pathway towards the waste chamber when the fluid reaches the constriction. Small holes in the gasket, together with a hydrophobic coating, are provided to prevent flow from the first conduit to the second conduit until sufficient pressure is applied. Features that control the flow of liquids within and between the conduits of the present invention are herein collectively termed valves.

One embodiment of the invention, therefore, provides a single-use cartridge with a sample holding chamber connected to a first conduit which contains an analyte sensor or array of analyte sensors. A second conduit, partly containing a fluid, is connected to the first conduit and air segments can be introduced into the fluid in the second conduit in order to segment it. Pump means are provided to displace the sample within the first conduit, and this displaces fluid from the second conduit into the first conduit. Thus, the sensor or sensors can be contacted first by a sample and then by a second fluid.

In another embodiment, the cartridge includes a closeable valve located between the first conduit and a waste chamber. This embodiment permits displacement of the fluid from the second conduit into the first conduit using only a single pump means connected to the first conduit. This embodiment further permits efficient washing of the conduits of the cartridge of the present invention, which is an important feature of a small single-use cartridge. In operation, the sample is displaced to contact the sensors, and is then displaced through the closeable valve into the waste chamber. Upon wetting, the closeable valve seals the opening to the waste chamber, providing an airtight seal that allows fluid in the second conduit to be drawn into contact with the sensors using only the pump means connected to the first conduit. In this embodiment, the closeable valve
permits the fluid to be displaced in this manner and prevents air from entering the first conduit from the waste chamber.

In another embodiment, both a closeable valve and means for introducing segments into the conduit are provided. This embodiment has many advantages, among which is the ability to reciprocate a segmented fluid over the sensor or array of sensors. Thus a first segment or set of segments is used to rinse a sensor, and then a fresh segment replaces it for taking measurements. Only one pump means (that connected to the first conduit) is required.

In another embodiment, analyte measurements are performed in a thin-film of liquid coating an analyte sensor. Such thin-film determinations are preferably performed amperometrically. This cartridge differs from the foregoing embodiments in having both a closeable valve that is sealed when the sample is expelled through the valve, and an air vent within the conduits that permits at least one air segment to be subsequently introduced into the measuring fluid, thereby increasing the efficiency with which the sample is rinsed from the sensor, and further permitting removal of substantially all the liquid from the sensor prior to measurement, and still further permitting segments of fresh liquid to be brought across the sensor to permit sequential, repetitive measurements for improved accuracy and internal checks of reproducibility.

In non-competitive assay embodiments, as discussed above, the analysis scheme for the detection of low concentrations of immunoactive analyte relies on the formation of an enzyme labeled antibody/analyte/surface-bound antibody "sandwich" complex, as discussed above. The concentration of analyte in a sample is converted into a proportional surface concentration of an enzyme. The enzyme is capable of amplifying the analyte's chemical signal by converting a substrate to a detectable product. For example, where alkaline phosphatase is the enzyme, a single enzyme molecule can produce about nine thousand detectable molecules per minute, providing several orders of magnitude improvement in the detectability of the analyte compared to schemes in which an electroactive species is attached to the antibody in place of alkaline phosphatase.
In immunosensor embodiments, it is advantageous to contact the sensor first with a sample and then with a wash fluid prior to recording a response from the sensor. In specific embodiments, in addition to being amended with an IgG-coated microparticle in order to reduce leukocyte interference, the sample is amended with an antibody-enzyme conjugate (signal antibody) that binds to the analyte of interest within the sample before the amended sample contacts the sensor. Binding reactions in the sample produce an analyte/antibody-enzyme complex. The sensor comprises an immobilized antibody to the analyte, attached close to an electrode surface. Upon contacting the sensor, the analyte/antibody-enzyme complex binds to the immobilized antibody near the electrode surface. It is advantageous at this point to remove from the vicinity of the electrode as much of the unbound antibody-enzyme conjugate as possible to minimize background signal from the sensor. The enzyme of the antibody-enzyme complex is advantageously capable of converting a substrate, provided in the fluid, to produce an electrochemically active species. This active species is produced close to the electrode and provides a current from a redox reaction at the electrode when a suitable potential is applied (amperometric operation). Alternatively, if the electroactive species is an ion, it can be measured potentiometrically. In amperometric measurements the potential may either be fixed during the measurement, or varied according to a predetermined waveform. For example, a triangular wave can be used to sweep the potential between limits, as is used in the well-known technique of cyclic voltammetry. Alternatively, digital techniques such as square waves can be used to improve sensitivity in detection of the electroactive species adjacent to the electrode. From the current or voltage measurement, the amount or presence of the analyte in the sample is calculated. These and other analytical electrochemical methods are well known in the art.

In embodiments in which the cartridge comprises an immunosensor, the immunosensor is advantageously microfabricated from a base sensor of an unreactive metal such as gold, platinum or iridium, and a porous permselective layer which is overlaid with a bioactive layer attached to a microparticle, for example latex particles. The microparticles are dispensed onto the porous layer covering the electrode surface, forming an adhered, porous bioactive layer. The bioactive layer has the property of binding specifically to the analyte of interest, or of manifesting a detectable change when
the analyte is present, and is most preferably an immobilized antibody directed against
the analyte.

Referring to the Figures, the cartridge of the present invention comprises a cover,
FIGS. 1 and 2, a base, FIG. 4, and a thin-film adhesive gasket, FIG. 3, disposed between
the base and the cover. Referring now to FIG. 1, the cover 1 is made of a rigid material,
preferably plastic, and capable of repetitive deformation at flexible hinge regions 5, 9, 10
without cracking. The cover comprises a lid 2, attached to the main body of the cover by
a flexible hinge 9. In operation, after introduction of a sample into the sample holding
chamber 34, the lid can be secured over the entrance to the sample entry port 4,
preventing sample leakage, and the lid is held in place by hook 3. The cover further
comprises two paddles 6, 7, that are moveable relative to the body of the cover, and
which are attached to it by flexible hinge regions 5, 10. In operation, when operated upon
by a pump means, paddle 6 exerts a force upon an air bladder comprised of cavity 43,
which is covered by thin-film gasket 21, to displace fluids within conduits of the
cartridge. When operated by a second pump means, paddle 7 exerts a force upon the
gasket 21, which can deform because of slits 22 cut therein. The cartridge is adapted for
insertion into a reading apparatus, and therefore has a plurality of mechanical and
electrical connections for this purpose. It should also be apparent that manual operation
of the cartridge is possible. Thus, upon insertion of the cartridge into a reading apparatus,
the gasket transmits pressure onto a fluid-containing foil pack filled with approximately
130 μL of analysis/wash solution ("fluid") located in cavity 42, rupturing the package
upon spike 38, and expelling fluid into conduit 39, which is connected via a short
transecting conduit in the base to the sensor conduit. The analysis fluid fills the front of
the analysis conduit first pushing fluid onto a small opening in the tape gasket that acts as
a capillary stop. Other motions of the analyzer mechanism applied to the cartridge are
used to inject one or more segments into the analysis fluid at controlled positions within
the analysis conduit. These segments are used to help wash the sensor surface and the
surrounding conduit with a minimum of fluid.
The cover further comprises a hole covered by a thin pliable film 8. In operation, pressure exerted upon the film expels one or more air segments into a conduit 20 through a small hole 28 in the gasket.

Referring to FIG. 2, the lower surface of the base further comprises second conduit 11, and first conduit 15. Second conduit 11 includes a constriction 12, which controls fluid flow by providing resistance to the flow of a fluid. Optional coatings 13, 14 provide hydrophobic surfaces, which together with gasket holes 31, 32, control fluid flow between second and first conduits 11, 15. A recess 17 in the base provides a pathway for air in conduit 34 to pass to conduit 34 through hole 27 in the gasket.

Referring to FIG. 3, thin-film gasket 21 comprises various holes and slits to facilitate transfer of fluid between conduits within the base and the cover and to allow the gasket to deform under pressure where necessary. Thus, hole 24 permits fluid to flow from conduit 11 into waste chamber 44; hole 25 comprises a capillary stop between conduits 34 and 15; hole 26 permits air to flow between recess 18 and conduit 40; hole 27 provides for air movement between recess 17 and conduit 34; and hole 28 permits fluid to flow from conduit 19 to waste chamber 44 via optional closeable valve 41. Holes 30 and 33 permit the plurality of electrodes that are housed within cutaways 35 and 37, respectively, to contact fluid within conduit 15. In a specific embodiment, cutaway 37 houses a ground electrode, and/or a counter-reference electrode, and cutaway 35 houses at least one analyte sensor and, optionally, a conductimetric sensor. In FIG. 3 the tape 21 is slit at 22 to allow the tape enclosed by the three cuts 22 to deform when the instrument applies a downward force to rupture the calibrant pouch within element 42 on the barb 38. The tape is also cut at 23 and this allows the tape to flex downwards into element 43 when the instrument provides a downward force, expelling air from chamber 43 and moving the sample fluid through conduit 15 towards the sensors. Element 29 in FIG. 3 acts as an opening in the tape connecting a region in the cover FIG. 2 with the base FIG. 4.

Referring to FIG. 4, conduit 34 is the sample holding chamber that connects the sample entry port 4 to first conduit 11 in the assembled cartridge. Cutaway 35 houses the
analyte sensor or sensors, or an analyte responsive surface, together with an optional conductimetric sensor or sensors. Cutaway 37 houses a ground electrode if needed as a return current path for an electrochemical sensor, and may also house an optional conductimetric sensor. Cutaway 36 provides a fluid path between gasket holes 31 and 32 so that fluid can pass between the first and second conduits. Recess 42 houses a fluid-containing package, e.g., a rupturable pouch, in the assembled cartridge that is pierced by spike 38 because of pressure exerted upon paddle 7 upon insertion into a reading apparatus. Fluid from the pierced package flows into the second conduit at 39. An air bladder is comprised of recess 43 which is sealed on its upper surface by gasket 21. The air bladder is one embodiment of a pump means, and is actuated by pressure applied to paddle 6 which displaces air in conduit 40 and thereby displaces the sample from sample chamber 34 into first conduit 15.

The location at which air enters the sample holding chamber (gasket hole 27) from the bladder, and the capillary stop 25, together define a predetermined volume of the sample holding chamber. An amount of the sample corresponding to this volume is displaced into the first conduit when paddle 6 is depressed. This arrangement is therefore one possible embodiment of a metering means for delivering a metered amount of an unmetered sample into the conduits of the cartridge.

In the present cartridge, a means for metering a sample segment is provide in the base plastic part. The segment size is controlled by the size of the compartment in the base and the position of the capillary stop and air pipe holes in the tape gasket. This volume can be readily varied from 2 to 200 μL. Expansion of this range of sample sizes is possible within the context of the present invention.

The fluid is pushed through a pre-analytical conduit 11 that can be used to amend a reagent (e.g., particles, soluble molecules, or the IgM or fragments thereof) into the sample prior to its presentation at the sensor conduit 19. Alternatively, the amending reagent may be located in portion 15, beyond portion 16. Pushing the sample through the pre-analytical conduit also serves to introduce tension into the diaphragm pump paddle 7 which improves its responsiveness for actuation of fluid displacement.
In some assays, metering is advantageous if quantification of the analyte is required. A waste chamber is provided, 44, for sample and/or fluid that is expelled from the conduit, to prevent contamination of the outside surfaces of the cartridge. A vent connecting the waste chamber to the external atmosphere is also provided, 45. One desirable feature of the cartridge is that once a sample is loaded, analysis can be completed and the cartridge discarded without the operator or others contacting the sample.

Referring now to FIG. 5, a schematic diagram of the features of a cartridge and components is provided, wherein 51-57 are portions of the conduits and sample chamber that can optionally be coated with dry reagents to amend a sample or fluid. The sample or fluid is passed at least once over the dry reagent to dissolve it. Reagents used to amend the sample may include one or more of the following: antibody-enzyme conjugates (signal antibodies), IgM and/or fragments thereof, IgG and/or fragments thereof, and other blocking agents that prevent either specific or non-specific binding reactions among assay compounds, and/or the above-described IgG-coated microparticles for reducing leukocyte interference. A surface coating that is not soluble but helps prevent non-specific adsorption of assay components to the inner surfaces of the cartridges can also be provided.

In specific embodiments, a closeable valve is provided between the first conduit and the waste chamber. In one embodiment, this valve, 58, is comprised of a dried sponge material that is coated with an impermeable substance. In operation, contacting the sponge material with the sample or a fluid results in swelling of the sponge to fill the cavity 41 (FIG. 4), thereby substantially blocking further flow of liquid into the waste chamber 44. Furthermore, the wetted valve also blocks the flow of air between the first conduit and the waste chamber, which permits the first pump means connected to the sample chamber to displace fluid within the second conduit, and to displace fluid from the second conduit into the first conduit in the following manner.

Referring now to FIG. 6, which illustrates the schematic layout of an immuno-sensor cartridge, there are provided three pumps, 61-63. While these pumps have
been described in terms of specific embodiments, it will be readily understood that any 
pumping device capable of performing the respective functions of pumps 61-63 may be 
used within the present invention. Thus, pump 1, 61, should be capable of displacing the 
sample from the sample holding chamber into the first conduit; pump 2, 62, should be 
capable of displacing fluid within the second conduit; and pump 3, 63, should be capable 
of inserting at least one segment into the second conduit. Other types of pumps that are 
evised in the present application include, but are not limited to, an air sac contacting a 
pneumatic means whereby pressure is applied to the air sac, a flexible diaphragm, a 
piston and cylinder, an electrodynamic pump, and a sonic pump. With reference to pump 
3, 63, the term "pump" includes all devices and methods by which one or more segments 
are inserted into the second conduit, such as a pneumatic means for displacing air from an 
air sac, a dry chemical that produces a gas when dissolved, or a plurality of electrolysis 
electrodes operably connected to a current source. In a specific embodiment, the segment 
is produced using a mechanical segment generating diaphragm that may have more than 
one air bladder or chamber. As shown, the well 8 has a single opening which connects the 
inner diaphragm pump and the fluid filled conduit into which a segment is to be injected 
20. The diaphragm can be segmented to produce multiple segments, each injected in a 
specific location within a fluid filled conduit. In FIG. 6, element 64 indicates the region 
where the immunosensor performs the capture reaction to form a sandwich comprising 
the immobilized antibody, the analyte and the signal antibody.

In alternative embodiments, a segment is injected using a passive feature. A well 
in the base of the cartridge is sealed by the tape gasket. The tape gasket covering the well 
has two small holes on either end. One hole is open while the other is covered with a 
filter material which wets upon contact with a fluid. The well is filled with a loose 
hydrophilic material such as a cellulose fiber filter, paper filter or glass fiber filter. This 
hydrophilic material draws the liquid into the well in the base via capillary action, 
placing the air that was formerly in the well. The air is expelled through the opening in 
the tape gasket creating a segment whose volume is determined by the volume of the well 
and the void volume of the loose hydrophilic material. The filter used to cover one of the 
inlets to the well in the base can be chosen to meter the rate at which the fluid fills the 
well and thereby control the rate at which the segment is injected into the conduit in the
cover. This passive feature permits any number of controlled segments to be injected at specific locations within a fluid path and requires a minimum of space.

Based on the present disclosure it is apparent the present method provides a way of reducing or eliminating interference from leukocytes in an analyte immunoassay where a sample, e.g., whole blood sample, is first collected and then amended by dissolving a dry reagent comprising sacrificial beads into the sample. Preferably, the kit or method includes sufficient sacrificial beads to provide an excess of beads with respect to leukocytes in a blood sample. This yields a sample with a dissolved sacrificial bead concentration of at least 5 micrograms per microliter of sample, e.g., at least 10 micrograms per microliter of sample, or at least 15 micrograms per microliter of sample, which is sufficient to substantially engage any leukocytes in the sample. In terms of ranges, the dry reagent preferably dissolves into the sample to give a sacrificial bead concentration of from about 5 micrograms to about 40 micrograms beads per microliter of sample, preferably from about 10 to about 20 micrograms beads per microliter of sample. Depending on the size of the beads, this corresponds to at least about $10^4$ beads per microliter of sample, at least about $10^5$ beads per microliter of sample, or approximately from about $10^5$ to about $10^6$ beads per microliter of sample. Thus, in some preferred embodiments, the sacrificial beads are present in an amount sufficient to provide a dissolved sacrificial bead concentration of at least $10^4$ beads per microliter of sample, e.g., at least about $10^5$ beads per microliter of sample, or from about $10^5$ to about $10^6$ beads per microliter of sample.

Once this step is completed, it is possible to perform an immunoassay, e.g., an electrochemical immunoassay, on the amended sample to determine the concentration of an analyte.

Note that the dissolution of the dry reagent and the sandwich formation step can occur concurrently or in a stepwise manner. The method is directed mainly to analytes that are cardiovascular markers, e.g., Tnl, TnT, CKMB, myoglobin, BNP, NT-proBNP, and proBNP, but can also be used for other markers such as, for example, beta-HCG, TSH, myeloperoxidase, myoglobin, D-dimer, CRP, NGAL and PSA. To ensure that the
majority of the leukocytes are sequestered before the detection step, it is preferable that
the sample amendment step is for a selected predetermined period in the range of about 1
minute to about 30 minutes.

The method is preferably performed in a cartridge comprising an immunosensor,
a conduit, a sample entry port and a sample holding chamber, where at least a portion of
at least one of these elements is coated with the dry reagent. Note that the dry reagent
can include one or more of: sacrificial beads for reducing leukocyte interference, buffer,
salt, surfactant, stabilizing agent, a simple carbohydrate, a complex carbohydrate and
various combinations. In addition the dry reagent can also include an enzyme-labeled
antibody (signal antibody) to the analyte.

As suggested above, in addition to or instead of coating the sacrificial beads using
whole IgG molecules, where the individual monomers are formed from an Fc region
attached to a F(ab')2 region, which in turn comprises two Fab regions, it is also possible
to use fragments of IgG. IgG fragmentation can be achieved variously using
combinations of disulphide bond reduction (-S-S- to -SH HS-) and enzymatic pepsin or
papain digestion, to create some combination of F(ab')2 fragments, Fab fragments, and/or
Fc fragments. These fragments can be separated for use separately by chromatography, or
used in combination. For example, where the blocking site is on the Fc fragment, this
can be used instead of the whole IgG molecule. The same applies to the Fab fragment
and the F(ab')2 fragment.

In the actual assay step, it is preferred that once the sandwich is formed between
the immobilized and signal antibodies, the sample medium is subsequently washed to a
waste chamber, followed by exposing the sandwich to a substrate capable of reacting
with an enzyme to form a product capable of electrochemical detection. The preferred
format is an electrochemical enzyme-linked immunosorbent assay.

Preferably, the device is one that performs an immunoassay of an analyte in a
sample, e.g., blood sample, with reduced interference from leukocytes. The device is a
housing with an electrochemical immunosensor, a conduit and a sample entry port, where
the conduit permits the sample to pass from the entry port to the immunosensor in a
controlled manner. In one aspect, at least a portion of the housing is coated with a dry reagent which can comprise non-human IgG-coated sacrificial beads. The important feature is that the dry reagent is capable of dissolving into the sample and engaging leukocytes in binding and preferably phagocytosis. This is generally sufficient to sequester potentially interfering leukocytes in the sample. In a preferred embodiment, the device also comprises an immuno-reference sensor. The immunosensor is preferably directed to detect a cardiovascular marker, e.g., analytes such as Tnl, TnT, CKMB, myoglobin, BNP, NT-proBNP, and proBNP. The system in which the device operates generally allows the sample to remain in contact with the reagent for a predetermined period, e.g., from 1 to 30 minutes. Preferably the device is a single-use cartridge, e.g., filled with a single sample, used once for the test and then discarded. Generally, the device includes a wash fluid capable of washing the sample to a waste chamber, and a substrate capable of reacting with the enzyme sandwich at the immunosensor to form a product suitable for electrochemical detection.

More broadly the invention relates to reducing interference from leukocytes in an analyte immunoassay for any biological sample where leukocytes are generally present. Furthermore, performing an immunoassay on the amended sample to determine the concentration of the selected analyte can be based on various techniques including electrochemical ones, e.g., amperometric and potentiometric, and also optical ones, e.g., absorbance, fluorescence and luminescence.

While the present invention has been described in the context of a BNP test cartridge, it is equally applicable to any immunoassay where leukocytes are present and can be the cause of interference. For example it can be in the form of a kit for performing an immunoassay for an analyte suspected of being present in a blood sample where the kit comprises sacrificial beads opsonized to leukocytes, an immobilized first antibody to the analyte and a second labeled antibody to the analyte. In addition a current immunoassay format known in the art may be modified to include the sacrificial beads, for example by adding the beads in a sample pre-treatment step. This pretreatment may be accomplished by incorporating the sacrificial beads in a blood collection device, in a
separate vessel, or may take place in the analytical (immunoassay) device itself by incorporation of the sacrificial beads in the test cycle of the device.

The method or kit is not limited to BNP but can be adapted to any immunoassay, including but not limited to proBNP, NTproBNP, cTnl, TnT, HCG, TSH, PSA, D-dimer, CRP, myoglobin, NGAL, CKMB and myeloperoxidase. Furthermore the method and kit is applicable to assays where the sacrificial beads are coated with any non-human IgG or a fragment thereof, including murine, caprine, bovine and lupine, and alternatively sacrificial beads coated with an activated human IgG or fragment thereof. The sacrificial beads may comprise substrate beads coated with a material or fragment thereof selected from a protein, a bacterium, a virus and a xenobiotic, or may be afforded by dormant or otherwise stabilized bacterial cells, spores or fragment thereof, e.g. E. coli, optionally without substrate beads.

While the preferred assay described above use an immobilized first antibody attached to an assay bead which is in turn attached to a porous layer with an underlying electrode, the first antibody may be immobilized directly onto an electrode or any other surface, or immobilized on a soluble bead.

The kit or method can comprise a second labeled antibody that is in the form of a dissolvable dry reagent that includes the opsonized sacrificial beads as part of the dissolvable dry reagent, or where the two are in separate dry reagent locations. Note that both the immobilized and labeled antibodies can be monoclonal, polyclonal, fragments thereof and combinations thereof. In addition, the second antibody can be labeled with various labels including a radionlabel, enzyme, chromophore, fluorophore, chemiluminescent species and other known in the immunoassay art. Where the second antibody is labeled with an enzyme, it is preferably ALP, horseradish peroxidase, or glucose oxidase.

The kit or method is applicable to any sample containing leukocytes, e.g. whole blood, and can be a blood sample amended with an anticoagulant, e.g., EDTA, heparin, fluoride, citrate and the like.
Where the method or kit is used to perform a non-competitive immunoassay there may be a sequence of mixing steps including: (i) mixing a blood sample suspected of containing an analyte with opsonized sacrificial beads; (ii) mixing the blood sample with an immobilized first antibody to the analyte and forming a complex between the immobilized antibody and said analyte; and (iii) mixing the blood sample with a labeled second antibody to form a complex with said analyte and said immobilized antibody. Note that these mixing steps can be performed at the same time or in an ordered sequence. For example, steps (ii) and (iii) may occur at the same time, or steps (i) and (iii) may be performed before step (ii). In the final step there is a determination of the amount of complex formed between the immobilized first antibody, the analyte and the labeled second antibody.

The present method is particularly directed to substantially ameliorating white blood cell accumulation on an analyte immunosensor made from antibody-coated assay beads to the analyte that are immobilized on an electrode. After mixing a sample suspected of containing an analyte with opsonized sacrificial beads to form an amended sample where white blood cells in the sample preferentially seek to phagocytose the sacrificial beads, the amended sample is then contacted with the immunosensor. As a result there is minimal accumulation of white cells on the assay beads and phagocytosis of the assay beads, and a reliable assay may be achieved.

The present method is directed to performing an immunoassay for an analyte suspected of being present in a blood sample comprising: mixing a blood sample suspected of containing an analyte with an excess of opsonized sacrificial beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads; contacting the amended sample with an immunosensor comprising antibody-coated beads to the analyte immobilized on an electrode; forming a sandwich between said antibody-coated bead, said analyte and a second labeled antibody; washing said blood sample from said immunosensor; and determining the amount of said sandwiched label with said immunosensor and relating the amount of said label to the concentration of the analyte in the sample.
The present method is also directed to performing an immunoassay for an analyte suspected of being present in a blood sample comprising: mixing a blood sample suspected of containing an analyte with an excess of opsonized sacrificial beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads; contacting the amended sample with antibody-coated beads to the analyte; forming a sandwich between said antibody-coated bead, said analyte and a second labeled antibody; washing said blood sample from said antibody-coated beads; and determining the amount of said sandwiched label and relating the amount of said label to the concentration of the analyte in the sample.

The present invention is also directed to a test cartridge for performing an immunoassay for an analyte suspected of being present in a blood sample comprising: an immunosensor in a conduit wherein said immunosensor having an immobilized first antibody to the analyte. In this embodiment, the conduit preferably has a dry reagent coating or separate coatings comprising sacrificial beads opsonized to leukocytes and a second labeled antibody to said analyte. In operation, the dry reagent dissolves into said blood sample.

The present invention will be better understood in view of the following non-limiting Examples.

**EXAMPLE 1**

FIG. 7 illustrates the principle of an amperometric immunoassay according to specific embodiments of related pending US application 12/41 1,325 for determining the presence and amount of troponin I (TnI), a marker of cardiac necrosis. A blood sample was introduced into the sample holding chamber of a cartridge and was amended by dissolution of a dry reagent coated into the sample holding chamber. The dry reagent includes IgM 77, which upon dissolution into the sample selectively binds to complementary heterophile antibodies 78 that may be contained in the sample. As
shown, the dry reagent also comprises IgG 79, which also selectively binds to complementary antibodies 78 after dissolution into the sample.

FIG 10 illustrates the principle of an amperometric immunoassay according to specific embodiments of the present inventions for determining the presence and amount of a marker of cardiac function, e.g., BNP and Tnl. A blood sample was introduced into the sample holding chamber of a cartridge and was amended by dissolution of a dry reagent coated into the sample holding chamber. The dry reagent includes sacrificial beads 102, which upon dissolution into the sample selectively bind to leukocytes 103 that may be contained in the sample. Note that the dry reagent may also and preferably comprises IgM and IgG as described for FIG 7.

In addition, FIGS. 7 and 10 show a conjugate molecule comprising alkaline phosphatase enzyme (AP) covalently attached to a signal antibody 71, e.g. polyclonal anti-troponin I antibody, also was dissolved into the sample. This conjugate specifically binds to the analyte 70, e.g., Tnl or BNP, in the blood sample producing a complex made up of analyte bound to the AP conjugate. In a capture step, this complex binds to the capture antibody 72 (immobilized antibody) attached on, or close to, the immunosensor. The sensor chip has a conductivity sensor, which is used to monitor when the sample reaches the sensor chip. The time of arrival of the fluid can be used to detect leaks within the cartridge: a delay in arrival signals a leak. The position of the sample segment within the sensor conduit can be actively controlled using the edge of the fluid as a position marker. As the sample/air interface crosses the conductivity sensor, a precise signal is generated which can be used as a fluid marker from which controlled fluid excursions can be executed. The fluid segment is preferentially oscillated edge-to-edge over the sensor in order to present the entire sample to the immunosensor surface. A second reagent can be introduced in the sensor conduit beyond the sensor chip, which becomes homogenously distributed during the fluid oscillations.

The sensor chip contains a capture region or regions coated with antibodies for the analyte of interest. These capture regions are defined by a hydrophobic ring of polyimide or another photolithographically produced layer. A microdroplet or several
microdroplets (approximately 5 to 40 nanoliters in size) containing antibodies in some form, for example bound to latex microspheres, is dispensed on the surface of the sensor or on a permselective layer on the sensor. The photodefmed ring contains this aqueous droplet allowing the antibody coated region to be localized to a precision of a few microns. The capture region can be made from 0.03 to roughly 2 square millimeters in size. The upper end of this size is limited by the size of the conduit and sensor in present embodiments, and is not a limitation of the invention.

Thus, the gold electrode 74 is coated with a biolayer 73, e.g., a covalently attached anti-troponin I antibody, to which the Tnl/AP-aTnl complex binds. AP is thereby immobilized close to the electrode in proportion to the amount of analyte initially present in the sample. In addition to specific binding, the enzyme-antibody conjugate may bind non-specifically to the sensor. Non-specific binding provides a background signal from the sensor that is undesirable and preferably is minimized. As described above, the rinsing protocols, and in particular the use of segmented fluid to rinse the sensor, provide efficient means to minimize this background signal. In a second step subsequent to the rinsing step, a substrate 75 that is hydrolyzed by, for example, alkaline phosphatase to produce an electroactive product 76 is presented to the sensor. In specific embodiments the substrate is comprised of a phosphorylated ferrocene or p-aminophenol. The amperometric electrode is either poised at a fixed electrochemical potential sufficient to oxidize or reduce a product of the hydrolyzed substrate but not the substrate directly, or the potential is swept one or more times through an appropriate range. Optionally, a second electrode may be coated with a layer where the complex of analyte/AP anti-analyte, e.g., Tnl/AP-aTnl, is made during manufacture to act as a reference sensor or calibration means for the measurement.

In the present example, the sensor comprises two amperometric electrodes which are used to detect the enzymatically produced 4-aminophenol from the reaction of 4-aminophenylphosphate with the enzyme label alkaline phosphatase. The electrodes are preferably produced from gold surfaces coated with a photodefmed layer of polyimide. Regularly spaced opening in the insulating polyimide layer define a grid of small gold electrodes at which the 4-aminophenol is oxidized in a two electron per molecule
reaction. Sensor electrodes further comprise a biolayer, while reference electrodes can be constructed, for example, from gold electrodes lacking a biolayer, or from silver electrodes, or other suitable material. Different biolayers can provide each electrode with the ability to sense a different analyte.

Substrates, such as p-aminophenol species, can be chosen such that the $E(l/2)$ of the substrate and product differ substantially. Preferably, the voltammetric half-wave potential $E(l/2)$ of the substrate is substantially higher (more positive) than that of the product. When the condition is met, the product can be selectively electrochemically measured in the presence of the substrate.

The size and spacing of the electrode play an important role in determining the sensitivity and background signal. The important parameters in the grid are the percentage of exposed metal and the spacing between the active electrodes. The position of the electrode can be directly underneath the antibody capture region or offset from the capture region by a controlled distance. The actual amperometric signal of the electrodes depends on the positioning of the sensors relative to the antibody capture site and the motion of the fluid during the analysis. A current at the electrode is recorded that depends upon the amount of electroactive product in the vicinity of the sensor.

The detection of alkaline phosphatase activity in this example relies on a measurement of the 4-aminophenol oxidation current. This is achieved at a potential of about +60 mV versus the Ag/AgCl ground chip. The exact form of detection used depends on the sensor configuration. In one version of the sensor, the array of gold microelectrodes is located directly beneath the antibody capture region. When the analysis fluid is pulled over this sensor, enzyme located on the capture site converts the 4-aminophenylphosphate to 4-aminophenol in an enzyme limited reaction. The concentration of the 4-aminophenylphosphate is selected to be in excess, e.g., 10 times the $K_m$ value. The analysis solution is 0.1 M in diethanolamine, 1.0 M NaCl, buffered to a pH of 9.8. Additionally, the analysis solution contains 0.5 mM MgCl$_2$, which is a cofactor for the enzyme. Alternatively, a carbonate buffer has the desired properties.
In another electrode geometry embodiment, the electrode is located a few hundred microns away from the capture region. When a fresh segment of analysis fluid is pulled over the capture region, the enzyme product builds with no loss due to electrode reactions. After a time, the solution is slowly pulled from the capture region over the detector electrode resulting in a current spike from which the enzyme activity can be determined.

An important consideration in the sensitive detection of alkaline phosphatase activity is the non-4-aminophenol current associated with background oxidations and reductions occurring at the gold sensor. Gold sensors tend to give significant oxidation currents in basic buffers at these potentials. The background current is largely dependent on the buffer concentration, the area of the gold electrode (exposed area), surface pretreatments and the nature of the buffer used. Diethanolamine is a particularly good activating buffer for alkaline phosphatase. At molar concentrations, the enzymatic rate is increased by about three times over a non-activating buffer such as carbonate.

In alternative embodiments, the enzyme conjugated to an antibody or other analyte-binding molecule is urease, and the substrate is urea. Ammonium ions produced by the hydrolysis of urea are detected in this embodiment by the use of an ammonium sensitive electrode. Ammonium-specific electrodes are well-known to those of skill in the art. A suitable microfabricated ammonium ion-selective electrode is disclosed in U.S. Pat. No. 5,200,051, incorporated herein by reference. Other enzymes that react with a substrate to produce an ion are known in the art, as are other ion sensors for use therewith. For example, phosphate produced from an alkaline phosphatase substrate can be detected at a phosphate ion-selective electrode.

Referring now to FIG. 8, there is illustrated the construction of an embodiment of a microfabricated immunosensor. Preferably a planar non-conducting substrate 80 is provided onto which is deposited a conducting layer 81 by conventional means or microfabrication known to those of skill in the art. The conducting material is preferably a noble metal such as gold or platinum, although other unreactive metals such as iridium may also be used, as may non-metallic electrodes of graphite, conductive polymer, or
other materials. An electrical connection 82 is also provided. A biolayer 83 is deposited onto at least a portion of the electrode. In the present disclosure, a biolayer means a porous layer comprising on its surface a sufficient amount of a molecule 84 that can either bind to an analyte of interest, or respond to the presence of such analyte by producing a change that is capable of measurement. Optionally, a permselective screening layer may be interposed between the electrode and the biolayer to screen electrochemical interferents as described in U.S. Pat. No. 5,200,051.

In specific embodiments, a biolayer is constructed from latex beads of specific diameter in the range of about 0.001 to 50 microns. The beads are modified by covalent attachment of any suitable molecule consistent with the above definition of a biolayer. Many methods of attachment exist in the art, including providing amine reactive N-hydroxysuccinimide ester groups for the facile coupling of lysine or N-terminal amine groups of proteins. In specific embodiments, the biomolecule is chosen from among ionophores, cofactors, polypeptides, proteins, glycopeptides, enzymes, immunoglobulins, antibodies, antigens, lectins, neurochemical receptors, oligonucleotides, polynucleotides, DNA, RNA, or suitable mixtures. In most specific embodiments, the biomolecule is an antibody selected to bind one or more of human chorionic gonadotrophin, troponin I, troponin T, troponin C, a troponin complex, creatine kinase, creatine kinase subunit M, creatine kinase subunit B, myoglobin, myosin light chain, or modified fragments of these. Such modified fragments are generated by oxidation, reduction, deletion, addition or modification of at least one amino acid, including chemical modification with a natural moiety or with a synthetic moiety. Preferably, the biomolecule binds to the analyte specifically and has an affinity constant for binding analyte ligand of about 10^7 to 10^15 M.

In one embodiment, the biolayer, comprising beads having surfaces that are covalently modified by a suitable molecule, is affixed to the sensor by the following method. A microdispensing needle is used to deposit onto the sensor surface a small droplet, preferably about 20 nL, of a suspension of modified beads. The droplet is permitted to dry, which results in a coating of the beads on the surface that resists displacement during use.
In addition to immuno sensors in which the biolayer is in a fixed position relative to an amperometric sensor, the present invention also envisages embodiments in which the biolayer is coated upon particles, e.g., assay beads, that are mobile. The cartridge can contain mobile microparticles capable of interacting with an analyte, for example magnetic particles that are localized to an amperometric electrode subsequent to a capture step, whereby magnetic forces are used to concentrate the particles at the electrode for measurement. One advantage of mobile microparticles in the present invention is that their motion in the sample or fluid accelerates binding reactions, making the capture step of the assay faster. For embodiments using non-magnetic mobile microparticles, a porous filter is used to trap the beads at the electrode. Note that with respect to the sacrificial beads of the present invention, where the assay beads are magnetic, the sacrificial beads are preferably non-magnetic and sequestered separately. In addition, where the assay beads are non-magnetic, the sacrificial beads are preferably magnetic and sequestered separately.

Referring now to FIG. 9, there is illustrated a mask design for several electrodes upon a single substrate. By masking and etching techniques, independent electrodes and leads can be deposited. Thus, a plurality of immuno sensors, 94 and 96, and conductimetric sensors, 90 and 92, are provided in a compact area at low cost, together with their respective connecting pads, 91, 93, 95, and 97, for effecting electrical connection to the reading apparatus. In principle, a very large array of sensors can be assembled in this way, each sensitive to a different analyte or acting as a control sensor or reference immuno sensor.

Specifically, immuno sensors may be prepared as follows. Silicon wafers are thermally oxidized to form approximately a 1 micron insulating oxide layer. A titanium/tungsten layer is sputtered onto the oxide layer to a preferable thickness of between 100 to 1000 Angstroms, followed by a layer of gold that is most preferably 800 Angstroms thick. Next, a photoresist is spun onto the wafer and is dried and baked appropriately. The surface is then exposed using a contact mask, such as a mask corresponding to that illustrated in FIG. 9. The latent image is developed, and the wafer is exposed to a gold-etchant. The patterned gold layer is coated with a photodefinable
polyimide, suitably baked, exposed using a contact mask, developed, cleaned in an \( \text{O}_2 \) plasma, and preferably imidized at 350°C for 5 hours. An optional metallization of the back side of the wafer may be performed to act as a resistive heating element, where the immunosensor is to be used in a thermostatted format. The surface is then printed with antibody-coated particles. Droplets, preferably of about 20 nL volume and containing 1% solid content in deionized water, are deposited onto the sensor region and are dried in place by air drying. Optionally, an antibody stabilization reagent (supplied by SurModica Corp. or AET Ltd) is overcoated onto the sensor.

Drying the particles causes them to adhere to the surface in a manner that prevents dissolution in either sample or fluid containing a substrate. This method provides a reliable and reproducible immobilization process suitable for manufacturing sensor chips in high volume.

**EXAMPLE 2**

With respect to the method of use of a cartridge, an unmetered fluid sample is introduced into sample holding chamber 34 of a cartridge, through sample entry port 4. Capillary stop 25 prevents passage of the sample into conduit 15 at this stage, and holding chamber 34 is filled with the sample. Lid 2 or element 200 is closed to prevent leakage of the sample from the cartridge. The cartridge is then inserted into a reading apparatus, such as that disclosed in U.S. Pat. No. 5,821,399 to Zelin, which is hereby incorporated by reference. Insertion of the cartridge into a reading apparatus activates the mechanism which punctures a fluid-containing package located at 42 when the package is pressed against spike 38. Fluid is thereby expelled into the second conduit, arriving in sequence at 39, 20, 12 and 11. The constriction at 12 prevents further movement of fluid because residual hydrostatic pressure is dissipated by the flow of fluid via second conduit portion 11 into the waste chamber 44. In a second step, operation of a pump means applies pressure to air bladder 43, forcing air through conduit 40, through cutaways 17 and 18, and into conduit 34 at a predetermined location 27. Capillary stop 25 and location 27 delimit a metered portion of the original sample. While the sample is within sample holding chamber 34, it is amended with the dry reagent coating comprising
sacrificial beads and other materials on the inner surface of the chamber. The metered portion of the sample is then expelled through the capillary stop by air pressure produced within air bladder 43. The sample passes into conduit 15 and into contact with the analyte sensor or sensors located within cutaway 35.

In embodiments employing an immunosensor located within cutout 35, the sample is amended prior to arriving at the sensor by, for example, an enzyme-antibody conjugate (signal antibody). To promote efficient binding of the analyte to the sensor, the sample containing the analyte is optionally passed repeatedly over the sensor in an oscillatory motion. Preferably, an oscillation frequency of between about 0.2 and 2 Hz is used, most preferably 0.7 Hz. Thus, the signal enzyme associated with the signal antibody is brought into close proximity to the amperometric electrode surface in proportion to the amount of analyte present in the sample.

Once an opportunity for the analyte/enzyme-antibody conjugate complex to bind to the immunosensor has been provided, the sample is ejected by further pressure applied to air bladder 43, and the sample passes to waste chamber 44. A wash step next removes non-specifically bound enzyme-conjugate and sacrificial beads from the sensor chamber. Fluid in the second conduit is moved by a pump means 43, into contact with the sensors. The analysis fluid is pulled slowly until the first air segment is detected at a conductivity sensor.

The air segment or segments can be produced within a conduit by any suitable means, including but not limited to: (1) passive means, as shown in FIG. 14 and described below; (2) active means including a transient lowering of the pressure within a conduit using a pump whereby air is drawn into the conduit through a flap or valve; or (3) by dissolving a compound pre-positioned within a conduit that liberates a gas upon contacting fluid in the conduit, where such compound may include a carbonate, bicarbonate or the like. This segment is extremely effective at clearing the sample-contaminated fluid from conduit 15. The efficiency of the rinsing of the sensor region is greatly enhanced by the introduction of one or more air segments into the second conduit as described. The leading and/or trailing edges of air segments are passed one or more
times over the sensors to rinse and re-suspend extraneous material that may have been
deposited from the sample. Extraneous material includes any material other than
specifically bound analyte or analyte/antibody-enzyme conjugate complex. However, it
is an object of the invention that the rinsing is not sufficiently protracted or vigorous as to
promote dissociation of specifically bound analyte or analyte/antibody-enzyme conjugate
complex from the sensor.

A second advantage of introducing air segments into the fluid is to segment the
fluid. For example, after a first segment of the fluid is used to rinse a sensor, a second
segment is then placed over the sensor with minimal mixing of the two segments. This
feature further reduces background signal from the sensor by more efficiently removing
unbound antibody-enzyme conjugate. After the front edge washing, the analysis fluid is
pulled slowly until the first air segment is detected at a conductivity sensor. This
segment is extremely effective at clearing the sample-contaminated fluid which was
mixed in with the first analysis fluid sample. For measurement, a new portion of fluid is
placed over the sensors, and the current or potential, as appropriate to the mode of
operation, is recorded as a function of time.

EXAMPLE 3

Referring now to FIG. 15, there is shown a top view of an immunosensor
cartridge. Cartridge 150 comprises a base and a top portion, preferably constructed of a
plastic. The two portions are connected by a thin, adhesive gasket or thin pliable film.
As in previous embodiments, the assembled cartridge comprises a sample holding
chamber 151 into which a sample containing an analyte of interest is introduced via a
sample inlet 167. A metered portion of the sample is delivered to the sensor chip 153, via
the sample conduit 154 (first conduit) as before by the combined action of a capillary
stop 152, preferably formed by a 0.012 inch (0.3 mm) laser cut hole in the gasket or film
that connects the two portions of the cartridge, and an entry point 155 located at a
predetermined point within the sample holding chamber whereby air introduced by the
action of a pump means, such as a paddle pushing upon a sample diaphragm 156. After
contacting the sensor to permit binding to occur, the sample is moved to vent 157, which
contains a wicking material that absorbs the sample and thereby seals the vent closed to
the further passage of liquid or air. The wicking material is preferably a cotton fiber
material, a cellulose material, or other hydrophilic material having pores. It is important
in the present application that the material is sufficiently absorbent (i.e., possesses
sufficient wicking speed) that the valve closes within a time period that is commensurate
with the subsequent withdrawal of the sample diaphragm actuating means described
below, so that sample is not subsequently drawn back into the region of the sensor chip.

As in the specific embodiment shown, there is provided a wash conduit (second
conduit) 158, connected at one end to a vent 159 and at the other end to the sample
conduit at a point 160 of the sample conduit that is located between vent 157 and sensor
chip 153. Upon insertion of the cartridge into a reading apparatus, a fluid is introduced
into conduit 158. Preferably, the fluid is present initially within a foil pouch 161 that is
punctured by a pin when an actuating means applies pressure upon the pouch. There is
also provided a short conduit 162 that connects the fluid to conduit 154 via a small
opening in the gasket 163. A second capillary stop initially prevents the fluid from
reaching capillary stop 160, so that the fluid is retained within conduit 158.

After vent 157 has closed, the pump is actuated, creating a lowered pressure
within conduit 154. Air vent 164, preferably comprising a small flap cut in the gasket or
a membrane that vibrates to provide an intermittent air stream, provides a means for air to
enter conduit 158 via a second vent 165. The second vent 165 preferably also contains
wicking material capable of closing the vent if wetted, which permits subsequent
depression of sample diaphragm 156 to close vent 165, if required. Simultaneously with
the actuation of sample diaphragm 156, fluid is drawn from conduit 158, through
capillary stop 160, into conduit 154. Because the flow of fluid is interrupted by air
entering vent 164, at least one air segment (a segment or stream of segments) is
introduced.

Further withdrawal of sample diaphragm 156 draws the liquid containing at least
one air segment back across the sensing surface of sensor chip 153. The presence of air-
liquid boundaries within the liquid enhances the rinsing of the sensor chip surface to
remove remaining sample. Preferably, the movement of the sample diaphragm 156 is controlled in conjunction with signals received from the conductivity electrodes housed within the sensor chip adjacent to the analyte sensors. In this way, the presence of liquid over the sensor is detected, and multiple readings can be performed by movement of the fluid in discrete steps.

It is advantageous in this embodiment to perform analyte measurements when only a thin film of fluid coats the sensors, ground chip 165, and a contiguous portion of the wall of conduit 154 between the sensors and ground electrode. A suitable film is obtained by withdrawing fluid by operation of the sample diaphragm 156, until the conductimetric sensor located next to the sensor indicates that bulk fluid is no longer present in that region of conduit 154. It has been found that measurement can be performed at very low (nA) currents, the potential drop that results from increased resistance of a thin film between ground chip and sensor chip (compared to bulk fluid), is not significant.

The ground chip 165 is preferably silver/silver chloride. It is advantageous, to avoid air segments, which easily form upon the relatively hydrophobic silver chloride surface, to pattern the ground chip as small regions of silver/silver chloride interspersed with more hydrophilic regions, such as a surface of silicon dioxide. Thus, a preferred ground electrode configuration comprises an array of silver/silver chloride squares densely arranged and interspersed with silicon dioxide. There is a further advantage in the avoidance of unintentional segments if the regions of silver/silver chloride are somewhat recessed.

Referring now to FIG. 16, there is shown a schematic view of the fluidics of the preferred embodiment of an immunosensor cartridge. Regions R1-R7 represent specific regions of the conduits associated with specific operational functions. Thus R1 represents the sample holding chamber; R2 the sample conduit whereby a metered portion of the sample is transferred to the capture region, and in which the sample is optionally amended with a substance coated upon the walls of the conduit; R3 represents the capture region, which houses the conductimetric and analyte sensors; R4 and R5 represent
portions of the first conduit that are optionally used for further amendment of fluids with substances coated onto the conduit wall, whereby more complex assay schemes are achieved; R6 represents the portion of the second conduit into which fluid is introduced upon insertion of the cartridge into a reading apparatus; R7 comprises a portion of the conduit located between capillary stops 160 and 166, in which further amendment can occur; and R8 represents the portion of conduit 154 located between point 160 and vent 157, and which can further be used to amend liquids contained within.

EXAMPLE 4

With regard to the coordination of fluidics and analyte measurements, during the analysis sequence, a user places a sample into the cartridge, places the cartridge into the analyzer and in from 1 to 20 minutes, a quantitative measurement of one or more analytes is performed. Herein is a non-limiting example of a sequence of events that occur during the analysis:

(1) A 25 to 50 μL sample is introduced in the sample inlet 167 and fills to a capillary stop 151 formed by a 0.012 inch (0.3 mm) laser cut hole in the adhesive tape holding the cover and base components together. One or more dry reagent coatings comprising sacrificial beads plus optionally other materials for ameliorating interference and preferably a signal antibody are dissolved into the sample. The user rotates a latex rubber disk mounted on a snap flap to close the sample inlet 167 and places the cartridge into the analyzer.

(2) The analyzer makes contact with the cartridge, and a motor driven plunger presses onto the foil pouch 161 forcing the wash/analysis fluid out into a central conduit 158.

(3) A separate motor driven plunger contacts the sample diaphragm 156 pushing a measured segment of the sample along the sample conduit (from reagent region R1 to R2). The sample is detected at the sensor chip 153 via the conductivity sensors. The sensor chip is located in capture region R3.
(4) The sample is oscillated by means of the sample diaphragm 156 between R2 and R5 in a predetermined and controlled fashion for a controlled time to promote binding to the sensor.

(5) The sample is pushed towards the waste region of the cartridge (R8) and comes in contact with a passive pump 157 in the form of a cellulose or similar absorbent wick. The action of wetting this wick seals the wick to air flow thus eliminating its ability to vent excess pressure generated by the sample diaphragm 156. The active vent becomes the "controlled air vent" of FIG. 16.

(6) Rapid evacuation of the sample conduit (effected by withdrawing the motor driven plunger from the sample diaphragm 156) forces a mixture of air (from the vent) and wash/analysis fluid from the second conduit to move into the inlet located between R5 and R4 in FIG. 16. By repeating the rapid evacuation of the sample conduit, a series of air separated fluid segments are generated which are pulled across the sensor chip towards the sample inlet (from R4 to R3 to R2 and R1). This washes the sensor free of excess reagents and wets the sensor with reagents appropriate for the analysis. The wash/analysis fluid which originates in the foil pouch can be further amended by addition of reagents in R7 and R6 within the central wash/analysis fluid conduit.

(7) The wash/analysis fluid segment is drawn at a slower speed towards the sample inlet to yield a sensor chip which contains only a thin layer of the analysis fluid. The electrochemical analysis is performed at this point. The preferred method of analysis is amperometry but potentiometry or impedance detection is also used.

(8) And the mechanism retracts allowing the cartridge to be removed from the analyzer.

**EXAMPLE 5**

In some embodiments, the device employs an immuno-reference sensor for purposes of assessing the degree of non-specific binding occurring during an assay. The immuno-reference sensor is fabricated in much the same way as the analyte immunosensor with the exception that the immuno reagent is an anti-HSA (human serum
albumin) antibody rather than an anti-analyte antibody. Upon exposure to a human whole blood or plasma sample, the reference sensor becomes coated with specifically bound HSA, an abundant endogenous protein present in all human blood samples thus affording a common reference for all individual tests run using the present immunoassay format. NSB arising due to inadequate washing or due to the presence of interferences can be monitored by means of this second sensor.

The net signal from the assay is comprised of the specific signal arising from the analyte immunosensor corrected by subtracting the non-specific signal arising from the reference sensor, e.g., Net Signal = Analyte Sensor Signal - Reference Sensor Signal - Offset, as shown in equation 4 above. The "offset" is a coefficient that accounts for the difference in the tendency of the two sensors to be subject to NSB. In effect, it accounts for the relative "stickiness" of each sensor with respect to their ability to bind conjugate non-specifically and is established based on the responses of samples that are free of analyte and free of interference. This is done by independent experimentation.

The amount of signal tolerated at the reference sensor is subject to limits defined by a quality control algorithm that seeks to safeguard the integrity of results at low analyte concentration where the effects of NSB have the greatest potential to affect assay results in a manner that can alter decision-making in a clinical environment. The essential principal is that the existence of excessive signal at the reference sensor acts as a flag for the presence of NSB, due either to an inadequate wash step or interference.

While the present invention as described above is generally directed to reducing or eliminating interference from leukocytes in an analyte immunoassay with a whole blood sample, it is also applicable to immunoassays performed in other types of biological samples where leukocytes may be present, e.g., cerebrospinal fluid. In addition it is applicable to samples where residual leukocytes may be present despite an intention to remove them by centrifugation or filtration, e.g., plasma. It is also applicable to samples that may have been diluted, e.g., with a buffer. Furthermore, while the invention is generally directed to amending the sample by dissolving into the sample a dry reagent, it is also practical in other embodiments to add the reagent as a liquid to the
sample during the analysis or during sample collection. It is also apparent that the present invention has been described herein in terms of electrochemical detection approaches, e.g., amperometric and potentiometric approaches, although it is equally applicable to other detection modes, notably optical sensing approaches such as luminescence, fluorescence and absorbance based approaches.

While the invention has been described in terms of various preferred embodiments, those skilled in the art will recognize that various modifications, substitutions, omissions and changes can be made without departing from the spirit of the present invention. For example, while portions of the description are directed to non-competitive sandwich immunoassays, the devices and processes of the invention similarly may be employed in competitive immunoassays. Additionally, it is intended that the scope of the present invention be limited solely by the scope of the following claims.
What is claimed is:

1. A kit for performing a sandwich immunoassay for an analyte suspected of being present in a blood sample, comprising sacrificial beads opsonized to leukocytes, an immobilized first antibody to the analyte and a labeled second antibody to the analyte.

2. The kit of claim 1, wherein the analyte is selected from the group consisting of BNP, proBNP, NTproBNP, cTnl, TnT, HCG, TSH, PSA, D-dimer, CRP, myoglobin, NGAL, CKMB and myeloperoxidase.

3. The kit of claim 1, wherein the sacrificial beads comprise substrate beads coated with non-human IgG or fragments thereof.

4. The kit of claim 3, wherein the substrate beads are formed of a material selected from the group consisting of polystyrene, polyacrylic acid, and dextran.

5. The kit of claim 1, wherein the sacrificial beads comprise substrate beads coated with a material or fragment thereof selected from the group consisting of a protein, a bacterium, a virus and a xenobiotic.

6. The kit of claim 1, wherein the sacrificial beads are stabilized bacterium or bacterial spores.

7. The kit of claim 1, wherein the sacrificial beads have an average particle size of from 0.01 µm to 20 µm.

8. The kit of claim 1, wherein the sacrificial beads have an average particle size of from 0.1 µm to 5 µm.

9. The kit of claim 1, wherein the sacrificial beads are present in an amount sufficient to provide a dissolved sacrificial bead concentration of at least $10^4$ beads per microliter of sample.
10. The kit of claim 1, wherein the immobilized first antibody is attached to a sensor selected from the group consisting of an amperometric electrode, a potentiometric electrode, a conductimetric electrode, an optical wave guide, a surface plasmon resonance sensor, an acoustic wave sensor and a piezoelectric sensor.

11. The kit of claim 1, wherein the immobilized first antibody is attached to an assay bead, and the assay bead is attached to an amperometric electrode.

12. The kit of claim 1, wherein the sacrificial beads and the second labeled antibody are in one or more dissolvable dry reagent coatings.

13. The kit of claim 1, wherein said labeled second antibody is labeled with a label selected from the group consisting of a radiolabel, an enzyme, a chromophore, a fluorophore and a chemiluminescent species.

14. The kit of claim 1, wherein said labeled second antibody is labeled with an enzyme selected from the group consisting of alkaline phosphatase, glucosidase, diaphorase, horse radish peroxidase and glucose oxidase.

15. A cartridge for performing a sandwich immunoassay for an analyte suspected of being present in a blood sample, the cartridge comprising:

(a) a sample inlet for receiving the blood sample;
(b) a metering chamber for metering the blood sample to form a metered sample;
(c) one or more dry reagent coating layers comprising sacrificial beads opsonized to leukocytes and a labeled antibody to the analyte;
(d) an electrode comprising an immobilized antibody to the analyte; and
(e) one or more pumping elements for moving a metered sample, fluidized sacrificial beads, and the labeled antibody to the electrode.
16. The cartridge of claim 15, wherein the analyte is selected from the group consisting of BNP, proBNP, NTproBNP, cTnl, TnT, HCG, TSH, PSA, D-dimer, CRP, myoglobin, NGAL, CKMB and myeloperoxidase.

17. The cartridge of claim 15, wherein the sacrificial beads comprise substrate beads coated with non-human IgG or fragments thereof.

18. The cartridge of claim 17, wherein the substrate beads are formed of a material selected from the group consisting of polystyrene, polyacrylic acid, and dextran.

19. The cartridge of claim 15, wherein the sacrificial beads have an average particle size of from 0.01 µm to 20 µm.

20. The cartridge of claim 15, wherein the sacrificial beads are present in an amount sufficient to provide a dissolved sacrificial bead concentration of at least $10^4$ beads per microliter of sample.

21. The cartridge of claim 15, wherein the one or more dry reagent coating layers are disposed within the metering chamber.

22. A method of performing a sandwich immunoassay for an analyte suspected of being present in a blood sample comprising:

   (a) exposing a blood sample suspected of containing the analyte to sacrificial beads opsonized to leukocytes; an immobilized first antibody to the analyte; and a labeled second antibody to form a complex comprising said first antibody, said analyte and said second antibody; and

   (b) determining the amount of complexed label.

23. The method of claim 22, wherein the sacrificial beads contact the blood sample under conditions effective for leukocytes in the sample to preferentially phagocytose the sacrificial beads.
24. The method of claim 22, wherein the analyte is selected from the group consisting of BNP, proBNP, NTproBNP, cTnl, TnT, HCG, TSH, PSA, D-dimer, CRP, myoglobin, NGAL, CKMB and myeloperoxidase.

25. The method of claim 22, wherein the sacrificial beads comprise substrate beads coated with non-human IgG or fragments thereof.

26. The method of claim 25, wherein the substrate beads are formed of a material selected from the group consisting of polystyrene, polyacrylic acid, and dextran.

27. The method of claim 22, wherein the sacrificial beads have an average particle size of from 0.01 µm to 20 µm.

28. The method of claim 22, wherein the sacrificial beads have an average particle size of from 0.1 µm to 20 µm.

29. The method of claim 22, wherein the sacrificial beads are present in an amount sufficient to provide a dissolved sacrificial bead concentration of at least \(10^4\) beads per microliter of sample.

30. The method of claim 22, wherein said blood sample is whole blood amended with an anticoagulant.

31. The method of claim 22, wherein the blood sample is mixed with the sacrificial beads, then mixed with the immobilized first antibody, and then mixed with the labeled second antibody.

32. The method of claim 22, wherein the blood sample is mixed with the sacrificial beads, the immobilized first antibody, and the labeled second antibody at substantially the same time.
33. The method of claim 22, wherein the blood sample is mixed with the immobilized first antibody and the labeled second antibody at substantially the same time.

34. The method of claim 22, wherein the blood sample is mixed with the sacrificial beads and the labeled second antibody at substantially the same time, and before the blood sample is mixed with the immobilized first antibody.

35. A method of substantially ameliorating white blood cell accumulation on an analyte immunosensor comprising antibody-coated beads to the analyte immobilized on an electrode comprising, the method comprising the steps of:
   (a) mixing a sample suspected of containing an analyte with sacrificial beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads, and
   (b) contacting the amended sample with an immunosensor.

36. The method of claim 35, wherein the sacrificial beads are present in an amount sufficient to provide a dissolved sacrificial bead concentration of at least $10^4$ beads per microliter of sample.

37. A method of performing an immunoassay for an analyte suspected of being present in a blood sample comprising:
   (a) mixing a blood sample suspected of containing an analyte with an excess of sacrificial beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads;
   (b) contacting the amended sample with an immunosensor comprising antibody-coated beads to the analyte immobilized on an electrode forming a sandwich between said antibody-coated bead, said analyte and a second labeled antibody;
   (c) washing said blood sample from said immunosensor; and
38. A method of performing a sandwich immunoassay for an analyte suspected of being present in a blood sample, comprising:
   (a) mixing a blood sample suspected of containing an analyte with an excess of opsonized sacrificial beads to form an amended sample wherein white blood cells in the sample preferentially seek to phagocytose the sacrificial beads;
   (b) contacting the amended sample with antibody-coated beads to the analyte under conditions effective to form a sandwich between said antibody-coated bead, said analyte and a second labeled antibody;
   (c) washing said blood sample from said antibody-coated beads; and
   (d) determining the amount of said sandwiched label and relating the amount of said label to the concentration of the analyte in the sample.

39. A test cartridge for performing an immunoassay for an analyte suspected of being present in a blood sample, the test cartridge comprising an immunosensor in a conduit, said immunosensor having an immobilized first antibody to the analyte, and said conduit having a dry reagent coating disposed therein, the dry reagent coating comprising sacrificial beads and a second labeled antibody to said analyte and being configured to dissolve into said blood sample.
Simultaneous Sandwich ELISA for Troponin I and other Cardiac Marker tests

1: Capture Step
- Troponin I (Tnl)
- Alkaline phosphatase/aTnl conjugate (polyclonal)
- Capture aTnl antibody (monoclonal)
- Heterophile Antibody
- IgM
- IgG

2: Wash and Analysis
- Non-specifically adsorbed enzyme/antibody conjugate
- Enzyme Substrate Product

**FIG. 7**

**FIG. 8**
Fluidic Schematic for i-STAT immunocartridge

Controlled Air Vent

R5

R4

Capture R3

R2

R8

Pump 2

Fluid Pouch

Vent

R6

R7

R1

Pump 1

Pump 3 (passive)

FIG. 16
**FIG. 23**

**μParticle region**
- pH 9.2
- pH 9.2

**e**lectrode region
- Good Wash

**Normal Sample Amperometric Signals**
- Current (pA)
- Time (s)

**Aberrant Sample Amperometric Signals**
- Current (pA)
- Time (s)

**Bad Wash**
- pH 9.2
- pH 7.4
- Relaxing pH Gradient and dynamic signal
- pH 8.5
- pH 8.5
## INTERNATIONAL SEARCH REPORT

### A. CLASSIFICATION OF SUBJECT MATTER

**INV. G01N33/543**

According to International Patent Classification (IPC) or to both national classification and IPC

### B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

G01N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic database consulted during the international search (name of database and, where practical, search terms used)

EPO-Internal, WPI Data

### C. DOCUMENTS CONSIDERED TO BE RELEVANT

<table>
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<tr>
<th>Category*</th>
<th>Citation of document, with indication, where appropriate, of the relevant passages</th>
<th>Relevant to claim No.</th>
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</thead>
<tbody>
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<td>WO 00/51814 AI (BIO RAD LABORATORIES [US]) 8 September 2000 (2000-09-08) page 18, paragraph 2 - paragraph 3; figure 1; examples 5, 9</td>
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<td>EP 0 768 530 AI (NI POND PAINT CO LTD [JP]) 16 April 1 1997 (1997-04-16) claims; example 1</td>
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### Notes

- **X**: Further documents are listed in the continuation of Box C.
- **X**: See patent family annex.
- **X**: Special categories of cited documents:
  - "A" document defining the general state of the art which is not considered to be of particular relevance
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- **A**: document member of the same patent family

**Date of the actual completion of the international search**: 
25 January 2011

**Date of mailing of the international search report**: 
10/02/2011

**Name and mailing address of the ISA**

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**Authorized officer**

Luis Alves, Dulce

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