

ELECTRODE FOR PLASMA TORCH WITH NOVEL ASSEMBLY METHOD AND ENHANCED HEAT TRANSFER

FIELD

Embodiments of the present invention relate to electrode assemblies for plasma arc torches and, in particular, to electrodes and electrode holders held to each other or to the plasma arc torch by way of a threaded connection. Further, some embodiments
5 relate to electrode assemblies having defined passages for providing coolant to the electrode.

BACKGROUND

Plasma arc torches are commonly used for the working of metal including cutting,
10 welding, surface treatment, melting and annealing. Such torches include an electrode that supports an arc that extends from the electrode to a workpiece in a transferred-arc mode of operation. To facilitate operation, current is passed to the electrode to create the arc, which heats the electrode to high temperatures, causing erosion and reduction in electrode life. Thus, it is conventional to surround the arc with a vortex flow of plasma
15 gas, and in some torch designs the plasma gas and arc are surrounded by a flow of secondary fluid such as a gas or water.

SUMMARY OF THE INVENTION

In an effort to improve the electrode life and reduce manufacturing costs,
20 embodiments of the present invention provide an electrode for a plasma arc torch with novel assembly method and enhanced heat transfer properties.

One example embodiment is an electrode for a plasma arc torch, the electrode comprising a generally tubular outer wall, an end wall, and a protrusion. The end wall is joined to a distal end of the outer wall and supports an emissive element in a generally
25 central region of the end wall. The protrusion extends from the generally central region of the end wall and is configured to connect with an electrode holder by a releasable connection, wherein the protrusion is configured such that at least one coolant passage forms between the protrusion and the electrode holder when the electrode is connected

with the electrode holder. In some embodiments, the releasable connection may comprise a threaded connection and the protrusion may be threaded to releasably connect the protrusion to a threaded coolant tube of the electrode holder. In other embodiments at least one coolant passage may be defined by the threaded connection.

5 Another embodiment of the present invention is a plasma arc torch comprising a torch body, a nozzle supported adjacent one end of the torch body, an electrode, and an electrode holder. The electrode holder is supported by the torch body and is configured to provide coolant through an interior of the electrode holder. The electrode comprises an end wall that supports an emissive element and a protrusion extending from a generally
10 central region of the end wall. The protrusion connects to the electrode holder by a releasable connection, wherein at least one coolant passage is formed between the protrusion and the electrode holder. The at least one coolant passage allows coolant to flow therethrough and impinge on the end wall of the electrode. In some embodiments, the releasable connection comprises a threaded connection and the protrusion may be
15 threaded to releasably connect to a threaded coolant tube of the electrode holder. In other embodiments, the at least one coolant passage is defined by the threaded connection.

Other embodiments of the present invention include an electrode assembly for a plasma arc torch. The electrode assembly comprising an electrode and an electrode
20 holder. The electrode comprises a generally tubular outer wall, an end wall joined to a distal end of the outer wall and supporting an emissive element in a generally central region of the end wall, and a protrusion extending from the generally central region of the end wall. The electrode holder connects to the electrode by a releasable connection and comprises an inner coolant tube for providing coolant to the electrode and an outer
25 coolant tube surrounding the inner coolant tube for removing coolant from the electrode via a space between the inner and outer coolant tubes. The protrusion of the electrode is configured to connect with the inner coolant tube of the electrode holder by a releasable connection and at least one coolant passage forms between the protrusion of the electrode and the inner coolant tube of the electrode holder when the electrode is
30 connected with the electrode holder. In some embodiments, the releasable connection comprises a threaded connection and the protrusion may be threaded to releasably connect the protrusion to a threaded coolant tube of the electrode holder. In other embodiments, the at least one coolant passage is defined by the threaded connection.

Another embodiment of the present invention is a method for cooling an electrode
35 in a plasma arc torch, comprising the steps of connecting an electrode to an electrode holder by a releasable connection therebetween. The electrode has an end wall supporting an emissive element and a protrusion extending from a generally central

region of the end wall, wherein the protrusion is configured to connect with the electrode holder by the releasable connection. The method further comprises providing coolant through a coolant tube of the electrode holder and through at least one coolant passage defined by the releasable connection such that the end wall of the electrode is impinged
5 by the coolant.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING(S)

Having thus described the invention in general terms, reference will now be made
10 to the accompanying drawings, which are not necessarily drawn to scale, and wherein:

FIG. 1 is a cross-sectioned side view of a conventional shielding gas plasma arc torch illustrating an electrode assembly as used in the prior art;

FIG. 2 is a cross-sectioned side view of the torch taken along a different section from FIG. 1 to illustrate coolant flow therethrough;

15 FIG. 3 is an enlarged cross-sectioned view of the lower portion of the torch as seen in FIG. 1 and illustrating the conventional electrode assembly;

FIG. 4 is an enlarged cross-sectioned view of the lower portion of a plasma arc torch illustrating one example embodiment of an electrode assembly, in accordance with some embodiments discussed herein;

20 FIG. 5 is a cross-sectioned view of the electrode assembly of FIG. 4, in accordance with some embodiments discussed herein;

FIG. 6 is an enlarged cross-sectioned view of the lower portion of the electrode assembly of FIG. 4, in accordance with some embodiments discussed herein;

25 FIG. 7 is an enlarged cross-sectioned view of an electrode of the electrode assembly of FIG. 4, in accordance with some embodiments discussed herein;

FIG. 7A is a perspective view of the electrode of FIG. 7, in accordance with some embodiments discussed herein;

30 FIG. 8 is an enlarged cross-sectioned view of the lower portion of an electrode holder of the electrode assembly of FIG. 4, in accordance with some embodiments discussed herein;

FIG. 9 is an enlarged cross-sectioned view of the lower portion of another example embodiment of an electrode assembly, in accordance with some embodiments discussed herein;

35 FIG. 10 is an enlarged cross-sectioned view of an electrode of the electrode assembly of FIG. 9, in accordance with some embodiments discussed herein;

FIG. 10A is a perspective view of the electrode of FIG. 10, in accordance with some embodiments discussed herein;

FIG. 11 is an enlarged cross-sectioned view of the lower portion of an electrode holder of the electrode assembly of FIG. 9, in accordance with some embodiments discussed herein;

FIG. 12 is an enlarged cross-sectioned view of the lower portion of another embodiment of an electrode assembly, in accordance with some embodiments discussed herein;

FIG. 13 is an enlarged cross-sectioned view of an electrode of the electrode assembly of FIG. 12, in accordance with some embodiments discussed herein;

FIG. 13A is a perspective view of the electrode of FIG. 13, in accordance with some embodiments discussed herein;

FIG. 14 is an enlarged cross-sectioned view of an electrode holder of the electrode assembly of FIG. 12, in accordance with some embodiments discussed herein; and

FIG. 15 is a cross-sectioned view of another embodiment of an electrode assembly, in accordance with some embodiments discussed herein.

DETAILED DESCRIPTION

The present invention now will be described more fully hereinafter with reference to the accompanying drawings, in which some, but not all embodiments of the inventions are shown. Indeed, these inventions may be embodied in many different forms and should not be construed as limited to the embodiments set forth herein; rather, these embodiments are provided so that this disclosure will satisfy applicable legal requirements. Like numbers refer to like elements throughout.

Plasma arc torches often utilize electrodes that comprise an elongate tubular member composed of a material of high thermal conductivity (e.g., copper, copper alloy, silver, etc.). The forward or discharge end of the tubular electrode includes a bottom end wall having an emissive element embedded therein that supports the arc. The opposite end of the electrode holds the electrode in the torch by way of a releasable connection (e.g., threaded connection) to an electrode holder. The electrode holder is typically an elongate structure held to the torch body by a threaded connection at an end opposite the end at which the electrode is held. The electrode holder and the electrode define a threaded connection for holding the electrode to the electrode holder.

The emissive element of the electrode is composed of a material that has a relatively low work function, which is defined in the art as the potential step, measured in electron volts (eV), which promotes thermionic emission from the surface of a metal at a given temperature. In view of this low work function, the element is thus capable of

readily emitting electrons when an electrical potential is applied thereto. Commonly used emissive materials include hafnium, zirconium, tungsten, and alloys thereof.

A nozzle surrounds the discharge end of the electrode and provides a pathway for directing the arc towards the workpiece. To ensure that the arc is emitted through the nozzle and not from the nozzle surface during regular, transferred-arc operation, the electrode and the nozzle are maintained at different electrical potential relative to each other. Thus, it is important that the nozzle and the electrode are electrically separated, and this is typically achieved by maintaining a predetermined physical gap between the components. The volume defining the gap is most typically filled with flowing air or some other gas used in the torch operation.

The heat generated by the plasma arc is great. The torch component that is subjected to the most intense heating is the electrode. To improve the service life of a plasma arc torch, it is generally desirable to maintain the various components of the torch at the lowest possible temperature notwithstanding this heat generation. In some torches, a passageway or bore is formed through the electrode holder, and a coolant such as water is circulated through the passageway to internally cool the electrode.

Even with the water-cooling, the electrode has a limited life span and is considered a consumable part. Thus, in the normal course of operation, a torch operator must periodically replace a consumed electrode by first removing the nozzle and then unthreading the electrode from the electrode holder. A new electrode is then screwed onto the electrode holder and the nozzle is reinstalled so that the plasma arc torch can resume operation.

Other considerations for electrode design include constraints on the threaded connection between the electrode holder and the electrode. For example, the threaded connection must be structurally strong enough to securely hold the electrode to the electrode holder. Additionally, a considerable current is passed through the electrode holder to the electrode, in some cases up to 1,000 amperes of cutting current. Thus, the threaded connection should provide sufficient contact surface area between the electrode and the electrode holder to allow this current to pass through. Finally, the cost of manufacturing the electrode should be as small as possible, especially because the electrode is a frequently replaced consumable part.

Thus, there is a need to increase the useful life of the electrode by more efficient ways to provide coolant, while maintaining low cost of manufacture for the electrode and electrode holder.

The following discussion with respect to FIGS. 1-3 describes a prior plasma arc torch that would benefit from the invention. A plasma arc torch **300** using an electrode and electrode holder according to some embodiments of the present invention is

illustrated in FIG. 4. Thus, embodiments of the present invention are described in greater detail with respect to FIGS. 4-15.

FIGS. 1-3 show a prior plasma arc torch **10**. The torch **10** is a shielding gas torch, which provides a swirling curtain or jet of shielding gas surrounding the electric arc during a working mode of operation of the torch. The torch **10** includes a generally cylindrical upper or rear insulator body **12** which may be formed of a potting compound or the like, a generally cylindrical main torch body **14** connected to the rear insulator body **12** and generally made of a conductive material such as metal, a generally cylindrical lower or front insulator body **16** connected to the main torch body **14**, an electrode holder assembly **18** extending through the main torch body **14** and front insulator body **16** and supporting an electrode **20** at a free end of the electrode holder assembly, and a nozzle assembly **22** connected to the insulator body **16** adjacent the electrode **20**.

A plasma gas connector tube **24** extends through the rear insulator body **12** and is connected by screw threads (not shown) into a plasma gas passage **26** of the main torch body **14**. The plasma gas passage **26** extends through the main torch body **14** to a lower end face **28** thereof for supplying a plasma gas (sometimes referred to as a cutting gas), such as oxygen, air, nitrogen, or argon, to a corresponding passage in the insulator body **16**.

A shielding gas connector tube **30** extends through the rear insulator body **12** and is connected by screw threads into a shielding gas passage **32** of the main torch body **14**. The shielding gas passage **32** extends through the main torch body **14** to the lower end face **28** for supplying a shielding gas, such as argon or air, to a corresponding passage in the insulator body **16**.

The insulator body **16** has an upper end face **34** that abuts the lower end face **28** of the main torch body. A plasma gas passage **36** extends through the insulator body **16** from the upper end face **34** into a cylindrical counterbore **38** in the lower end of the insulator body **16**. As further described below, the counterbore **38**, together with the upper end of the nozzle assembly **22**, forms a plasma gas chamber **40** from which plasma gas is supplied to a primary or plasma gas nozzle of the torch. As such, plasma gas from a suitable source enters the plasma gas chamber **40** by flowing through the plasma gas connector tube **24**, through the plasma gas passage **26** in the main torch body **14**, into the plasma gas passage **36** of the insulator body **16**, which is aligned with the passage **26**, and into the chamber **40**.

The nozzle, which is illustrated as a two-part nozzle assembly **22**, includes an upper nozzle member **42**, which has a generally cylindrical upper portion slidably received within a metal insert sleeve **44** that is inserted into the counterbore **38** of the insulator body **16**. An O-ring **46** seals the sliding interconnection between the upper

nozzle member **42** and the metal insert sleeve **44**. A lower nozzle tip **48** of generally frustoconical form also forms a part of the nozzle assembly **22**, and is threaded into the upper nozzle member **42**. The lower nozzle tip **48** includes a nozzle exit orifice **50** at the tip end thereof. The lower nozzle tip **48** and upper nozzle member **42** could alternatively
5 be formed as one unitary nozzle. In either configuration, the nozzle channels the plasma gas from a larger distal opening **49** to the exit orifice **50**. A plasma gas flow path thus exists from the plasma gas chamber **40** through the nozzle chamber **41** for directing a jet of plasma gas out the nozzle exit orifice **50** to aid in performing a work operation on a workpiece.

10 The plasma gas jet preferably has a swirl component created, in a known manner; by a hollow cylindrical ceramic gas baffle **52** partially disposed in a counterbore recess **54** of the insulator body **16**. A lower end of the baffle **52** abuts an annular flange face of the upper nozzle member **42**. The baffle **52** has non-radial holes (not shown) for directing plasma gas from the plasma gas chamber **40** into a lower portion of the nozzle chamber
15 **41** with a swirl component of velocity.

The electrode holder assembly **18** includes a tubular electrode holder **56** which has its upper end connected by threads **11** within a blind axial bore **58** in the main torch body **14**. The electrode holder **56** is somewhat consumable, although usually less so than the electrode itself, and thus the electrode holder and the axial bore **58** can also be
20 provided with a threaded connection according to the present invention as discussed below. The upper end of electrode holder **56** extends through an axial bore **60** formed through the insulator body **16**, and the lower end of the electrode holder **56** includes an enlarged internally screw-threaded coupler **62** which has an outer diameter slightly smaller than the inner diameter of the ceramic gas baffle **52** which is sleeved over the
25 outside of the coupler **62**. The electrode holder **56** also includes internal screw threads spaced above the coupler **62** for threadingly receiving a coolant tube **64** which supplies coolant to the electrode **20**, as further described below, and which extends outward from the axial bore of the insulator body **16** into the central passage of the electrode **20**. To prevent improper disassembly or reassembly of the coolant tube **64** and the electrode
30 holder **56**, the screw thread connection between those items may be cemented or otherwise secured together during manufacture to form an inseparable electrode holder assembly **18**. The electrode **20** may be of the type described in U.S. Patent No. 5,097,111, assigned to the assignee of the present application, and incorporated herein by reference.

35 The prior art electrode **20** comprises a cup-shaped body whose open upper end is threaded by screw threads **63** into the coupler **62** at the lower end of the electrode holder **56**, and whose capped lower end is closely adjacent the lower end of the coolant tube **64**.

A coolant circulating space exists between the inner surface of the wall of the electrode **20** and the outer surface of the wall of the coolant tube **64**, and between the outer surface of the wall of the coolant tube **64** and the inner surface of the wall of the electrode holder **56**. The electrode holder **56** includes a plurality of holes **66** for supplying coolant from the space within the electrode holder to a space **68** between the electrode holder and the inner wall of the axial bore **60** in the insulator body **16**. A seal **69** located between the holes **66** and the coupler **62** seals against the inner wall of the bore **60** to prevent coolant in the space **68** from flowing past the seal **69** toward the coupler **62**. A raised annular rib or dam **71** on the outer surface of the electrode holder **56** is located on the other side of the holes **66** from the seal **69**, for reasons which will be made apparent below. A coolant supply passage **70** (FIG. 2) extends through the insulator body from the space **68** through the outer cylindrical surface of the insulator body **16** for supplying coolant to the nozzle assembly **22**, as further described below.

During starting of the torch **10**, a difference in electrical voltage potential is established between the electrode **20** and the nozzle tip **48** so that an electric arc forms across the gap therebetween. Plasma gas is then flowed through the nozzle assembly **22** and the electric arc is blown outward from the nozzle exit orifice **50** until it attaches to a workpiece, at which point the nozzle assembly **22** is disconnected from the electric source so that the arc exists between the electrode **20** and the workpiece. The torch is then in a working mode of operation.

For controlling the work operation being performed, it is known to use a control fluid such as a shielding gas to surround the arc with a swirling curtain of gas. To this end, the insulator body **16** includes a shielding gas passage **72** that extends from the upper end face **34** axially into the insulator body, and then angles outwardly and extends through the cylindrical outer surface of the insulator body. A nozzle retaining cup assembly **74** surrounds the insulator body **16** to create a generally annular shielding gas chamber **76** between the insulator body **16** and the nozzle retaining cup assembly **74**. Shielding gas is supplied through the shielding gas passage **72** of the insulator body **16** into the shielding gas chamber **76**.

The nozzle retaining cup assembly **74** includes a nozzle retaining cup holder **78** and a nozzle retaining cup **80** which is secured within the holder **78** by a snap ring **81** or the like. The nozzle retaining cup holder **78** is a generally cylindrical sleeve, preferably formed of metal, which is threaded over the lower end of a torch outer housing **82** which surrounds the main torch body **14**. Insulation **84** is interposed between the outer housing **82** and the main torch body **14**. The nozzle retaining cup **80** preferably is formed of plastic and has a generally cylindrical upper portion that is secured within the cup holder **78** by the snap ring **81** and a generally frustoconical lower portion which extends toward

the end of the torch and includes an inwardly directed flange **86**. The flange **86** confronts an outwardly directed flange **88** on the upper nozzle member **42** and contacts an O-ring **90** disposed therebetween. Thus, in threading the nozzle retaining cup assembly **74** onto the outer housing **82**, the nozzle retaining cup **80** draws the nozzle assembly **22** upward
5 into the metal insert sleeve **44** in the insulator body **16**. The nozzle assembly **22** is thereby made to contact an electrical contact ring secured within the counterbore **38** of the insulator body **16**. More details of the electrical connections within the torch can be found in commonly-owned US Patent No. 6,215,090, which is incorporated by reference herein in its entirety.

10 The nozzle retaining cup **80** fits loosely within the cup holder **78**, and includes longitudinal grooves **92** in its outer surface for the passage of shielding gas from the chamber **76** toward the end of the torch. Alternatively or additionally, grooves (not shown) may be formed in the inner surface of the cup holder **78**. A shielding gas cup **94** of generally frustoconical form concentrically surrounds and is spaced outwardly of the
15 lower nozzle tip **48** and is held by a shield retainer **96** that is threaded over the lower end of the cup holder **78**. A shielding gas flow path **98** thus extends from the longitudinal grooves **92** in retaining cup **80**, between the shield retainer **96** and the retaining cup **80** and upper nozzle member **42**, and between the shielding gas cup **94** and the lower nozzle tip **48**.

20 The shielding gas cup **94** includes a diffuser **100** that in known manner imparts a swirl to the shielding gas flowing into the flow path between the shielding gas cup **94** and the lower nozzle tip **48**. Thus, a swirling curtain of shielding gas is created surrounding the jet of plasma gas and the arc emanating from the nozzle exit orifice **50**.

With primary reference to FIG. 2, the coolant circuits for cooling the electrode **20**
25 and nozzle assembly **22** are now described. The torch **10** includes a coolant inlet connector tube **112** that extends through the rear insulator body **12** and is secured within a coolant inlet passage **114** in the main torch body **14**. The coolant inlet passage **114** connects to the center axial bore **58** in the main torch body. Coolant is thus supplied into the bore **58** and thence into the internal passage through the electrode holder **56**, through
30 the internal passage of the coolant tube **64**, and into the space between the tube **64** and the electrode **20**. Heat is transferred to the liquid coolant (typically water or antifreeze) from the lower end of the electrode (from which the arc emanates) and the liquid then flows through a passage between the lower end of the coolant tube **64** and the electrode
35 electrode **20**, and then into the annular space between the coolant tube **64** and the electrode holder **18**.

The coolant then flows out through the holes **66** into the space **68** and into the passage **70** through the insulator body **16**. The seal **69** prevents the coolant in the space **68** from flowing toward the coupler **62** at the lower end of the holder **56**, and the dam **71** substantially prevents coolant from flowing past the dam **71** in the other direction,
5 although there is not a positive seal between the dam **71** and the inner wall of the bore **60**. Thus, the coolant in space **68** is largely constrained to flow into the passage **70**. The insulator body **16** includes a groove or flattened portion **116** that permits coolant to flow from the passage **70** between the insulator body **16** and the nozzle retaining cup **80** and into a coolant chamber **118** which surrounds the upper nozzle member **42**. The coolant
10 flows around the upper nozzle member **42** to cool the nozzle assembly.

Coolant is returned from the nozzle assembly via a second groove or flattened portion **120** angularly displaced from the portion **116**, and into a coolant return passage **122** in the insulator body **16**. The coolant return passage **122** extends into a portion of the axial bore **60** that is separated from the coolant supply passage **70** by the dam **71**.
15 The coolant then flows between the electrode holder **56** and the inner wall of the bore **60** and the bore **58** in the main torch body **14** into an annular space **126** which is connected with a coolant return passage **128** formed in the main torch body **14**, and out the coolant return passage **128** via a coolant return connector tube **130** secured therein. Typically, returned coolant is recirculated in a closed loop back to the torch after being cooled.

20 In use, and with reference to FIG. 1, one side of an electrical potential source **210**, typically the cathode side, is connected to the main torch body **12** and thus is connected electrically with the electrode **20**, and the other side, typically the anode side, of the source **210** is connected to the nozzle assembly **22** through a switch **212** and a resistor **214**. The anode side is also connected in parallel to the workpiece **216** with no resistor
25 interposed therebetween. A high voltage and high frequency are imposed across the electrode and nozzle assembly, causing an electric arc to be established across a gap therebetween adjacent the plasma gas nozzle discharge. Plasma gas is flowed through the nozzle assembly to blow the pilot arc outward through the nozzle discharge until the arc attaches to the workpiece. The switch **212** connecting the potential source to the
30 nozzle assembly is then opened, and the torch is in the transferred arc mode for performing a work operation on the workpiece. The power supplied to the torch is increased in the transferred arc mode to create a cutting arc, which is of a higher current than the pilot arc.

Example embodiments of the present invention are illustrated in FIGS. 4-15. FIG.
35 4 shows one example embodiment of a plasma arc torch **300** comprising an electrode holder assembly **318** and novel threaded connection. The electrode holder assembly **318** comprises an electrode holder **356** and an electrode **320**. Although illustrated herein with

a torch that uses a high-frequency pilot signal to start an arc, the electrode and electrode holder according to the invention can also be used with blowback-type torches.

With reference to FIGS. 4-6, the electrode holder **356** is tubular and comprises an upper end connected by threads **11** within the blind axial bore in the main torch body, as described above, and a lower end connected to the electrode **320**. The electrode holder **356** comprises an inner coolant tube **352** and an outer coolant tube **354**. The inner coolant tube **352** supplies coolant to the electrode **320**. The outer coolant tube **354** is generally tubular shaped and annularly surrounds the inner coolant tube **352**. The outer coolant tube **354** is configured to remove coolant from the electrode **320**. The electrode holder **356** can be formed from a variety of different electrically conductive materials, but in one embodiment the electrode holder **356** is made of brass or a brass alloy.

The electrode **320**, shown in cross-sectional view in FIG. 7 and perspective view in FIG. 7A, is generally cup-shaped. In the depicted embodiment, the electrode **320** comprises an outer wall **335**, an end wall **330**, and a protrusion **325**. The outer wall **335** is generally tubular shaped and, with reference to FIG. 6, may be configured to engage with the electrode holder **356** such that an outer passage **337** is formed between the exterior surface of the inner coolant tube **352** and the interior surface of the outer wall **335**, allowing coolant to pass through the outer passage **337** to the outer coolant tube **354**. The end wall **330** joins to a distal end of the outer wall **335** and supports an emissive element **332** in a generally central region of the end wall **330**. The protrusion **325** extends from the generally central region of the end wall **330** and is configured to connect with the electrode holder **356** by a releasable connection, such as a threaded connection shown in the depicted embodiment. The electrode **320** can be formed from a variety of different electrically conductive materials, but in one embodiment the electrode **320** comprises a body made of copper or a copper alloy.

With reference to FIGS. 6 and 7, threads **310** secure the electrode **320** to the electrode holder **356**. In the depicted embodiment, the inner coolant tube **352** of the electrode holder **356** has a female threaded portion **317** formed therein on the interior surface of the inner coolant tube **352**. The protrusion **325** of the electrode **320** has a male threaded portion **319** formed thereon on the exterior surface of the protrusion **325**. The female threaded portion **317**, shown in FIG. 8, may be formed on the lower end of the inner coolant tube **352** and configured to releasably receive the male threaded portion **319** of the protrusion **325**. The male threaded portion **319** may comprise threads **310** configured as any type of thread, such as a double start screw thread, a metric screw thread, a unified screw thread, a British standard pipe thread, a Whitworth screw thread, or a screw thread having a stub acme profile as described in U.S. Patent No. 7,081,597, assigned to assignee of the present invention, and which is hereby incorporated herein by

reference. The female threaded portion **317** may also be configured with a thread profile to match a male threaded portion **319** with threads **310** configured as any type of thread, such as those screw threads listed above.

In some embodiments, the protrusion **325** may be further configured such that at least one coolant passage **360** forms between the protrusion **325** and the electrode holder **356** when the electrode **320** is connected to the electrode holder **356**. In the depicted embodiment, the male threaded portion **319** and the female threaded portion **317** are configured with extra space between the threads **310** so that coolant can flow between the threads **310**. In particular, as shown in FIG. 6, the extra space can form at least one coolant passage **360** between the protrusion **325** and the inner coolant tube **352** of the electrode holder **356**. In the depicted embodiment, the coolant passage **360** comprises a helically extending space between the thread profile of the male threaded portion **319** on the protrusion **325** and the thread profile of the female threaded portion **317** on the inner coolant tube **352**. Thus, coolant enters the coolant passage **360** from the inner coolant tube **352**, spirals around the coolant passage **360** within the threads, and exits the coolant passage **360** to impinge the end wall **330**. The coolant then flows into the outer passage **337** and away from the electrode **320** through the outer coolant tube **354**. These novel coolant passages **360**, which follow the threaded connection of the electrode assembly **318**, allow the flowing coolant to contact inner surfaces of the electrode for a greater amount of time relative to an electrode such as shown in FIGS. 1-3. Additionally, higher coolant velocity may be achieved, which will improve convective heat transfer from the electrode to the coolant. The net result should be enhanced cooling of the electrode **320**, which in turn should prolong the life of the electrode **320**.

In the depicted embodiment, the inner coolant tube **352** of the electrode holder **356** comprises a bottom end **353** extending generally toward the electrode **320**. Different configurations of the electrode assembly **318** may require the bottom end **353** of the inner coolant tube **352** to be positioned properly with respect to the electrode **320** for the plasma arc torch to function properly. For example, in some embodiments, an opening **363** may be configured to allow coolant to flow from the coolant passage **360** to the outer passage **337** formed between the inner coolant tube **352** and the outer wall **335** of the electrode **320**, thereby allowing the coolant to be ultimately removed from the electrode **320** through the outer coolant tube **354**. In the depicted embodiment, the opening **363** is configured as additional space between the bottom end **353** of the inner coolant tube **352** and the end wall **330** of the electrode **320**. In some embodiments, this may be accomplished by configuring the female threaded portion **317** to extend only partially up the lower end of the inner coolant tube **352** such that the protrusion **325** can be screwed into the female threaded portion **317** for only a certain distance, ensuring the opening **363**

to form. Alternatively or additionally, a stopper (not shown) can be positioned within the female threaded portion **317** to prevent the male threaded portion **319** of the protrusion **325** from being advanced past a certain point (i.e., the position of the stopper), thereby ensuring the opening **363** forms.

5 Alternatively or additionally, in other embodiments, the opening **363** may comprise a slot (not shown) in the inner coolant tube **352** that connects the coolant passage **360** to the outer passage **337**. The slot may be configured adjacent to the bottom of the coolant passage **360** such that coolant flows through the entire coolant passage **360**, out of the slot, into the outer passage **337**, and up through the outer coolant tube **354**. In some
10 embodiments, the slot can allow the coolant to flow through the electrode assembly **318** with greater velocity, improving the convective heat transfer and prolonging the life of the electrode **320**.

FIGS. 9-11 show another embodiment of the present invention, wherein an electrode assembly **418** utilizes a double start screw thread for the releasable connection
15 between the electrode **420** and the electrode holder **456**. However, the electrode assembly **418** may be used in a plasma arc torch in similar manner as the electrode assembly **318** described above with respect FIGS. 4-8, as well as with other embodiments of the present invention as described herein.

In the depicted embodiment of FIG. 9, the electrode assembly **418** comprises an
20 electrode **420** and an electrode holder **456**. The electrode **420** comprises a protrusion **425** with a male threaded portion **419** defined by threads **410** that form a double-start screw thread. The electrode holder **456** comprises an inner coolant tube **452** with a female threaded portion **417** configured with a thread profile that matches the double start screw thread of the male threaded portion **419** to allow for a releasable connection.
25 Furthermore, the thread profile of the male and female threaded portions **419**, **417**, similar to the male and female threaded portions **319**, **317** of the electrode assembly **318**, may also form at least one coolant passage **460**. In the depicted embodiment, the electrode assembly **418** comprises two coolant passages **460** and **460'**, formed separately due to the thread profile of the double start screw thread. As such, in some embodiments,
30 coolant may flow through both coolant passages **460**, **460'** out of respective openings **463**, **463'** and away from the electrode **420** through the outer coolant passage **454**. In the depicted embodiment, the openings **463**, **463'** comprise slots formed in the inner coolant tube **452**.

FIGS. 12-14 show another embodiment of the present invention, wherein the
35 electrode assembly **518** comprises an electrode **520** and an electrode holder **556** having a threaded connection between an exterior surface of an inner coolant tube **552** and an interior surface of a protrusion **525**. The electrode assembly **518** may also be used in a

plasma arc torch in similar manner as the electrode assembly **318** described with respect to FIGS. 4-8, as well as with other embodiments of the present invention as described herein.

With reference to FIG. 12, the electrode **520** comprises an annularly shaped protrusion **525** having a female threaded portion **517**. The electrode holder **556** comprises an inner coolant tube **552** having a male threaded portion **519** comprising threads **510**. The thread profile of the male threaded portion **519** and the corresponding female threaded portion **517** may be any type of screw thread, such as a double start screw thread, a metric screw thread, a unified screw thread, a British standard pipe thread, a Whitworth screw thread, or a screw thread having a stub acme profile.

In the depicted embodiment, the inner coolant tube **552** and the central bore of the protrusion **525** define an inner passage **536** configured to allow coolant to flow to the electrode **520**. In some embodiments, the inner passage **536** defines a reservoir positioned directly above an end wall **530** and an emissive element **532** contained within the end wall **530**. Thus, coolant in the reservoir will directly contact the portion of the electrode **520** with the highest temperature (i.e., the portion near the emissive element **532**).

Additionally, in the depicted embodiment, the electrode **520** further comprises at least one passage or slot **576**. One end of the slot **576** connects the inner passage **536** to an outer passage **537** defined between the protrusion **525** and the outer wall **535**. Therefore, the slot **576** allows coolant to flow from the inner passage **536** to the outer passage **537**, so that the coolant can ultimately flow away from the electrode through the outer coolant tube **554** of the electrode holder **556**.

FIG. 15 shows another embodiment of an electrode assembly **618** with an electrode holder **656** and an attached electrode **620**. In the depicted embodiment, the electrode **620** comprises a tubular outer wall **635** that extends past the protrusion **625**. Coolant can flow through the inner coolant tube **652** of the electrode holder **656** and around the protrusion **625** to cool the electrode **620**, as described in various embodiments above. Furthermore, the coolant can flow between the exterior surface of the inner coolant tube **652** and the interior surface of the outer wall **635** to the outer coolant tube **654** for removal from the electrode **620**.

Another embodiment of the present invention includes a method for cooling an electrode in a plasma arc torch comprising providing coolant to the electrode through various embodiments of the invention as described herein. In particular, the method may comprise the steps of connecting an electrode to an electrode holder by a releasable connection therebetween, the electrode having an end wall supporting an emissive element and a protrusion extending from a generally central region of the end wall, the

protrusion being configured to connect with the electrode holder by the releasable connection. The method may further comprise providing coolant through a coolant tube of the electrode holder and through at least one coolant passage defined by the releasable connection such that the end wall of the electrode is impinged by the coolant.

5 In some embodiments, the method may further comprise removing coolant from the at least one coolant passage through at least one slot adjacent to the coolant passage. The method may also further comprise removing coolant from the electrode through an outer coolant tube defined in the electrode holder. In other embodiments, the step of providing coolant through the at least one coolant passage comprises passing coolant through a
10 helically extending space between a thread profile on the protrusion of the electrode body and a thread profile on the coolant tube of the electrode holder.

Embodiments of the present invention as described herein address releasable connections and the issue of heat transfer for electrode cooling methods. In particular, some embodiments utilize cooling passages formed between the thread profile of the
15 electrode and the inner coolant tube of the electrode holder to increase coolant flow velocity and increase the surface area used for heat transfer between the electrode and the coolant. Other embodiments described herein also advantageously utilize slots to facilitate coolant flow. In fact, the combination of the coolant passages and the slots has shown to increase flow velocity by three fold. Thus, embodiments of the present
20 invention improve heat transfer by increasing flow velocity and increasing the surface area of the electrode that interacts with the coolant, thereby increasing the useable life of the electrode in a plasma arc torch.

Many modifications and other embodiments of the inventions set forth herein will come to mind to one skilled in the art to which these inventions pertain having the benefit
25 of the teachings presented in the foregoing descriptions and the associated drawings. Therefore, it is to be understood that the inventions are not to be limited to the specific embodiments disclosed and that modifications and other embodiments are intended to be included herein. Although specific terms are employed herein, they are used in a generic and descriptive sense only and not for purposes of limitation.

CLAIMS

1. An electrode for a plasma arc torch, the electrode comprising;

a generally tubular outer wall;

an end wall joined to a distal end of the outer wall and supporting an emissive
5 element in a generally central region of the end wall; and

a protrusion extending from the generally central region of the end wall and
configured to connect with an electrode holder by a releasable connection, wherein the
protrusion is configured such that at least one coolant passage forms between the
protrusion and the electrode holder when the electrode is connected with the electrode
10 holder.

2. The electrode of claim 1, wherein the releasable connection comprises a threaded
connection, the protrusion being threaded to releasably connect the protrusion to a
threaded coolant tube of an electrode holder.

15

3. The electrode of claim 2, wherein at least one coolant passage is defined by the
threaded connection.

4. The electrode of claim 2, wherein a proximal end of the outer wall is configured to
20 mate with an outer coolant tube of the electrode holder such that the outer wall defines an
outer passage configured to remove coolant from the electrode to the outer coolant tube
of the electrode holder.

5. The electrode of claim 2, wherein the threaded connection is configured as one of
25 a double start screw thread, a metric screw thread, a unified screw thread, a British
standard pipe thread, a Whitworth screw thread, and a screw thread having a stub acme
profile.

6. The electrode of claim 3, wherein the at least one coolant passage comprises a
30 helically extending space between a thread profile on the protrusion of the electrode and
a thread profile on the coolant tube of the electrode holder.

7. The electrode of claim 2, wherein at least a portion of an exterior surface of the protrusion is configured to connect with the coolant tube of the electrode holder by the threaded connection.

5 8. The electrode of claim 7, wherein the protrusion is further configured such that a gap forms between the end wall and the coolant tube of the electrode holder when the electrode is connected to the electrode holder.

9. The electrode of claim 2, wherein the protrusion is annular and comprises an interior surface, and wherein at least a portion of the interior surface of the protrusion is configured to connect with the coolant tube of the electrode holder by the threaded connection.

10 10. The electrode of claim 9, wherein the electrode comprises an inner passage defined by the protrusion and an outer passage defined between the protrusion and the outer wall, and wherein the protrusion is further configured with at least one slot connecting the inner passage to the outer passage.

11. A plasma arc torch comprising:

20 a torch body;

a nozzle supported adjacent one end of the torch body;

an electrode holder supported by the torch body and configured to provide coolant through an interior of the electrode holder; and

25 an electrode having an end wall that supports an emissive element and a protrusion extending from a generally central region of the end wall, the protrusion being connected to the electrode holder by a releasable connection, wherein at least one coolant passage is formed between the protrusion and the electrode holder, the at least one coolant passage allowing coolant to flow therethrough and impinge on the end wall of the electrode.

30

12. The plasma arc torch of claim 11, wherein the releasable connection comprises a threaded connection, the protrusion being threaded to releasably connect the protrusion to a threaded coolant tube of the electrode holder.

13. The plasma arc torch of claim 12, wherein the at least one coolant passage is defined by the threaded connection.

5 14. The plasma arc torch of claim 11, wherein the electrode holder comprises an inner coolant tube and an outer coolant tube, wherein the inner coolant tube has the releasable connection with the protrusion and is configured to provide coolant to the electrode, and wherein the outer coolant tube is configured to remove coolant from the electrode.

10 15. The plasma arc torch of claim 14, wherein the electrode holder further comprises at least one slot located adjacent to the at least one coolant passage such that coolant can flow from the coolant passage through the at least one slot to the outer coolant tube.

15 16. The plasma arc torch of claim 15, wherein the at least one coolant passage has a proximal end where coolant enters and a distal end where coolant exits, and wherein the at least one slot is located adjacent to the distal end of the coolant passage.

17. The plasma arc torch of claim 12, wherein the threaded connection is configured as one of a double start screw thread, a metric screw thread, a unified screw thread, a British standard pipe thread, a Whitworth screw thread, and a screw thread having a stub acme profile.

25 18. The plasma arc torch of claim 12, wherein the at least one coolant passage comprises a helically extending space between a thread profile on the protrusion of the electrode and a thread profile on the coolant tube of the electrode holder.

19. The plasma arc torch of claim 14, the releasable connection being between at least a portion of an exterior surface of the protrusion and at least a portion of an interior surface of the inner coolant tube.

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20. The plasma arc torch of claim 14, wherein the inner coolant tube comprises a bottom end facing the electrode, and wherein the inner coolant tube is configured to

provide a space between the bottom end and the end wall of the electrode when the electrode holder is connected to the electrode.

21. The plasma arc torch of claim 12, wherein the protrusion is annular and comprises an interior surface, and wherein at least a portion of the interior surface of the protrusion is configured to connect with the coolant tube of the electrode holder by the threaded connection.

22. The plasma arc torch of claim 21, wherein the electrode comprises an inner passage defined by the protrusion and an outer passage defined between the protrusion and the outer wall, and wherein the protrusion is further configured with at least one slot connecting the inner passage to the outer passage.

23. A method for cooling an electrode in a plasma arc torch, comprising the steps of:
connecting an electrode to an electrode holder by a releasable connection therebetween, the electrode having an end wall supporting an emissive element and a protrusion extending from a generally central region of the end wall, the protrusion being configured to connect with the electrode holder by the releasable connection; and
providing coolant through a coolant tube of the electrode holder and through at least one coolant passage defined by the releasable connection such that the end wall of the electrode is impinged by the coolant.

24. The method of claim 23 further comprising removing coolant from the at least one coolant passage through at least one slot adjacent to the coolant passage.

25. The method of claim 24 further comprising removing coolant from the electrode through an outer coolant tube defined in the electrode holder.

26. The method of claim 23, wherein the step of providing coolant through the at least one coolant passage comprises passing coolant through a helically extending space between a thread profile on the protrusion of the electrode body and a thread profile on the coolant tube of the electrode holder.

27. An electrode assembly for a plasma arc torch, comprising:

an electrode comprising;

a generally tubular outer wall;

5 an end wall joined to a distal end of the outer wall and supporting an emissive element in a generally central region of the end wall; and

a protrusion extending from the generally central region of the end wall; and

10 an electrode holder connected to the electrode by a releasable connection, the electrode holder comprising;

an inner coolant tube for providing coolant to the electrode; and

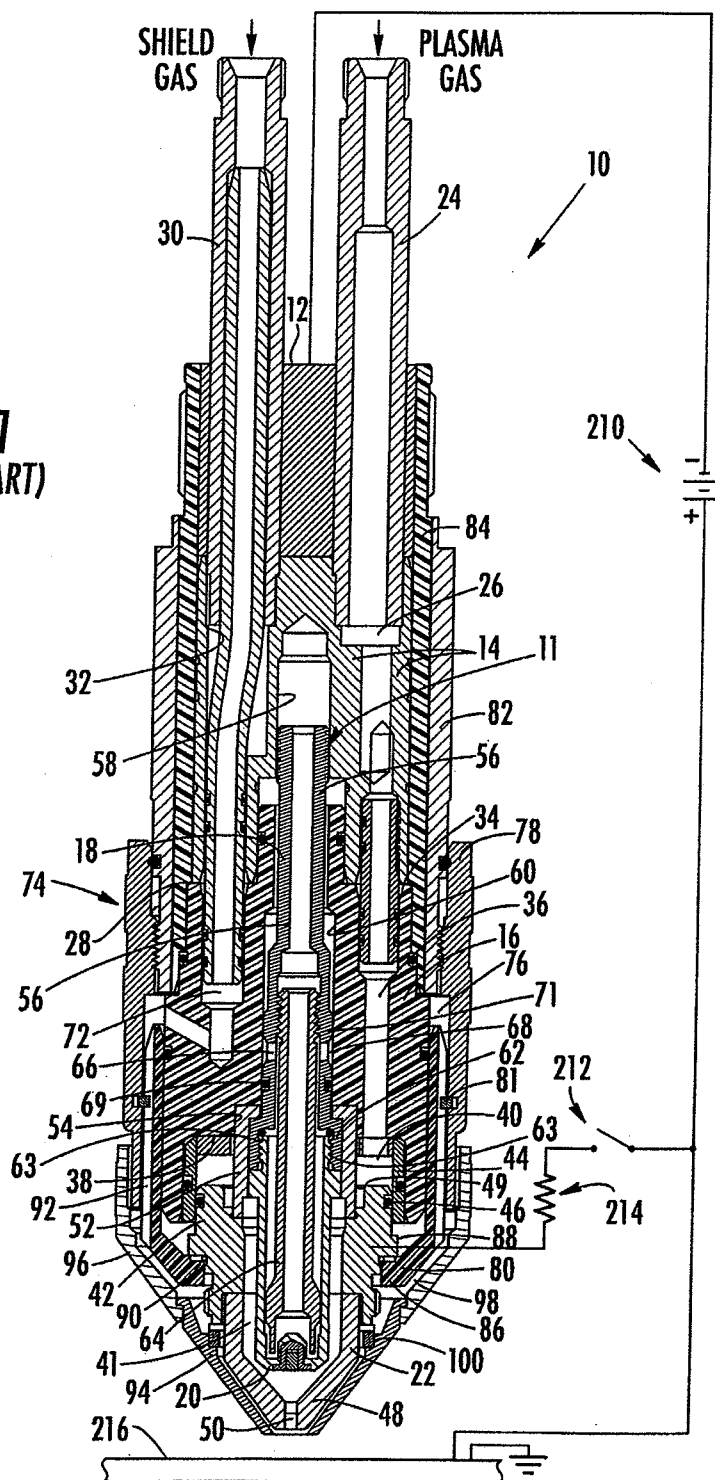
an outer coolant tube surrounding the inner coolant tube for removing coolant from the electrode via a space between the inner and outer coolant tubes;

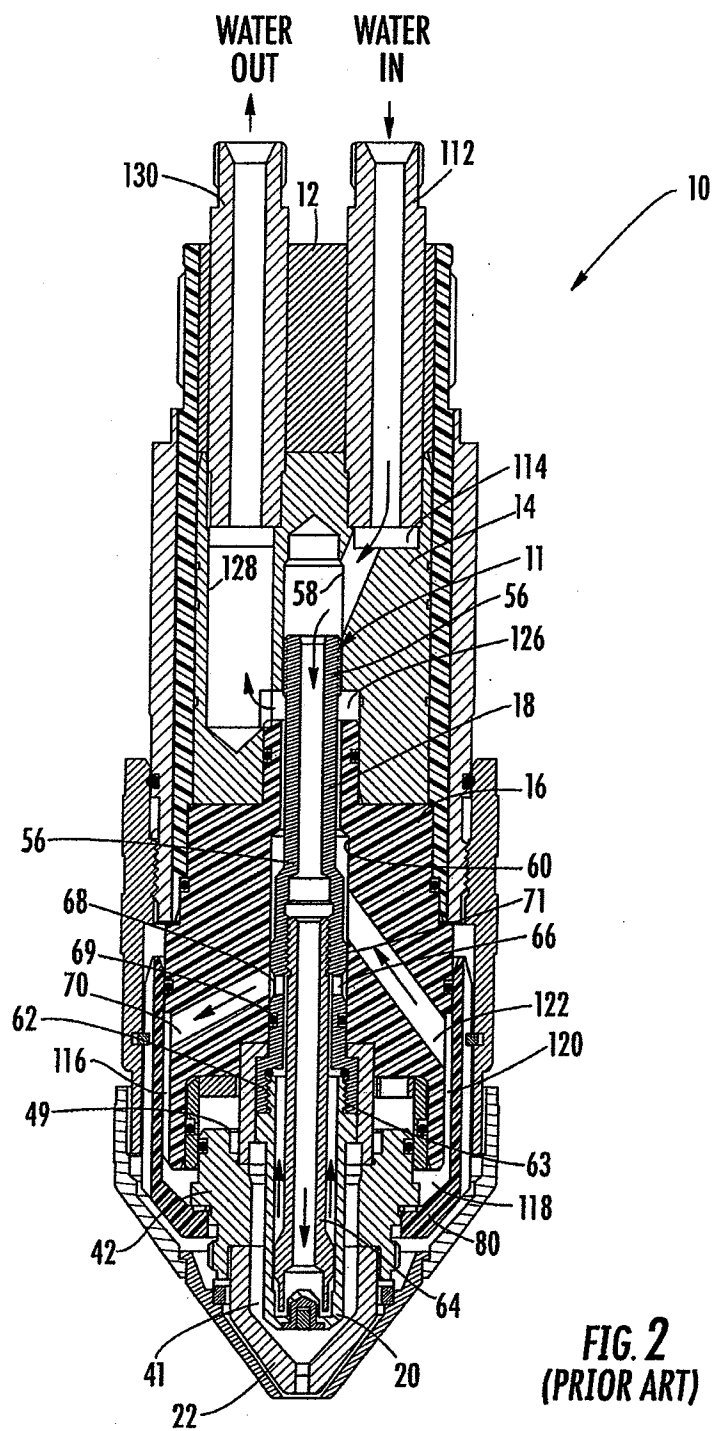
15 wherein the protrusion of the electrode is configured to connect with the inner coolant tube of the electrode holder by a releasable connection, wherein at least one coolant passage forms between the protrusion of the electrode and the inner coolant tube of the electrode holder when the electrode is connected with the electrode holder.

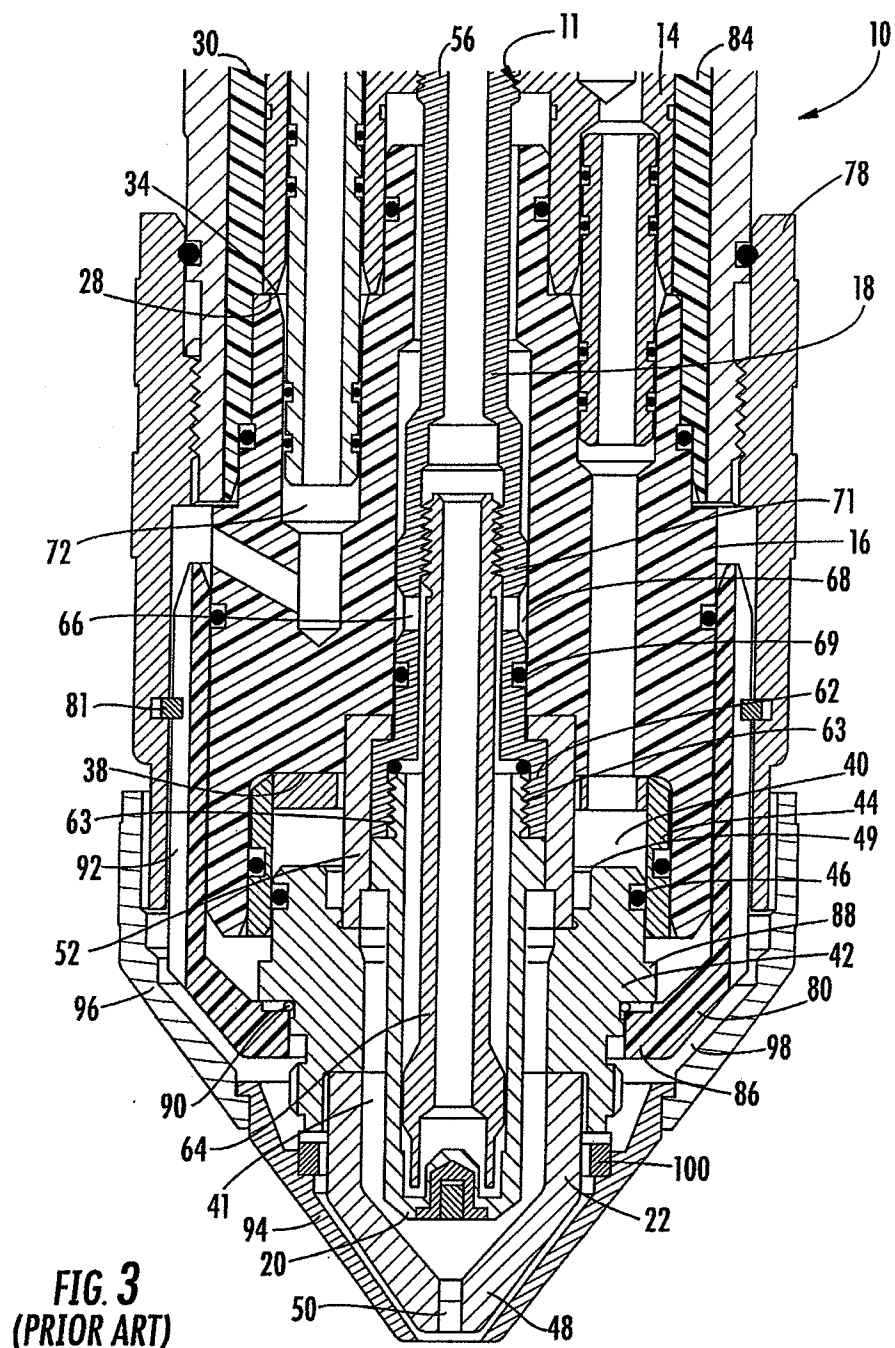
28. The electrode assembly of claim 27, wherein the releasable connection comprises
20 a threaded connection, the protrusion being threaded to releasably connect the protrusion to a threaded coolant tube of the electrode holder.

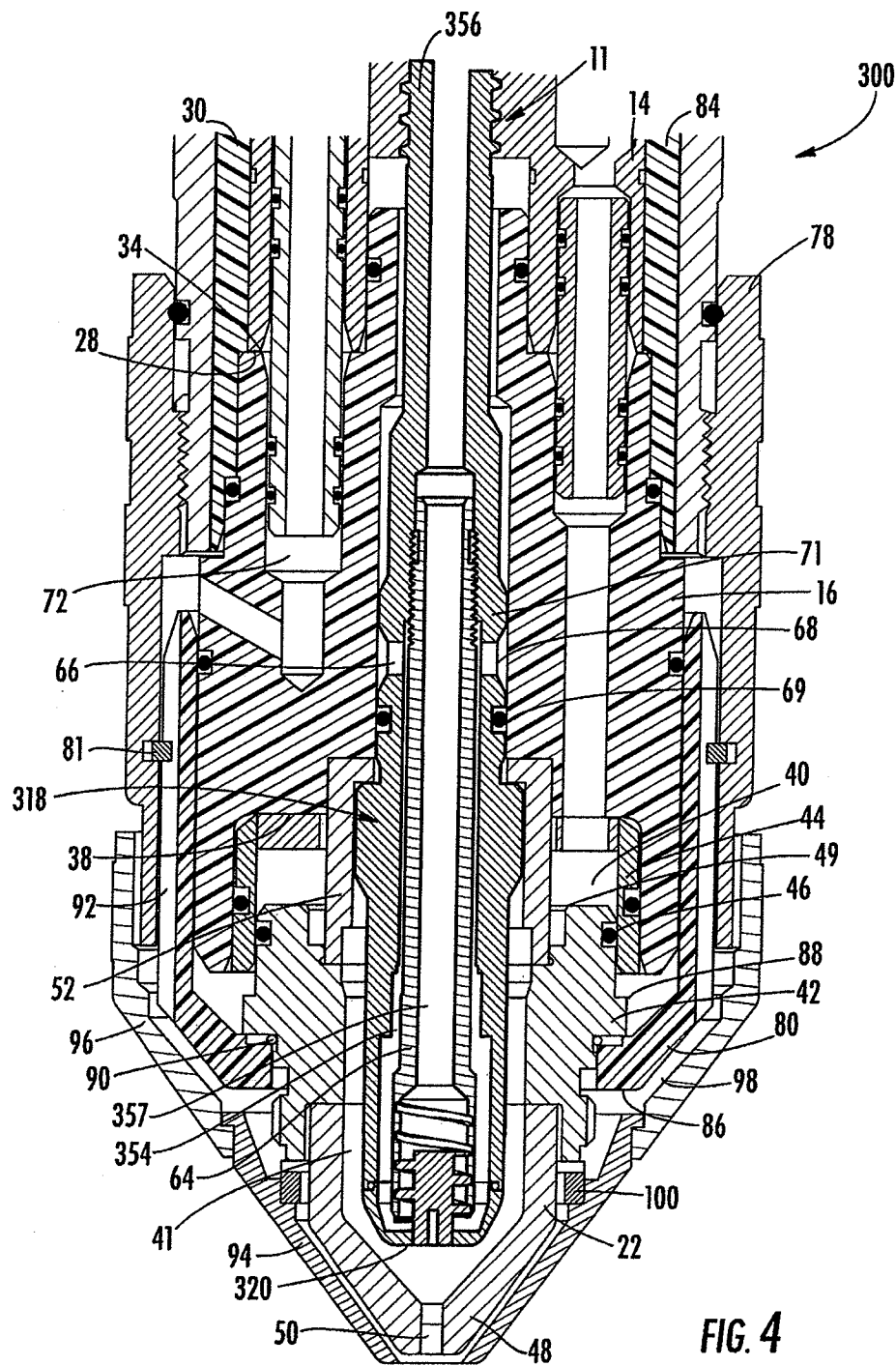
29. The electrode assembly of claim 28, wherein the at least one coolant passage is defined by the threaded connection.

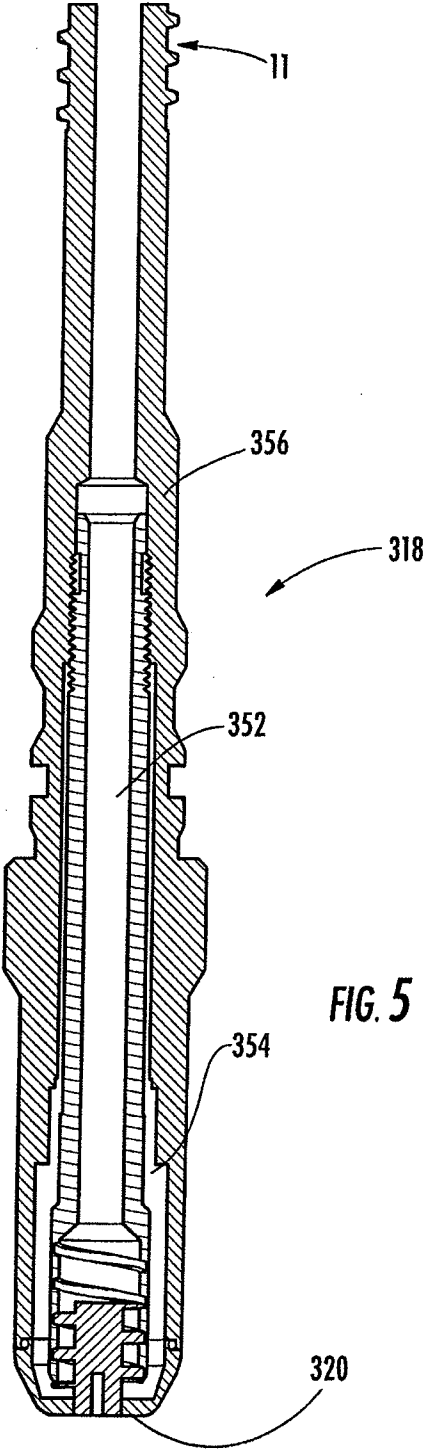
FIG. 1
(PRIOR ART)











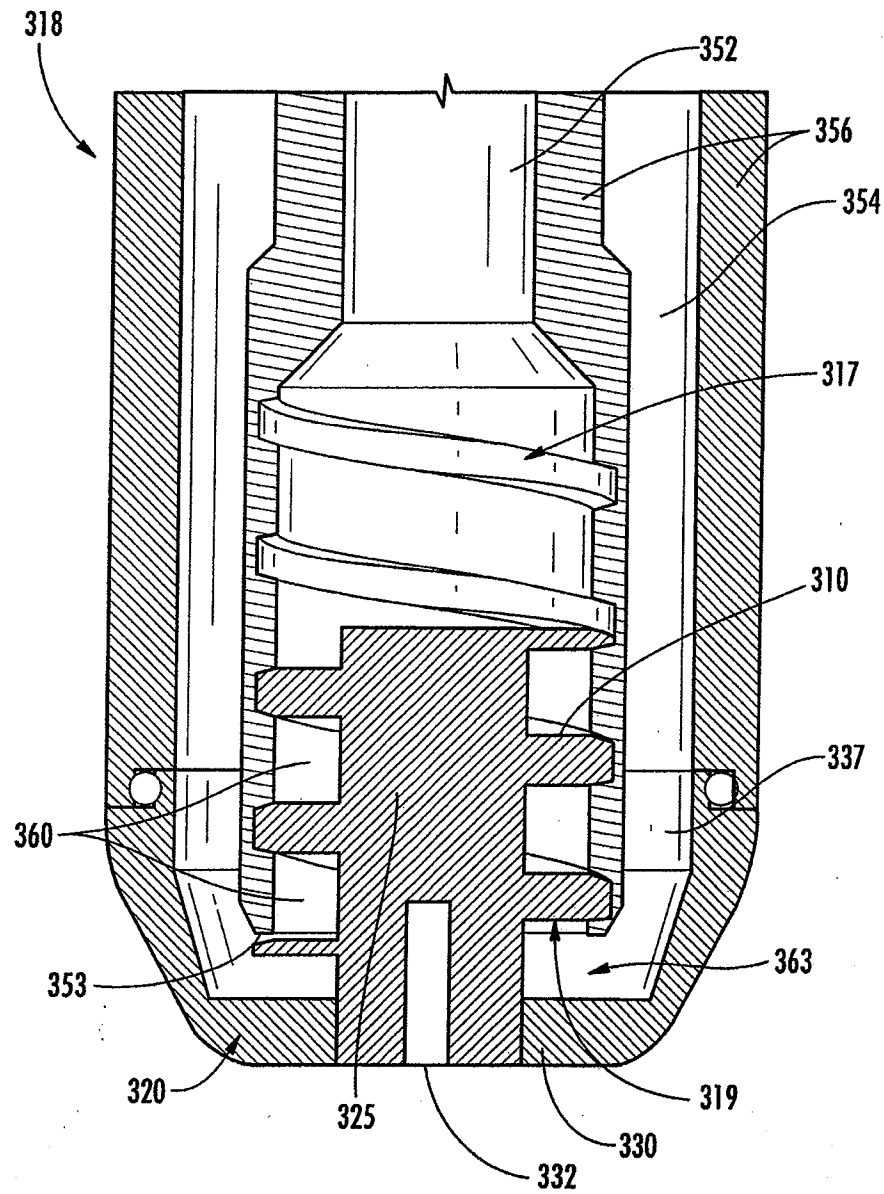
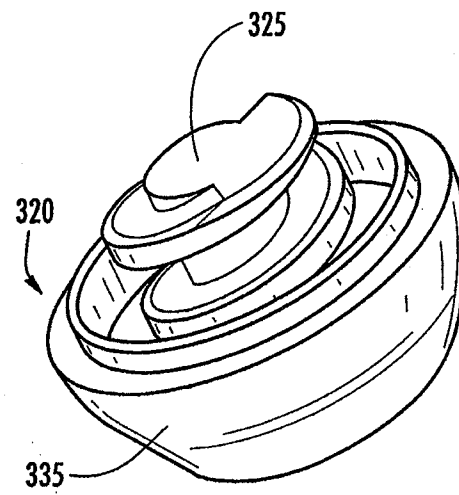
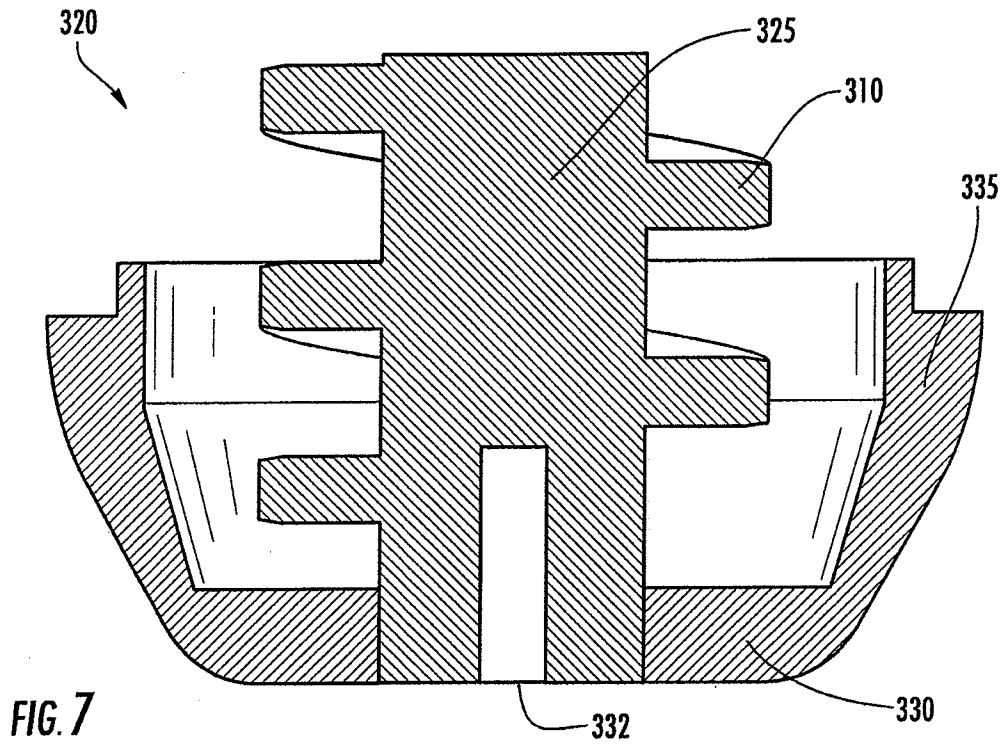


FIG. 6

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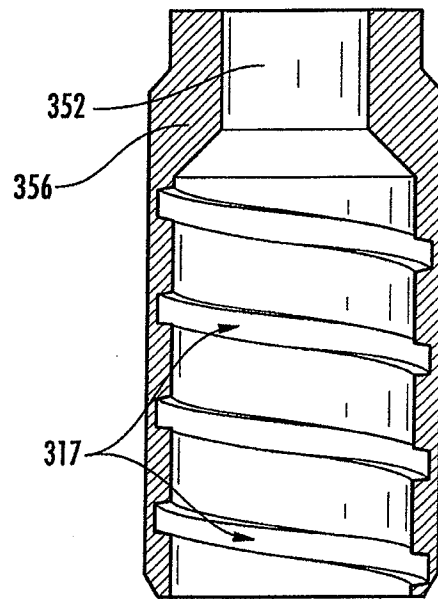


FIG. 8

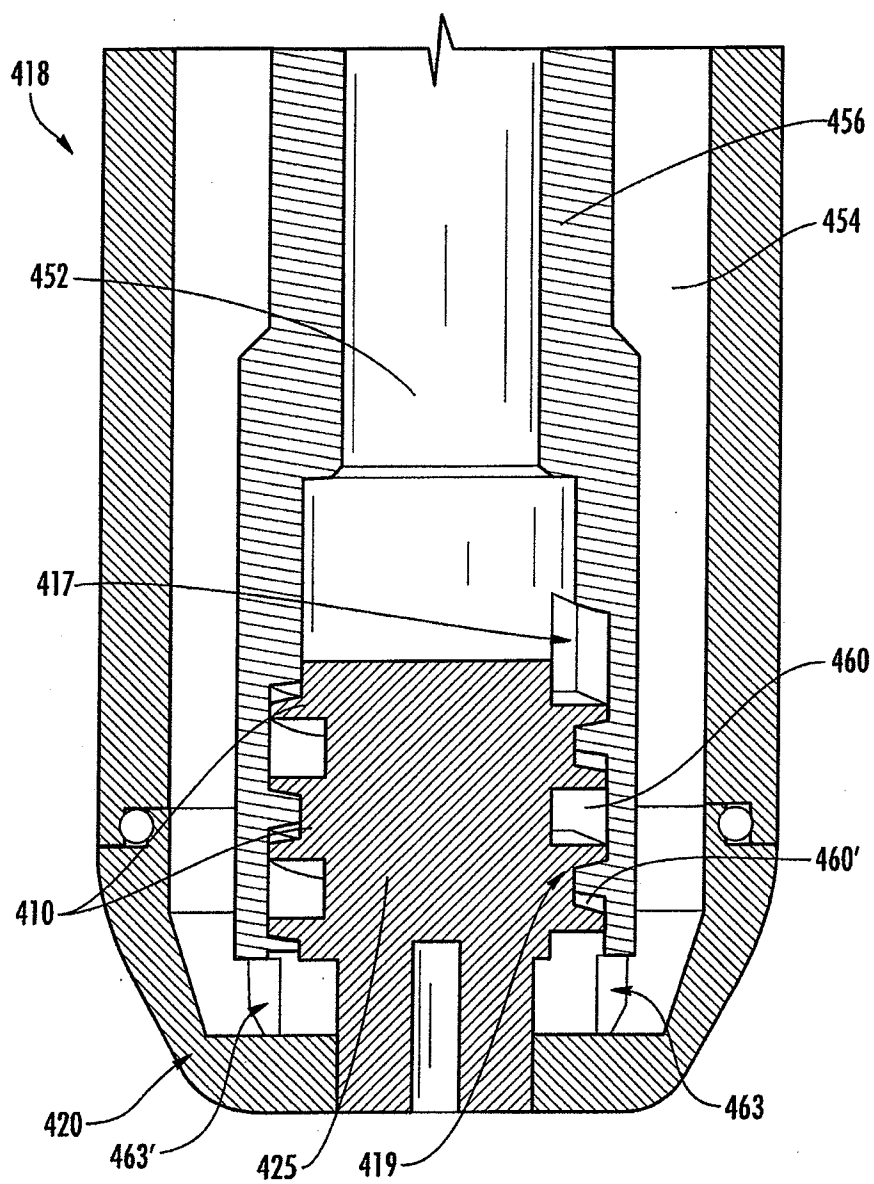
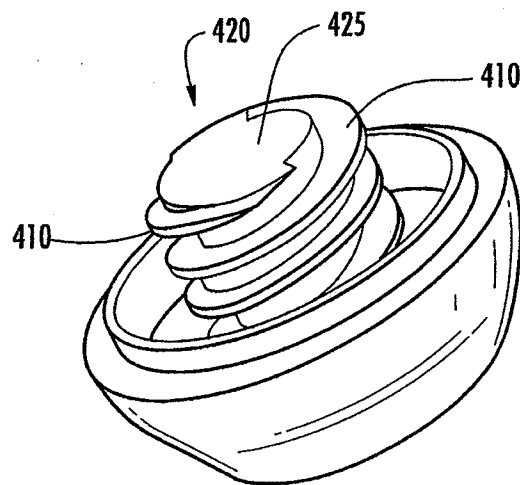
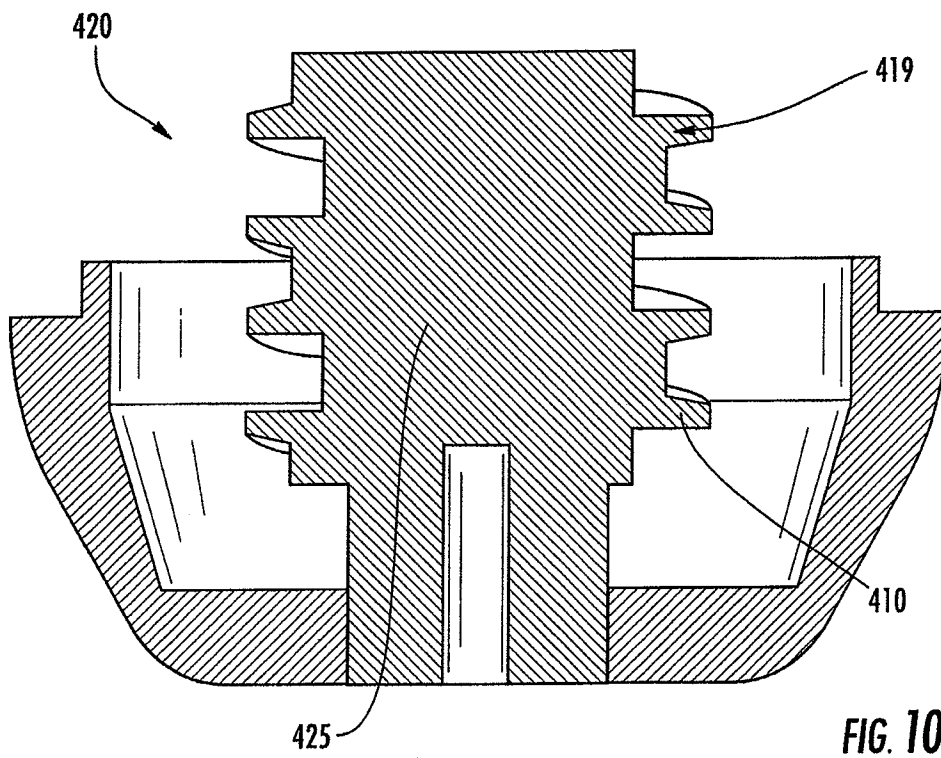


FIG. 9

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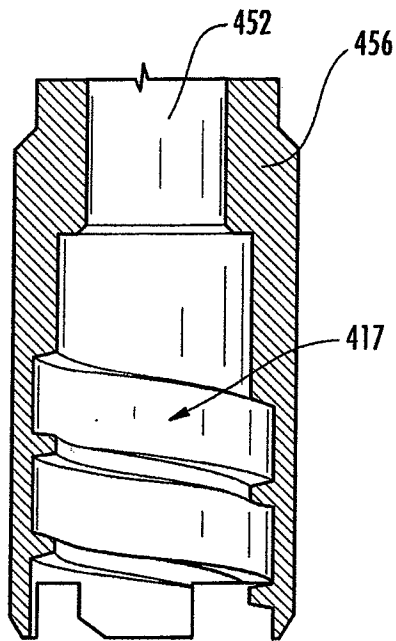


FIG. 11

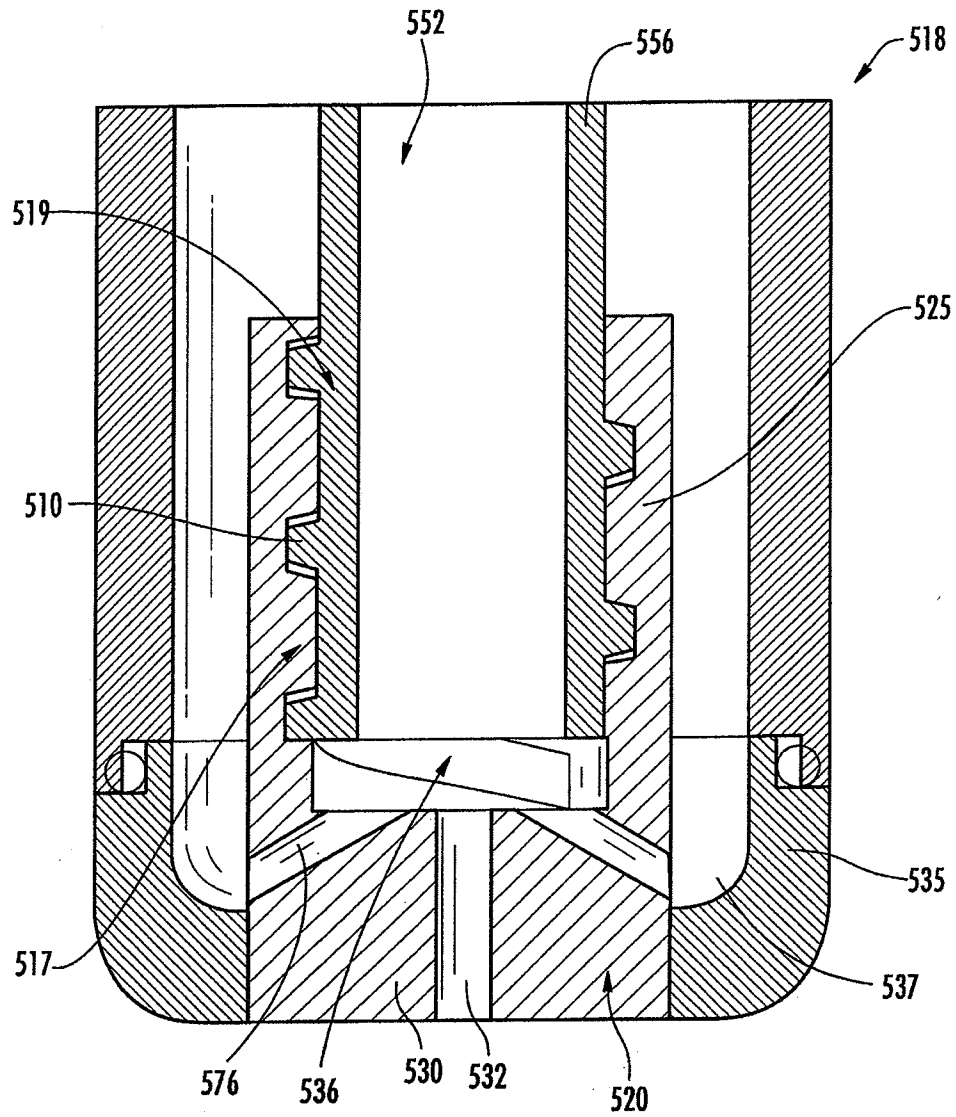


FIG. 12

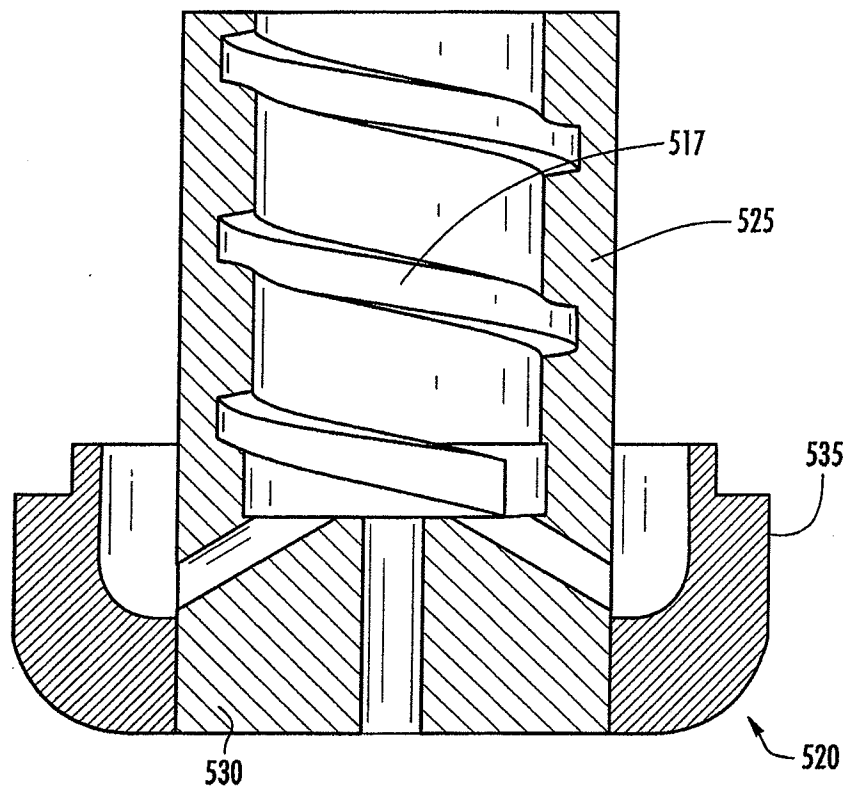


FIG. 13

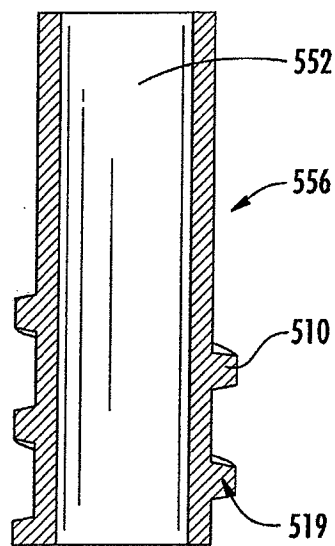
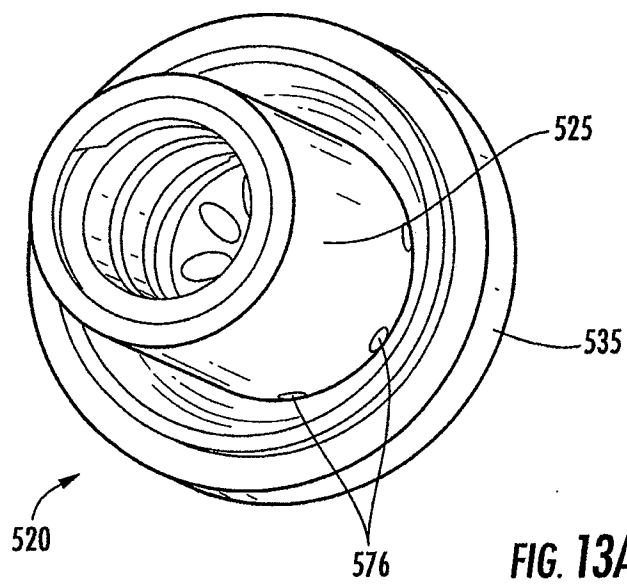


FIG. 14

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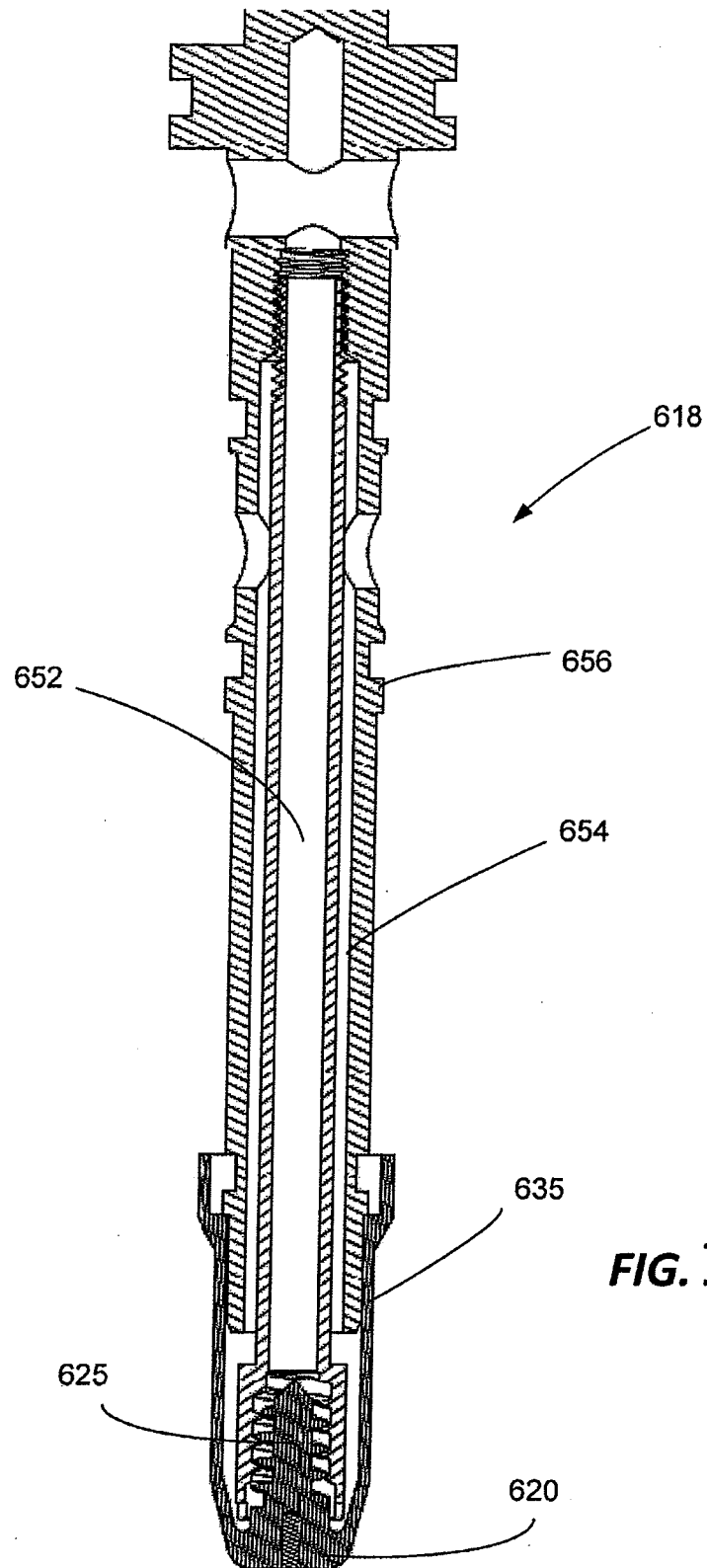


FIG. 15

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2011/050121

A. CLASSIFICATION OF SUBJECT MATTER
INV. H05H1/28 H05H1/34
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
H05H

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EP0-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 2008/116179 A1 (COOK DAVID J [US] ET AL) 22 May 2008 (2008-05-22) abstract; figures 10,11,18 -----	1-29
A	WO 2010/115397 A2 (KJELLBERG FINSTERWALDE PLASMA [DE]; LAURISCH FRANK [DE]; KRINK VOLKER) 14 October 2010 (2010-10-14) figures 5-8 -----	1-29
A	EP 0 505 285 A1 (SOUDURE AUTOGENE FRANCAISE [FR]) 23 September 1992 (1992-09-23) figure 9 -----	1-29
A	US 2006/049150 A1 (SEVERANCE WAYNE S JR [US] SEVERANCE JR WAYNE STANLEY [US]) 9 March 2006 (2006-03-09) figure 4 -----	1-29

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Further documents are listed in the continuation of Box C.

☒

See patent family annex.

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Date of the actual completion of the international search

15 December 2011

Date of mailing of the international search report

30/12/2011

Name and mailing address of the ISA/

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Authorized officer

Crescenti, Massimo

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/US2011/050121

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2008116179 A1	22-05-2008	CN 101884253 A	10-11-2010
		EP 2082622 A1	29-07-2009
		US 2008116179 A1	22-05-2008
		WO 2009070362 A1	04-06-2009

WO 2010115397 A2	14-10-2010	DE 102009016932 A1	21-10-2010
		WO 2010115397 A2	14-10-2010

EP 0505285 A1	23-09-1992	CA 2063693 A1	23-09-1992
		DE 69204331 D1	05-10-1995
		DE 69204331 T2	01-02-1996
		EP 0505285 A1	23-09-1992
		FR 2674161 A1	25-09-1992
		US 5278387 A	11-01-1994

US 2006049150 A1	09-03-2006	CA 2517639 A1	03-03-2006
		EP 1633172 A2	08-03-2006
		JP 2006173088 A	29-06-2006
		US 2006049150 A1	09-03-2006
		US 2006196854 A1	07-09-2006
		US 2008293320 A1	27-11-2008
		US 2011073574 A1	31-03-2011
