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(54) Title: RANDOM ENGAGEMENT ROLLER CHAIN SPROCKET WITH STAGED MESHING AND FLANK RELIEF TO PROVIDE IMPROVED NOISE CHARACTERISTICS (57) Abstract A random engagement roller chain sprocket for use primarily in automotive engine chain drive applications which incorporates different asymmetrical tooth profiles for improved noise reduction. In particular, the sprocket includes a first plurality of sprocket teeth each having a first tooth profile including a first engaging flank, a first engaging root, and a first flat positioned between the first engaging flank and first engaging root wherein a first roller initially contacts the first flat at the onset of the first roller meshing with the sprocket. The sprocket also includes a second plurality of sprocket teeth each having a second tooth profile different from the first tooth profile and including a second engaging flank, a second engaging root, and a second flat tangent to the second engaging root remote from the second engaging flank wherein a second roller initially contacts the second flat at the onset of meshing between the second roller and the sprocket.		

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**RANDOM ENGAGEMENT ROLLER CHAIN SPROCKET WITH
STAGED MESHING AND FLANK RELIEF TO PROVIDE
IMPROVED NOISE CHARACTERISTICS**

Cross Reference to Related Applications

This application claims the benefit of U.S. Provisional Patent Application Serial No. 60/032,379, filed December 19, 1996.

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Background of the Invention

The present invention relates to the automotive timing chain art. It finds particular application in conjunction with a unidirectional roller chain sprocket for use in automotive camshaft drive applications and will be described with particular reference thereto. However, the present invention may also find application in conjunction with other types of chain drive systems and applications where reducing the noise levels associated with chain drives is desired.

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Roller chain sprockets for use in camshaft drives of automotive engines are typically manufactured according to ISO (International Organization for Standardization) standard 606:1994(E). The ISO-606 standard specifies requirements for short-pitch precision roller chains and associated chain wheels or sprockets.

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Figure 1 illustrates a symmetrical tooth space form for an ISO-606 compliant sprocket. The tooth space

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has a continuous fillet or root radius R_1 from one tooth flank (i.e., side) to the adjacent tooth flank. A chain with a link pitch P has rollers of diameter D_1 in contact with the tooth spaces. The ISO sprocket has a chordal pitch also of length P , a root diameter D_2 , and Z number of teeth. The tooth flank radius R_f , pitch circle diameter PD , tip diameter OD , tooth angle A (equal to $360^\circ/Z$), and roller seating angle α further define the ISO-606 compliant sprocket. The maximum and minimum roller seating angle α is defined as:

$$\alpha_{\max} = (140^\circ - 90^\circ)/Z \quad \text{and} \quad \alpha_{\min} = (120^\circ - 90^\circ)/Z$$

With reference to Figure 2, an exemplary ISO-606 compliant roller chain drive system **10** rotates in a clockwise direction as shown by arrow **11**. The chain drive system **10** includes a drive sprocket **12**, a driven sprocket **14** and a roller chain **16** having a number of rollers **18**. The sprockets **12**, **14**, and chain **16** each generally comply with the ISO-606 standard.

The roller chain **16** engages and wraps about sprockets **12** and **14** and has two spans extending between the sprockets, slack strand **20** and taut strand **22**. The roller chain **16** is under tension as shown by arrows **24**. The taut strand **22** may be guided from the driven sprocket **14** to the drive sprocket **12** with a chain guide **26**. A first roller **28** is shown at the onset of meshing at a 12 o'clock position on the drive sprocket **12**. A second roller **30** is adjacent to the first roller **28** and is the next roller to mesh with the drive sprocket **12**.

Chain drive systems have several components of undesirable noise. A major source of roller chain drive noise is the sound generated as a roller leaves the span

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and collides with the sprocket during meshing. The resultant impact noise is repeated with a frequency generally equal to that of the frequency of the chain meshing with the sprocket. The loudness of the impact noise is a function of the impact energy (E_A) that must be absorbed during the meshing process. The impact energy absorbed is related to engine speed, chain mass, and the impact velocity between the chain and the sprocket at the onset of meshing. The impact velocity is affected by the chain-sprocket engagement geometry, of which an engaging flank pressure angle γ (Fig. 3) is a factor, where:

$$E_A = \frac{wP}{2000} V_A^2 ;$$

$$V_A = \frac{\pi n P}{30000} \sin \left(\frac{360}{Z} + \gamma \right);$$

$$\gamma = \frac{180 - A - \alpha}{2}; \text{ and}$$

	E_A	=	Impact Energy [N·m]
	V_A	=	Roller Impact Velocity [m/s]
15	γ	=	Engaging Flank Pressure Angle
	n	=	Engine Speed [RPM]
	w	=	Chain Mass [Kg/m]
	Z	=	Number of Sprocket Teeth
	A	=	Tooth Angle ($360^\circ/Z$)
20	α	=	Roller Seating Angle
	P	=	Chain Pitch (Chordal Pitch)

The impact energy (E_A) equation presumes the chain drive kinematics will conform generally to a quasi-static analytical model and that the roller-sprocket driving contact will occur at a tangent point TP (Fig. 3) of the flank and root radii as the sprocket collects a roller from the span.

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As shown in Figure 3, the pressure angle γ is defined as the angle between a line A extending from the center of the engaging roller **30** normal to and through the tangent point TP of engaging flank radius R_f and root radius R_i , and a line B connecting the centers of an imaginary roller fully seated on the theoretical pitch diameter PD and the engaging roller **30** when fully seated on the theoretical pitch diameter PD. The roller seating angles α and pressure angles γ listed in Figure 27 are calculated from the equations defined above. It should be appreciated that γ is a minimum when α is a maximum. The exemplary 18-tooth, ISO-606 compliant, sprocket **12** of Figure 3 will have a pressure angle γ in the range of 12.5° to 22.5° as shown in Figure 27.

Figure 3 also shows the engagement path (phantom rollers) and the meshing contact position of roller **30** (solid) as the drive sprocket **12** rotates in the direction of arrow **11**. Figure 3 depicts the theoretical case with chain roller **28** seated on root diameter D_2 of a maximum material sprocket with both chain pitch and sprocket chordal pitch equal to theoretical pitch P . For this theoretical case, the noise occurring at the onset of roller engagement has a radial component F_{Ir} as a result of roller **30** colliding with the root surface R_i and a tangential component F_{It} generated as the same roller **30** collides with the engaging tooth flank at point TP as the roller moves into driving contact. It is believed that the radial impact occurs first, with the tangential impact following nearly simultaneously. Roller impact velocity V_A is shown to act through, and is substantially normal to, engaging flank tangent point TP with roller **30** in driving contact at point TP.

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The impact energy (E_A) equation accounts only for a tangential roller impact during meshing. The actual roller engagement, presumed to have a tangential and radial impact (occurring in any order), would therefore seem to be at variance with the impact energy (E_A) equation. The application of this quasi-static model, which is beneficially used as a directional tool, permits an analysis of those features that may be modified to reduce the impact energy that must be absorbed during the tangential roller-sprocket collision at the onset of meshing. The radial collision during meshing, and its effect on noise levels, can be evaluated apart from the impact energy (E_A) equation.

Under actual conditions as a result of feature dimensional tolerances, there will normally be a pitch mismatch between the chain and sprocket, with increased mismatch as the components wear in use. This pitch mismatch serves to move the point of meshing impact, with the radial collision still occurring at the root surface R_i but not necessarily at D_2 . The tangential collision will normally be in the proximity of point TP, but this contact could take place high up on the engaging side of root radius R_i or even radially outward from point TP on the engaging flank radius R_f as a function of the actual chain-sprocket pitch mismatch.

Reducing the engaging flank pressure angle γ reduces the meshing noise levels associated with roller chain drives, as predicted by the impact energy (E_A) equation set forth above. It is feasible but not recommended to reduce the pressure angle γ while maintaining a symmetrical tooth profile, which could be accomplished by simply increasing the roller seating angle α , effectively decreasing the pressure angle for both flanks. This profile as described requires that a

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worn chain would, as the roller travels around a sprocket wrap (discussed below), interface with a much steeper incline and the rollers would necessarily ride higher up on the coast flank prior to leaving the wrap.

5 Another source of chain drive noise is the broadband mechanical noise generated in part by shaft torsional vibrations and slight dimensional inaccuracies between the chain and the sprockets. Contributing to a greater extent to the broadband mechanical noise level
10 is the intermittent or vibrating contact that occurs between a worn roller chain and sprocket as the rollers travel around the sprocket wrap. In particular, ordinary chain drive system wear comprises sprocket tooth face wear and chain wear. The chain wear is
15 caused by bearing wear in the chain joints and can be characterized as pitch elongation. It is believed that a worn chain meshing with an ISO standard sprocket will have only one roller in driving contact and loaded at a maximum loading condition.

20 With reference again to Figure 2, driving contact at maximum loading occurs as a roller enters a drive sprocket wrap **32** at engagement. Engaging roller **28** is shown in driving contact and loaded at a maximum loading condition. The loading on roller **28** is
25 primarily meshing impact loading and the chain tension loading. The next several rollers in the wrap **32** forward of roller **28** share in the chain tension loading, but at a progressively decreasing rate. The loading of roller **28** (and to a lesser extent for the next several
30 rollers in the wrap) serves to maintain the roller in solid or hard contact with the sprocket root surface **34**.

A roller **36** is the last roller in the drive sprocket wrap **32** prior to entering the slack strand **20**. Roller **36** is also in hard contact with drive sprocket

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12, but at some point higher up (e.g., radially outwardly) on the root surface **34**. With the exception of rollers **28** and **36**, and the several rollers forward of roller **28** that share the chain tension loading, the remaining rollers in the drive sprocket wrap **32** are not in hard contact with the sprocket root surface **34**, and are therefore be free to vibrate against the sprocket root surfaces as they travel around the wrap, thereby contributing to the generation of unwanted broadband mechanical noise.

A roller **38** is the last roller in a sprocket wrap **40** of the driven sprocket **14** before entering the taut strand **22**. The roller **38** is in driving contact with the sprocket **14**. As with the roller **36** in the drive sprocket wrap **32**, a roller **42** in the sprocket wrap **40** is in hard contact with a root radius **44** of driven sprocket **14**, but generally not at the root diameter.

It is known that providing pitch line clearance (PLC) between sprocket teeth promotes hard contact between the chain rollers and sprocket in the sprocket wrap as the roller chain wears. The amount of pitch line clearance added to the tooth space defines a length of a short arc that is centered in the tooth space and forms a segment of the root diameter D_2 . The root fillet radius R_i is tangent to the flank radius R_f and the root diameter arc segment. The tooth profile is still symmetrical, but R_i is no longer a continuous fillet radius from one flank radius to the adjacent flank radius. This has the effect of reducing the broadband mechanical noise component of a chain drive system. However, adding pitch line clearance between sprocket teeth does not reduce chain drive noise caused by the roller-sprocket collision at impact.

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Chordal action, or chordal rise and fall, is another important factor affecting the operating smoothness and noise levels of a chain drive, particularly at high speeds. Chordal action occurs as the chain enters the sprocket from the free span during meshing and it can cause a movement of the free chain in a direction perpendicular to the chain travel but in the same plane as the chain and sprockets. This chain motion resulting from chordal action will contribute an objectionable noise level component to the meshing noise levels, so it is therefore beneficial to reduce chordal action inherent in a roller chain drive.

Figures 4a and 4b illustrate the chordal action for an 18-tooth, ISO-606 compliant, sprocket having a chordal pitch of 9.525 mm. Chordal rise **45** may conventionally be defined as the displacement of the chain centerline as the sprocket rotates through an angle $A/2$, where:

$$\text{Chordal rise} = r_p - r_c = r_p [1 - \cos(180^\circ/Z)]$$

where r_c is the chordal radius, or the distance from the sprocket center to a pitch chord of length P ; r_p is the actual theoretical pitch radius; and Z is the number of sprocket teeth.

It is known that a short pitch chain provides reduced chordal action compared to a longer pitch chain having a similar pitch radius. Figures 4a and 4b show only the drive sprocket and assume a driven sprocket (not shown) also having 18-teeth and in phase with the drive sprocket shown. In other words, at $T = 0$ (Fig. 4a), both sprockets will have a tooth center at the 12 o'clock position. Accordingly, this chain drive arrangement under quasi-static conditions will have a

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top or taut strand that will move up and down in a uniform manner a distance equal to that of the chordal rise. At $T = 0$, a roller **46** is at the onset of meshing, with chordal pitch P horizontal and in line with taut strand. At $T = 0 + (A/2)$, (Fig. 4b), roller **46** has moved to the 12 o'clock position.

For many chain drives, the drive and driven sprockets will be of different sizes and will not necessarily be in phase. The chain guide **26** (Fig. 2) has the primary purpose to control chain strand vibration in the free span. The geometry of the guide-chain interface also defines the length of free span chain over which chordal rise and fall is allowed to articulate. Figure 5 is an enlarged view of Figure 2 showing the first roller **28** at the onset of engagement and the second roller **30** as the next roller about to mesh with sprocket **12**. In this example, the chain guide **26** controls and guides the engaging portion of the taut strand **22** except for five (5) unsupported or "free" link pitches extending between the chain guide **26** and the engaging roller **28**. This length of unsupported link pitches for the engaging portion of taut strand **22** in this example is horizontal when roller **28** is at the 12 o'clock position.

With reference to Figures 6 and 7, the drive sprocket **12** is rotated in a clockwise direction to advance roller **28** to a new angular position $(A/2) + \omega$, where ω is the added rotation angle as determined by a quasi-static engagement geometry with roller **28** being fully seated and roller **30** is at the instant of sprocket engagement. As shown in Figure 6, roller **28** is considered to be seated and in hard contact with the root surface at D_2 at the onset of meshing of roller **30**,

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and a straight line is assumed for the chain span from roller **28** to a chain pin center **48**, about which the unsupported or "free" span from pin **48** to engaging roller **30** is considered to rotate.

5 As a result of the chordal action, the engaging free span is no longer horizontal to satisfy the roller engaging geometry. This is in contrast to the chain drive as described in Figure 4a in which chordal action causes the taut strand to move uniformly,
10 but in a horizontal path because the drive and driven sprockets have the same number of teeth and the sprocket teeth are in phase. It should be appreciated that the straight line assumption is valid only in a quasi-static model. The amount of movement or deviation from the
15 straight line assumption will be a function of the drive dynamics, the chain control devices and drive and sprocket geometry. The location and chain-interfacing contour of the chain guide **26** will determine the number of free span pitches about which articulation will take
20 place as a result of the chordal rise and fall during the roller meshing process.

As best seen in Figure 7, assuming that rollers **28** and **30** are in hard contact with the sprocket root surfaces at D_2 , the chordal rise is the
25 perpendicular displacement of the center of roller **30** (located on the pitch diameter PD) from the taut span **22** path as it moves from its initial meshing position shown to the position presently occupied by roller **28**.

Accordingly, it is desirable to develop a new
30 and improved roller chain drive system which meets the above-stated needs and overcomes the foregoing disadvantages and others while providing better and more advantageous results.

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Summary of the Invention

In accordance with one aspect of the present invention, a sprocket is disclosed. The sprocket includes a first plurality of sprocket teeth each having
5 a first tooth profile including a first engaging flank, a first engaging root, and a first flat positioned between the first engaging flank and first engaging root, a first roller initially contacting the first flat at the onset of the first roller meshing with the
10 sprocket. The sprocket further includes a second plurality of sprocket teeth each having a second tooth profile different from the first tooth profile and including a second engaging flank, a second engaging root, and a second flat tangent to the second engaging
15 root remote from the second engaging flank, a second roller initially contacting the second flat at the onset of meshing between the second roller and the sprocket.

In accordance with another aspect of the present invention, a sprocket is disclosed. The
20 sprocket includes a first plurality of sprocket teeth each having a first asymmetrical tooth profile which is constructed for providing a tangential contact with a first roller at an onset of the first roller meshing with the sprocket, and a second plurality of sprocket
25 teeth each having a second asymmetrical tooth profile which is constructed for providing a radial contact with a second roller at an onset of the second roller meshing with the sprocket.

In accordance with a further aspect of the present invention, a unidirectional roller chain drive
30 system is disclosed. The unidirectional roller chain drive system includes a first sprocket, a second sprocket, and a roller chain having rollers in engaging contact with the first and second sprockets. At least

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one of the first and second sprockets includes a first plurality of sprocket teeth each having a first tooth profile including a first engaging flank, a first engaging root, and a first flat positioned between the first engaging flank and first engaging root wherein a
5 first roller initially contacts the first flat at the onset of the first roller meshing with the sprocket. At least one of the first and second sprockets also includes a second plurality of sprocket teeth each
10 having a second tooth profile different from the first tooth profile and including a second engaging flank, a second engaging root, and a second flat tangent to the second engaging root remote from the second engaging flank, a second roller initially contacting the second
15 flat at the onset of meshing between the second roller and the sprocket.

In accordance with yet another aspect of the present invention, a method of modifying a meshing impact frequency of a roller chain meshing with a
20 sprocket is disclosed. The method includes (a) rotating the sprocket to cause a first roller of the roller chain to tangentially contact an engaging flank of a first sprocket tooth at an onset of the first roller meshing with the first sprocket tooth, and (b) rotating the
25 sprocket to cause a second roller of the roller chain to radially contact a root surface of a second sprocket tooth at an onset of the second roller meshing with the second sprocket tooth.

One advantage of the present invention is the
30 provision of a roller chain sprocket which incorporates a flank flat on an engaging tooth surface which facilitates altering a meshing contact from a first tooth profile to a second tooth profile.

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Another advantage of the present invention is the provision of a roller chain sprocket which incorporates a flank flat on an engaging tooth surface which effects a time delay between an initial roller-to
5 first sprocket tooth profile contact and an initial roller-to-second sprocket tooth profile contact.

Another advantage of the present invention is the provision of a roller chain sprocket which incorporates a flank flat on an engaging tooth surface
10 of a first tooth profile which facilitates phasing a frequency of initial roller-to-engaging flank contacts of the first tooth profile relative to initial roller-to-engaging flank contacts of a second tooth profile to alter the rhythm of the initial roller-to-first engaging
15 flank and the roller-to-second engaging flank contacts.

Another advantage of the present invention is the provision of a roller chain sprocket which incorporates added pitch mismatch between the sprocket and roller chain to facilitate a "staged" roller-to-
20 sprocket impact.

Still another advantage of the present invention is the provision of a roller chain sprocket which incorporates an inclined root surface on an engaging flank, a coast flank, or both an engaging flank
25 and a coast flank to provide tooth space clearance.

Yet another advantage of the present invention is the provision of a roller chain sprocket which minimizes impact noise generated by a roller-sprocket collision during meshing.

30 A further advantage of the present invention is the provision of a roller chain sprocket which minimizes broadband mechanical noise generated by unloaded rollers in a sprocket wrap.

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A still further advantage of the present invention is the provision of a roller chain sprocket which provides a "staged" roller impact wherein a tangential impact occurs first followed by a radial impact at full mesh.

Yet a further advantage of the present invention is the provision of a roller chain sprocket which spreads roller engagement over a significant time interval to provide for a more gradual load transfer, thereby minimizing roller-sprocket impact and the inherent noise generated therefrom.

Yet a further advantage of the present invention is the provision of a roller chain sprocket having two sets of sprocket teeth incorporating different tooth profiles which cooperate to reduce chain drive system noise levels below a noise level which either tooth profile used alone would produce.

Further advantages of the present invention will become apparent to those of ordinary skill in the art upon reading and understanding the following detailed description of the preferred embodiments.

Brief Description of the Drawings

The invention may take form in various components and arrangements of components, and in various steps and arrangements of steps. The drawings are only for purposes of illustrating a preferred embodiment and are not to be construed as limiting the invention.

Figure 1 illustrates a symmetrical tooth space form for a ISO-606 compliant roller chain sprocket;

Figure 2 is an exemplary roller chain drive system having a ISO-606 compliant drive sprocket, driven sprocket, and roller chain;

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Figure 3 shows an engagement path (phantom) and a roller (solid) in a driving position as a ISO-606 compliant drive sprocket rotates in a clockwise direction;

5 Figure 4a shows a roller at the onset of meshing with an exemplary 18-tooth sprocket;

 Figure 4b shows the drive sprocket of Figure 4a rotated in a clockwise direction until the roller is at a 12 o'clock position;

10 Figure 5 is an enlarged view of the drive sprocket of Figure 2 with a roller fully seated in a tooth space and a second roller about to mesh with the drive sprocket;

 Figure 6 shows the drive sprocket of Figure 5 rotated in a clockwise direction until the second roller initially contacts the drive sprocket;

 Figure 7 is an enlarged view of Figure 6 showing that the second roller initially contacts a root surface (i.e., radial impact) of the drive sprocket, under theoretical conditions;

 Figure 8 illustrates a roller chain drive system having a roller chain drive sprocket and driven sprocket which incorporate the features of the present invention therein;

25 Figure 9 illustrates the roller chain drive sprocket of Figure 8 with an asymmetrical tooth space form in accordance with one embodiment of the present invention;

 Figure 10 is an enlarged view of the asymmetrical tooth space form of Figure 9 showing a roller in two-point contact with the sprocket;

 Figure 11 shows an engagement path (phantom) and the instant of full mesh (solid) of a roller as the

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drive sprocket of Figure 8 rotates in a clockwise direction;

5 Figure 12 is an enlarged view of the drive sprocket of Figure 8 with a first roller fully seated in a tooth space and a second roller as the next roller to be collected from a taut span of the roller chain;

Figure 13 shows the drive sprocket of Figure 12 rotated in a clockwise direction until the second roller initially contacts the drive sprocket;

10 Figure 14 is an enlarged view of Figure 13 showing the first roller in two-point contact and second roller at initial tangential contact with the drive sprocket;

15 Figure 14a illustrates the progression of the first and second rollers as the drive sprocket of Figure 14 is rotated in a clockwise direction;

Figure 14b is an enlarged view of the drive sprocket of Figure 14 rotated in a clockwise direction to advance the second roller to the instant of full mesh at a 12 o'clock position;

20 Figure 15 illustrates a roller chain drive sprocket with an asymmetrical tooth space form in accordance with another embodiment of the present invention;

25 Figure 16 is an enlarged partial view of Figure 8, showing the contact progression as the rollers travel around the drive sprocket wrap;

Figure 17 is an enlarged view of a roller exiting a sprocket wrap of the sprocket of Figure 16;

30 Figure 18 illustrates a roller chain sprocket with an asymmetrical tooth space form in accordance with another embodiment of the present invention;

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Figure 19 illustrates a roller chain sprocket with an asymmetrical tooth space form in accordance with a further embodiment of the present invention;

5 Figure 20 is a side view of an exemplary random-engagement roller chain sprocket which incorporates the features of the present invention therein;

10 Figure 21 is an enlarged view of the sprocket of Figure 20 showing an asymmetrical tooth space form which incorporates engaging flank relief and tooth space clearance in accordance with the present invention;

Figure 21a is an enlarged view of the sprocket of Figure 21 showing an inclined root surface thereof which provides flank relief and tooth space clearance;

15 Figure 22 is another embodiment of the inclined root surface of Figure 21a which only provides flank relief;

20 Figure 23 illustrates the asymmetrical tooth space form of Figure 9 overlaid with the asymmetrical tooth space form of Figure 21;

Figure 24 illustrates the meshing progression of a first roller and the meshing of a second adjacent roller with the sprocket of Figure 20 as the sprocket is rotated in a clockwise direction;

25 Figure 25 illustrates the sprocket of Figure 20 with a first roller in two-point contact, a second roller at initial tangential contact, and a third roller about to mesh with the drive sprocket;

30 Figure 26 illustrates the sprocket of Figure 25 rotated in a clockwise direction until the instant of initial engagement of the third roller at a root surface of the sprocket;

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Figure 27 is a table listing roller seating angles α and pressure angles γ for a number of different ISO-606 complaint sprocket sizes; and

5 Figure 28 is a table listing the maximum Beta (β) angles and the corresponding pressure angles (γ) for three different asymmetrical tooth space profiles (1-3) of varying sprocket sizes.

Detailed Description of the Preferred Embodiments

10 With reference now to Figure 8, a roller chain drive system **110** includes a drive sprocket **112** and a driven sprocket **114** which incorporate the features of the present invention therein. The roller chain drive system **110** further includes a roller chain **116** having a number of rollers **118** which engage and wrap about sprockets **112**, **114**. The roller chain rotates in a clockwise direction as shown by arrow **11**.

15 The roller chain **116** has two spans extending between the sprockets, slack strand **120** and taut strand **122**. The roller chain **116** is under tension as shown by arrows **124**. A central portion of the taut strand **122** may be guided from the driven sprocket **114** to the drive sprocket **112** with a chain guide **126**. A first roller **128** is shown fully seated at a 12 o'clock position on the drive sprocket **112**. A second roller **130** is adjacent to the first roller **128** and is about to mesh with the drive sprocket **112**.

20 To facilitate a description of the asymmetrical tooth profiles of the present invention, reference will be made only to the drive sprocket **112**. However, the asymmetrical tooth profiles of the present invention can be equally applied to the driven sprocket **114**, as well as to other types of sprockets such as

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idler sprockets and sprockets associated with counter rotating balance shafts.

Referring now to Figures 9 and 10, the sprocket **112** includes a first tooth **132** having an engaging flank **134**, and a second tooth **136** having a coast or disengaging flank **138**. The engaging flank **134** and coast flank **138** cooperate to define a tooth space **140** which receives the engaging roller **128** (shown in phantom). The engaging roller **128** has a roller diameter D_1 , and is shown fully seated in two-point contact within the tooth space **140** as described further below. More particularly, the engaging roller **128**, when fully seated in the tooth space, contacts two lines B and C that extend axially along each sprocket tooth surface or face (i.e., in a direction orthogonal to the plane of the drawings). However, to facilitate a description thereof, the lines A, B, and C are hereafter shown and referred to as contact points within the tooth space.

The engaging flank **134** has a radius R_f which is tangent to a radially outer end of a flank flat **144**. The asymmetrical engaging flank radius R_f is smaller than the R_{fISO} radius specified by the ISO-606 standard. However, the magnitude of the asymmetrical engaging flank radius R_f should be as large as possible while still satisfying the roller meshing (engaging) and disengaging geometry. The location of the flank flat **144** is defined by an angle β , with the flat orientation being normal or perpendicular to a line that passes through Point B and the center of roller **128** when the roller is contacting the sprocket at Points B and C. The length of the flank flat, which extends radially outward from Point B, affects a time delay between an initial tangential impact between sprocket **112** and

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roller **128** at a first contact Point A along the flank flat **144**, and a subsequent radial impact at Point C. It is believed that the roller stays in contact with the flank flat from its initial tangential contact at Point A until the roller moves to a fully engaged two-point contact position at Points B and C. The pressure angle γ , the amount of pitch mismatch between the chain and the sprocket, and the length of the flank flat can be varied to achieve a desired initial roller contact Point A at the onset of roller-sprocket meshing.

It should be appreciated that flank (tangential) contact always occurs first, with radial contact then occurring always at Point C regardless of chain pitch length. In contrast, with known tooth space forms (e.g., ISO-606 compliant and asymmetrical) incorporating single-point contact (e.g. single line contact), an engaging roller must move to a driving position after making radial contact. The pressure angles γ therefore assume that the engaging roller will contact at the flank radius/root radius tangent point. Thus, the meshing contact location of the known single point/line tooth space forms is pitch "sensitive" to determine where the radial impact as well as tangential impact will occur.

The engaging flank roller seating angle β (Fig. 9) and a disengaging flank roller seating angle β' replace the ISO-606 roller seating angle α (ISO profile shown in phantom). The pressure angle γ is a function of the engaging flank roller seating angle β . That is, as β increases, γ decreases. A minimum asymmetrical pressure angle can be determined from the following equation, where:

$$\gamma_{\min} = \beta_{\max} - (\alpha_{\max} / 2 + \gamma_{\text{ISO min}})$$

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Therefore, an asymmetrical pressure angle γ_{\min} = 0 when $\beta_{\max} = (\alpha_{\max} / 2 + \gamma_{\text{ISO min}})$ as illustrated in Figure 28. Figure 28 lists the maximum Beta (β) angles and the corresponding pressure angles (γ) for several sprocket sizes of three different asymmetrical tooth space profiles (1-3). It should be appreciated that reducing the engaging flank pressure angle γ reduces the tangential impact force component F_{IA} (Fig. 14) and thus the tangential impact noise contribution to the overall noise level at the onset of engagement.

That is, the impact force F_{IA} is a function of the impact velocity which in turn is related to pressure angle γ . As pressure angle γ is reduced, it provides a corresponding reduction in the impact velocity between the chain and the sprocket at the onset of meshing. A minimum pressure angle γ also facilitates a greater separation or distance between tangential contact points A and B to further increase or maximize engagement "staging". In the preferred embodiment, the engaging flank pressure angle γ is in the range of about -2.0° to about $+5^\circ$ to optimize the staged impact between the roller and the sprocket.

In the embodiment being described, roller seating angle β is greater than ISO $\alpha_{\max}/2$ at a maximum material condition and β can be adjusted until a desired engaging flank pressure angle γ is achieved. For instance, the roller seating angle β of Figure 9 provides a pressure angle γ that is less than zero, or a negative value. The negative pressure angle γ is best seen in Figure 11, as contrasted with the ISO-606 compliant tooth profile of Figure 3 with a positive pressure angle γ . It is believed that a small negative pressure angle for the theoretical chain/sprocket interface beneficially provides a pressure angle γ

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closer to zero (0) for a "nominal" system or for a system with wear. However, the engaging flank roller seating angle β may be beneficially adjusted so as to provide any engaging flank pressure angle γ having a value less than the minimum ISO-606 pressure angle.

Referring again to Figures 9 and 10, a first root radius R_i is tangent to a radially inner end of the flank flat **144**, and tangent to a radially outer end of an inclined root surface **146**. As best seen in Figure 10, a maximum root radius R_i must be equal to, or less than, a minimum roller radius $0.5D_1$ to facilitate the fully engaged two-point/line contact at Points B and C. Accordingly, this will define a small clearance between R_i at the engaging flank **134** and the roller **128** at the two-point/line engagement. The flank flat **144** and the inclined root surface **146** necessarily extend inside Points B and C respectively to facilitate the two-point/line roller contact at engagement as well as the required clearance R_i to the roller **128**. A second root radius R_i' is tangent to a radially inner end of the inclined root surface **146** at line **150**. The coast flank has a radius R_f' with its arc center defined by disengaging side roller seating angle β' . The radius R_f' can have a value in the ISO-606 range.

The inclined root surface **146** is a flat surface having a finite length which defines a tooth space clearance (TSC). The tooth space clearance compensates for chain pitch elongation or chain wear by accommodating a specified degree of chain pitch elongation ΔP . In other words, the tooth space clearance TSC enables rollers of a worn chain to be maintained in hard contact with the inclined root surface of the sprocket teeth. In addition, the inclined root surface **146** facilitates reducing the

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radial reaction force thereby reducing the roller radial impact noise contribution to the overall noise level.

The inclined root surface **146** may be inclined at any angle ϕ necessary to satisfy a specific chain drive geometry and chain pitch elongation. As shown in Figure 9, the inclined root surface angle ϕ is measured from a line **152** passing through the center of roller **128** and the sprocket center to a second line **154** which also passes through the center of roller **128** and Point C. The inclined root surface **146** is normal to the line **154**, and the inclined root surface extends radially inward to line **150** where it is tangent to R_1' . In the embodiment being described, the inclined root surface angle ϕ is preferably in the range of about 20° to about 35° .

Figure 12 is an enlarged view of Figure 8 showing the first roller **128** at full engagement in two-point/line contact across the thickness or width of the sprocket tooth profile, and the second roller **130** as the next roller about to mesh with sprocket **112**. As with the ISO-606 compliant drive system **10**, the chain guide **126** controls and guides a central portion of the taut strand **122** except for five unsupported link pitches extending between the chain guide **126** and the engaging roller **128** (and except for the unsupported link pitches extending between the driven sprocket and the chain guide). The taut strand **122** is horizontal when roller **128** is at the 12 o'clock position.

Figure 13 shows the drive sprocket **112** rotated in a clockwise direction $(A/2) + \omega$, as determined by the instant of sprocket engagement by roller **130**. A straight line is assumed for the chain span from roller **128** to a chain pin center **156**, about which the unsupported span from pin center **156** to engaging roller

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130 is considered to rotate. It should be appreciated that the straight line assumption is valid only in a quasi-static model. The amount of movement (or deviation from the straight line assumption) previously mentioned will be a function of the drive dynamics as well as the drive and sprocket geometry.

The sprocket contact at the onset of mesh for roller 130 occurs earlier than for the ISO-606 counterpart, thereby reducing the amount of chordal rise and, just as importantly, allows the initial contact to beneficially occur at a desired pressure angle γ on the engaging flank at Point A. Furthermore, the radial sprocket contact for roller 130, with its contribution to the overall noise level, does not occur until the sprocket rotation places roller 130 at the 12 o'clock position. This is referred to as staged engagement.

Figure 14, an enlarged view of Figure 13, more clearly shows the onset of meshing for roller 130. Just prior to the onset of mesh, roller 128 is assumed to carry the entire taut strand load $F_{TB} + F_{\theta}$, which load is shown as force vector arrows. Actually, the arrows represent reaction forces to the taut strand chain force. At the instant of mesh for roller 130, a tangential impact occurs as shown by impact force vector F_{IA} . The tangential impact is not the same as the taut strand chain loading. In particular, impact loading or impact force is related to the impact velocity V_A . It is known that impact occurs during a collision between two bodies, resulting in relatively large forces over a comparatively short interval of time. A radial impact force vector F_{IC} is shown only as an outline in that the radial impact does not occur until the sprocket has rotated sufficiently to place roller 130 at a 12 o'clock position.

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Figure 14a shows the same roller positions (solid) for rollers **128** and **130** as shown in Figure 14, but in addition, shows the roller positions (in phantom) relative to the sprocket profile once roller **130** reaches its two-point/line mesh at the 12 o'clock position. As a result of the pitch mismatch between the chain and sprocket, roller **128** must move to a new position. In particular, as roller **130** moves from initial contact to full mesh, roller **128** progresses forward in its tooth space. Small clearances in the chain joints, however, reduce the amount of forward progression required for roller **128**. Also occurring at the onset of meshing is the beginning of the taut strand load transfer from roller **128** to roller **130**.

The asymmetrical profile provides for the previously described "staged" meshing. In particular, referring again to Figure 14, the Point A tangential contact occurs at the onset of mesh, with its related impact force F_{IA} . The roller **130** is believed to stay in hard contact with the engaging flank **134** as the sprocket rotation moves the roller into full mesh with its resulting radial contact at Point C. The radial impact force F_{IC} (force vector shown as an outline) does not occur until the sprocket has rotated sufficiently to bring roller **130** into radial contact at Point C.

Figure 14b is an enlarged view of Figure 14, except that sprocket **112** has been rotated to advance roller **130** to the instant of full mesh at the 12 o'clock position. At this instant of full mesh, the radial impact force F_{IC} occurs and the taut strand load transfer is considered to be complete. At the instant of the radial collision by roller **130** at Point C, with its resultant radial impact force F_{IC} , the tangential impact

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force of F_{IA} has already occurred and is no longer a factor. The time delay ("staged" engagement) between the tangential and radial roller-sprocket collisions effectively spreads the impact energy that must be absorbed during the meshing process over a greater time interval, thereby reducing its contribution to the generated noise level at mesh frequency. Additionally, it is believed that the present asymmetrical sprocket tooth profile beneficially permits a more gradual taut strand load transfer from a fully engaged roller **128** to a meshing roller **130** as the meshing roller **130** moves from its Point A initial mesh to its full two-point mesh position.

Referring again to Figure 14, the chordal rise (and fall) with the present asymmetrical profile is the perpendicular displacement of the center of roller **130** from the taut strand **122** path as it moves from its initial meshing contact Point A to the mesh position presently occupied by roller **128**. It is believed that roller **130** will stay in hard contact with the engaging flank **134** as the roller moves from initial tangential contact to full mesh, and accordingly, the chordal rise is reduced as the distance between Points A and B is increased. As shown in Figure 14, chain pitch P_c is beneficially greater than sprocket **112** chordal pitch P_s .

Referring now to Figure 15, the length of the inclined root surface **146** (Fig. 10) may be reduced to zero (0), thereby eliminating the inclined roof surface **146** and permitting root radius R_1' to be tangent to the root surface and the roller **128** at Point C. That is, R_1' is tangent to a short flat at Point C, and the flat is tangent to R_1 . If the inclined root surface **146** is eliminated, the engaging flank pressure angle γ would

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generally be in the range of some positive value to zero, but normally not less than zero. The reason is that a negative γ requires chordal pitch reduction so that the roller can exit the sprocket wrap **60** (Fig. 16) without interfering with R_f .

Figure 16 shows the roller contact to the sprocket **112** profile for all the rollers in the wrap **60**. Roller **128** is in full two-point mesh as shown. Line **160** shows the contact point for each of the rollers, as well as the contact progression as the rollers travel around the wrap. The inherent pitch mismatch between the sprocket and roller chain causes the rollers to climb up the coast side flank as the rollers progress around the sprocket wrap. With the addition of appreciable chordal pitch reduction, the extent to which the rollers climb up the coast side flank is increased.

It is important to note that chordal pitch reduction is required when the pressure angle γ has a negative value. Otherwise, as shown in Figures 16 and 17, roller **136** would interfere with the engaging flank (with a maximum material sprocket and a theoretical pitch [shortest] chain) as it exits the wrap **60** back into the span. That is, chordal pitch reduction permits the roller **136** to exit the wrap **60** with a clearance **163** for the engaging flank. Also, the reduced chordal pitch assists the staged mesh as previously mentioned. Figure 17, showing the roller contact progression in the wrap **60**, serves also to show why the shallow β' angle and tooth space clearance TSC helps maintain "hard" roller-sprocket contact for the rollers in the wrap.

In addition, the disengaging flank roller seating angle β' (Fig. 9) may be adjusted to have a maximum value which is equal to $\alpha_{\min}/2$ or even less. This reduced roller seating angle β' promotes faster

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separation when the roller leaves the sprocket and enters the span. This reduced angle β' also allows for the roller in a worn chain to ride up the coast flank surface to a less severe angle as the roller moves
5 around the sprocket in the wrap. Accordingly, chordal pitch reduction, if used in this embodiment, should be a small value.

It is contemplated that the above-described asymmetrical tooth profile features can be altered
10 without substantially deviating from the chain and sprocket meshing kinematics that produce the noise reduction advantages of the present invention. For example, the engaging asymmetrical flank profile could be approximated by an involute form, and the disengaging
15 asymmetrical flank profile could be approximated by a different involute form. Slight changes to the asymmetrical tooth profiles may be for manufacturing and/or quality control reasons, or simply to improve part dimensioning. These changes are within the scope
20 of the invention as disclosed herein.

In a further embodiment, the engaging flank inclined root surface **146** (Fig. 9) may be replaced with a coast flank inclined root surface **164** as shown in Figure 18. The coast flank inclined root surface **164**
25 provides tooth space clearance (TSC) in the same manner as described above with regard to the inclined root surface **146**. In addition, the engaging flank inclined root surface **164** beneficially moves the roller to a preferred radially outward position as the chain wears.

30 Alternatively, the coast flank inclined root surface **164** may be included with the engaging flank inclined root surface **146** as shown in Figure 19. The engaging flank and coast flank inclined root surfaces

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146, 164 cooperate to provide tooth space clearance (TSC) in the same manner as previously described.

Referring now to Figure 20, any one of the above-described asymmetrical tooth profile embodiments of Figures 9, 15, 18, and 19 may be incorporated into a random-engagement roller chain sprocket **300**. The sprocket **300** is shown as an 18-tooth sprocket. However, the sprocket **300** may have more or less teeth, as desired. The sprocket **300** includes a first group of arbitrarily positioned sprocket teeth **302** each having a profile which incorporates the flank flat **144** shown in Figures 9, 15, 18 and 19. Further, the sprocket teeth **302** can incorporate none, one or both inclined root surfaces **146, 164** as shown in Figs. 9, 15, 18 and 19. The remaining sprocket teeth **304** (sprocket teeth 1, 3, 4, 9, 13, 14, and 16) are randomly positioned around the sprocket and incorporate a tooth profile different from that of the first group of sprocket teeth **302**. As described further below, the first and second groups of sprocket teeth **302, 304** cooperate to reduce chain drive system noise levels below a noise level which either tooth profile used alone would produce.

Figure 21 illustrates an exemplary tooth profile for one of the sprocket teeth **304**. An engaging flank **306** and a coast or disengaging flank **308** of an adjacent tooth cooperate to define a tooth space **310** which receives an engaging roller **314** (shown in phantom). The engaging roller **314** has a roller diameter D_1 and is shown fully seated with single point (line) contact within the tooth space **310**. As best seen in Figure 21a, the engaging roller **314** does not contact the engaging flank **306** at the onset of meshing, moving instead directly from the span to full-mesh root contact

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on a inclined root surface **316** at a contact point C' located radially outward of contact point C in a direction toward the engaging flank **306**. Contact point C' is a roller/tooth contact line that extends axially
5 along each sprocket tooth surface (i.e., in a direction orthogonal to the plane of the drawings).

As shown in Figures 21 and 21a, the first or engaging root radius R_i is tangent to inclined root surface **316** at line **319**, and also tangent to R_f as
10 defined by angle β . Angle β has no functional requirements specific to the onset of roller meshing since roller/flank contact will not take place with tooth profile **304**. It should be noted that R_i can be equal to the ISO-606 root radius for tooth profile 304.

15 The length of the inclined root surface from point C to its radially outer end at line **319** is determined by the amount of flank offset required to ensure that the roller will not have engaging flank contact for any expected chain pitch elongation (wear)
20 throughout its design life. In the preferred embodiment, the flank offset **323** is in the range of about 0.025 to about 0.13 mm. The flank offset **323** is an extension of inclined root surface **316** which provides tooth space clearance (TSC) in the same manner described
25 above with regard to inclined root surface **146**.

As previously mentioned, tooth space clearance compensates for chain pitch elongation or chain wear by accommodating a specified degree of chain pitch elongation. In other words, the tooth space clearance
30 TSC enables rollers of a worn chain to be maintained in hard contact with the inclined root surface of the sprocket teeth. In addition, the inclined root surface **316** facilitates reducing the radial reaction force

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thereby reducing the roller radial impact noise contribution to the overall noise level.

The inclined root surface **316** may be inclined at any angle ϕ necessary to satisfy a specific chain drive geometry and chain pitch elongation. The inclined root surface angle ϕ is measured from a line **320** passing through the center of roller **314** and the sprocket center to a second line **322** which also passes through the center of roller **314** and through contact point C. The inclined root surface **316** is normal to the line **322**, and the inclined root surface extends radially inward to line **318** where it is tangent to R_1' . In the embodiment being described, the inclined root surface angle ϕ is preferably in the range of about 20° to about 35° .

Figure 22 shows another embodiment of the tooth profile **304** where no tooth space clearance TSC is provided. That is, the flat surface portion of the inclined root surface from line **318** to line **322** is not present. Thus, the profile of the tooth **304** from point C to the outside or tip diameter at the disengaging side of the tooth space is substantially identical to the tooth profile shown in Figure 15. The remaining flat surface portion **323** of the inclined root surface **316** from line **322** to line **329** functions only to provide the engaging flank offset as described above.

It should be appreciated that the portion of the engaging flank inclined root surface from line **318** to line **322** may be replaced with a coast flank inclined root surface **164** as in Figure 18. That is, the tooth profile **304** may be substantially identical to the sprocket **112** shown in Figure 18 from contact point C to the outer diameter of the coast flank **138**. The coast flank inclined root surface **164** provides tooth space

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clearance (TSC) in the same manner as the inclined root surface **316**. In addition, the coast flank inclined root surface beneficially moves the roller to a preferred radially outward position as the chain wears.

5 Alternatively, the coast flank inclined root surface **164** may be included with the engaging flank inclined root surface **316** as in Figure 19. Thus, the tooth profile **304** may also be substantially identical to the sprocket **112** shown in Figure 19 from contact point C to the outer

10 diameter of the coast flank **138**.

Pitch mismatch is inherent in a chain/sprocket interface except at one condition - the theoretical condition which is defined as a chain at its shortest pitch (shortest being theoretical pitch) and a maximum

15 material sprocket. This theoretical condition therefore defines one limit (zero, or no pitch mismatch) of the tolerance range of the pitch mismatch relationship of chain and sprocket. The other limit is defined when a longest "as built" chain is used with a sprocket at

20 minimum material conditions - or in other words, a sprocket having a minimum profile. This limit produces the greatest amount of pitch mismatch. The pitch mismatch range is therefore determined by the part feature tolerances.

25 Additional pitch mismatch may be introduced to facilitate a greater time delay, or "staged" meshing, between the initial tangential contact at point A and the full seated contact at points B and C for tooth profile **302**. It should be appreciated that staged

30 contact for profile **302** is enhanced due to the flank flat **144** which causes initial contact to occur higher up on the engaging flank. This will result in reduced mesh frequency noise levels because the point and rhythm of the initial roller-to-sprocket contacts are altered for

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each tooth profile **302**, **304** since profile **304** does not have a tangential contact.

5 The sprocket chordal pitch is necessarily shorter than the chain pitch to facilitate the "staged" roller-tooth contact. In addition, chordal pitch reduction also provides roller-to-flank clearance as the roller exits the sprocket wrap back into the strand. Added chordal pitch reduction, when used, is preferably in the range of about 0.005 to about 0.030 mm.

10 The staged roller contact for tooth profile **302** may be further assisted by providing a sprocket tooth pressure angle γ that is substantially less than the ISO-606 standard. Pressure angles γ equal to or very close to zero (0), or even negative pressure angles, are contemplated.

15 Figure 23 illustrates the tooth profile **304** overlaid with the tooth profile **302**. An engaging roller is shown at the onset of initial tangential contact at point A along the engaging flank of the tooth profile **302**. The engaging roller will maintain contact with the engaging flank until it is at full mesh and seated at points B and C as previously described with reference to Figure 9. The tooth profile **304** is overlaid on the tooth profile **302** to show that an engaging roller only has radial contact on the inclined root surface of the tooth profile **304** (see Figs. 21a and 22) and does not have tangential contact with the tooth profile **304**.

25 The pressure angle γ for tooth profile **304** has no functional purpose during the onset of roller meshing since the roller does not contact the engaging flank. The pressure angle γ_{302} for the tooth profile **302** is shown as a negative value. Thus γ_{\min} may be a small negative value, and γ_{\max} may be a positive value equal to some value less than the ISO-606 minimum pressure angle γ .

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As a result, initial roller-to-sprocket contact for tooth profile **302** of sprocket **300** (Fig. 20) occurs at point A followed by full engagement contact at points B and C. The sprocket **300** may, or may not incorporate additional chordal pitch reduction, and may, or may not incorporate tooth space clearance (TSC), as described above.

Figure 24 shows the engagement path of an additional roller **342** from initial contact at point A (phantom) to fully-seated, two-point contact (solid) in a sprocket tooth **302**, and an engagement path of the roller **314** engaging an adjacent sprocket tooth **304** of the random engagement sprocket **300**. At the onset of meshing for roller **314**, a small portion of the chain load transfer takes place with tooth **304** picking up a share of the loading. However, tooth **302** continues to carry a larger portion of the chain loading until an engaging roller meshes with another tooth **304** with its attendant flank contact. The reference **l** in Figure 24 indicates the amount of "staging" for the tooth **302** from the initial contact at point A to the full mesh contact at points B and C.

Figures 25 and 26 illustrate the meshing delay between the tooth profiles **302**, **304**. In particular, as shown in Figure 25, the sprocket **300** has a further roller **344** fully-seated in two-point contact with a sprocket tooth incorporating the tooth profile **302**. The roller **342** is shown at the instant of initial tangential contact at point A of a second sprocket tooth also incorporating the tooth profile **302**. The roller **314** is the next roller in the span and will mesh with a sprocket tooth incorporating the tooth profile **304**. The sprocket **300** must rotate through an angle τ for roller

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342 to move from its initial contact position at point A to full mesh, seated in two-point contact with the tooth profile **302** at a 12 o'clock position.

With reference to Figure 26, the sprocket **300**
5 of Figure 25 is shown rotated in a clockwise direction until roller **314** is at the onset of meshing with the tooth profile **304**. The sprocket **300** must now rotate through a smaller angle κ to have roller **314** seated at the 12 o'clock position. Thus, the sprocket **300** must
10 rotate through an additional angle $\tau - \kappa$ for an engaging roller to be fully seated in the tooth profile **302**.

Referring again to Figure 20, the two sets of tooth profiles **302**, **304** are arranged in a random pattern in order to modify the meshing impact frequency by
15 altering the point and rhythm of initial roller-to-sprocket contact. However, the two sets of tooth profiles **302**, **304** could be arranged in many different random patterns. Further, it is also contemplated that the two sets of tooth profiles **302**, **304** could be
20 arranged in many regular patterns that would work equally as well. In all cases, the arrangement of two sets of different tooth profiles on a sprocket provides a means for breaking up the mesh frequency impact noise normally associated with and induced by a full
25 complement of substantially identically shaped sprocket teeth. The mesh frequency noise reduction is achieved by altering the point and rhythm of initial roller-to-sprocket contact.

The crankshaft sprocket, generally the
30 smallest sprocket in the chain drive, is usually the major noise contributor. The typically larger driven camshaft sprocket, however, will also contribute to the generated noise levels, but generally to a lesser extent

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than the crankshaft sprocket. However, the driven sprocket, particularly if it is nearly the same size or smaller than the driving sprocket, may be the prime noise generator, as in the case with balance shaft sprockets and pump sprockets. Thus, the features of the present invention may also be used advantageously with camshaft or driven sprockets as well.

It should be appreciated that the tooth profile features of Figures 20-26 can be altered slightly without substantially deviating from the chain and sprocket meshing kinematics that produce the noise reduction advantages of the present invention. For example, the engaging asymmetrical flank profile could be approximated by an involute form, and the disengaging asymmetrical flank profile could be approximated by a different involute form. Slight changes to the profile may be done for manufacturing and/or quality control reasons - or simply to improve part dimensioning.

The invention has been described with reference to the preferred embodiments. Obviously, modifications will occur to others upon a reading and understanding of this specification and this invention is intended to include same insofar as they come within the scope of the appended claims or the equivalents thereof.

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Having thus described the preferred embodiments, the invention is now claimed to be:

1. A sprocket comprising:

5 a first plurality of sprocket teeth each having a first tooth profile including a first engaging flank, a first engaging root, and a first flat positioned between the first engaging flank and first engaging root, a first roller initially contacting the first flat at the onset of the first roller meshing with the sprocket; and

10 a second plurality of sprocket teeth each having a second tooth profile different from the first tooth profile and including a second engaging flank, a second engaging root, and a second flat tangent to the second engaging root remote from the second engaging flank, a second roller initially contacting the second flat at the onset of meshing between the second roller and the sprocket.

2. The sprocket of claim 1, wherein the first and second tooth profiles are asymmetrical tooth profiles.

3. The sprocket of claim 1, wherein the first plurality of sprocket teeth are arbitrarily positioned relative to the second plurality of sprocket teeth.

4. The sprocket of claim 1, wherein the second flat includes a first portion and a second portion, the first portion providing a flank offset and the second portion providing a tooth space clearance.

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5. The sprocket of claim 1, wherein the second plurality of sprocket teeth include a disengaging flank and a third flat positioned along the disengaging flank for providing a tooth space clearance.

6. The sprocket of claim 1, wherein the first plurality of sprocket teeth each include a third flat tangent to the first engaging root remote from the first engaging flank for providing a tooth space
5 clearance.

7. The sprocket of claim 1, wherein the first plurality of sprocket teeth include a disengaging flank and a third flat positioned along the disengaging flank for providing a tooth space clearance.

8. The sprocket of claim 1, wherein the first roller contacts the sprocket at two points along the first asymmetrical tooth profile in a full mesh position.

9. The sprocket of claim 1, wherein a radius of the first engaging root is less than a radius of the first roller.

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10. A sprocket comprising:

a first plurality of sprocket teeth each having a first asymmetrical tooth profile including means for providing a tangential contact with a first roller at an onset of the first roller meshing with the sprocket; and

a second plurality of sprocket teeth each having a second asymmetrical tooth profile including means for providing a radial contact with a second roller at an onset of the second roller meshing with the sprocket.

11. The sprocket of claim 10, wherein:

the first means includes a first engaging flank, a first engaging root, and a first flat positioned between the first engaging flank and the first engaging root, the first roller initially contacting the first flat at the onset of the first roller meshing with the sprocket; and

the second means includes a second engaging flank, a second engaging root, and a second flat tangent to the second engaging root remote from the second engaging flank, the second roller initially contacting the second flat at the onset of meshing between the second roller and the sprocket.

12. The sprocket of claim 11, wherein the first and second tooth profiles are asymmetrical tooth profiles.

13. The sprocket of claim 11, wherein the first plurality of sprocket teeth are arbitrarily positioned relative to the second plurality of sprocket teeth.

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14. The sprocket of claim 11, wherein the second flat includes a first portion and a second portion, the first portion providing a flank offset and the second portion providing a tooth space clearance.

15. The sprocket of claim 11, wherein the first roller contacts the sprocket at two points along the first asymmetrical tooth profile in a full mesh position.

16. The sprocket of claim 11, wherein a radius of the first engaging root is less than a radius of the first roller.

17. A unidirectional roller chain drive system including a first sprocket, a second sprocket, and a roller chain having rollers in engaging contact with the first and second sprockets, wherein at least
5 one of the first and second sprockets comprises:

a first plurality of sprocket teeth each having a first tooth profile including a first engaging flank, a first engaging root, and a first flat positioned between the first engaging flank
10 and first engaging root, a first roller initially contacting the first flat at the onset of the first roller meshing with the sprocket; and

a second plurality of sprocket teeth each having a second tooth profile different from the
15 first tooth profile and including a second engaging flank, a second engaging root, and a second flat tangent to the second engaging root remote from the second engaging flank, a second roller initially contacting the second flat at the onset of meshing
20 between the second roller and the sprocket.

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18. The roller chain drive system of claim 17, wherein the first and second tooth profiles are asymmetrical tooth profiles.

19. The roller chain drive system of claim 17, wherein the first plurality of sprocket teeth are arbitrarily positioned relative to the second plurality of sprocket teeth.

20. The roller chain drive system of claim 17, wherein the second flat includes a first portion and a second portion, the first portion providing a flank offset and the second portion providing a tooth space clearance.

5

21. The roller chain drive system of claim 17, wherein the first roller contacts the sprocket at two points along the first asymmetrical tooth profile in a full mesh position.

22. The roller chain drive system of claim 17, wherein a radius of the first engaging root is less than a radius of the first roller.

- 42 -

23. A method of modifying a meshing impact frequency of a roller chain meshing with a sprocket, comprising:

5 (a) rotating the sprocket to cause a first roller of the roller chain to tangentially contact an engaging flank of a first sprocket tooth at an onset of the first roller meshing with the first sprocket tooth; and

10 (b) rotating the sprocket to cause a second roller of the roller chain to radially contact a root surface of a second sprocket tooth at an onset of the second roller meshing with the second sprocket tooth.

24. The method of claim 23, wherein step (a) includes the step of:

5 rotating the sprocket to cause the first roller of the roller chain to contact a flank flat at an onset of the first roller meshing with the first sprocket tooth.

25. The method of claim 23, wherein step (b) includes the step of:

5 rotating the sprocket to cause the second roller of the roller chain to contact an inclined flat at an onset of the second roller meshing with the second sprocket tooth.

26. The method of claim 23, further including the step of:

5 (c) after step (a), further rotating the sprocket to cause the first roller of the roller chain to contact the first sprocket tooth at two other points along the first asymmetrical tooth profile in a full mesh position of the first roller.

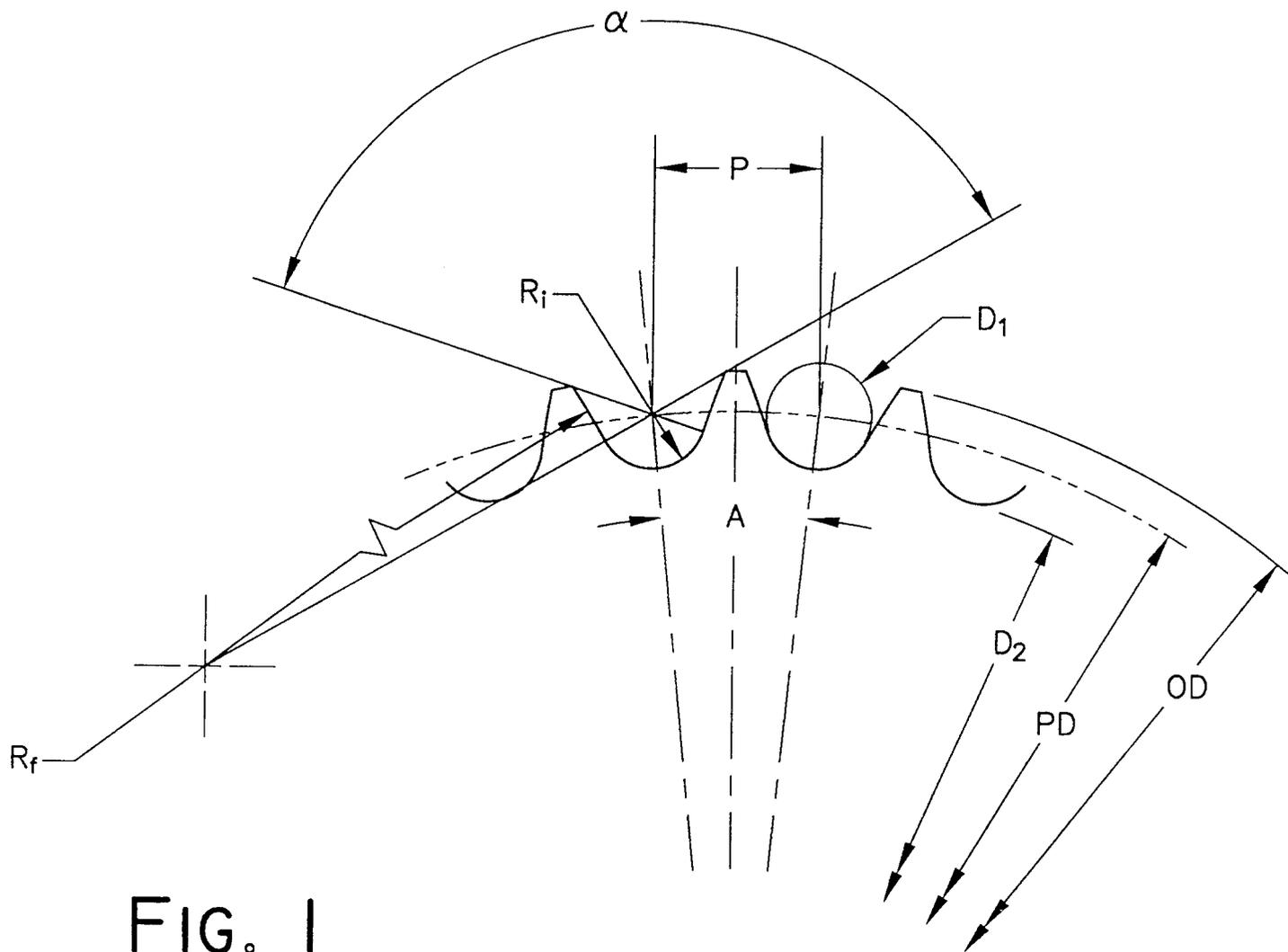


FIG. 1
PRIOR ART

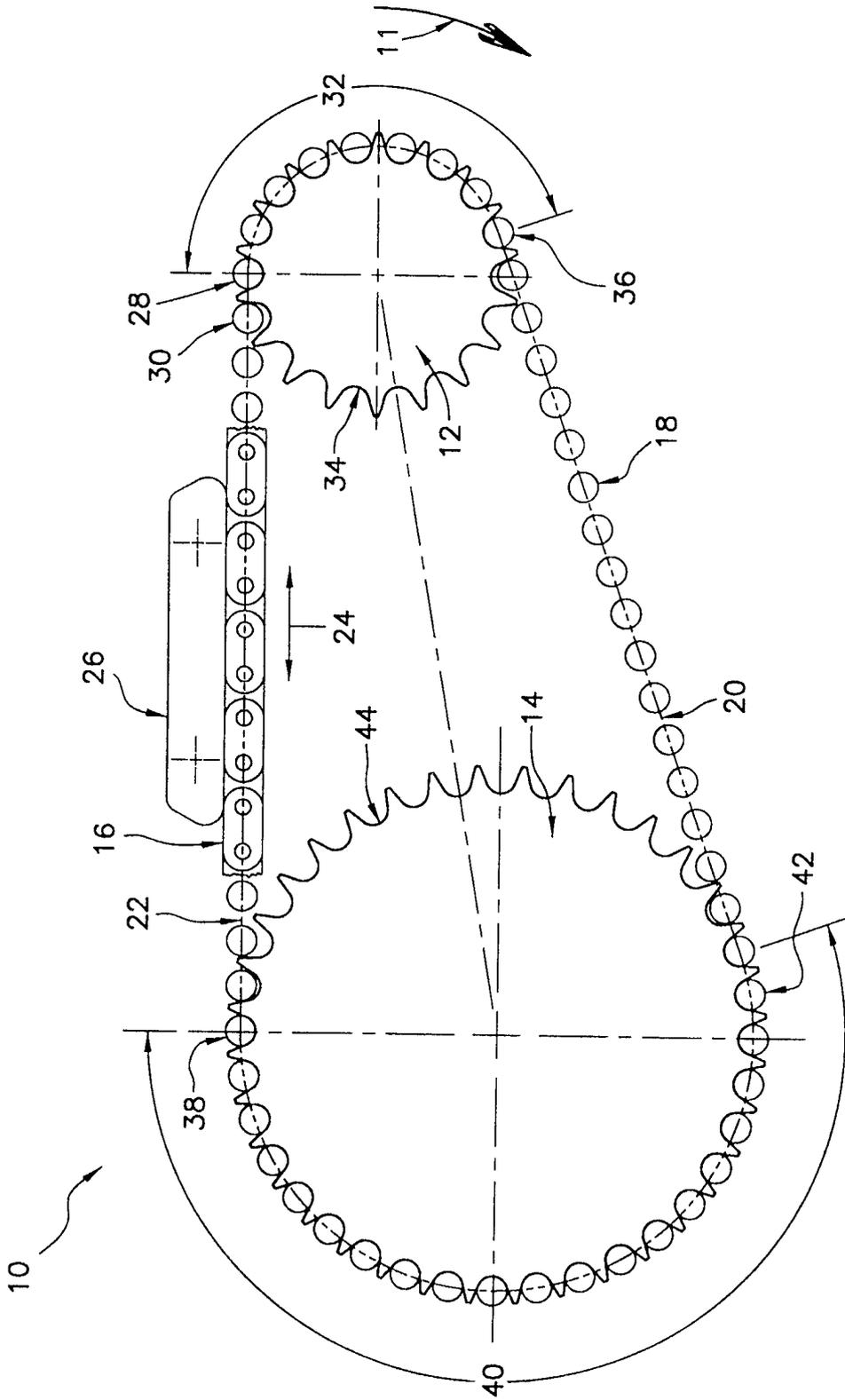
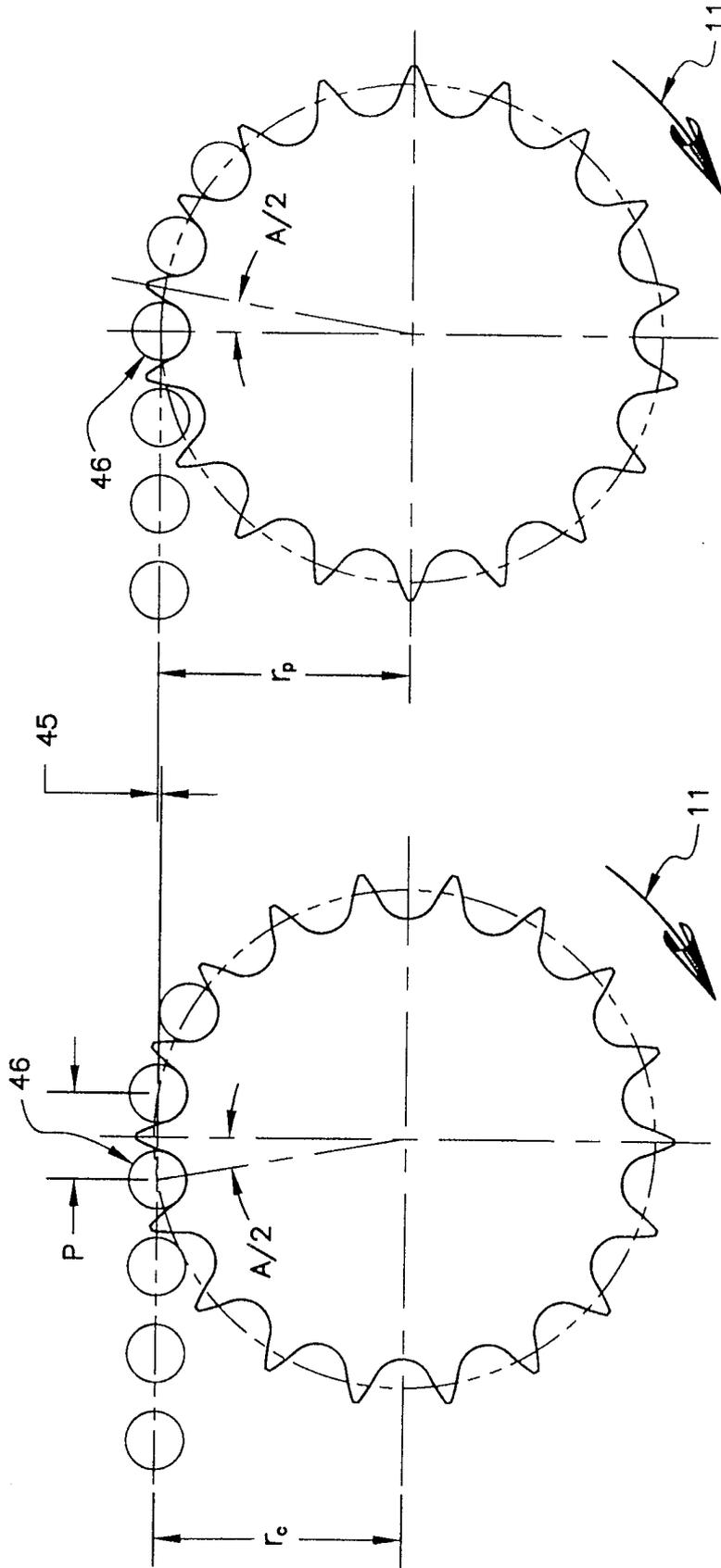


FIG. 2
PRIOR ART



AT T = 0

FIG. 4a
PRIOR ART

AT T = 0 + (A/2)

FIG. 4b
PRIOR ART

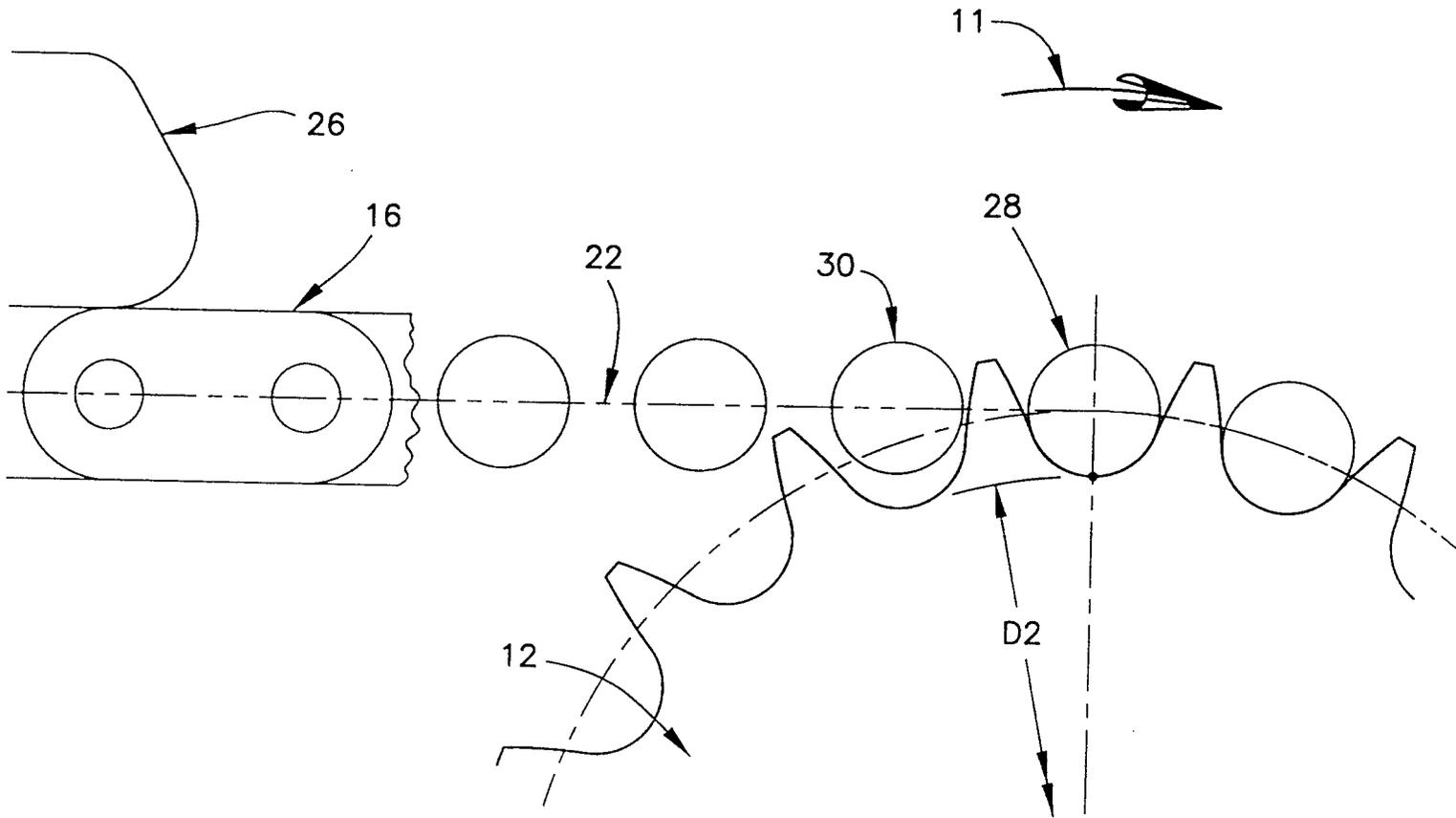


FIG. 5
PRIOR ART

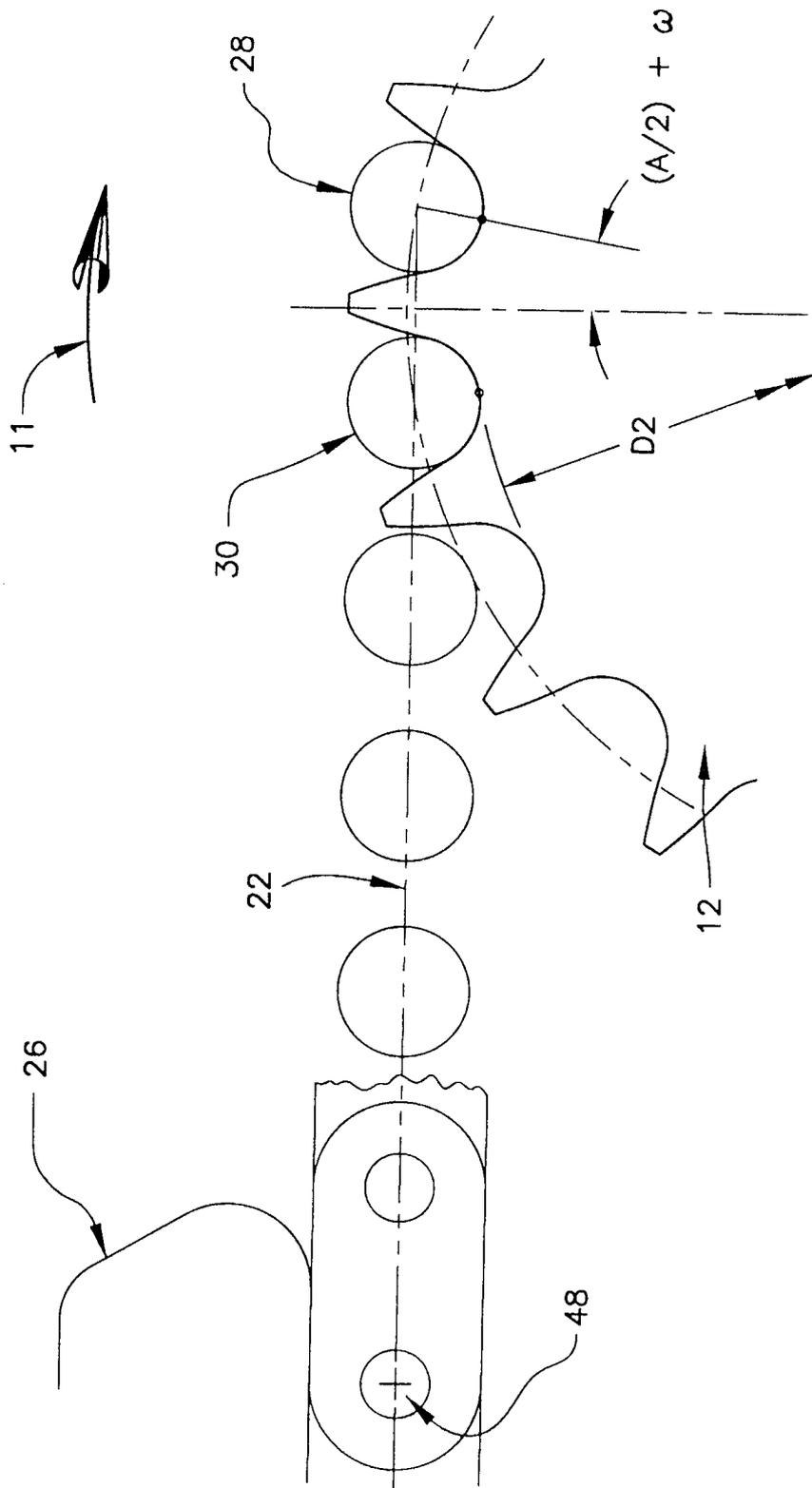


FIG. 6
PRIOR ART

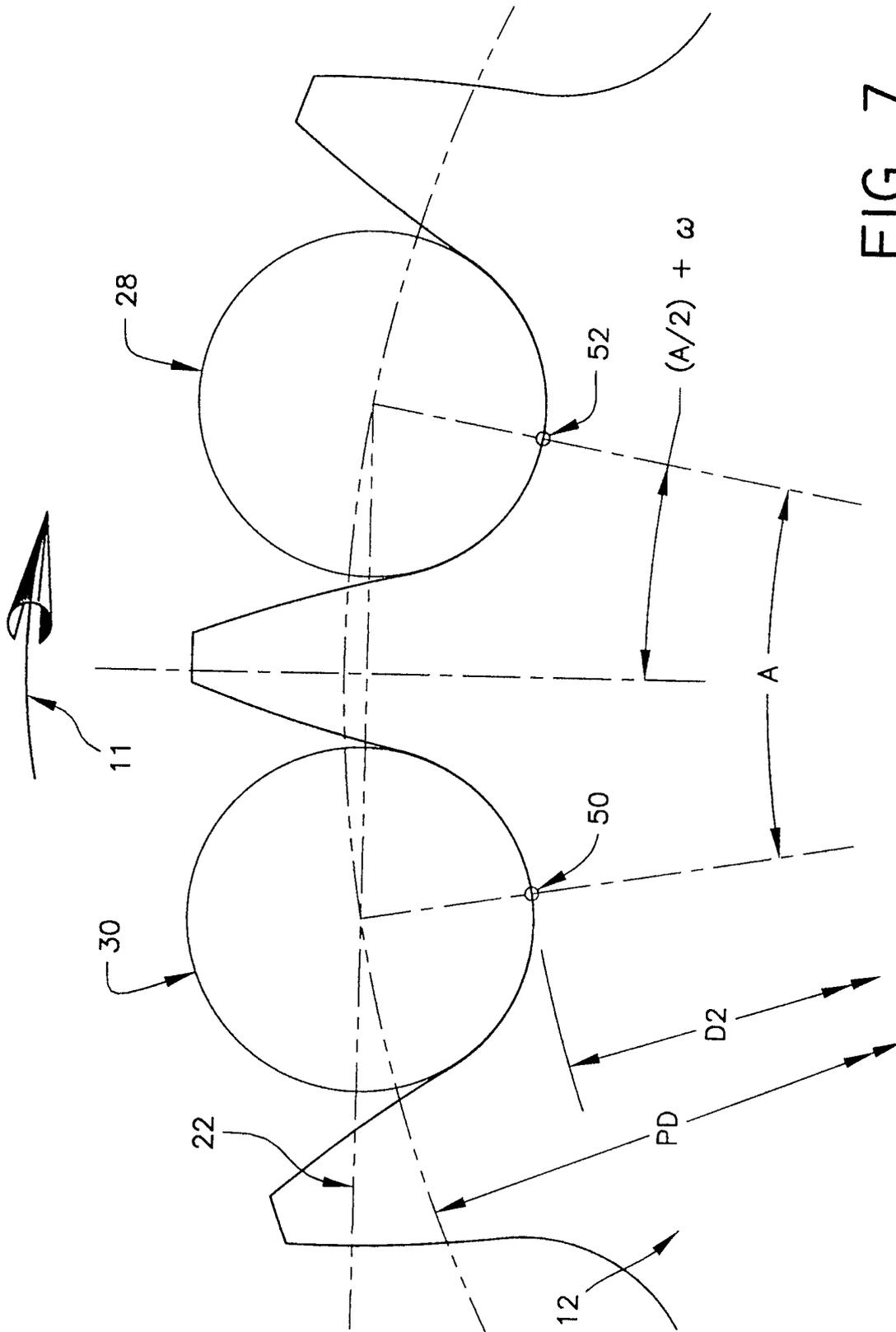


FIG. 7
PRIOR ART

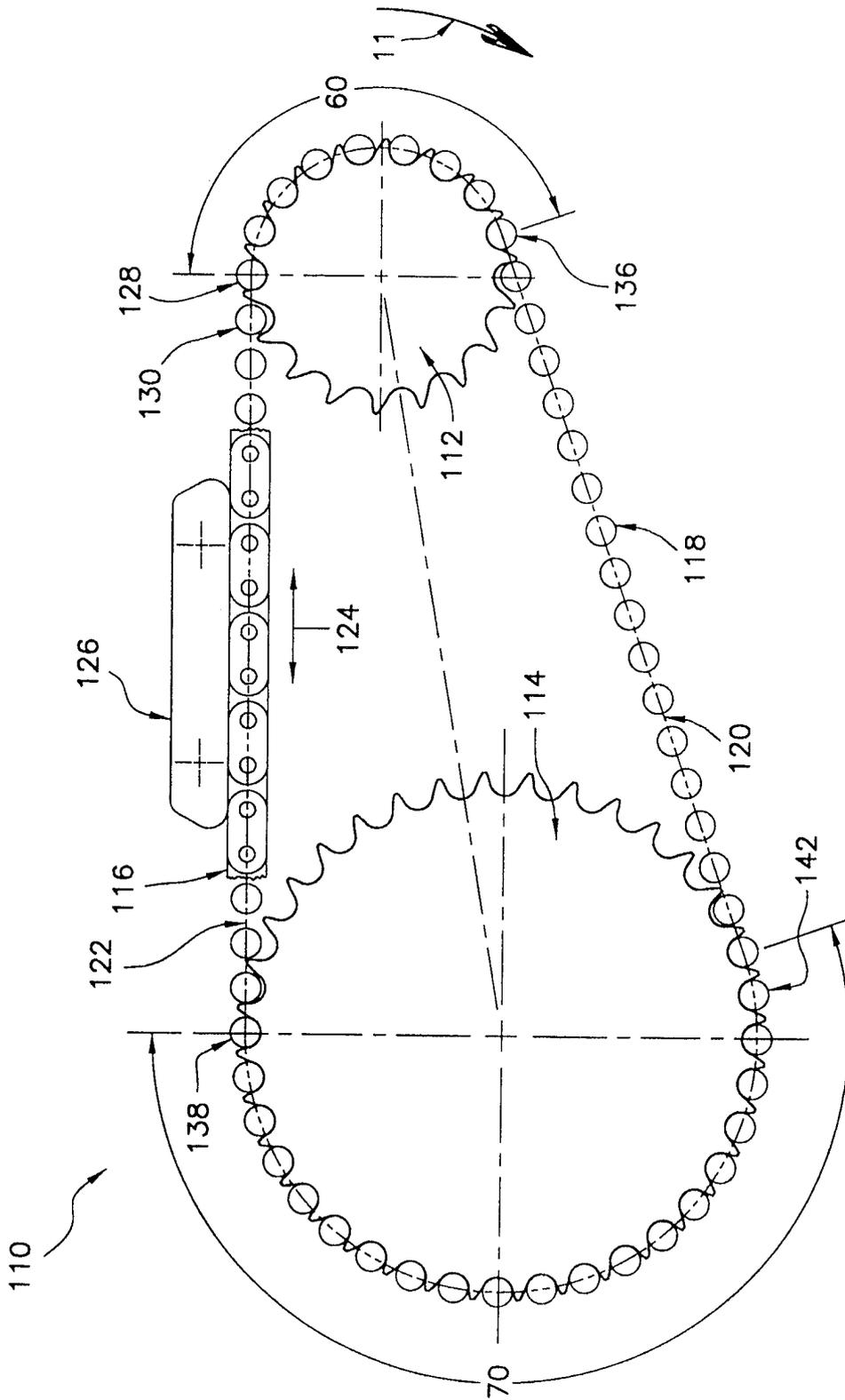


FIG. 8

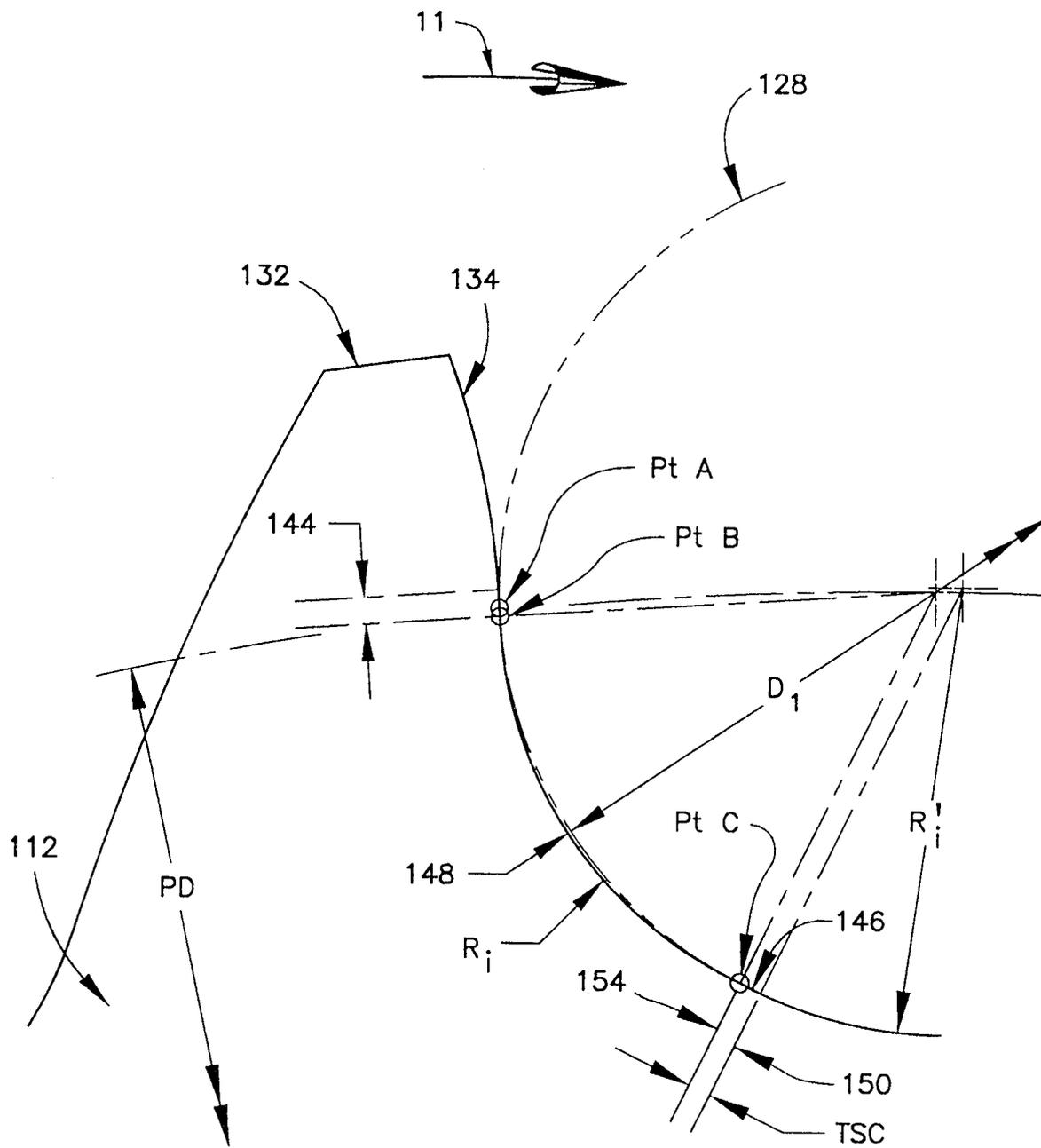


FIG. 10

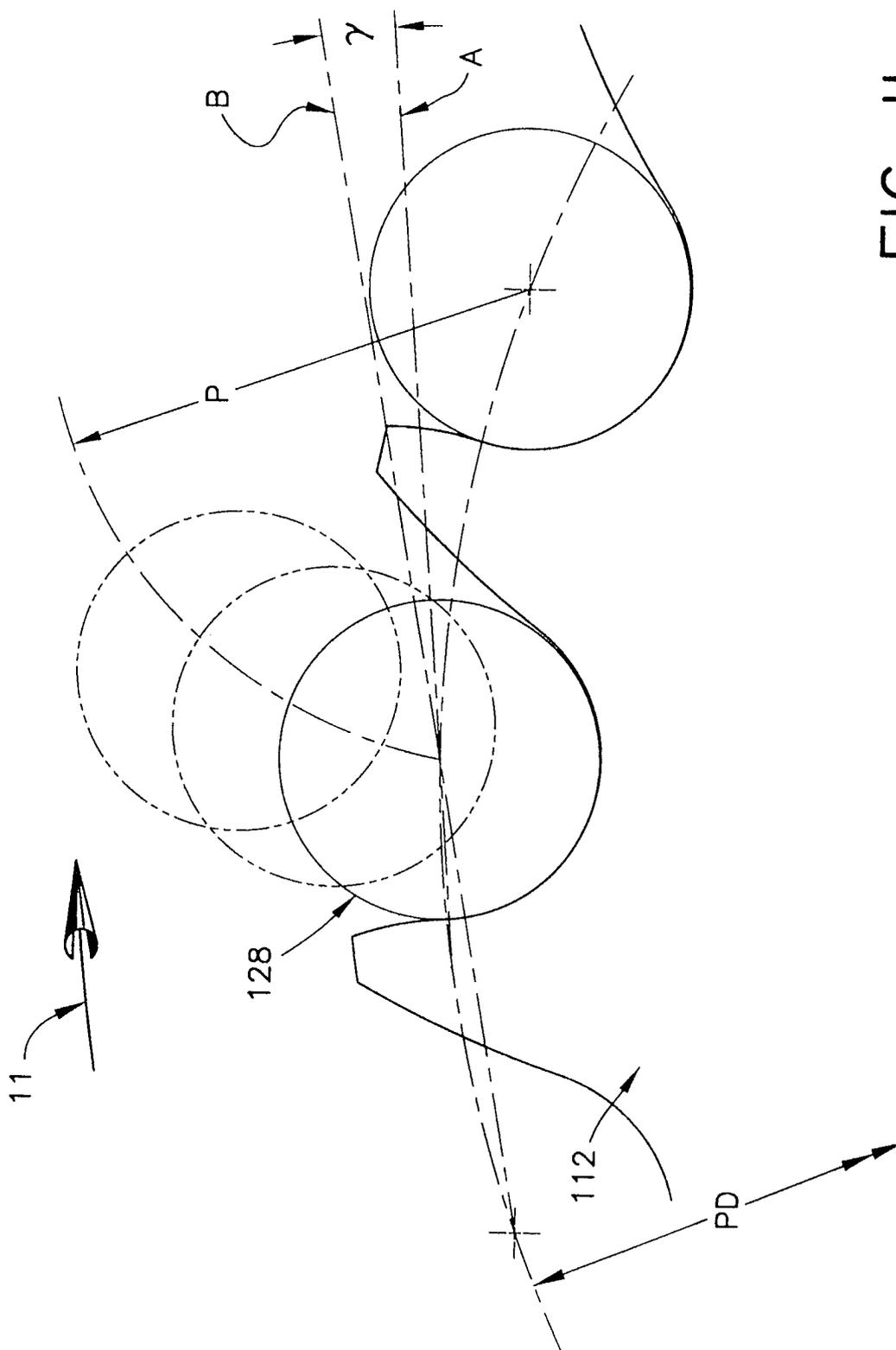


FIG. II

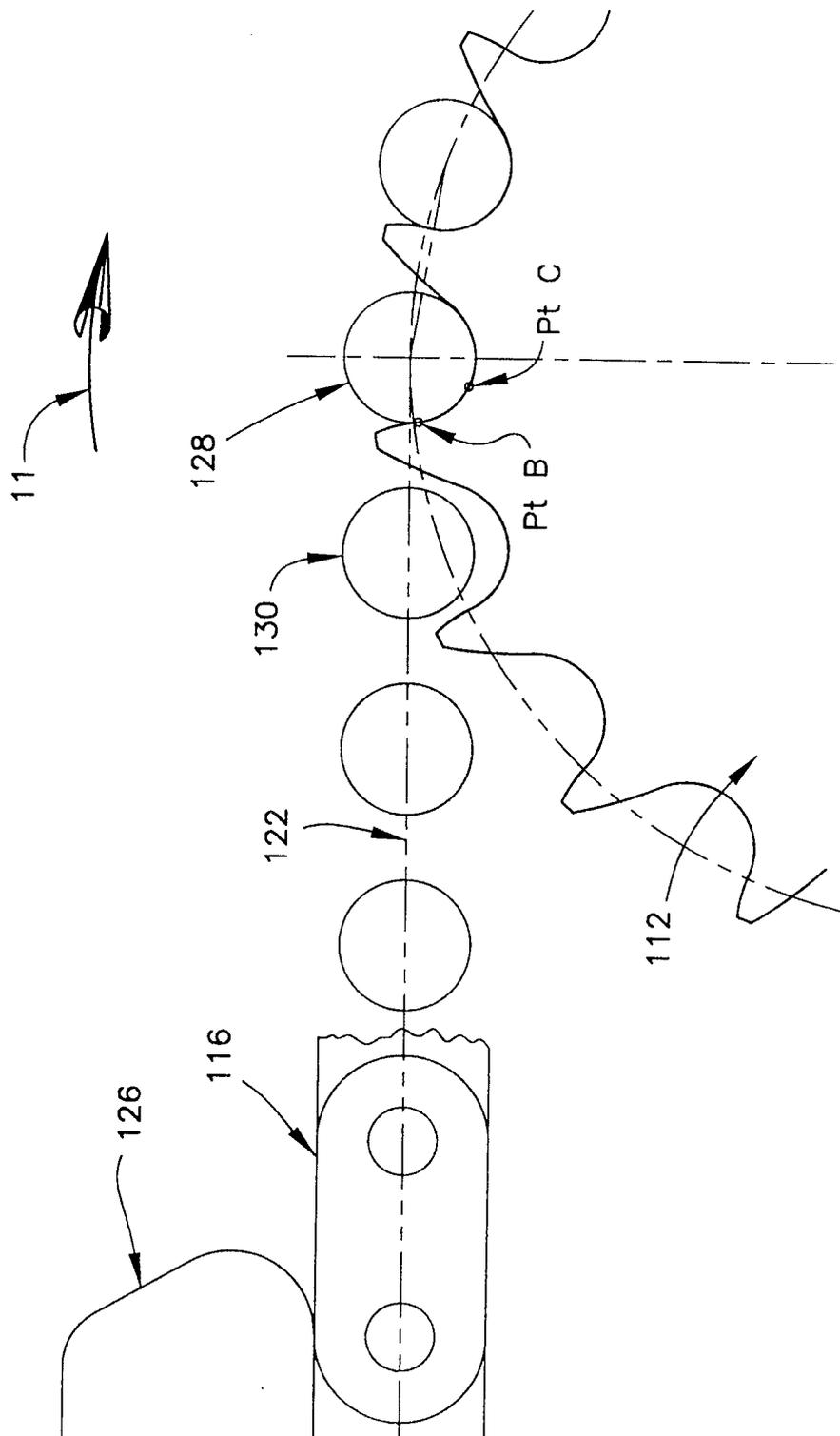


FIG. 12

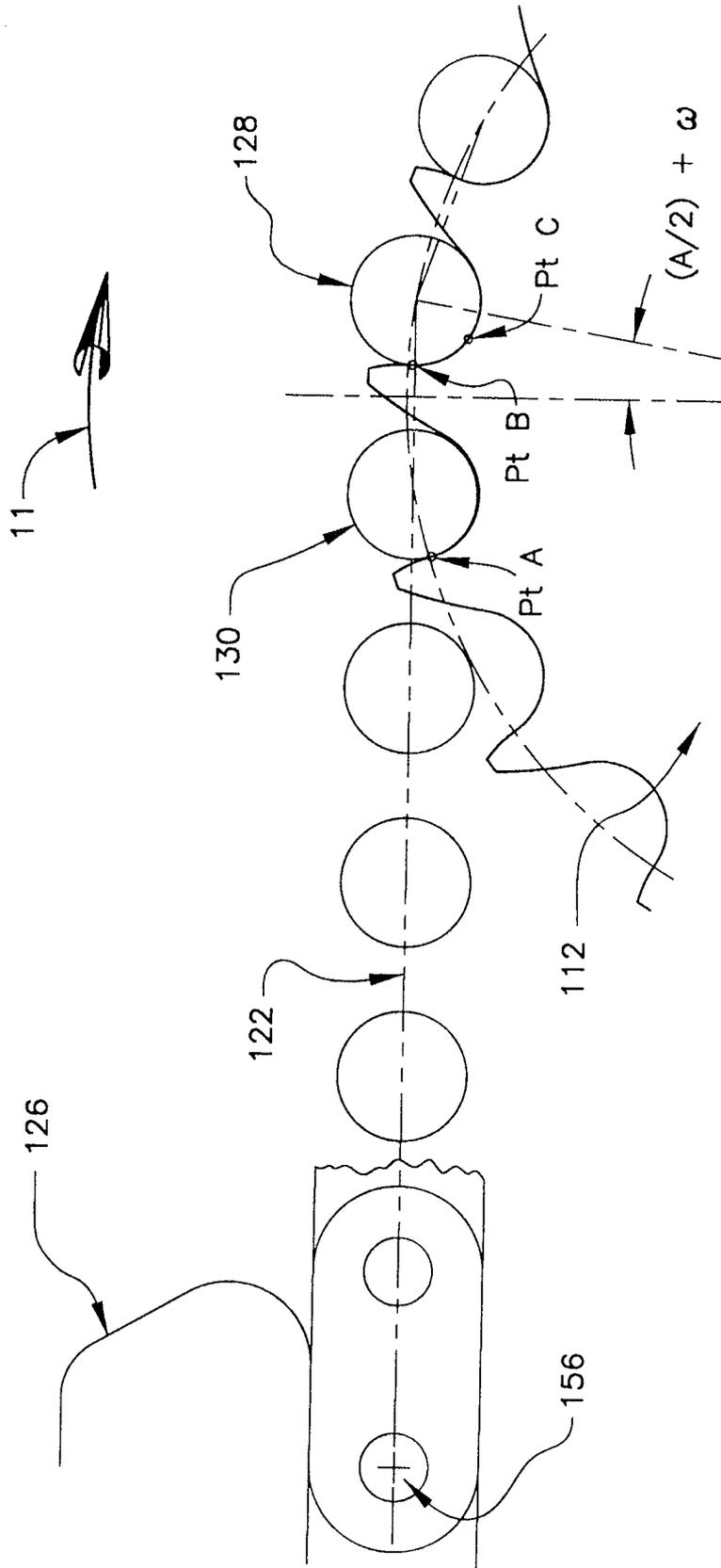


FIG. 13

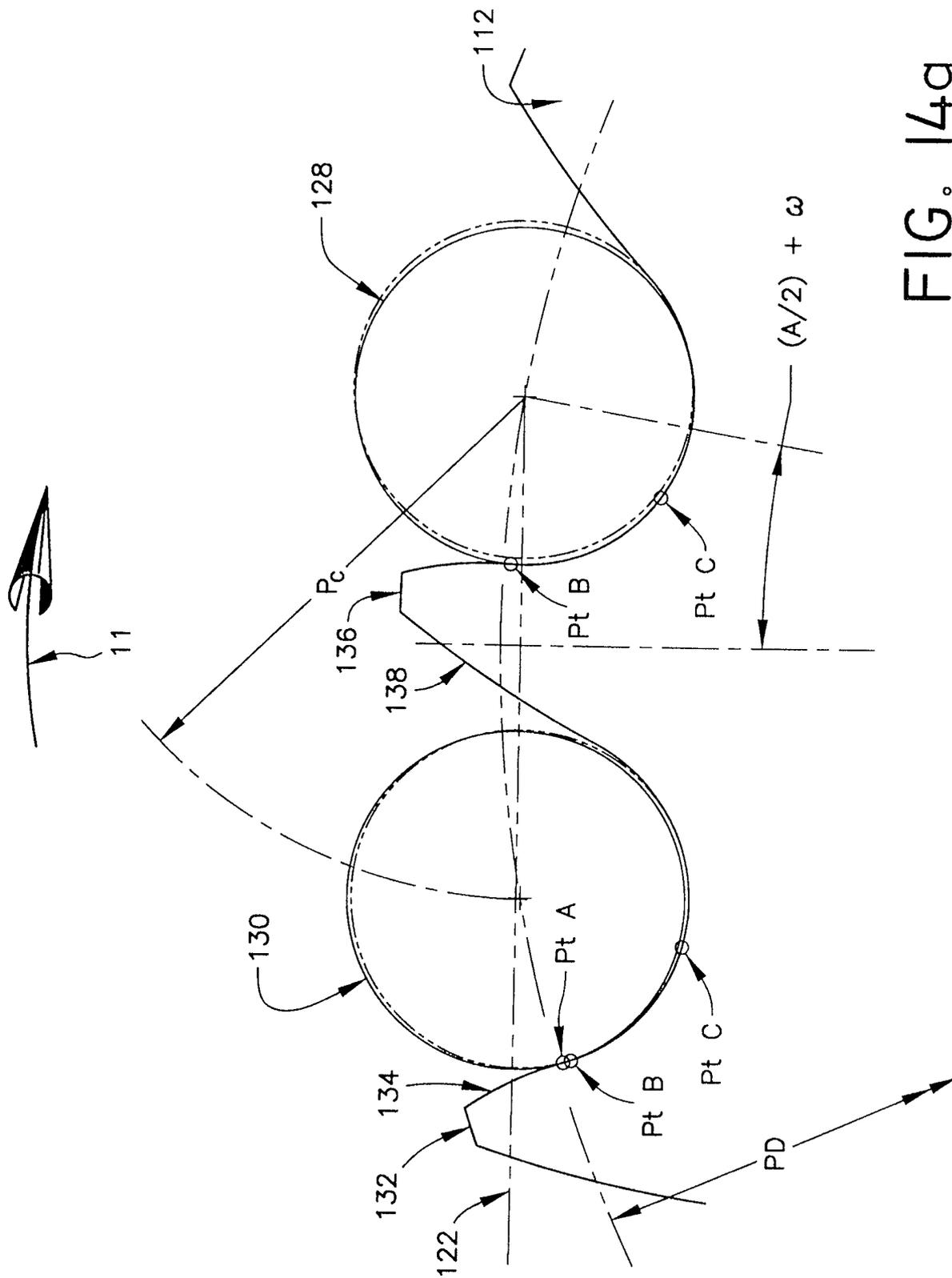


FIG. 14a

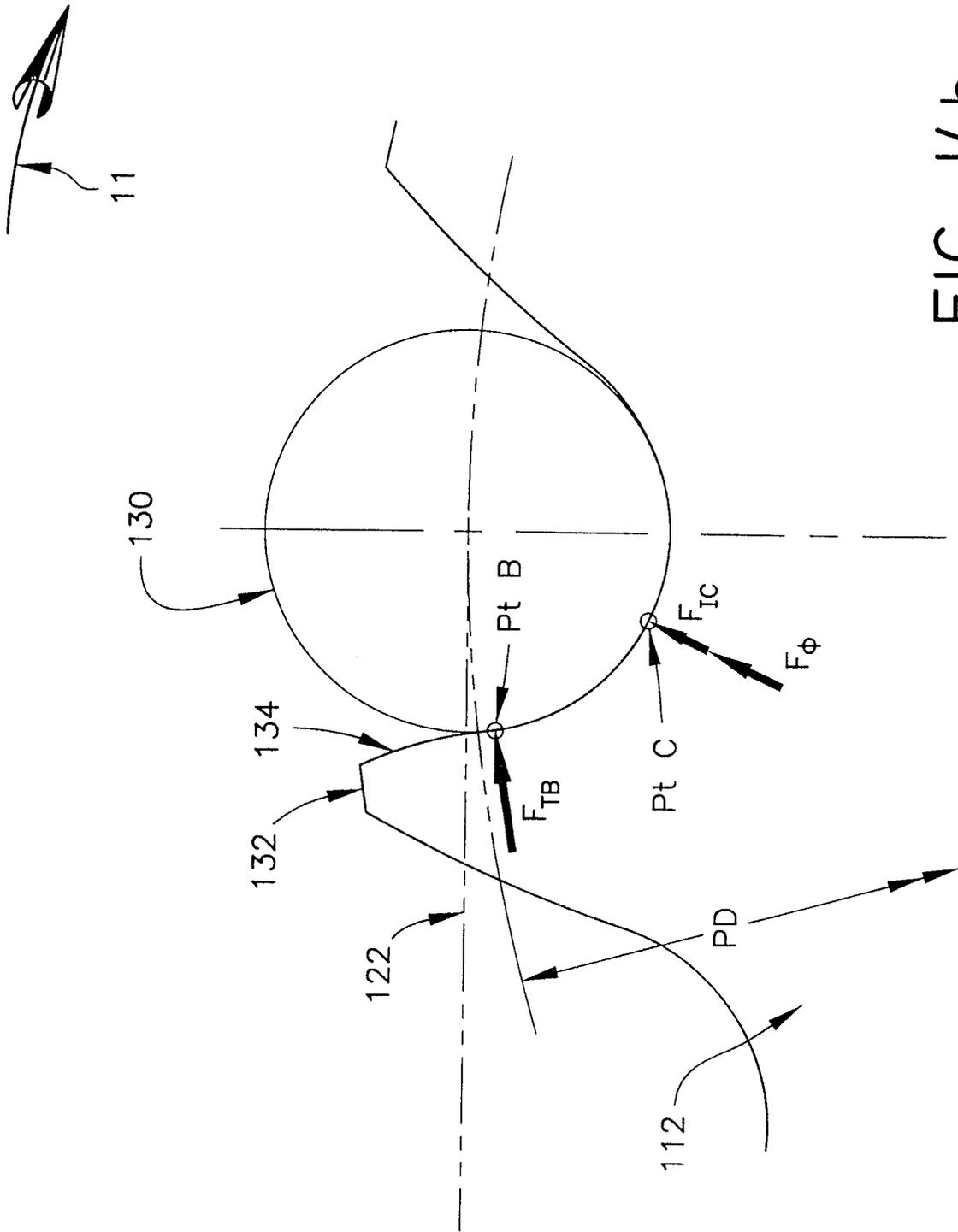


FIG. 14b

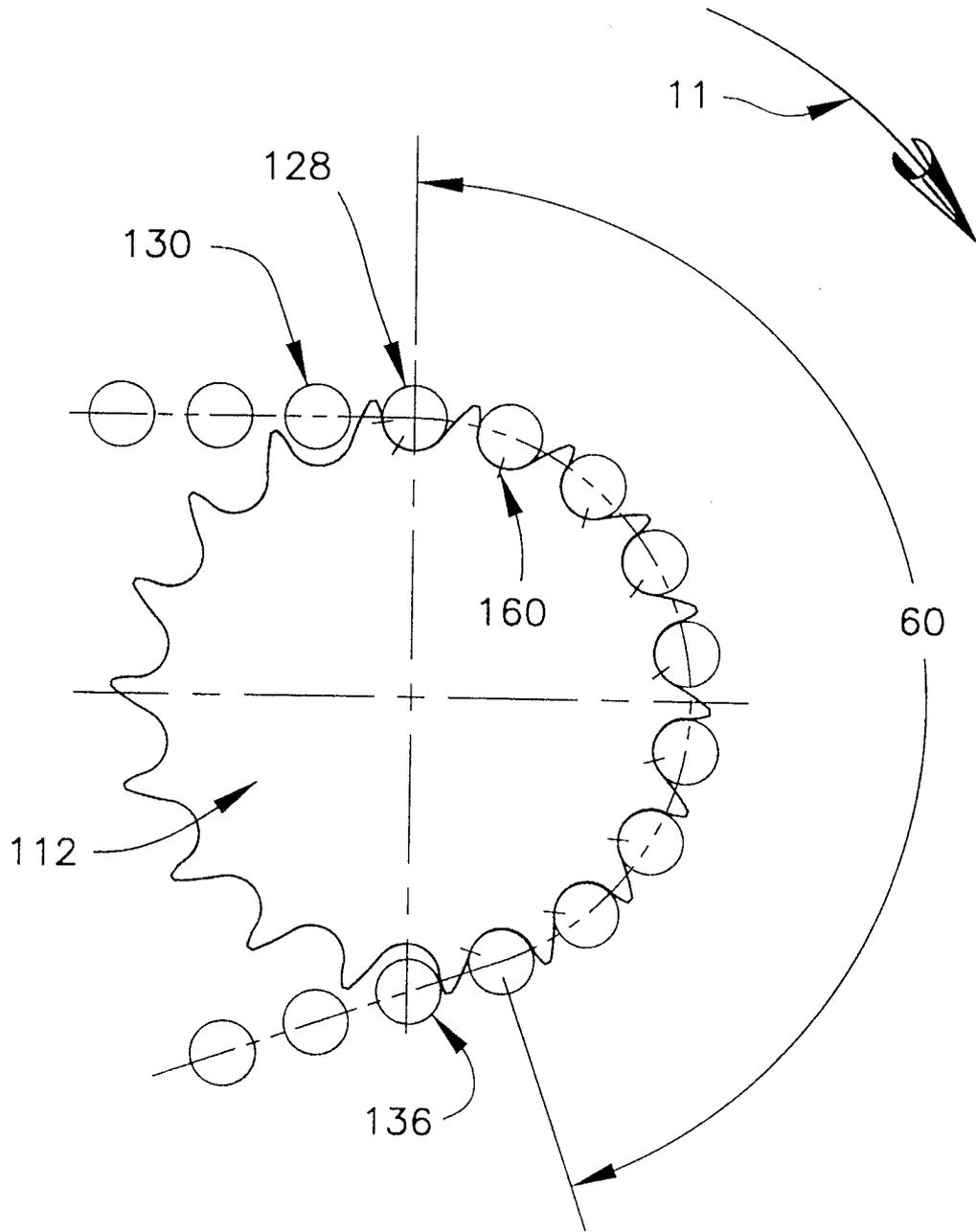


FIG. 16

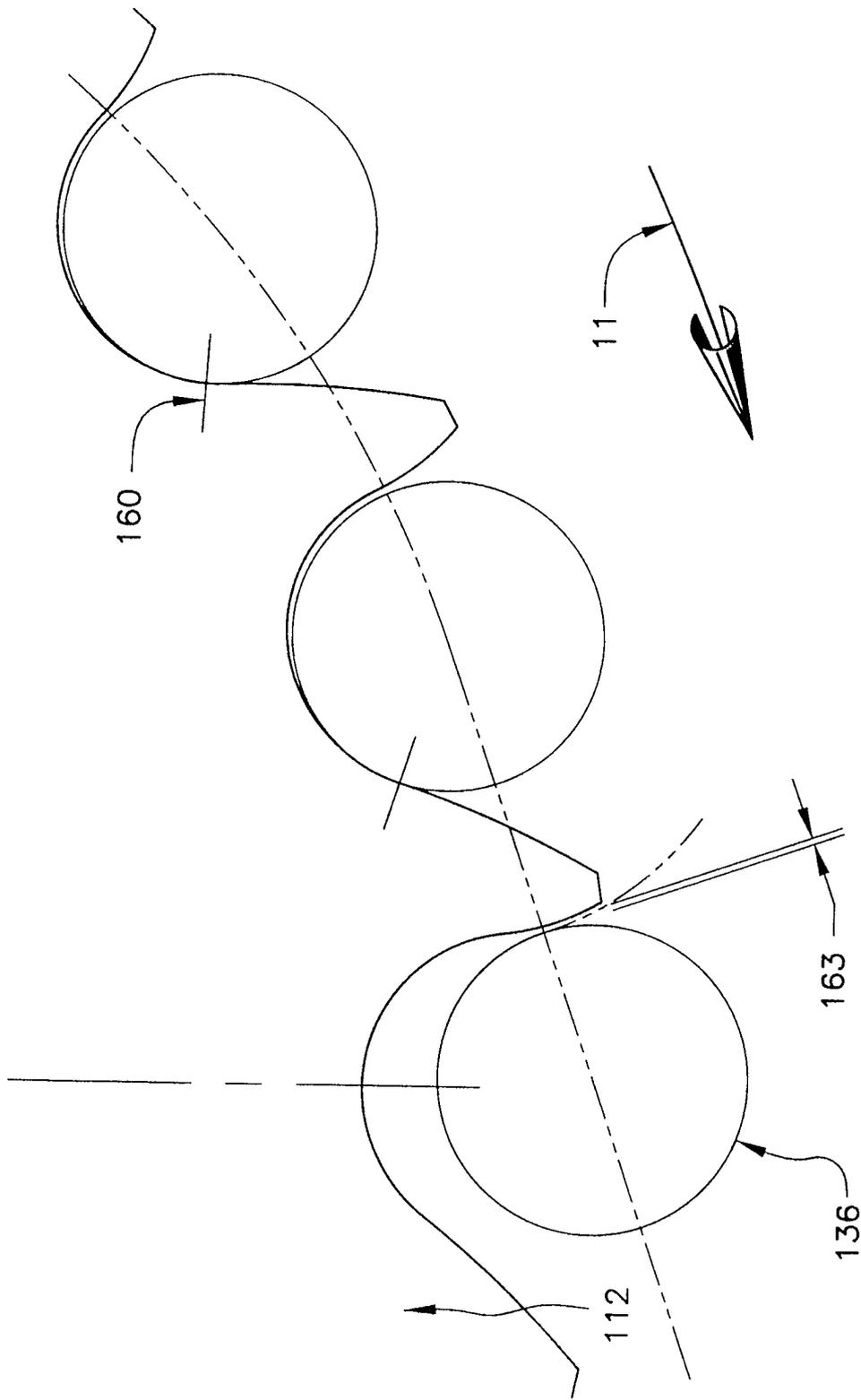


FIG. 17

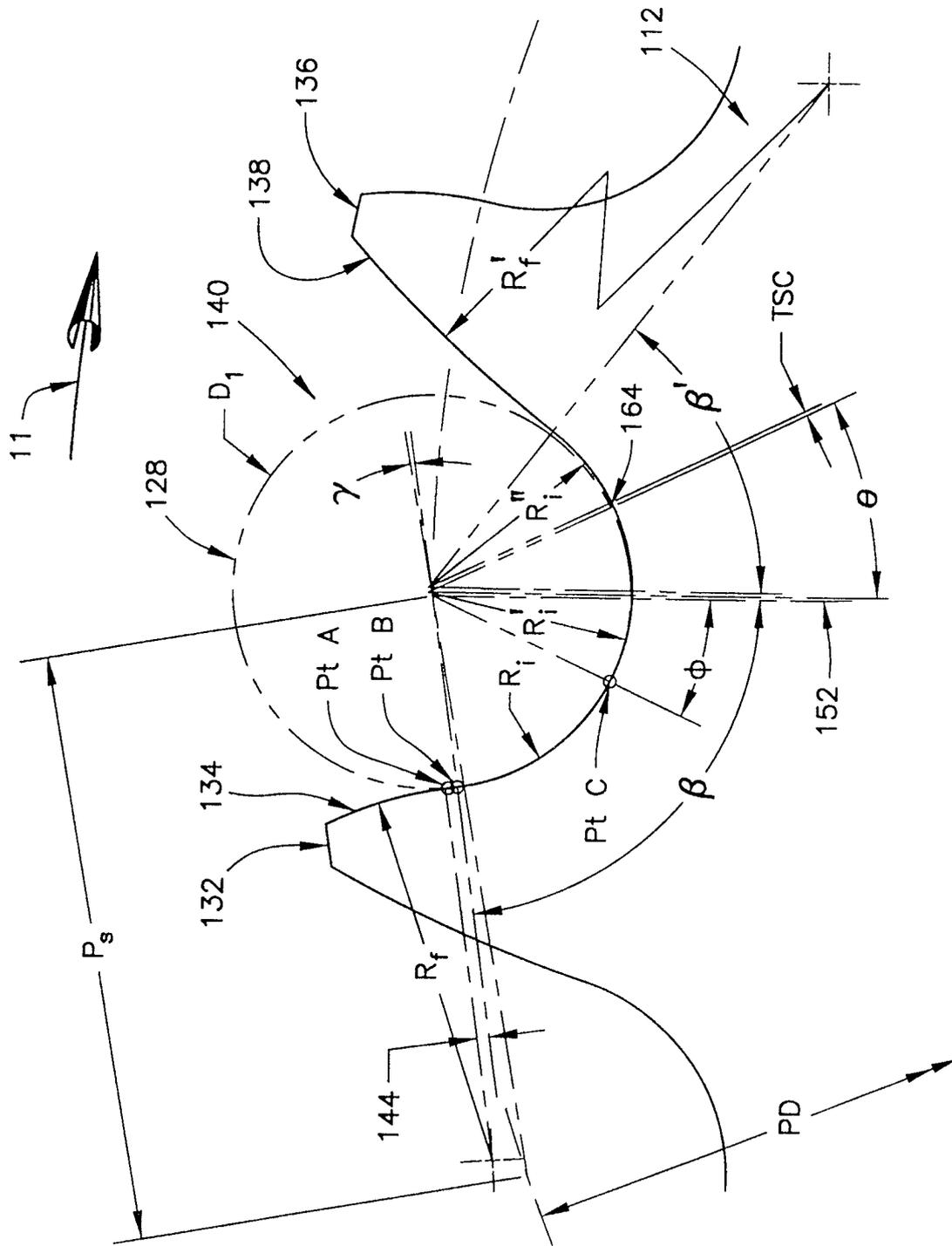


FIG. 18

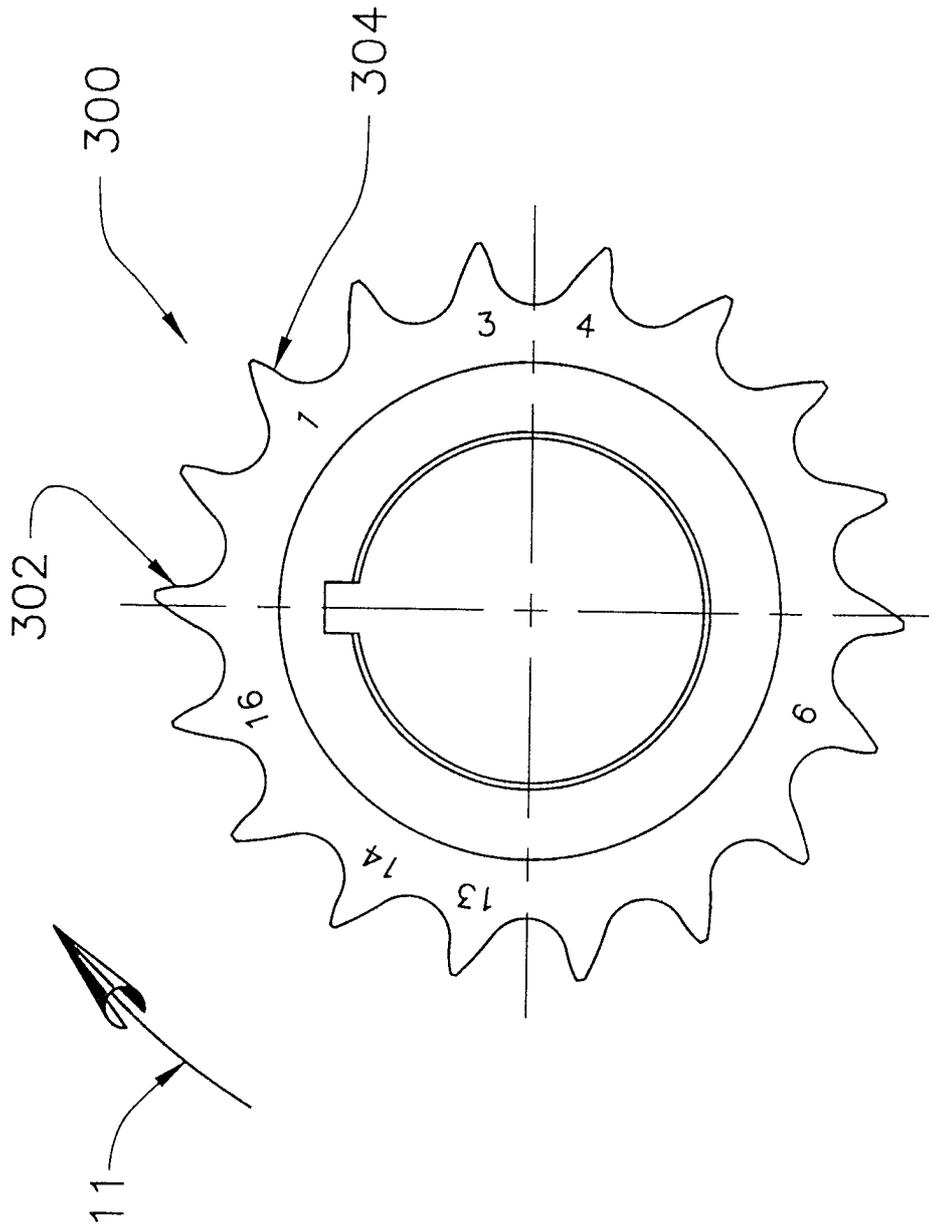


FIG. 20

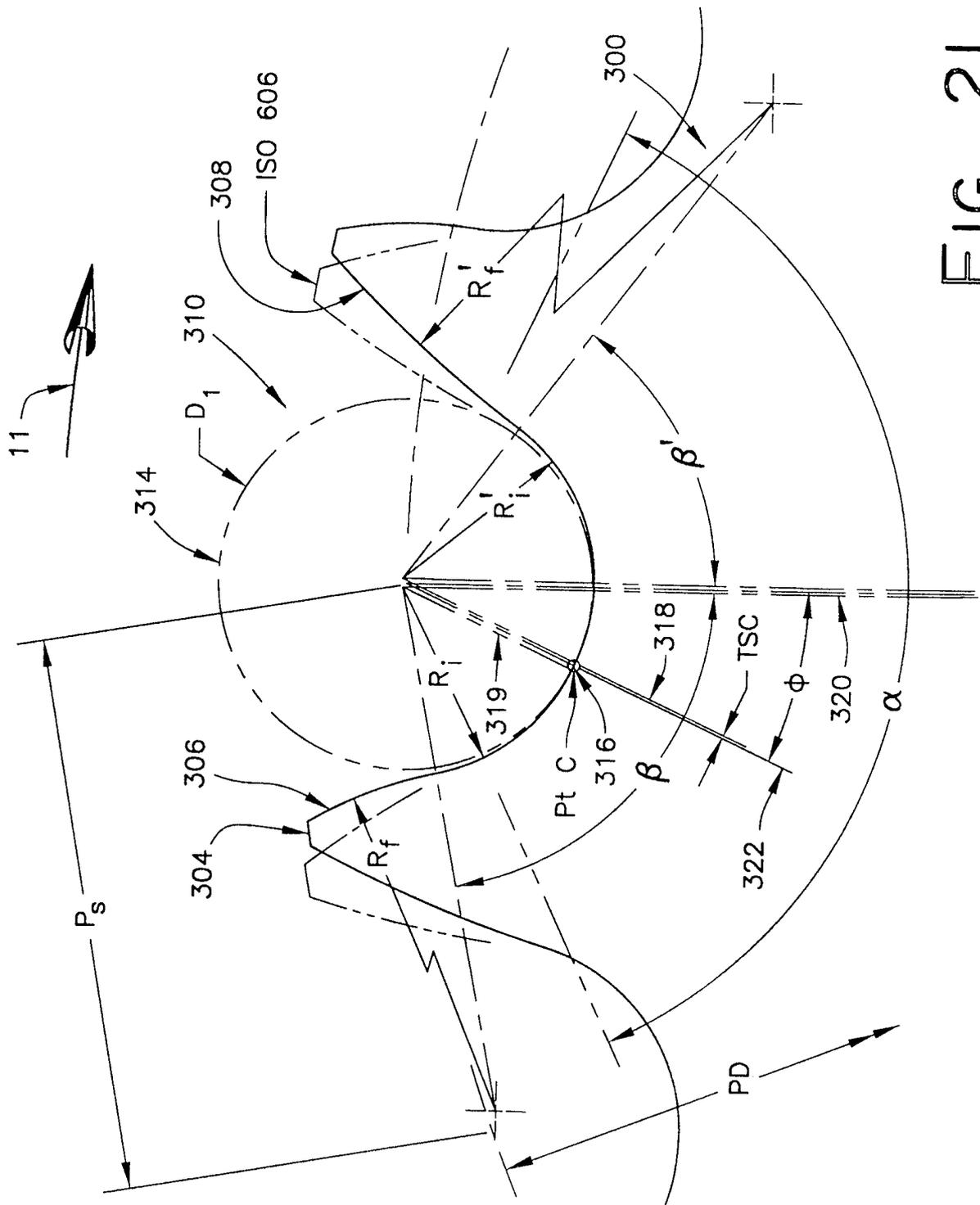


FIG. 21

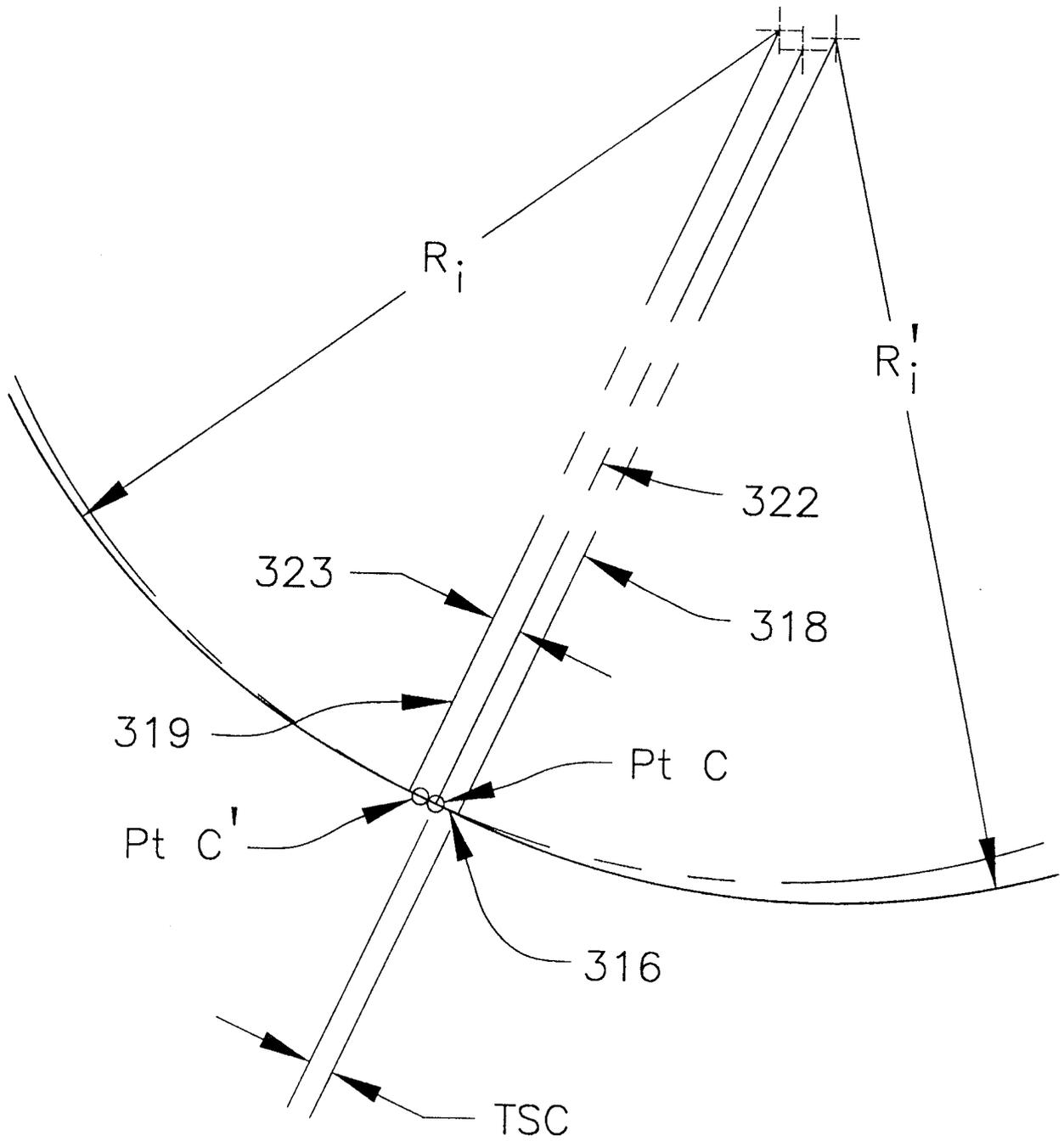


FIG. 21a

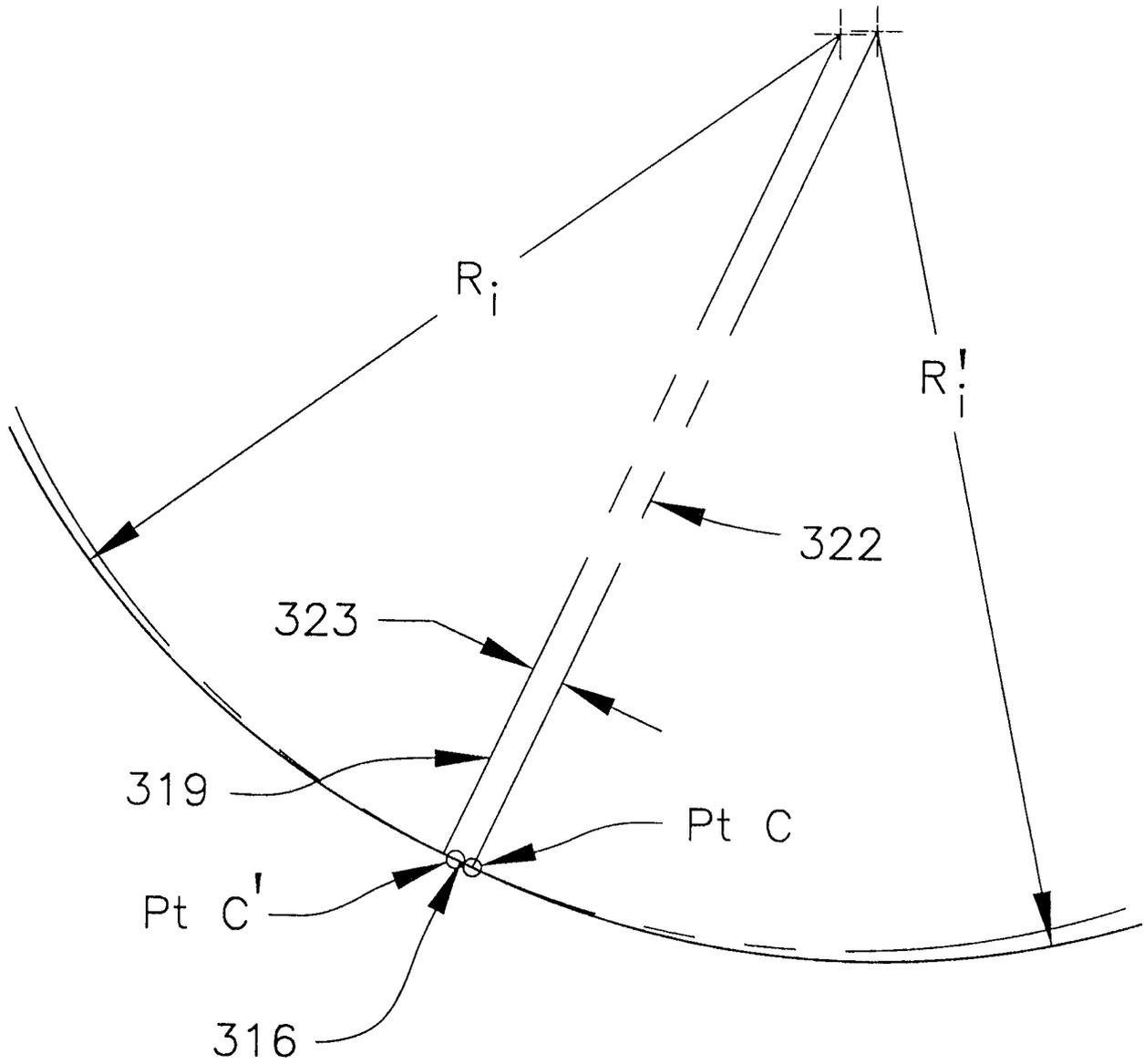


FIG. 22

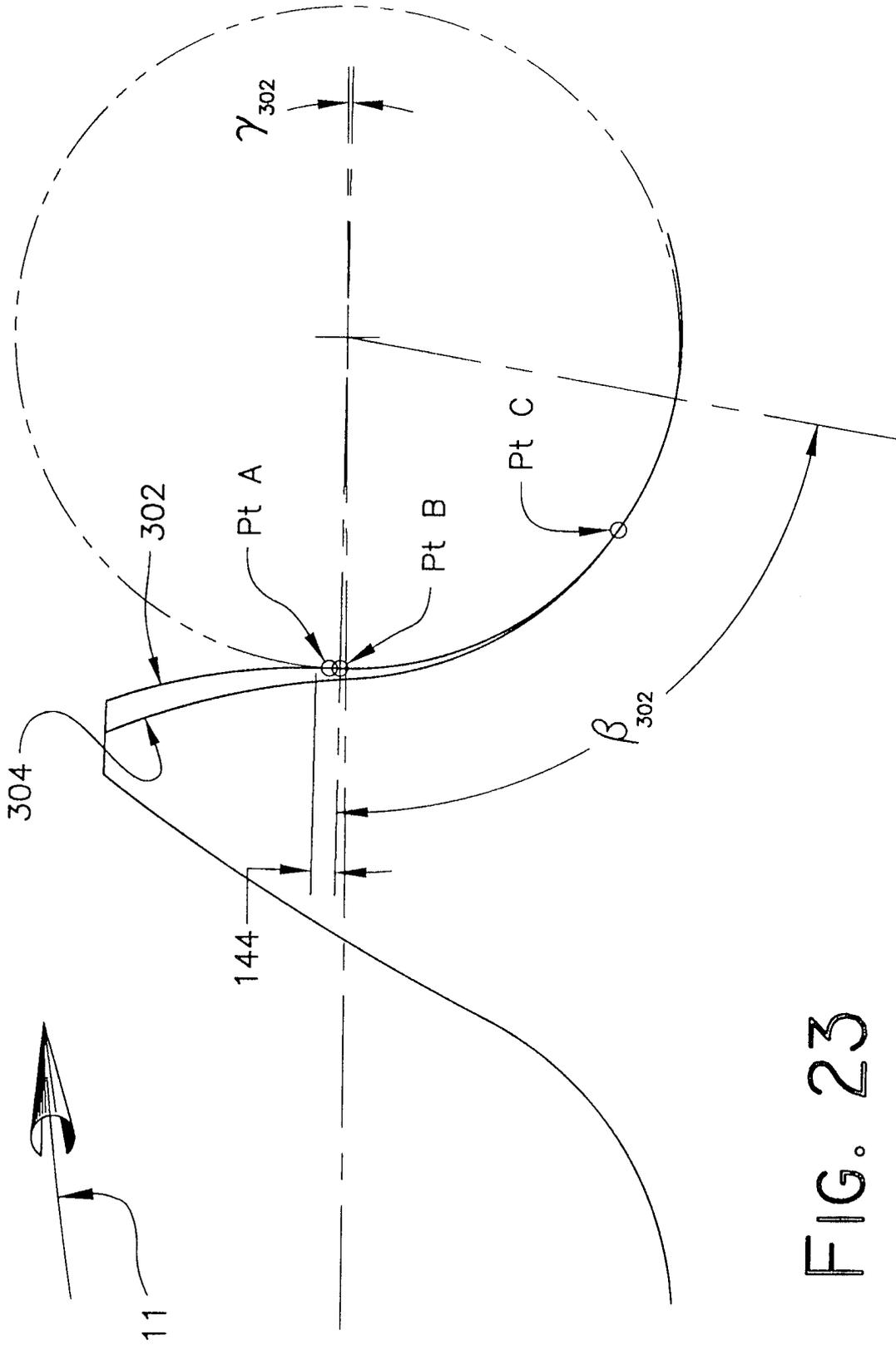


FIG. 23

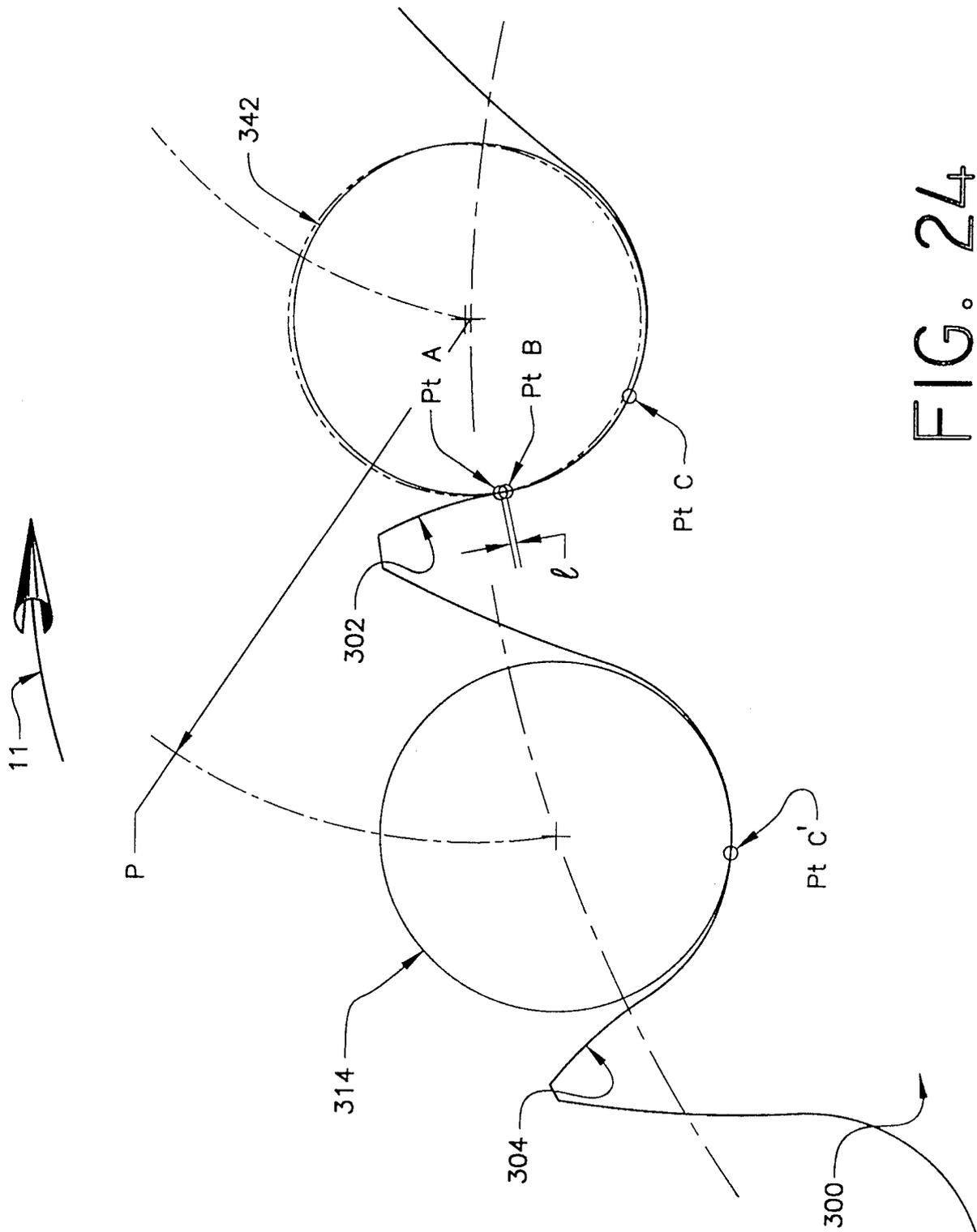


FIG. 24

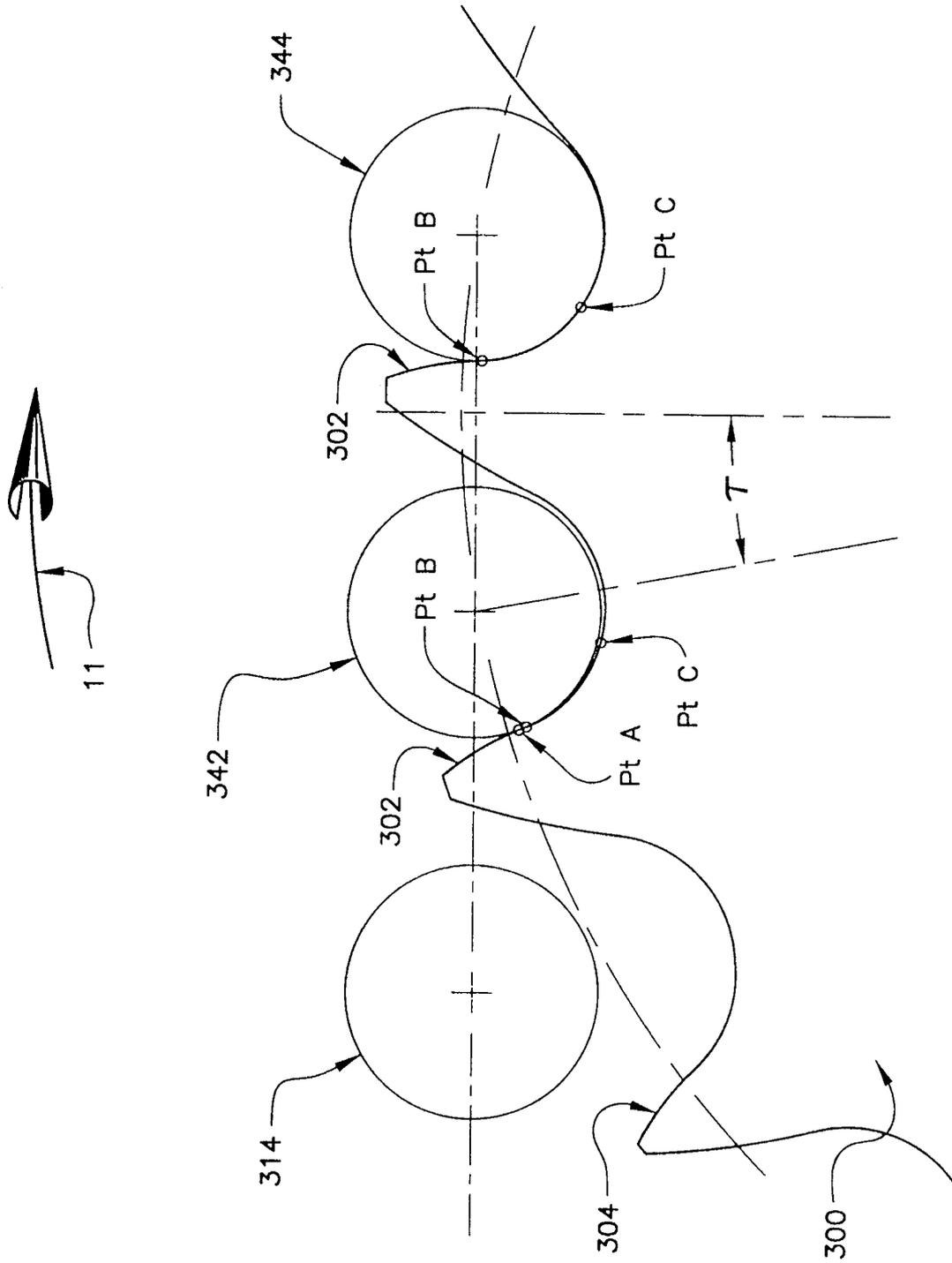


FIG. 25

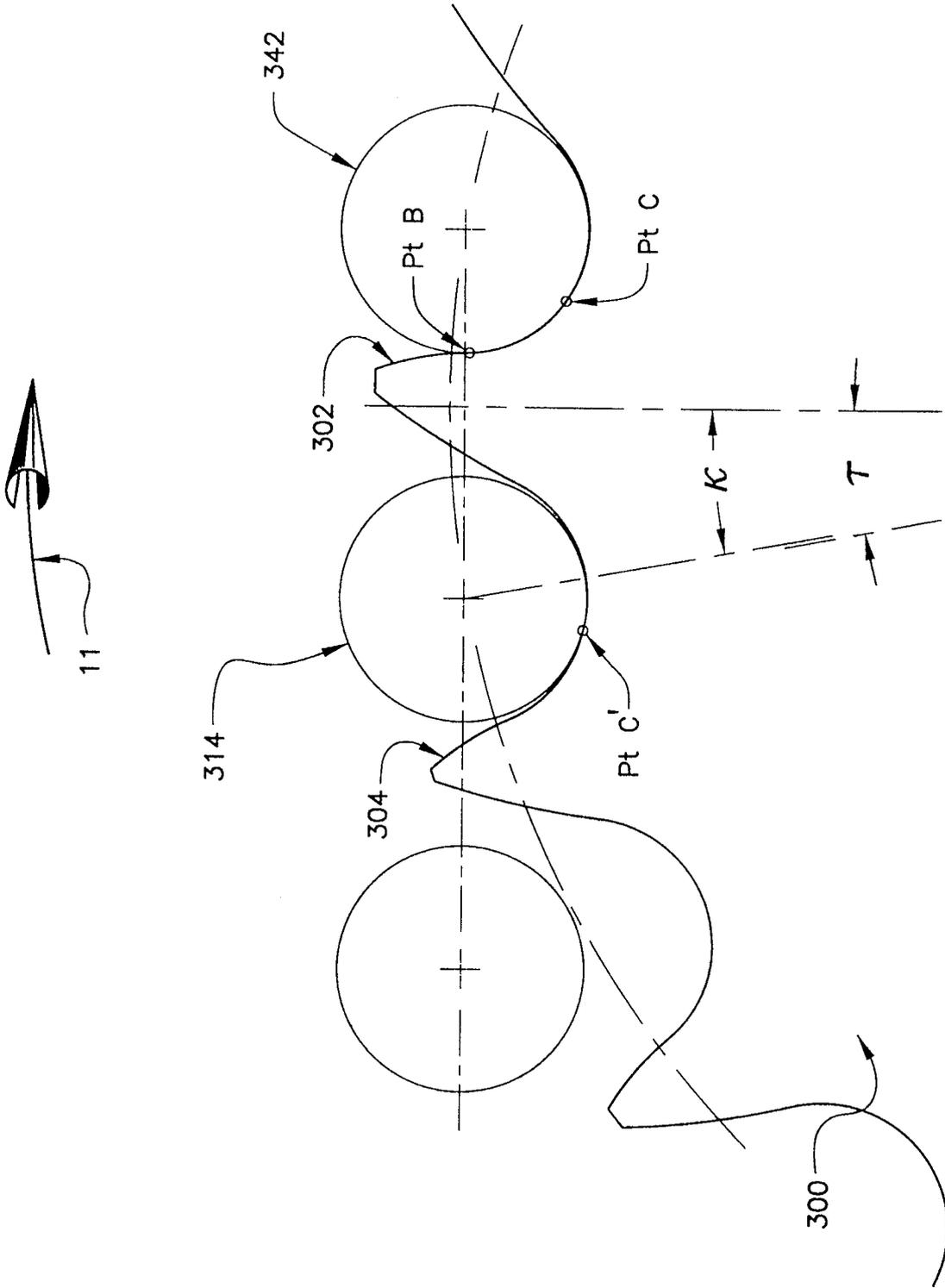


FIG. 26

ISO

Z	A	α		γ	
		(MIN)	(MAX)	(MAX)	(MIN)
18	20.000	115.00	135.00	22.500	12.500
19	18.947	115.26	135.26	22.895	12.895
20	18.000	115.50	135.50	23.250	13.250
21	17.143	115.71	135.71	23.571	13.571
22	16.364	115.91	135.91	23.864	13.864
23	15.652	116.09	136.09	24.130	14.130
24	15.000	116.25	136.25	24.375	14.375
25	14.400	116.40	136.40	24.600	14.600
26	13.846	116.54	136.54	24.808	14.808
27	13.333	116.67	136.67	25.000	15.000
28	12.857	116.79	136.79	25.179	15.179
29	12.414	116.90	136.90	25.345	15.345
30	12.000	117.00	137.00	25.500	15.500

FIG. 27
PRIOR ART

ASYMMETRICAL

Z	A	1		2		3	
		β (MAX)	γ (MIN)	β (MAX)	γ (MIN)	β (MAX)	γ (MIN)
18	20.000	73.75	6.25	80.00	0	82.00	-2
19	18.947	74.08	6.45	80.53	0	82.53	-2
20	18.000	74.38	6.63	81.00	0	83.00	-2
21	17.143	74.64	6.79	81.43	0	83.43	-2
22	16.364	74.89	6.93	81.82	0	83.82	-2
23	15.652	75.11	7.07	82.17	0	84.17	-2
24	15.000	75.31	7.19	82.50	0	84.50	-2
25	14.400	75.50	7.30	82.80	0	84.80	-2
26	13.846	75.67	7.40	83.08	0	85.08	-2
27	13.333	75.83	7.50	83.33	0	85.33	-2
28	12.857	75.98	7.59	83.57	0	85.57	-2
29	12.414	76.12	7.67	83.79	0	85.79	-2
30	12.000	76.25	7.75	84.00	0	86.00	-2

FIG. 28