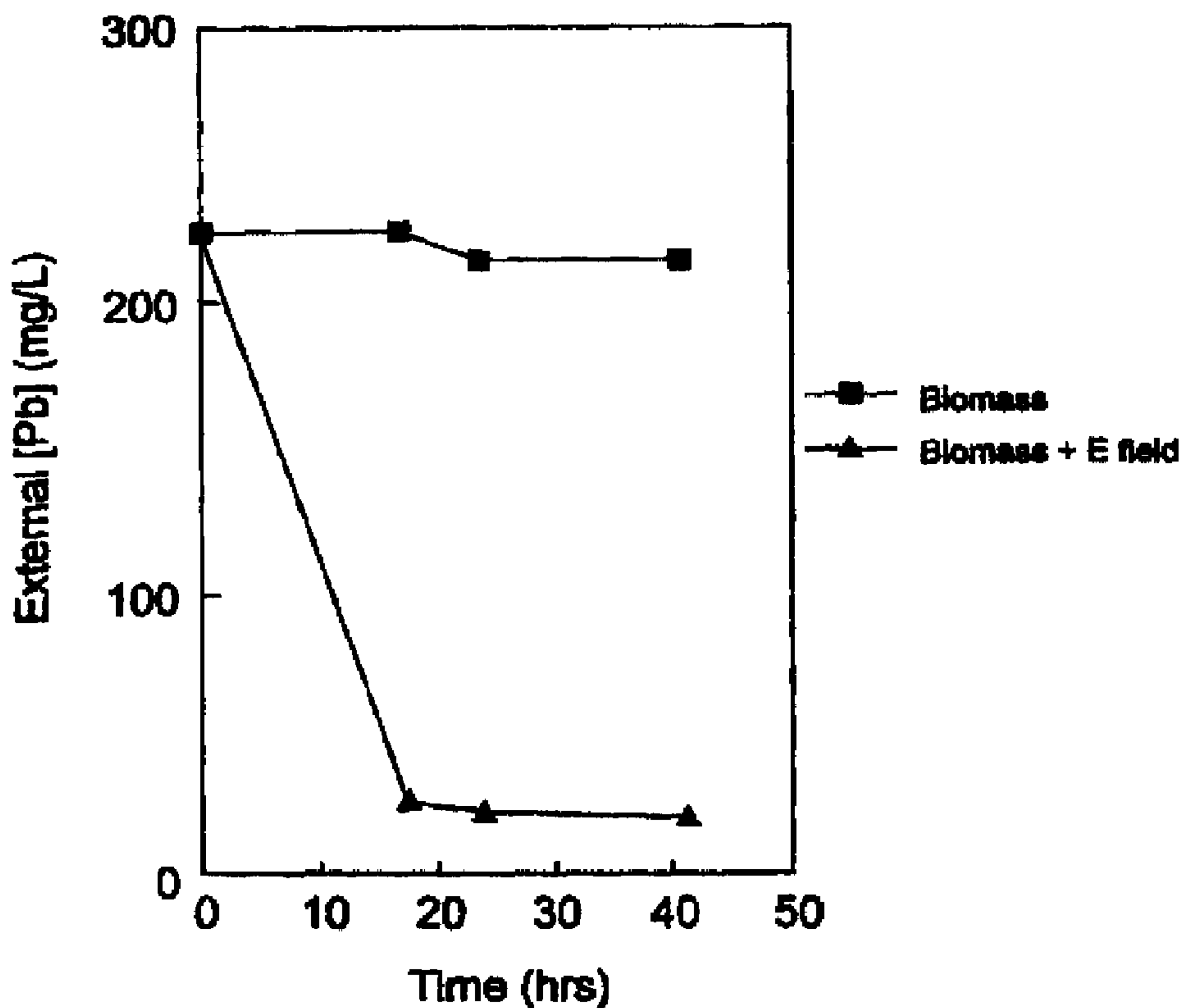




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(54) Titre : SYSTEME DE BIOSORPTION
 (54) Title: BIOSORPTION SYSTEM



(57) Abrégé/Abstract:

The invention relates to a system, process and apparatus for separating biosorbent and sorbate. Biomass enclosed within a membrane system is coupled to an electrode, which is capable of being placed in contact with the sorbate containing material in the presence of a counter electrode. An electric field may be discharged across the electrodes and ionic species will migrate into the membrane enclosed system. The migrated species within the membrane can be taken up and processed by the biosorbitive processes of the biomass. The system may be used to remove dye stuffs, metal, heavy metals, radionuclides and other pollutants from natural and artificial sources.

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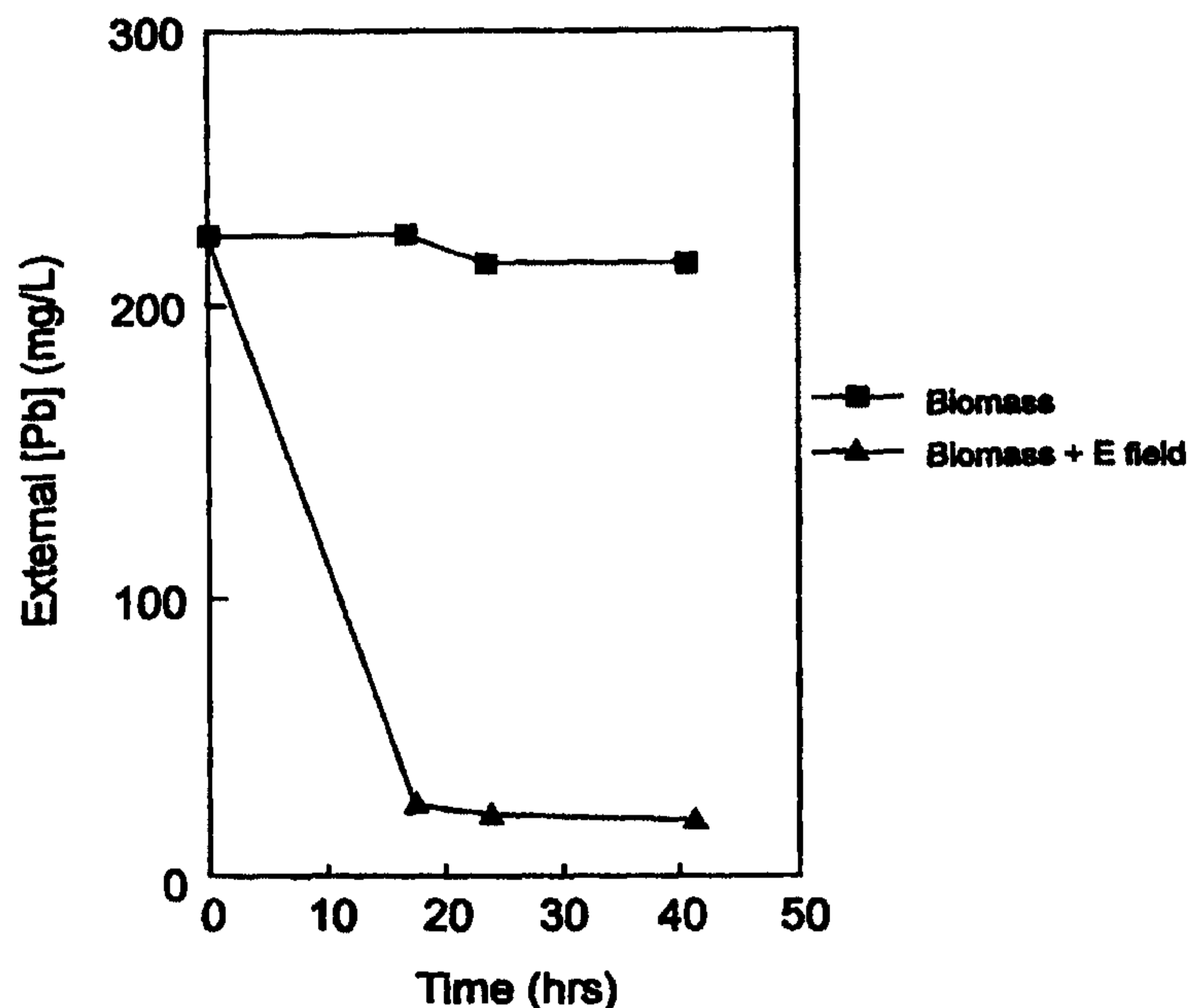
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(54) Title: BIOSORPTION SYSTEM



(57) Abstract

The invention relates to a system, process and apparatus for separating biosorbent and sorbate. Biomass enclosed within a membrane system is coupled to an electrode, which is capable of being placed in contact with the sorbate containing material in the presence of a counter electrode. An electric field may be discharged across the electrodes and ionic species will migrate into the membrane enclosed system. The migrated species within the membrane can be taken up and processed by the biosorbent processes of the biomass. The system may be used to remove dye stuffs, metal, heavy metals, radionuclides and other pollutants from natural and artificial sources.

1 **"Biosorption System"**

2

3 This invention relates to biosorption processes for
4 removal and recovery of heavy metals, radionuclides,
5 pollutants and other materials from the environment.

6

7 The existence of heavy metals and radionuclides and
8 pollutants such as dye stuffs in the environment
9 represent a long-term environmental hazard (Gadd and
10 White [1993] Trends in Biotechnol., 11, 353). In many
11 cases, when these materials are introduced into the
12 environment they are taken up by biological systems
13 including plant and microbial materials. It has been
14 proposed that this phenomenon, known as biosorption,
15 might be exploited in biotechnological processes
16 relating to metal removal/recovery from mining wastes,
17 domestic and industrial wastes and removal of
18 radionuclide contaminants present in waste waters from
19 the nuclear industry (McHale & McHale, [1994]
20 Biotechnol. Advances, 12, 647).

21

22 Although biosorption results in the uptake of metals
23 and radionuclides by microorganisms, no single
24 mechanism responsible for uptake has been identified.
25 The term "adsorption" suggests binding of a material to

1 the surface of an adsorbent. The term "absorption"
2 implies penetration of the sorbate through the surface
3 to an inner matrix. Since the uptake of
4 metals/radionuclides and other agents by microbes
5 appears to involve both types of process, the term
6 "biosorption" is most commonly applied to describe the
7 phenomenon.

8
9 In any previously proposed bioremediation systems
10 concerned with exploiting biosorptive processes, one of
11 the major problems encountered has been the efficient
12 separation of the biosorbent material from the relevant
13 waste water stream, particularly if large volumes are
14 to be processed. In many cases workers in the field
15 have suggested the use of immobilization systems in
16 order to facilitate re-use of the biosorbent material.
17 It has also been proposed that this would also
18 facilitate efficient separation from the relevant
19 waste-water stream and aid in the regeneration of the
20 biosorbent (McHale & McHale [1994] (Biotechnol
21 Advances), 12, 647).

22
23 In addition to the above complications associated with
24 the exploitation of biosorptive processes, solutions of
25 metals/radionuclides and other pollutants in waste-
26 water streams tend to be very dilute. Since
27 biosorptive processes, particularly using non-living
28 biomass are in many cases equilibrium events, the
29 inventors have found that uptake of the relevant
30 sorbate is usually enhanced by positively disturbing
31 those equilibria. They postulate that increasing the
32 concentration of the sorbate in the vicinity of the
33 biosorbent may tend to increase the degree of uptake
34 exhibited by any form of biomass.

35
36 Distribution of ions across a semipermeable membrane is

1 also an equilibrium event. However, removal of free or
2 soluble ions from solution within a membrane enclosed
3 compartment tends to unbalance that equilibrium and the
4 net flow of ions into the membrane enclosed space. The
5 inventors suggest that placing biosorbent material
6 inside a membrane-enclosed compartment and exposing
7 this to an external solution of ions would result in a
8 net flow of those ions into the enclosed space. In
9 effect this would achieve ion removal from the external
10 solution by a mechanism known as non-equilibrium
11 dialysis. It has the added advantage of ensuring
12 biosorbent and sorbate separation before, during and
13 after the ion removal/recovery process.

14
15 Although this offers many advantages over conventional
16 biosorption processes, this type of system would be
17 highly dependant on the rate of diffusion into the
18 inner compartment. It has previously been shown
19 however that it is possible to attract ions into
20 membrane-enclosed compartments using an electric field
21 and this is referred to a electrodialysis (Bobrinskaya
22 *et al.*, [1995] Russian J. Applied Chem. 68, 1205;
23 Ishimaru [1994] Desalination, 98, 485.). It has been
24 suggested that this may be exploited in processes such
25 as desalination of water although it is worth noting
26 that removal of the applied electric field in
27 conventional electrodialysis modalities, results in
28 leakage of the relevant ions from the membrane-enclosed
29 space.

30
31 It is one object of the present invention to provide a
32 system to remove and/or recover heavy
33 metals/metals/ionic species/radionuclides and/or
34 pollutants in general from the environment.

35
36

1 According to the present invention there is provided a system
2 for separating biosorbent and sorbate: the system comprising
3 biomass enclosed within a membrane system coupled to an
4 electrode capable of being placed in contact with sorbate
5 containing material in the presence of a counter electrode such
6 that an electric field may be discharged across the electrodes
7 and ionic species will migrate into the membrane enclosed
8 system.

9
10 According to another aspect of the invention there is provided
11 a biosorption process comprising the steps of exposing sorbate
12 containing material to biomass enclosed within a membrane and
13 generating an electric field in the sorbate containing material
14 in the vicinity of the membrane thereby causing sorbate to
15 migrate to the biomass.

16
17 According to another aspect of the invention there is provided
18 a biosorption apparatus comprising non-living biomass enclosed
19 within a membrane coupled to an electrode.

20
21 In another aspect, the invention relates to the use of
22 immobilized biomass in a system, apparatus or process as
23 described herein.

24
25 The biomass material may be living or non-living, modified or
26 non-modified, free or immobilized or any combination of these
27 forms.

28
29 In a particular embodiment, the biomass is distillery biomass.

30
31 In the system, the migrated species within the membrane can be
32 taken up and processed by the biosorptive process of the
33 biomass.

1 The electric field in the system may be generated in a
2 conventional manner and/or from renewable energy
3 sources including solar, wind and wave energy forms.

4

5 Suitably the system may be used to remove metals/heavy
6 metals/radionuclides and/or other pollutants from
7 natural and artificial sources and/or combinations
8 thereof.

9

10 In one embodiment the invention provides an apparatus
11 comprising modified non-living biomass enclosed within
12 a membrane system coupled to a platinum electrode.

13

14 Alternatively the biomass may be non-living.

15

16 The electrode may be of any other electrode material.

17

18 The apparatus may be placed in contact with the
19 sorbate-containing material in the present of a counter
20 electrode. An electric field will be discharged across
21 the electrodes and the ionic species will migrate into
22 the membrane enclosed system. The migrated species
23 within the membrane enclosed space will then be taken
24 up by the biosorptive processes exhibited by the
25 biomass.

26

27 The living or non-living biomass may be modified.

28

29 The living or non-living biomass may be immobilised.

30

31 In the embodiment described above the electric field
32 may be generated in the conventional manner and/or from
33 renewable energy resources including, although not
34 exclusively, solar, wind and wave energy forms.

35

36

1 In another embodiment the invention provides a device
2 (or derivative thereof) based on the use of
3 electrodiffusion-assisted biosorption and capable of
4 removing metals/heavy metals/ radionuclides/and/or
5 other pollutants from natural and artificial sources
6 and/or combinations thereof) for the purposes of
7 bioremediation and/or substance recovery.

8
9 The device (or derivative thereof) based on the use of
10 eletrodiffusion-assisted biosorption may be capable of
11 concentrating agents for analytical purposes.

12
13 In a third embodiment the invention provides a system
14 capable of generation of ionic species and subsequent
15 sequestration of these by the systems described herein.

16
17 The embodiments of the invention may be operated in
18 batch, fed-batch and/or continuous modes including
19 combinations thereof.

20
21 The embodiments of the invention may be operated in
22 conjunction with other processes.

23
24 The invention will comprise any of the above systems
25 and/or combinations of the above.

26
27 The invention will be described with reference to the
28 following examples and the accompanying drawings
29 wherein:

30
31 Figure 1 illustrates the sequestration of uranium at
32 relatively high concentrations using the
33 electrodiffusion-assisted biosorption system/process.

34
35
36

1 Figure 2 illustrates removal of uranium (at relatively
2 low concentrations) for solution using the
3 electrodiffusion-assisted biosorption system/process.
4

5 Figure 3 illustrates removal of lead from solution
6 using the electrodiffusion-assisted biosorption
7 system/process.
8

9 Figure 4 illustrates biosorption of Remazol red, golden
10 yellow and black B dyes by 1g/L distillery biomass.
11

12 **EXAMPLE 1**

13

14 *Removal of relatively high concentrations of uranium*
15 *from solution using electrodiffusion-assisted*
16 *biosorption:*
17

18 In these studies waste biomass was obtained from
19 industrial processes concerned with alcohol production
20 for the beverage industry. The biomass was washed by
21 centrifugation at 10,000xg for 20min. and subsequently
22 freeze dried. In the experiments described here 1g
23 (dry weight) biomass was resuspended in 10ml of
24 distilled water. This was then placed in dialysis
25 tubing (Visking tubing) which was closed at one end.
26 The membrane-enclosed system was fixed in place in a
27 beaker containing 500ml of 1mM uranyl acetate. A
28 platinum wire electrode (negative in this case) was
29 placed inside the open end of the dialysis tubing which
30 was vented to the air. The other electrode was placed
31 in the external solution. The electrodes were
32 connected to a power pack which was set to deliver a
33 constant voltage of 20V (it should be noted that the
34 proposed devices and/or systems described herein will
35 not be restricted with respect to delivered electric
36 parameters or electric field strengths). Samples from

1 the external solution were harvested at various times
2 and the concentration of uranium was determined using
3 the method described by Savvin ([1961], Talanta, 8,
4 673). In these experiments control systems consisted
5 of either biomass inside the dialysis membrane without
6 an applied electric field and using the dialysis
7 membrane without biomass but with an applied electric
8 field. The results obtained from these experiments are
9 shown in Fig.1. In the control consisting of the
10 biomass and no applied electric field (■) the external
11 concentration of uranium decreased from 195mg/L to 119
12 mg/L over a 25 hour period (Fig.1). In the control
13 involving the use of the electric field in the absence
14 of biomass (▼) the external uranium concentration
15 decreased from 190mg/L to 79mg/L over a 21 hour period.
16 In the test system consisting of the biomass and
17 electrodiffusion-assisted transfer of uranium into the
18 enclosed compartment (▲), the external uranium
19 concentration decreased from 195mg/L to 33mg/L over a
20 23 hour period. This demonstrated that 162mg of
21 uranium had concentrated within the 10ml volume inside
22 the dialysis tubing. It is also worth noting that at
23 each time point the external concentration of uranium
24 in the electrodiffusion system containing the biomass
25 was lower than that in the system without the biomass,
26 hence our use of the term "electrodiffusion-assisted
27 biosorption".

28

29 **EXAMPLE 2**

30

31 *Removal of relatively low concentrations of uranium from*
32 *solution using the electrodiffusion-assisted*
33 *biosorption system:*

34

35 The experimental configuration described for Example 1
36 was similar in these experiments except that the

1 external concentration of uranium was adjusted from 1mM
2 to 0.074mM. In addition 0.5g of biomass was suspended
3 in 5 ml of distilled water and this was placed inside
4 the dialysis tubing. This was then inserted into a
5 beaker containing 250ml of the uranium solution. In
6 this case the control consisted of biomass but in the
7 absence of applied electric field. The results are
8 shown in Fig.2. In the control system (▲) the
9 concentration of uranium decreased from 17.4mg/L to
10 2.86mg/L within 24 hours and to 1.42mg/L within 48
11 hours. In the test system (■) however the
12 concentration of uranium decreased from 17.6mg/L to
13 0.5mg/L in 24 hours and to 0.3mg/L within 48 hours. It
14 should be noted that the figure of 0.3mg/L for the
15 concentration of uranium is outside the lower
16 confidence limits of the assay used to detect uranium.

17

18 **EXAMPLE 3**

19

20 *Removal of lead from solution using the*
21 *elctrodifffusion-assisted biosorption system:*

22

23 In this part of the study a similar configuration to
24 that used in Example 2 above was used except that the
25 uranium solution was replaced with lead nitrate at a
26 concentration of 230mg/L. In addition the
27 concentration of lead was determined using atomic
28 absorption spectrophotometry. The control consisted of
29 biomass within the membrane-enclosed compartment and no
30 electric field was applied. The results are shown in
31 Fig.3. In the control system (■) the external
32 concentration of lead decreased to a concentration of
33 216.7mg/L after 41 hours. In the test system (▲) the
34 external concentration of lead decreased to 18.7mg/L
35 indicating a 91.9% overall decrease in external
36 concentrations.

1 **EXAMPLE 4**

2

3 *Biosorption of textile dyes by distillery-derived*
4 *biomass:*

5

6 The objective of this part of the study was to
7 demonstrate that the distillery-derived biomass was
8 capable of textile dye biosorption. In fulfilling this
9 objective it was decided to employ commonly used
10 textile dyes including Remazol red, golden yellow and
11 Remazol black B. Solutions of dye were prepared in
12 distilled water and used as the sorbate. The
13 concentrations of the Remazol red, Remazol golden
14 yellow and the Remazol black B were measured
15 spectrophotometrically at 520, 410 and 600nm,
16 respectively. Biomass was placed in contact with the
17 dye solution in 10ml contact reactions and those
18 reactions were allowed to continue for a period of 12
19 hours. The biomass was then removed (by either
20 centrifugation or membrane filtration [0.2 μ m filtration
21 units]) and the residual concentration of dye (C_e mg/L)
22 remaining in solution was determined using a
23 spectrophotometer. From those values the amount of dye
24 associated with the biomass q (mg/g dry weight biomass)
25 was determined and the data were used to construct
26 biosorption isotherms. The results are shown in Fig.4
27 which is a graph of q (mg/g) vs C_e (mg/L). The error
28 bars represent S.E.M, $n=6$. This experiment
29 demonstrates that the biomass is capable of binding
30 significant quantities of dye. From the data presented
31 maximum biosorption capacities (q_{max} mg/g dry weight
32 biomass) of 97, 107 and 62 mg/g were obtained for the
33 Remazol red, Remazol golden yellow and Remazol black B,
34 respectively.

35

36

1 **EXAMPLE 5**

2

3 *Electrodifusion assisted treatment of a textile dye*
4 *containing effluent from William Clark & Sons Limited,*
5 *a local textile processing plant: in Upperlands,*
6 Maghera, Co Londonderry.

7

8 One objective in this part of the study was to
9 determine whether or not the electrodiffusion assisted
10 system might provide a novel and alternative means of
11 treating and decolorising textile dye containing
12 effluent. In order to do this, it was decided to
13 obtain a sample of effluent from a local textile
14 processing plant, William Clark & Sons Limited,
15 Upperlands, Maghera, Co Londonderry. Raw effluent was
16 obtained from a holding tank outlet at the plant. It
17 had a murky blue green appearance and contained a
18 significant quantity of particulate material. This
19 effluent was placed in the membrane-excluded space of
20 the electrodiffusion apparatus as described in Example
21 1 for the metal-bearing solutions. The normal
22 electrode configuration involved placing the negative
23 electrode in the membrane-enclosed space together with
24 the biomass. The positive electrode was placed in the
25 effluent which was in the membrane-excluded space. The
26 system was operated under the same conditions described
27 in Example 1 for a period of 12-24 hours. Results from
28 a typical run are summarized in Table 1. Parameters
29 such as suspended solids, the degree of decolorisation
30 and removal of COD were measured before and after
31 treatment.

32

Table 1 - Treatment of textile processing effluent using the electrodiffusion-assisted biosorption system

Parameter measured	Before	After
Suspended Solids (mg/L)	50-55	0-0.6
Decolorisation (%)	0	96-98
Control 1*	0	33.9
Control 2*	0	34.6
COD (mg/L)	171	89

Control 1 for the decolorisation experiments consisted of the system using only the electrodes and excluding the biomass from the system whereas Control 2 consisted of the biomass without the application of an electric field.

1 Suspended solid content was measured using dry weight
2 analysis in combination with filtration through Whatman
3 grade I filter paper. In the untreated material the
4 suspended solids were determined to be in the region of
5 50-55mg/L and this was reduced to 0.6mg/L within a 12
6 hour period. In this case it appeared the evolution of
7 gas from the positive electrode in the membrane-
8 excluded space resulted in floatation of particulate
9 material and this could be recovered by skimming from
10 the top of the treated solution. This also resulted in
11 a significant degree of decolorisation. In studying
12 decolorisation it was found that the effluents had a
13 λ_{max} at 600nm and therefore spectrophotometry could be
14 used to examine this parameter. It was found that the
15 system was capable of removing 96-98% of the colour
16 from the effluent and it should be stated that the
17 liquid in the membrane-excluded compartment was
18 colourless to the naked eye. In measuring the chemical
19 oxygen demand (COD) of the treated and untreated
20 effluent a commercial kit was used (Hach Europe Ltd.,

1 Belgium). It was found that almost 50% of the OD of
2 the untreated effluents could be removed using the
3 system. The results demonstrate that the
4 electrodiffusion system is capable of very effective
5 treatment of textile processing effluents, particularly
6 with respect to decolorisation.

7

8 In summary, the examples described herein demonstrate
9 the ability of the invention to significantly reduce
10 concentrations of a variety of pollutants and other
11 materials in the environment.

12

13 The invention is not limited to the embodiments
14 described above which may clearly be modified and/or
15 varied without departing from the scope of the
16 invention.

17

18

CLAIMS

1. A system for separating biosorbent and sorbate: the system comprising biomass enclosed within a membrane system coupled to an electrode capable of being placed in contact with sorbate containing material in the presence of a counter electrode such that an electric field may be discharged across the electrodes and ionic species will migrate into the membrane enclosed system.
2. A biosorption process comprising the steps of exposing sorbate containing material to biomass enclosed within a membrane and generating an electric field in the sorbate containing material in the vicinity of the membrane thereby causing sorbate to migrate to the biomass.
3. A biosorption apparatus comprising non-living biomass enclosed within a membrane coupled to an electrode.
4. A system as claimed in Claim 1 wherein the biomass material is living or non-living, modified or non-modified, free or immobilized or any combination of these forms.
5. A system as claimed in Claim 1 or Claim 4, wherein the electric field in the system is generated in a conventional manner and/or from renewable sources including solar, wind and wave energy forms.
6. Use of a system for separating biosorbents and sorbate as claimed in claim 1 to remove metals, heavy metals, radionuclides and/or other pollutants from natural and artificial sources and/or combinations thereof.
7. A system for separating biosorbent and sorbate as claimed in Claim 1 or 4, wherein the system is operated in batch, batch-fed and/or continuous mode including combinations thereof.

8. A system as claimed in claim 1 wherein the biomass is immobilized for biosorption.
9. A process as claimed in Claim 2 wherein the biomass material is living or non-living, modified or non-modified, free or immobilized, or any combination of these forms.
10. A process as claimed in Claim 2 or 9 wherein the electric field in the system is generated in a conventional manner and/or from renewable sources including solar, wind and wave energy forms.
11. A process as claimed in claim 2 wherein the biomass is immobilized for biosorption.
12. An apparatus as claimed in Claim 3 wherein the biomass material is living or non-living, modified or non-modified, free or immobilized or any combination of these forms.

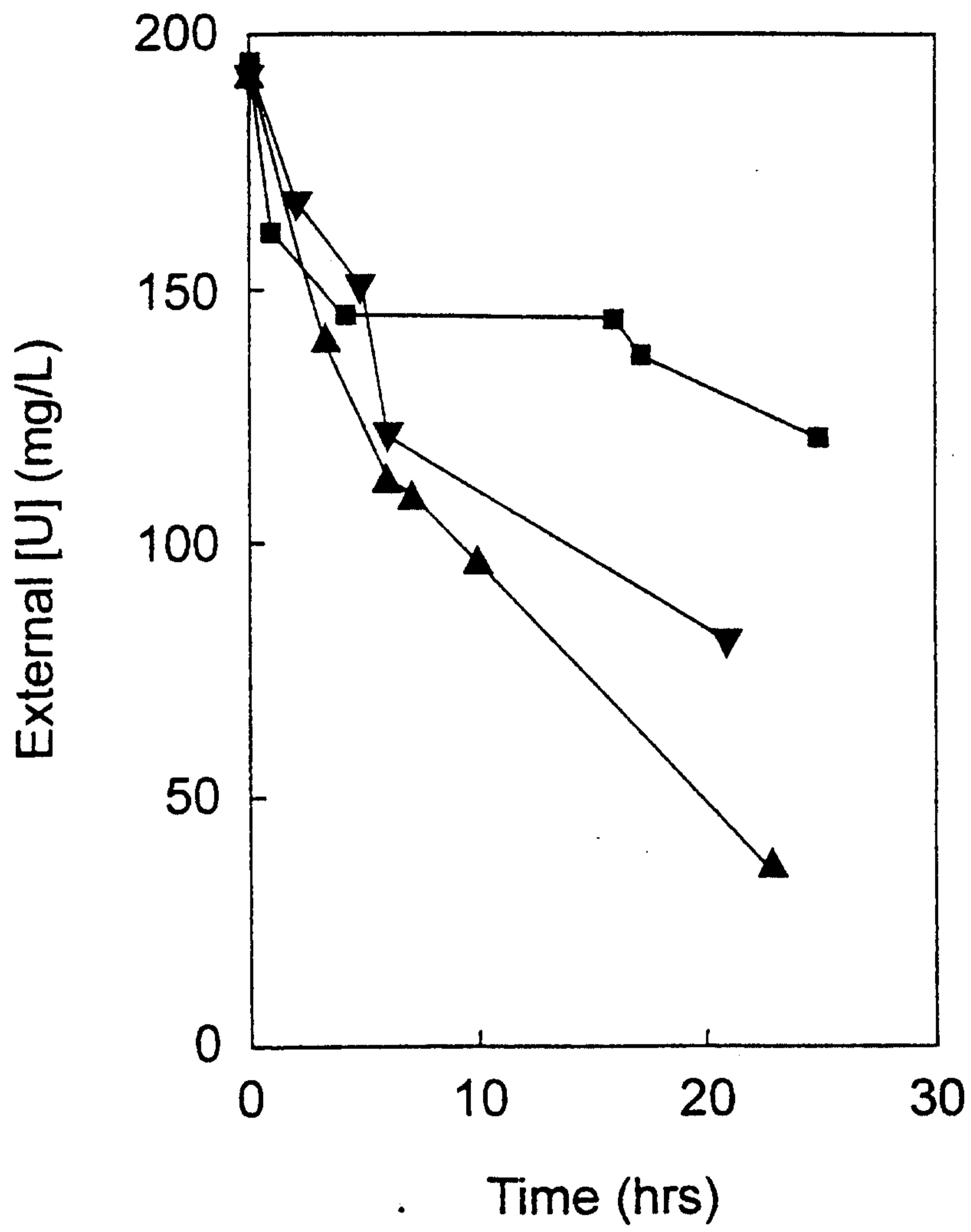
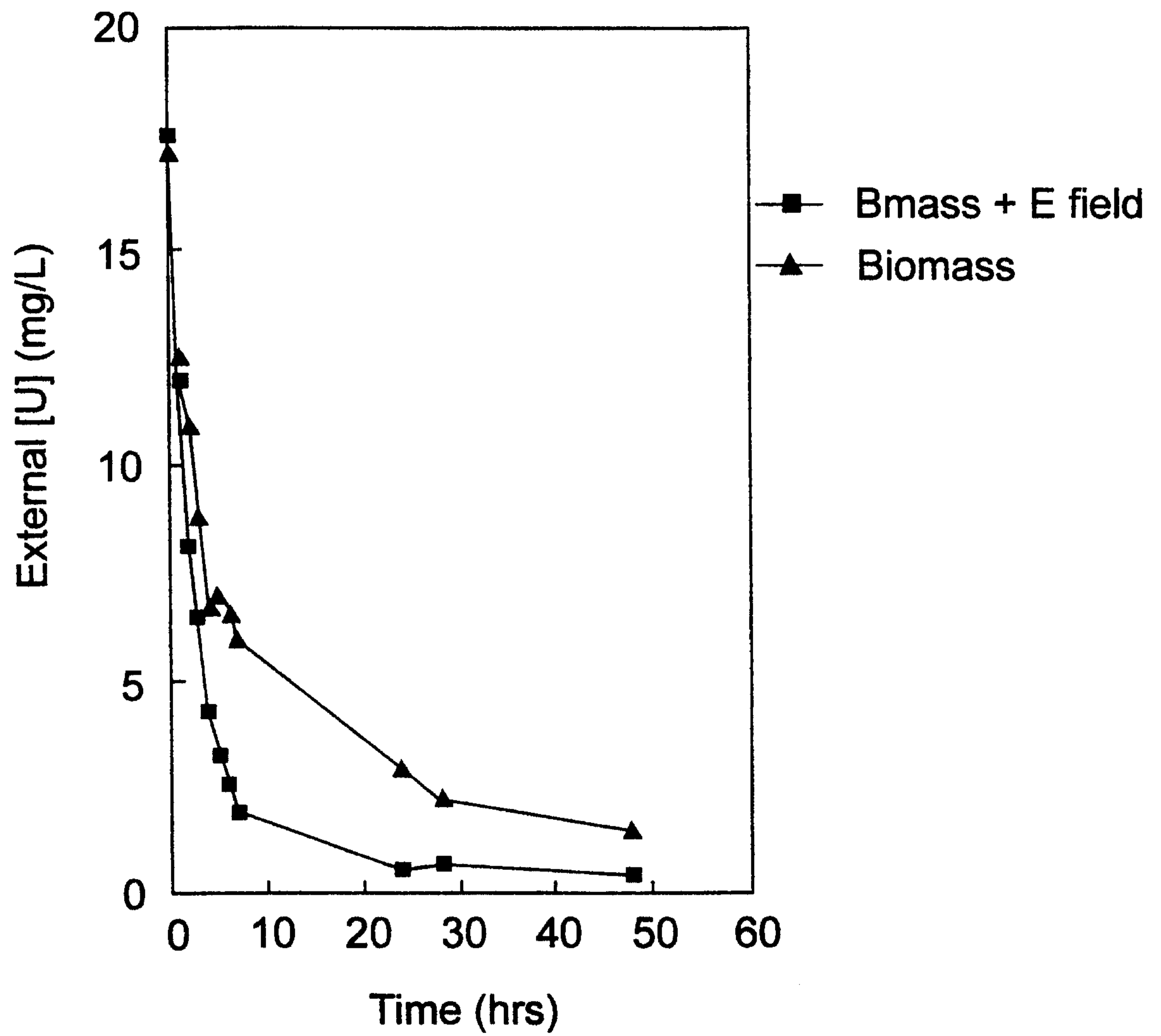
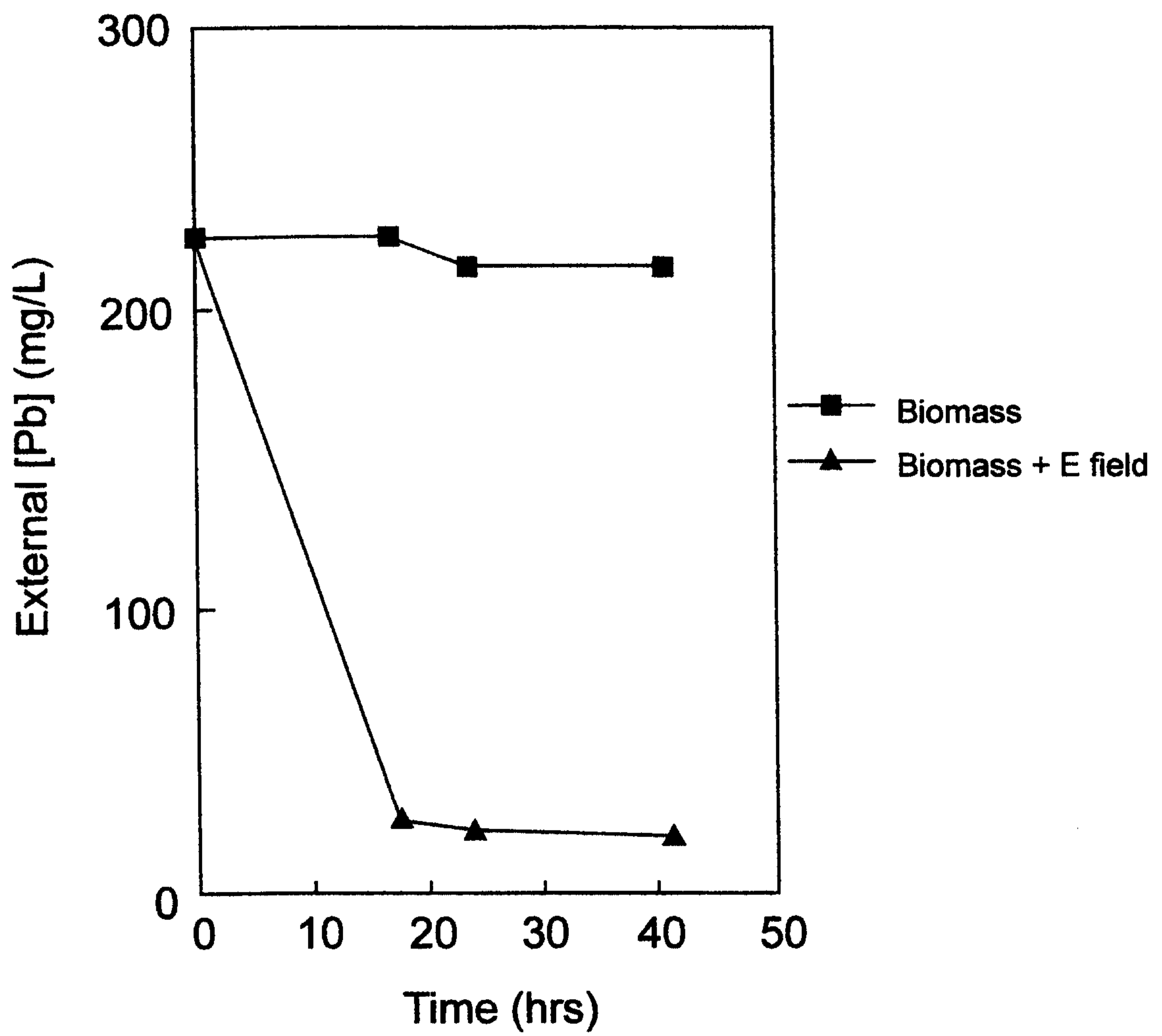


Fig. 1

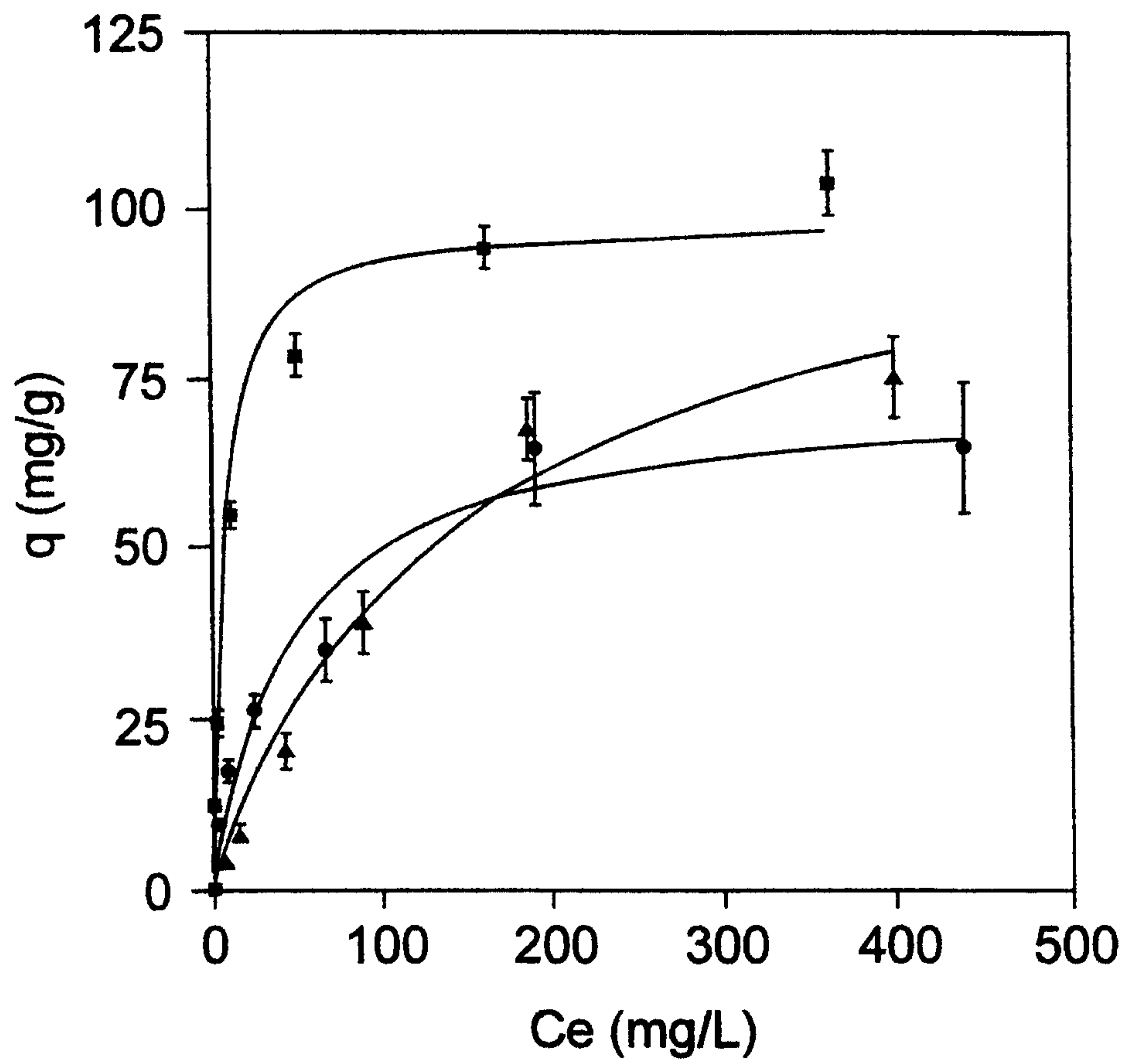
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*Fig. 2*

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*Fig. 3*

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*Fig. 4*

