

(19)



Europäisches Patentamt
European Patent Office
Office européen des brevets



(11)

EP 1 604 118 B1

(12)

EUROPEAN PATENT SPECIFICATION

(45) Date of publication and mention
of the grant of the patent:
26.07.2006 Bulletin 2006/30

(21) Application number: **04714279.9**

(22) Date of filing: **25.02.2004**

(51) Int Cl.:
F15B 13/042 ^(2006.01)

(86) International application number:
PCT/EP2004/001823

(87) International publication number:
WO 2004/079206 (16.09.2004 Gazette 2004/38)

(54) **A METHOD FOR GENERATING A VALVE COMMAND SIGNAL**

VERFAHREN ZUR ERZEUGUNG EINES VENTILSTEUERSIGNALS

PROC D PERMETTANT DE PRODUIRE UN SIGNAL DE COMMANDE DE VANNE

(84) Designated Contracting States:
**AT BE BG CH CY CZ DE DK EE ES FI FR GB GR
HU IE IT LI LU MC NL PT RO SE SI SK TR**

(30) Priority: **07.03.2003 US 383923**

(43) Date of publication of application:
14.12.2005 Bulletin 2005/50

(73) Proprietor: **DEERE & COMPANY**
Moline
Illinois 61265-8098 (US)

(72) Inventors:
• **ALEXANDER, William, Guy**
Waterloo, IA 50701 (US)

• **BOEGE, David, James**
Cedar Falls, IA 50613 (US)

(74) Representative: **Holst, Sönke et al**
Deere & Company,
European Office,
Patent Department
Steubenstrasse 36-42
68163 Mannheim (DE)

(56) References cited:
EP-A- 0 532 195 WO-A-03/019017
US-B1- 6 308 516

EP 1 604 118 B1

Note: Within nine months from the publication of the mention of the grant of the European patent, any person may give notice to the European Patent Office of opposition to the European patent granted. Notice of opposition shall be filed in a written reasoned statement. It shall not be deemed to have been filed until the opposition fee has been paid. (Art. 99(1) European Patent Convention).

Description

[0001] The present invention relates to a system and method for processing command signals, such as command signals for an electro-hydraulic control valve which operates a hydraulic device.

[0002] It is known to provide work vehicles, such as agricultural tractors, with a loader having a bucket which is movable by a hydraulic bucket cylinder. It is known to control the bucket cylinder with a conventional electro-hydraulic (EH) selective control valve (SCV), which, in turn, is controlled by an electronic valve controller. Bucket position and movement commands are generated by a control lever which is manipulated by an operator. In some commercially available systems, the position of the lever is monitored by an electronic lever unit which is communicated with the electronic valve controller. For example, in John Deere 7030 tractors, the lever and the electronic lever unit are mounted on an armrest in the tractor cab, and the electronic lever unit is communicated with a remote valve controller via a relatively slow speed serial communications data link. A further example can be found in EP0532195.

[0003] In such systems, the response of the EH valve response is dependent upon the sample rate of the control lever position, the serial transmission rate of the serial data link and update rate at which the valve controller updates the valve command signal which is communicated to the SCV.

[0004] Typically, with such a system the actual bucket position and movement will not accurately match the control lever position and movement because of the slow serial communications data link. In addition, delays in the system may result in SCV conditions which conflict with the control lever. In some situations, such as when it is desired to dislodge debris from a loader bucket, an operator may desire to produce a vigorous and rapid SCV response by rapidly moving the control lever. If the transmission rate of the lever position to the EH valve controller is too slow, the SCV will typically not respond as desired by the operator, and the bucket movement may not be abrupt enough to loosen the debris. During a worst case, the transmission of the lever position over the serial communications link may occur when the control lever is near its center position instead of at maximum displaced position. As a result the lever command signal may not match the actual lever position and desired movement of the bucket may not be achieved.

[0005] Accordingly, an object of this invention is to provide a system for vigorously extending and retracting a hydraulic cylinder in a system which slowly transmits command signals which are generated in response to manual movement of a control lever.

[0006] Another object of the invention is to provide such a system wherein the magnitude of the command signals will be a function of the magnitude of the displacements of the lever from its center position.

[0007] A further object of the invention is to provide such a system wherein the timing of command signals is a function of a frequency at which the lever is moved.

[0008] These and other objects are achieved by the present invention, wherein a hydraulic function, such as a loader bucket cylinder, can be extended and retracted under the control of an electrohydraulic valve unit. An operator movable command lever is movable into extend, center and retract regions. A position sensor generates lever position signal. An electronic lever command unit receives the lever position signals and generates a valve command signal. An electronic valve control unit (VCU) is remote from the lever command unit and receives the command signals via a signal transmission link. The electronic valve control unit controls communication of hydraulic fluid to the hydraulic function in response to the valve command signal. When the lever is moved relatively slowly, the lever command unit generates command signals which are proportional to the lever position signal. When the lever is moved relatively rapidly, the lever command unit generates command signals which are based on maximum excursions of the lever into the extend and retract regions. When the lever first moves from the center region into the extend or retract region, transmission of the command signal is delayed by a time delay which is related to the frequency at which the lever is oscillated back and forth between the extend and retract regions.

[0009] This system provides the operator with better and more consistent control over the electrohydraulic valve. The system overcomes slow-speed or bottleneck digital communications. The system detects when the operator intends to "rattle" the bucket, and generates valve command signals which carry out this intention, despite data link limitations. As a result, performance and repeatability is greatly enhanced. For example, by allowing the operator more control over a loader bucket, the operator can more precisely control the loads. Instead of a random shaking of debris, the load can be scattered over a larger area more precisely and consistently with the controlled abruptness.

[0010] The invention and further advantageous developments and arrangements of the invention will now be described and explained in more detail by way of example and with reference to the accompanying drawings in which:

[0011] Fig. 1 is a simplified schematic diagram of a loader bucket control system according to the present invention;

[0012] Fig. 2, consisting of Fig. 2A and Fig. 2B, forming a logic flow diagram illustrating an algorithm executed by the lever control unit of Fig. 1.

[0013] Referring to Fig. 1, the bucket control system 10 includes a bucket 12 pivotally mounted on the end of a boom 14 which is pivoted on a frame member 16 of a vehicle or loader (not shown). The boom 14 is pivoted by a boom cylinder 18 and the bucket is pivoted by a bucket cylinder 20 connected to the boom and bucket by links 11 and 13. Electro-hydraulic SCVs 22 control fluid flow to and from the cylinders 18 and 20. An electronic valve control unit (VCU) 28

provides control signals to the SCVs 22 in response to signals from a boom position sensor 30, bucket position sensor 32 and a valve command signal from an electronic lever unit 34.

[0014] An operator generates bucket command signals by manipulating a control lever 36. Control lever 36 may be moved from a centered or neutral position into an "extend" range of positions and into a "retract" range of positions, corresponding to extension and retraction, respectively, of the bucket cylinder 20. Lever position sensor 38 provides a lever position signal to lever unit 34. Lever unit 34 provides a lever command signal to VCU 28 via a data link 40, such as a serial data communication bus. Conventional rotary potentiometers could serve as the sensors 30, 32 and 38.

[0015] The lever unit 34 periodically, such as every 20 milliseconds, executes an algorithm 100 represented by Figs. 2A and 2B. The conversion of this flow chart into a standard language for implementing the algorithm described by the flow chart in a digital computer or microprocessor, will be evident to one with ordinary skill in the art.

[0016] In step 102 unit 34 reads and stores the current lever position value generated by sensor 38. From a lookup table stored in a memory of unit 34, step 104 determines a Normal Desired Command value which is preferably proportional to the lever position value read in step 102.

[0017] Step 106 determines the movement oscillation frequency F at which the lever 36 moves back and forth between its retract and extend regions. This is accomplished by using two software timers (not shown), each associated with one of the extend and retract regions. When the lever 36 moves out of either the extend and retract regions, then a) the timer associated with that region is reset and b) the value of the other timer is read and stored. Each timer is periodically decremented when the lever is not in the region associated with that timer. Ultimately, if the lever 36 is repeatedly moved back and forth between regions, the unit 34 will determine and store the total cycle time of a round trip of the lever. The inverse of this cycle time is the lever frequency F.

[0018] Step 108 compares the lever frequency F to a threshold, such as 1 Hz. If lever frequency F is not greater than 1 Hz, step directs the algorithm to step 110.

[0019] Step 110 determines whether the lever 36 is in a center region, the retract region or the extend region. Step 110 directs the algorithm to step 112 if lever 36 is in the extend region, to step 114 if lever 36 is in the retract region and to step 116 if lever 36 is in the center region.

[0020] Step 112, from the stored lever positions from step 102, determines and stores the maximum lever position Emax in the extend region, which corresponds to the farthest the lever 36 has moved into the extend region.

[0021] Step 114, from the stored lever positions from step 102, determines and stores the maximum lever position Rmax in the retract region, which corresponds to the farthest the lever 36 has moved into the retract region.

[0022] Step 116 determines whether the lever 36 was previously in the retract, center or the extend region. Step 116 directs the algorithm to step 118 if lever 36 was previously in the retract region, to step 120 if lever 36 is previously in the extend region and to step 122 if lever 36 was previously in the center region.

[0023] Step 118 calculates an average maximum retract region command value, Amax(r) as an average of the current maximum retract region lever position value Rmax, multiplied by a scaling factor C, and a stored previous Amax(r) value as follows:

$$A_{max}(r) = [R_{max} + ((C - 1) \times A_{max}(r))] \div C,$$

where the scaling factor C is preferably set to a value of 4.

[0024] Step 120 calculates an average maximum extend region command value, Amax(e) as an average of the current maximum extend region lever position value Emax, multiplied by the scaling factor C, and the stored previous Amax(e) value as follows:

$$A_{max}(e) = [E_{max} + ((C - 1) \times A_{max}(e))] \div C.$$

[0025] Following steps 112, 114, 116 or 118, step 122 sets the NEW COMMAND value equal to the Normal Desired Command (from step 104) and directs the algorithm to step 170.

[0026] Thus, when lever 36 is being moved relatively slowly, steps 110-122 operate to generate a new command signal, NEW COMMAND, which is essentially proportional to the position of lever 36.

[0027] Returning to step 108, if lever frequency F is greater than 1 Hz, step 108 directs the algorithm to step 130.

[0028] Step 130 determines a time delay value Td as a function of the lever frequency F, as follows $T_d = (1/F) / K$, where K is an empirically determined constant, such as 8. As a result, the more rapidly the lever 36 is moved back and forth, the shorter will be the time delay value. Td is preferably a fraction of the period of the back and forth movement of lever 36. It was found that when the lever 36 was moved at a high rate of speed a K value of 4 caused the command

EP 1 604 118 B1

signal to be sent to VCU 28 well after the lever 36 had reached its maximum position. It was found that a K value of 8 worked well with both fast and slow rates of lever movement.

[0029] Step 132 determines whether the lever 36 is in a center region, the retract region or the extend region. Step 132 directs the algorithm to step 140 if lever 36 is in the extend region, to step 150 if lever 36 is in the retract region, and to step 160 if lever 36 is in the center region.

[0030] Step 140, from the stored lever positions from step 102, determines and stores the maximum lever position Emax in the extend region, which corresponds to the farthest the lever 36 has moved into the extend region.

[0031] Steps 142 and 144 operate to repeatedly increment the send delay counter until the counter value reaches a value representing the time delay Td calculated in step 130. When the time period Td has expired, then step 144 directs the algorithm to step 146, which sets the NEW COMMAND value equal to the previously determined average maximum command value for the extend region, Amax(e). From step 146 control passes back to step 170. As a result of steps 130 and 142-144, the timing of the sending of command signals will be a function of a frequency at which the lever is moved.

[0032] If step 132 determines that the lever 36 is in the retract region, control passes to step 150.

[0033] Step 150, from the stored lever positions from step 102, determines and stores the maximum lever position Rmax in the retract region, which corresponds to the farthest the lever 36 has moved into the retract region.

[0034] Steps 152 and 154 operate to repeatedly increment the send delay counter until the counter value reaches a value representing the time delay Td calculated in step 130. When the time period Td has expired, then step 154 directs the algorithm to step 156, which sets the NEW COMMAND value equal to the average maximum command value for the retract, Amax(r). From step 156 control passes back to step 170.

[0035] As a result of steps 146 and 156, the magnitude of the command signals will be a function of the magnitude of the displacements of the lever from its center position.

[0036] If step 132 determines whether the lever 36 is in a center region, control passes to step 160.

[0037] Step 160 sets the NEW COMMAND value equal the OLD COMMAND value from previous operation of step 174.

[0038] Step 162 resets the send time delay counter value to zero.

[0039] Step 164 determines whether the lever 36 was previously in the retract, center or the extend region. Step 164 directs the algorithm to step 166 if lever 36 was previously in the retract region, to step 168 if lever 36 was previously in the extend region and to step 102 if lever 36 was previously in the center region.

[0040] Step 166, as described with respect to step 118, re-calculates the average maximum retract region command value Amax(r).

[0041] Step 168, as described with respect to step 120, re-calculates the average maximum extend region command value Amax(e).

[0042] Following steps 122, 166 or 168, the algorithm proceeds to step 170.

[0043] Step 170 directs the algorithm to step 172 if the command value is changed (NEW COMMAND $\neq$ OLD COMMAND) and if more than 50 milliseconds have elapsed since a command value was previously transmitted to the VCU 28, else to step 180. A software timer or counter "Transmit Timer" is utilized to determine the elapsed time since a command value was previously transmitted.

[0044] Step 180 directs the algorithm to step 172 if Transmit Timer indicates that a full second has elapsed since a command value was previously transmitted to the VCU 28, else to step 182.

[0045] Step 172 sends NEW COMMAND to the VCU 28, which in turn, causes the valve unit 22 to extend or retract the bucket cylinder 12.

[0046] Step 174 sets the OLD COMMAND equal to the NEW COMMAND.

[0047] Step 176 resets the Transmit Timer so the transmit timer can monitor the time expired since the operation of step 172.

[0048] After steps 180 or 176, step 182 increments the Transmit Timer and returns the algorithm to step 102.

[0049] As a result, when lever 36 is being moved relatively slowly, steps 110-122 and 170-172 operate to transmit to VCU 28 a new command signal which is essentially proportional to the position of lever 36.

[0050] However, if the operator rapidly moves the lever 36 back and forth, steps 130-172 operate to cause control unit 34 to send to VCU 28 command signals which are based on maximum extend and retract positions of the lever 36. This assures that the bucket 12 will be vigorously shaken despite slow signal transmission rates between the electronic lever unit 34 and the remote VCU 28. The command signals will be a function of both how fast the operator is moving the control lever and also of how far away from the center the lever moves. The frequency or timing of the command signals will be a function of the frequency at which the lever is moved, and the magnitude of the command signals will be a function of the magnitude the displacements of the lever from its center position.

[0051] The algorithm will attempt to transmit maximum command signals in phase with the actual lever position. For example, when the operator wishes to "shake" debris from a loader's bucket, the operator will rapidly actuate the control lever. Upon detection of rapid lever motion, the algorithm will begin transmitting a valve command based on an average peak lever position and only when the lever is near its peak position.

[0052] Steps 170, 180 and 182 operate to prevent transmission of a new command to VCU 28 for 1 second if the

command is unchanging.

[0053] Step 170 operates to transmit a new command to VCU 28 every 50 milliseconds if the command is changing.

[0054] While the present invention has been described in conjunction with a specific embodiment, it is understood that many alternatives, modifications and variations will be apparent to those skilled in the art in light of the foregoing description. Accordingly, this invention is intended to embrace all such alternatives, modifications and variations which fall within the scope of the appended claims.

Claims

1. A method for generating a valve command signal, where a system having a hydraulic function (20) which can be extended and retracted under the control of an electrohydraulic valve unit (22), an operator movable command lever (36) movable into extend, center and retract regions, a sensor (38) generating a lever position signal, an electronic lever command unit (34) receiving the lever position signal and generating a valve command signal, an electronic valve control unit (28) remote from and communicated with the lever command unit (34), the valve control unit (28) controlling communication - e.g. by supplying - of hydraulic fluid to the hydraulic function (20) in response to the valve command signal, the method comprising:

determining a movement oscillation frequency (F) of the lever (36); and
if the oscillation frequency (F) is greater than a threshold value, transmitting to the valve control unit (28) a command signal - especially a maximum extend command (Amax(e)) - derived from maximum lever position values when the lever (36) is in the extend region, and transmitting to the valve control unit (28) a command signal - especially a maximum retract command (Amax(r)) - derived from maximum lever position values when the lever (36) is in the retract region.

2. The method of claim 1, wherein:

if the oscillation frequency (F) is not greater than a threshold value, transmitting to the valve control unit (28) an extend command derived from a current lever position when the lever (36) is in the extend region, and transmitting to the valve control unit (28) a retract command derived from a current lever position when the lever (36) is in the retract region.

3. The method of claim 1 or 2, wherein:

the extend command is proportional to the current lever position when the lever (36) is in the extend region, and the retract command is proportional to the current lever position when the lever (36) is in the retract region.

4. The method of one of the claims 1 to 3, further comprising:

determining a send time delay value; and
transmitting commands to the valve control unit (28) upon expiration of the send time delay.

5. The method of claim 4, wherein:

the send time delay is a fraction of a period of the movement oscillation of the lever (36).

6. The method of claim 4 or 5, further comprising:

periodically incrementing a send time delay counter when the lever (36) is in the extend or retract region; and
resetting the send time delay counter when the lever (36) is in the center region.

7. The method of one of the claims 1 to 6, further comprising:

when the lever (36) moves into the center region, calculating an average maximum retract lever position value if the lever (36) was previously in the retract region, or calculating an average maximum extend lever position value if the lever (36) was previously in the extend region.

8. The method of one of the claims 1 to 7, further comprising:

transmitting a new command to the valve control unit (28) if the new command differs from a previous command and if a certain time period has elapsed since the previous command was transmitted to the valve control unit (28).

9. The method of one of the claims 1 to 8, further comprising:

preventing transmission of a command to the valve control unit (28) if the command is changing and less than a certain time period has elapsed since a previous command was transmitted to the valve control unit (28).

10. The method of one of the claims 1 to 9, wherein:

the average maximum retract lever position value $A_{max}(r)$ is an average of a current maximum retract region lever position value R_{max} , multiplied by the scaling factor C , and a stored previous $A_{max}(r)$ value; and the average maximum extend lever position value $A_{max}(e)$ is an average of the current maximum extend region lever position value E_{max} , multiplied by the scaling factor C , and the stored previous $A_{max}(e)$ value.

11. The method of one of the claims 1 to 10, further comprising:

determining and storing lever extend position values and lever retract position values as the lever (36) moves through the extend region;
determining from the stored lever extend position values a maximum lever extend value;
determining from the stored lever retract position values a maximum lever retract value.

12. A method for generating a valve command signal according to one of the claims 1 to 11 - comprising:

when lever (36) is moved relatively slowly, generating a command signal which is proportional to the lever position signal; and
when the lever (36) is moved relatively rapidly, generating a command signal which is based on a maximum excursion of the lever (36) into the extend and retract regions.

13. A method for generating a valve command signal according to one of the claims 1 to 12 - comprising:

generating command signals with a timing which is a function of a frequency (F) at which the lever (36) is moved; and
generating command signals having a magnitude which is a function of the magnitude of displacement of the lever (36) from its center position.

Patentansprüche

1. Verfahren zur Erzeugung eines Ventilsteuersignals, bei dem ein System aufweist: eine Hydraulikfunktion (20), welche unter dem Einfluss einer elektro-hydraulischen Ventileinheit (22) ausgefahren und eingefahren werden kann, einen durch eine Bedienungsperson bewegbaren Steuersignalhebel (36), welcher sich in Ausfahr-, mittlere und Einfahr-Regionen bewegen lässt, einen Sensor (38), der ein Hebelpositionssignal erzeugt, eine elektronische Hebelsteuersignaleinheit (34), die das Hebelpositionssignal empfängt und ein Ventilsteuersignal erzeugt, eine elektronische Ventilsteuereinheit (28), die entfernt von der Hebelsteuersignaleinheit (34) liegt und mit dieser verbunden ist und welche die Verbindung - z. B. durch Zuführung - der Hydraulikflüssigkeit zu der Hydraulikfunktion (20) in Abhängigkeit von dem Ventilsteuersignal steuert, das Verfahren umfasst:

Bestimmen einer Bewegungszustandsfrequenz (F) des Hebels (36), und wenn die Oszillationsfrequenz (F) größer als ein Grenzwert ist, Übertragen eines Steuersignals - vorzugsweise eines maximalen Ausfahrsteuersignals ($A_{max}(e)$) - an die Ventilsteuereinheit (28), welches von maximalen Hebelpositionswerten abgeleitet wird, sofern der Hebel (36) in der Ausfahr-Region ist, und Übertragen eines Steuersignals - vorzugsweise ein maximales Einfahrsteuersignal ($A_{max}(r)$) - an die Ventilsteuereinheit (28), welches von maximalen Hebelpositionswerten abgeleitet wird, sofern der Hebel (36) in der Einfahr-Region ist.

2. Verfahren nach Anspruch 1, worin:

wenn die Oszillationsfrequenz (F) nicht größer ist als ein Grenzwert, Übertragen eines Ausfahrsteuersignals

an die Ventilsteuereinheit (28), welches von einer aktuellen Hebelposition abgeleitet wird, wenn der Hebel (36) in der Ausfahr-Region ist, und Übertragen eines Einfahrsteuersignals an die Ventilsteuereinheit (28), welches von einer aktuellen Hebelposition abgeleitet wird, wenn der Hebel (36) in der Einfahr-Region ist.

5 **3.** Verfahren nach Anspruch 1 oder 2, worin:

das Ausfahrsteuersignal proportional zu der aktuellen Hebelposition ist, wenn der Hebel (36) in der Ausfahr-Region ist, und das Einfahrsteuersignal proportional zu der aktuellen Hebelposition ist, wenn der Hebel (36) in der Einfahr-Region ist.

10 **4.** Verfahren nach einem der Ansprüche 1 bis 3, des Weiteren umfassend:

Bestimmen eines Sendezeitverzögerungswertes, und Übertragen von Steuersignalen an die Ventilsteuereinheit (28) nach Ablauf der Sendezeitverzögerung.

15 **5.** Verfahren nach Anspruch 4, worin:

die Sendezeitverzögerung ein Bruchteil einer Periode der Bewegungssoszillation des Hebels (36) ist.

20 **6.** Verfahren nach Anspruch 4 oder 5, des Weiteren umfassend:

periodische Erhöhen eines Sendezeitverzögerungszählers, wenn der Hebel (36) in der Ausfahr- oder Einfahr-Region ist, und Zurücksetzen des Sendezeitverzögerungszählers, wenn der Hebel (36) in der mittleren Region ist.

25 **7.** Verfahren nach einem der Ansprüche 1 bis 6, des Weiteren umfassend:

wenn der Hebel (36) sich in die mittlere Region bewegt, Berechnen eines durchschnittlichen Einfahr-Hebelpositionshöchstwertes, sofern der Hebel (36) vorher in der Einfahr-Region war, oder Berechnen eines durchschnittlichen Ausfahr-Hebelpositionshöchstwertes, sofern der Hebel (36) vorher in der Ausfahr-Region war.

30 **8.** Verfahren nach einem der Ansprüche 1 bis 7, des Weiteren umfassend:

Übertragen eines neuen Steuersignals an die Ventilsteuereinheit (28), sofern sich das neue Steuersignal von einem vorhergehenden Steuersignal unterscheidet und sofern eine bestimmte Zeitperiode abgelaufen ist, seit das vorhergehende Steuersignal an die Ventilsteuereinheit (28) übertragen wurde.

35 **9.** Verfahren nach einem der Ansprüche 1 bis 8, des Weiteren umfassend:

Verhindern der Übertragung eines Steuersignals an die Ventilsteuereinheit (28), sofern das Steuersignal sich ändert und weniger als eine bestimmte Zeitperiode abgelaufen ist, seit ein vorhergehendes Steuersignal an die Ventilsteuereinheit (28) übertragen wurde.

40 **10.** Verfahren nach einem der Ansprüche 1 bis 9, worin:

der durchschnittliche Einfahr-Hebelpositionshöchstwert $A_{\max}(r)$ ein Durchschnittswert ist von einem aktuellen Einfahr-Hebelpositionshöchstwert $R_{\max}$ multipliziert mit dem Skalierfaktor C und einem gespeicherten vorhergehenden $A_{\max}(r)$ -Wert, und
der durchschnittliche Ausfahr-Hebelpositionshöchstwert $A_{\max}(e)$ ein Durchschnittswert ist von einem aktuellen Ausfahr-Hebelpositionshöchstwert $E_{\max}$ multipliziert mit dem Skalierfaktor C und dem gespeicherten vorhergehenden $A_{\max}(e)$ -Wert.

45 **11.** Verfahren nach einem der Ansprüche 1 bis 10, des Weiteren umfassend:

Bestimmen und Speichern von Hebelausfahrpositionswerten und Hebeleinfahrpositionswerten während der Hebel (36) sich durch die Ausfahr-Region bewegt,
Bestimmen eines maximalen Hebelausfahrwertes aus den gespeicherten Hebelausfahrpositionswerten,
Bestimmen eines maximalen Hebeleinfahrwertes aus den gespeicherten Hebeleinfahrpositionswerten.

12. Verfahren zur Erzeugung eines Ventilsteuersignals gemäß eines der Ansprüche 1 bis 11, einschließlich:

wenn der Hebel (36) relativ langsam bewegt wird, Erzeugen eines Steuersignals, welches proportional zu dem Hebelpositionssignal ist, und
wenn der Hebel (36) relativ schnell bewegt wird, Erzeugen eines Steuersignals, welches auf einer maximalen Auslenkung des Hebels (36) in die Ausfahr- oder die Einfahrregion basiert.

13. Verfahren zur Erzeugung eines Ventilsteuersignals gemäß eines der Ansprüche 1 bis 12, einschließlich:

Erzeugen eines Steuersignals mit einer zeitlichen Koordinierung, die eine Funktion einer Frequenz (F) ist, mit welcher der Hebel (36) bewegt wird, und
Erzeugen eines Steuersignals, welches eine Größe hat, die eine Funktion der Größe der Verschiebung des Hebels (36) aus seiner mittleren Position ist.

Revendications

1. Procédé de génération d'un signal de commande de soupape, où un système ayant une fonction hydraulique (20) peut être en extension et rétracté sous la commande d'une unité de soupape électrohydraulique (22), un levier de commande (36) pouvant être déplacé par opérateur dans des régions d'extension, centrale et de rétraction, un capteur (38) générant un signal de position de levier, une unité de commande de levier électronique (34) recevant le signal de position de levier et générant un signal de commande de soupape, une unité de commande de soupape électronique (28) éloignée de et en communication avec l'unité de levier (34), l'unité de commande de soupape (28) commandant une communication - par exemple en alimentant - de fluide hydraulique vers la fonction hydraulique (20) en réponse au signal de soupape, le procédé comprenant les étapes consistant à :

déterminer une fréquence d'oscillation de mouvement (F) du levier (36) ; et
si la fréquence d'oscillation (F) est supérieure à une valeur seuil, transmettre à l'unité de commande de soupape (28) un signal d'ordre - spécialement un ordre d'extension maximale (Amax(e)) - dérivé de valeurs de position du levier maximales lorsque le levier (36) est dans la région d'extension, et transmettre à l'unité de commande de soupape (28) un signal d'ordre - spécialement un ordre de rétraction maximale (Amax(f)) - dérivé de valeurs de position de levier maximales lorsque le levier (36) est dans la région de rétraction.

2. Procédé selon la revendication 1, dans lequel :

si la fréquence d'oscillation (F) n'est pas supérieure à une valeur seuil, exécuter les étapes consistant à transmettre à l'unité de commande de soupape (28) une commande d'extension dérivée d'une position actuelle de levier lorsque le levier (36) est dans la région d'extension, et transmettre à l'unité de commande de soupape (28) un ordre de rétraction dérivé d'une position actuelle de levier lorsque le levier (36) est dans la région de rétraction.

3. Procédé selon la revendication 1 ou 2, dans lequel :

l'ordre d'extension est proportionnel à la position de levier actuelle lorsque le levier (36) est dans la région d'extension, et l'ordre de rétraction est proportionnel à la position de levier actuelle lorsque le levier (36) est dans la région de rétraction.

4. Procédé selon l'une quelconque des revendications 1 à 3, comprenant en outre les étapes consistant à :

déterminer une valeur de délai d'envoi ; et
transmettre des commandes à l'unité de commande de soupape (28) à l'expiration du délai d'envoi.

5. Procédé selon la revendication 4, dans lequel :

le délai d'envoi est une fraction d'une période de l'oscillation de mouvement du levier (36).

6. Procédé selon la revendication 4 ou 5, comprenant en outre les étapes consistant à :

EP 1 604 118 B1

incrémenter périodiquement un compteur de période d'envoi lorsque le levier (36) est dans la région d'extension ou de rétraction ; et
remettre le compteur de délai à zéro d'envoi lorsque le levier (36) est dans la région centrale.

5 7. Procédé selon l'une quelconque des revendications 1 à 6, comprenant en outre les étapes consistant à :

lorsque le levier (36) se déplace dans la région centrale, calculer une valeur moyenne de position de levier de rétraction maximale si le levier (36) était précédemment dans la région de rétraction, ou calculer une valeur moyenne de position de levier d'extension maximale si le levier (36) était précédemment dans la région d'extension.
10

8. Procédé selon l'une quelconque des revendications 1 à 7, comprenant en outre les étapes consistant à :

transmettre un nouvel ordre à l'unité de commande de soupape (28) si le nouvel ordre diffère de l'ordre précédent et si un certain temps s'est écoulé depuis que l'ordre précédent avait été transmis à l'unité de commande de soupape (28).
15

9. Procédé selon l'une quelconque des revendications 1 à 8, comprenant en outre l'étape consistant à :

empêcher une transmission d'un ordre à l'unité de commande de soupape (28) si l'ordre change et que moins d'un certain temps s'est écoulé depuis que l'ordre précédent avait été transmis à l'unité d'ordre de soupape (28).
20

10. Procédé selon l'une quelconque des revendications 1 à 9, dans lequel :

la valeur moyenne de position de levier de rétraction maximale $A_{max}(r)$ est une moyenne d'une valeur actuelle de position de levier de région de rétraction maximale R_{max} , multipliée par le facteur de mise à l'échelle C, et une valeur $A_{max}(r)$ précédente stockée ; et
la valeur moyenne de position de levier d'extension maximale $A_{max}(e)$ est une moyenne de la valeur de position actuelle de levier de région d'extension maximale E_{max} , multipliée par le facteur de mise à l'échelle C, et la valeur $A_{max}(e)$ précédente stockée.
25
30

11. Procédé selon l'une quelconque des revendications 1 à 10, comprenant en outre les étapes consistant à :

déterminer et stocker les valeurs de position d'extension de levier et les valeurs de position de rétraction de levier lorsque le levier (36) se déplace à travers la région d'extension ;
déterminer à partir des valeurs de position d'extension de levier stockées une valeur d'extension de levier maximale ;
déterminer à partir des valeurs de position de rétraction de levier stockées une valeur de rétraction de levier maximale.
35
40

12. Procédé de génération d'un signal de commande de soupape selon l'une quelconque des revendications 1 à 11, comprenant les étapes consistant à :

lorsque le levier (36) est déplacé relativement lentement, générer un signal d'ordre qui est proportionnel au signal de position de levier ; et
lorsque le levier (36) est déplacé relativement rapidement, générer un signal d'ordre qui est basé sur une excursion maximale du levier (36) dans les régions d'extension et de rétraction.
45

13. Procédé de génération d'un signal de commande de soupape selon l'une quelconque des revendications 1 à 12, comprenant les étapes consistant à :

générer des signaux de commande avec une cadence qui est une fonction d'une fréquence (F) à laquelle le levier (36) est déplacé ; et
générer des signaux d'ordre ayant une grandeur qui est une fonction de l'ampleur du déplacement du levier (36) à partir de sa position centrale.
50
55

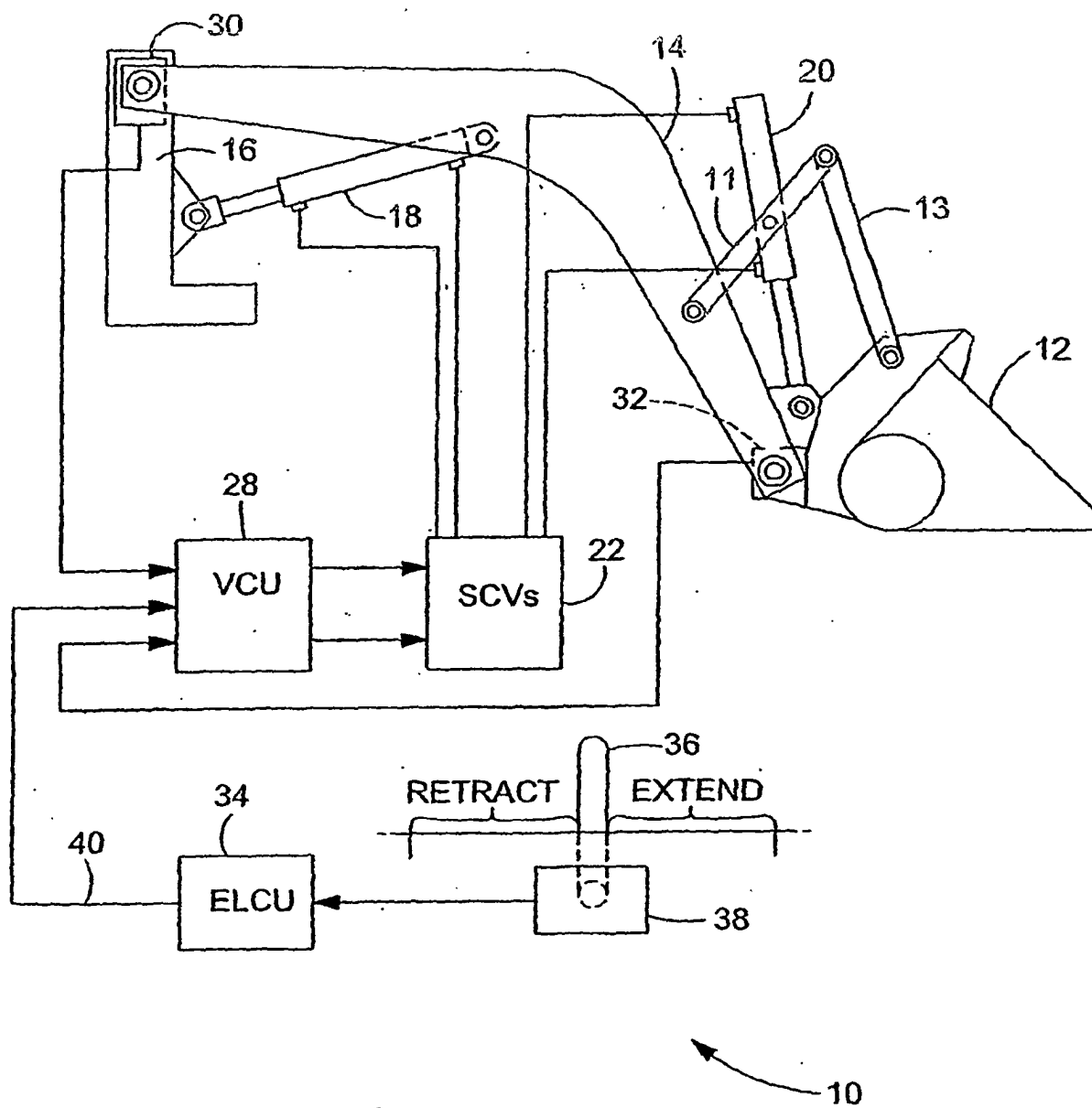


FIG. 1

FIG. 2A

FIG. 2A
FIG. 2B

FIG. 2

