

- (21) Application No. 31319/77 (22) Filed 26 July 1977
 (31) Convention Application No. 710 023
 (32) Filed 30 July 1976 in
 (33) United States of America (US)
 (44) Complete Specification published 9 July 1980
 (51) INT CL³ B21B 1/00
 (52) Index at acceptance B3M 19C 19G D



(54) IMPROVEMENTS IN ROLLING FERROUS BILLETS

(71) We, MORGAN CONSTRUCTION COMPANY, a corporation organised and existing under the laws of the State of Massachusetts, United States of America, of 15 Belmont Street, Worcester, Massachusetts, United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—

This invention relates generally to rolling mills, and is concerned in particular with a process for rolling a ferrous billet into a finished product having improved yield strength.

In accordance with the present invention there is provided a process for forming a ferrous billet into a finished product, comprising heating the billet, hot rolling the heated billet to produce a semifinished product having a bulk temperature below that of the heated billet, cooling the surface of the semifinished product to a temperature below a finish rolling bulk temperature, and finish rolling the semifinished product at the said finish rolling bulk temperature after allowing for substantial equalisation of the temperature between the surface and the centre of the semifinished product.

In a preferred embodiment of the invention the billet is initially heated to a temperature exceeding 2,000°F, and the bulk temperature of the semifinished product, prior to the cooling of its surface, lies in the range of 1700°F to 1900°F. The finish rolling bulk temperature should then not exceed 1,600°F.

Cooling the surface of the semifinished product is preferably achieved by direct application of a fluid coolant, for example water, to the surface of the semifinished product. Preferably, the semifinished product has a round cross-section to facilitate substantially uniform application of coolant to the surface thereof. Temperature equalization between the surface and centre portions of the cooled semifinished product thereafter takes place as the semifinished product continues through guide pipes to a finish rolling station. The finish rolling

station preferably includes at least two sets of work rolls, one set preferably being offset 90° relative to the other set. Typically, the first set of work rolls at the finishing station imparts an oval cross-section to the product, with the second and final set of work rolls imparting a finished round cross-section to the product. If desired, the final set of work rolls can be adapted to deform the surface of the finished product to produce concrete reinforcing bar, where maximum yield strength is of prime importance. After the finish rolling operation, the finished product is cooled to an ambient bulk temperature. Preferably, this final cooling step is accomplished at least in part by forming the finished product into overlapping non-concentric loops on a moving conveyor, and by exposing the thus-formed loops to a gaseous coolant, typically air.

Experience to date indicates that the thermo-mechanical treatment of the semifinished product by sequential cooling equalization, and finish rolling at a maximum bulk temperature of 1600°F will increase the yield strength to tensile strength ratio, with ratios in the range of 75% being possible. Such results may be achieved without altering the major portion of the rolling operation, it being sufficient to perform only the finish rolling operation at lower rolling temperatures. Thus, overall power requirements for the mill are not increased significantly.

A preferred embodiment of the invention will now be described in greater detail with reference to the accompanying drawings, wherein:

Figure 1 is a schematic plan view of a rolling mill layout adapted to practice the process of the present invention;

Figure 2 is a graphic illustration of the temperature of the product as it progresses through the mill layout shown in Figure 1. In this view, the heavy solid lines depict bulk temperatures, the dashed line depicts surface temperature, and the dot-dash line depicts the temperature of the center portion of the product; and,

Figure 3 is an enlarged side elevational view

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of the equipment outlined by dashed lines in Figure 1.

Referring now to the drawings wherein like members designate like components throughout the several views, there is shown at 10 a furnace of the type conventionally employed in a rolling mill to reheat billets in preparation for a rolling operation. A rolling mill generally indicated at 12 and having roll stands grouped into mill sections 12a, 12b and 12c is arranged on the delivery side of the furnace 10. Mill section 12c may preferably comprise a block of closely spaced stands having alternately inclined overhung work rolls as described in U.S. Patent No. RE 28,107. Conventional guide assemblies 14 and 16 are interposed on either side of mill section 12b.

In accordance with the process of the present invention, ferrous billets are heated in furnace 10 to an elevated bulk temperature preferably above 2000°F. As herein employed, the term "bulk temperature" is intended to designate an average cross-sectional temperature of the product. The thus heated billets are then extracted from the furnace by conventional means (not shown) and introduced into the mill 12 where they are rolled continuously by mill sections 12a, 12b and 12c into a semi-finished product which emerges from mill section 12c at an intermediate bulk temperature approximately in the range of 1700°F to 1900°F. Preferably the semifinished product emerging from mill section 12c has a round cross-section.

A cooling assembly 18 including multiple separately controlled sections 18a, 18b and 18c is arranged on the delivery side of mill section 12c. The separately controlled cooling sections preferably comprise water cooling boxes which apply a fluid coolant, for example water, to the surface of the semifinished product. The round cross-section of the semifinished product facilitates a uniform application of the coolant to the surface thereof. This cooling operation produces a drastic lowering of the surface temperature of the semifinished product to a level substantially below that of a desired maximum finish rolling temperature of approximately 1600°F. Thereafter, the semifinished product enters an elongated equalization zone 20 formed by guide pipes 21 leading to a finish rolling station 22. While passing through zone 22, the temperatures of the center and surface portions of the semifinished product equalize substantially to the maximum finish rolling bulk temperature.

As is best shown in Figure 3, the finish rolling station 22 preferably comprises at least two roll stands 22a and 22b. Preferably, each roll stand 22a, 22b has overhung rolls 22a' and 22b'. Roll stand 22 imparts an oval cross-section to the product, which is finish rolled by roll stand 22b. If desired, the rolls 22b' of roll stand 22b may be adapted to deform the surface of the finished product when rolling concrete reinforcing bar.

After the finish rolling operation has been completed at station 22, the finished product is cooled to an ambient bulk temperature. Preferably, the major portion of this final cooling operation is accomplished by directing the finished product through another water cooling box 24 to a conventional inclined laying head 26 which forms the finished product into loops 28 which are deposited in an overlapping Spencerian pattern on a moving conveyor 30. While on the conveyor 30, the loops are cooled by being exposed to a flow of fluid coolant, for example ambient air.

Figure 2 is a typical graphical representation of product temperature profiles for a ferrous billet 120 × 120 MM being rolled in accordance with the present invention to a bar 6.0 MM in diameter at a finish rolling speed of 50 meters/second. The billet is initially heated in furnace 10 to an elevated bulk temperature in excess of 2000°F. Thereafter, as the billet is rolled through mill 12, its bulk temperature (represented by heavy solid line 32) initially decreases to a level of approximately 1600°F in mill section 12b before gradually rising as a result of energy being imparted through rolling to approximately 1800°F as the semifinished product exits from mill section 12c.

At this point, the semifinished product enters cooling assembly 18 where it is subjected to a surface application of cooling water. The surface temperature of the semifinished product (represented by dashed line 34) is thus lowered to approximately 1000°F, while the temperature of the center portion (dot-dash line 36) drops gradually. Thereafter, as the thus cooled semifinished product progresses through equalization zone 20, the temperatures of its surface and center portions gradually equalize to a desired maximum finish rolling bulk temperature of approximately 1600°F (represented by line 38). The semifinished product is then finish-rolled at station 22 and thereafter cooled to an ambient bulk temperature. As previously indicated, the thermomechanical treatment of the semifinished product by (a) surface cooling at zone 18; (b) temperature equalization at zone 20, and (c) low temperature finish rolling at station 22 increases yield strength to tensile strength ratio, with ratios in the range of 75% being possible.

In the light of the foregoing, it will now be appreciated by those skilled in the art that numerous modifications can be made to the procedures and apparatus described above without departing from the spirit and scope of the invention. For example, the type and arrangement of equipment making up mill 12 can be varied to suit particular rolling requirements. Likewise, the type and number of cooling sections in cooling zone 18 can be varied, as well as the type and number of roll stands at the finish rolling station 22. The level to which the surface temperature of the semi-

finished product is cooled, as well as the cooling rate, can also be varied to suit each rolling operation.

WHAT WE CLAIM IS:—

- 5 1. A process for forming a ferrous billet into a finished product, comprising heating the billet, hot rolling the heated billet to produce a semifinished product having a bulk temperature below that of the heated billet, cooling the
- 10 surface of the semifinished product to a temperature below a finish rolling bulk temperature, and finish rolling the semifinished product at said finish rolling bulk temperature after allowing for substantial equalisation of
- 15 the temperature between the surface and the centre of the semifinished product.
2. A process as claimed in Claim 1 wherein the surface of the semifinished product is cooled by the application of a fluid coolant.
- 20 3. A process as claimed in Claim 2 wherein said fluid coolant is water.
4. A process as claimed in Claim 1 wherein the semifinished product has a round cross-section.
- 25 5. A process as claimed in Claim 4 wherein said finish rolling is accomplished by passing the semifinished product through at least two

sets of work rolls, the first set of work rolls being operative to produce an oval cross-section which is rolled by the second set of work rolls into the finished product. 30

6. A process as claimed in Claim 5 wherein the finished product is concrete reinforcing rod, and wherein said second set of work rolls is adapted to deform the surface of the finished product. 35

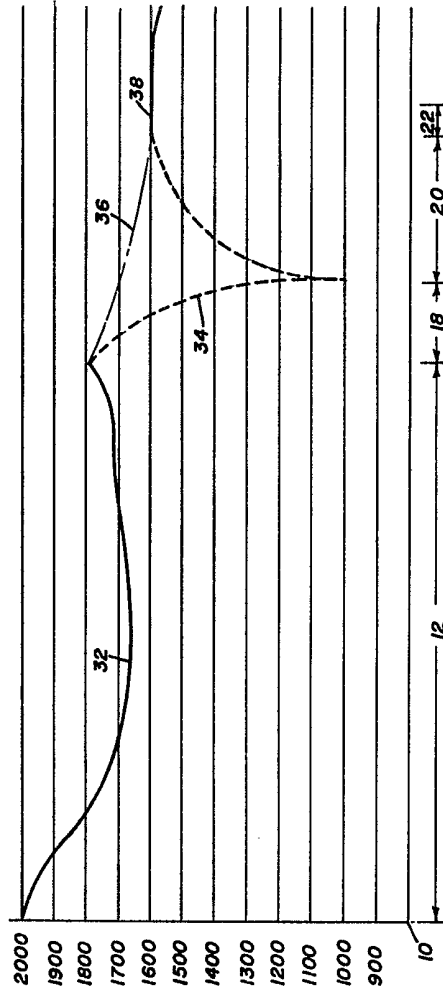
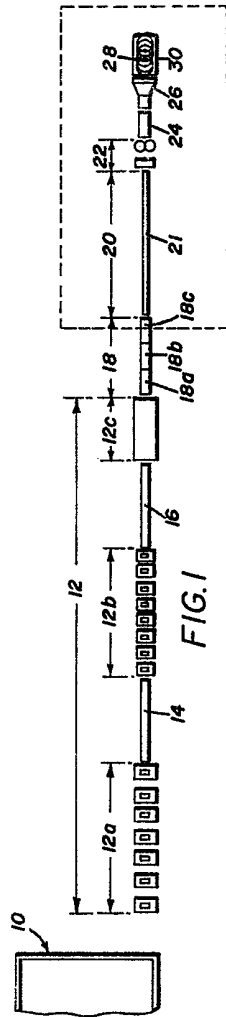
7. A process as claimed in any one of the preceding claims wherein the billet is heated initially to a bulk temperature above 2000°F.

8. The process as claimed in Claim 7 wherein the said bulk temperature of the semifinished product immediately prior to the cooling of its surface lies in the range of 1700°F to 1900°F. 40

9. A process as claimed in any one of the preceding claims wherein said finish rolling bulk temperature is a maximum of 1600°F. 45

10. A process according to Claim 1 and substantially as herein described with reference to the accompanying drawings. 50

BROOKES & MARTIN,
High Holborn House,
52—54 High Holborn,
London WC1V 6SE.
Agents for the Applicants.



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COMPLETE SPECIFICATION

2 SHEETS

*This drawing is a reproduction of
the Original on a reduced scale
Sheet 2*

