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(54) Title: FABRICATION OF THREE DIMENSIONAL OBJECTS WITH MULTIPLE OPERATING MODES

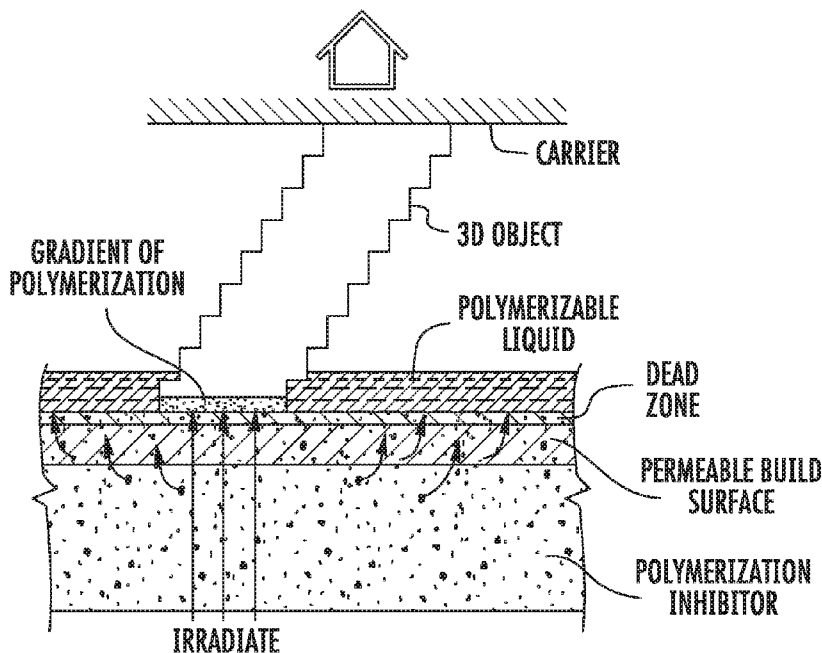


FIG. 1

(57) Abstract: A method of forming the body portion of a three-dimensional object from a polymerizable liquid by the process of continuous liquid interface printing is described. The body portion has a plurality of contiguous segments, and the process includes advancing a carrier for the object away from a build surface while irradiating a build region between the carrier and build surface in a pattern of advancing and irradiating defined by an operating mode. In the present invention, the operating mode is changed at least once during the formation of the body portion for different contiguous segments of the body portion.

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relatively shallow well or pool, a problem with such “bottom up” fabrication techniques, as commercially implemented, is that extreme care must be taken, and additional mechanical elements employed, when separating the solidified layer from the bottom plate due to physical and chemical interactions therebetween. For example, in US Patent No. 7,438,846, an elastic separation layer is used to achieve “non-destructive” separation of solidified material at the bottom construction plane. Other approaches, such as the B9Creator™ 3-dimensional printer marketed by B9Creations of Deadwood, South Dakota, USA, employ a sliding build plate. *See, e.g.*, M. Joyce, US Patent App. 2013/0292862 and Y. Chen et al., US Patent App. 2013/0295212 (both Nov. 7, 2013); *see also* Y. Pan et al., *J. Manufacturing Sci. and Eng.* **134**, 051011-1 (Oct. 2012). Such approaches introduce a mechanical step that may complicate the apparatus, slow the method, and/or potentially distort the end product.

Continuous processes for producing a three-dimensional object are suggested at some length with respect to “top down” techniques in US Patent No. 7,892,474, but this reference does not explain how they may be implemented in “bottom up” systems in a manner non-destructive to the article being produced. Accordingly, there is a need for alternate methods and apparatus for three-dimensional fabrication that can obviate the need for mechanical separation steps in “bottom-up” fabrication.

Summary of the Invention

Described herein are methods, systems and apparatus (including associated control methods, systems and apparatus), for the production of a three-dimensional object by additive manufacturing. In preferred (but not necessarily limiting) embodiments, the method is carried out continuously. In preferred (but not necessarily limiting) embodiments, the three-dimensional object is produced from a liquid interface. Hence they are sometimes referred to, for convenience and not for purposes of limitation, as “continuous liquid interphase printing” or “continuous liquid interface production” (“CLIP”) herein (the two being used interchangeably). *See, e.g.*, J. Tumbleston et al., *Continuous liquid interface production of 3D objects*, *Science* **347**, 1349-1352 (published online March 16, 2015). A schematic representation of one embodiment thereof is given in **Figure 1** herein.

The present invention provides a method of forming a three-dimensional object, comprising:

providing a carrier and an optically transparent member having a build surface, said carrier and said build surface defining a build region therebetween;

filling said build region with a polymerizable liquid,
continuously or intermittently irradiating said build region with light through said
optically transparent member to form a solid polymer from said polymerizable liquid, and
continuously or intermittently advancing (e.g., sequentially or concurrently with said
5 irradiating step) said carrier away from said build surface to form said three-dimensional
object from said solid polymer.

In some embodiments, illumination is carried out sequentially, and preferably at
higher intensity (e.g., in “strobe” mode), as described further below.

In some embodiments, fabrication is carried out in two or three sequential patterns,
10 from a base zone, through an optional transition zone, to a body zone, as described further
below.

In some embodiments, the carrier is vertically reciprocated with respect to the build
surface, to enhance or speed the refilling of the build region with the polymerizable liquid.

In some embodiments, operating mode and/or slice thickness is changed at least once
15 in the course of fabricating the three dimensional object.

In some preferred embodiments of CLIP, the filling, irradiating, and/or advancing
steps are carried out while also concurrently: (i) continuously maintaining a dead zone (or
persistent liquid interface) of polymerizable liquid in contact with said build surface, and (ii)
continuously maintaining a gradient of polymerization zone (which, as discussed below, may
20 also be described as an active surface on the bottom of the growing three dimensional object)
between said dead zone and said solid polymer and in contact with each thereof, said gradient
of polymerization zone comprising said polymerizable liquid in partially cured form. Stated
differently, in some preferred embodiments of CLIP, the three dimensional object, or at least
some contiguous portion thereof, is formed or produced in situ. “In situ” as used herein has
25 its meaning in the field of chemical engineering, and means “in place.” For example, where
both the growing portion of the three-dimensional object and the build surface (typically with
their intervening active surface or gradient of polymerization, and dead zone) are maintained
in place during formation of at least a portion of the 3D object, or sufficiently in place to
avoid the formation of fault lines or planes in the 3D object. For example, in some
30 embodiments according to the invention, different portions of the 3D object, which are
contiguous with one another in the final 3D object, can both be formed sequentially from or
within a gradient of polymerization or active surface. Furthermore, a first portion of the 3D
object can remain in the gradient of polymerization or contacting the active surface while a

second portion, that is contiguous with the first portion, is formed in the gradient of polymerization. Accordingly, the 3D object can be remotely fabricated, grown or produced continuously from the gradient of polymerization or active surface (rather than fabricated in discrete layers). The dead zone and gradient of polymerization zone/active surface may be maintained through some or all of the formation of the object being made, for example (and in some embodiments) for a time of at least 5, 10, 20, or 30 seconds, and in some embodiments for a time of at least 1 or 2 minutes.

Apparatus for carrying out the present invention generally comprises:

- (a) a support;
- 10 (b) a carrier operatively associated with said support on which carrier said three-dimensional object is formed;
- (c) an optically transparent member having a build surface, with said build surface and said carrier defining a build region therebetween;
- (d) a liquid polymer supply operatively associated with said build surface and
15 configured to supply liquid polymer into said build region for solidification or polymerization;
- (e) a radiation source configured to irradiate said build region through said optically transparent member to form a solid polymer from said polymerizable liquid;
- (f) optionally at least one drive operatively associated with either said transparent
20 member or said carrier;
- (g) a controller operatively associated with said carrier, and/or optionally said at least one drive, and said radiation source for advancing said carrier away from said build surface to form said three-dimensional object from said solid polymer,
with the controller preferably further configured to oscillate or reciprocate said carrier
25 with respect to said build surface to enhance or speed the refilling of said build region with said polymerizable liquid.

In the B9Creator™ 3-dimensional printer, a polydimethylsiloxane (PDMS) coating is applied to the sliding build surface. The PDMS coating is said to absorb oxygen and create a thin lubricating film of unpolymerized resin through its action as a polymerization inhibitor.
30 However, the PDMS coated build surface is directly replenished with oxygen by mechanically moving (sliding) the surface from beneath the growing object, while wiping unpolymerized resin therefrom with a wiper blade, and then returning it to its previous position beneath the growing object. While in some embodiments auxiliary means of

providing an inhibitor such as oxygen are provided (*e.g.*, a compressor to associated channels), the process still employs a layer-by-layer approach with sliding and wiping of the surface. Since the PDMS coating may be swollen by the resin, this swelling, along with these mechanical steps, may result in tearing of or damage to the PDMS coating.

5 In some embodiments, the polymerizable liquid comprises a mixture of *(i)* a light polymerizable liquid first component, and *(ii)* a second solidifiable component that is different from the first component. In this case, the method may further include, concurrently with or following the forming of the three dimensional object, solidifying and/or curing the second solidifiable component in the three-dimensional object (*e.g.*, by removing the three-
10 dimensional object as an “intermediate” object from the carrier, and heating and/or microwave irradiating the object).

In some embodiments, the second component comprises a polymerizable liquid solubilized in or suspended in the first component.

In some embodiments, the second component comprises: *(i)* a polymerizable solid
15 suspended in the first component; *(ii)* a polymerizable solid solubilized in the first component; or *(iii)* a polymer solubilized in the first component.

In some embodiments, the three-dimensional intermediate is collapsible or compressible.

In some embodiments, the three-dimensional object, following the further solidifying
20 and/or curing, comprises a polymer blend, interpenetrating polymer network, semi-interpenetrating polymer network, or sequential interpenetrating polymer network formed from the first component and the second component.

In some embodiments, the polymerizable liquid comprises: from 1 or 10 percent by
25 weight to 40, 90 or 99 percent by weight of the first component; and from 1, 10 or 60 percent by weight to 90 or 99 percent by weight of the second component.

In some embodiments, the further solidifying and/or curing step *(d)* is carried out
30 concurrently with the irradiating step *(c)* and: *(i)* the solidifying and/or curing step is carried out by precipitation; or *(ii)* the irradiating step generates heat from the polymerization of the first component in an amount sufficient to thermally solidify or polymerize the second component.

In some embodiments, the further solidifying and/or curing step is carried out
subsequent to the irradiating step *(c)* and is carried out by: *(i)* heating the second solidifiable component; *(ii)* irradiating the second solidifiable component with light at a wavelength

different from that of the light in the irradiating step (c); (iii) contacting the second polymerizable component to water; and/or (iv) contacting the second polymerizable component to a catalyst.

5 In some embodiments, the second component comprises the precursors to a polyurethane, polyurea, or copolymer thereof, a silicone resin, an epoxy resin, a cyanate ester resin, or a natural rubber; and the solidifying step is carried out by heating and/or microwave irradiating.

10 In some embodiments, the second component comprises the precursors to a polyurethane, polyurea, or copolymer thereof, and the solidifying and/or curing step is carried out by contacting the second component to water.

In some embodiments, the further solidifying and/or curing step is carried out subsequent to the irradiating step; and the solidifying and/or curing step is carried out under conditions in which the solid polymer scaffold degrades and forms a constituent necessary for the polymerization of the second component.

15 In some embodiments, the second component comprises precursors to a polyurethane, polyurea, or copolymer thereof, a silicone resin, a ring-opening metathesis polymerization resin, or a click chemistry resin, a cyanate ester resin, and the solidifying and/or curing step is carried out by contacting the second component to a polymerization catalyst.

20 In some embodiments, the polymerizable liquid comprises a first component (Part A) and at least one additional component (Part B), the first component comprising monomers and/or prepolymers that can be polymerized by exposure to actinic radiation or light; the second component solidifiable on contacting to heat, water, water vapor, light at a different wavelength than that at which the first component is polymerized, catalysts, evaporation of a solvent from the polymerizable liquid, exposure to microwave irradiation, and combinations thereof.

25 In some embodiments employing two-component polymerizable liquids, the three-dimensional object comprises an interpenetrating polymer network (IPN), the interpenetrating polymer network comprising a sol-gel composition, a hydrophobic-hydrophilic IPN, a phenolic resin, a polyimide, a conductive polymer, a natural product-based IPN, a sequential IPN, a polyolefin, or a combination thereof.

30 Non-limiting examples and specific embodiments of the present invention are explained in greater detail in the drawings herein and the specification set forth below. The

disclosure of all United States Patent references cited herein are to be incorporated herein by reference in their entirety.

Brief Description of the Drawings

5 **Figure 1** is a schematic illustration of one embodiment of a method of the present invention.

Figure 2 is a perspective view of one embodiment of an apparatus of the present invention.

10 **Figure 3** is a first flow chart illustrating control systems and methods for carrying out the present invention.

Figure 4 is a second flow chart illustrating control systems and methods for carrying out the present invention.

Figure 5 is a third flow chart illustrating control systems and methods for carrying out the present invention.

15 **Figure 6** is a graphic illustration of a process of the invention indicating the position of the carrier in relation to the build surface or plate, where both advancing of the carrier and irradiation of the build region is carried out continuously. Advancing of the carrier is illustrated on the vertical axis, and time is illustrated on the horizontal axis.

20 **Figure 7** is a graphic illustration of another process of the invention indicating the position of the carrier in relation to the build surface or plate, where both advancing of the carrier and irradiation of the build region is carried out stepwise, yet the dead zone and gradient of polymerization are maintained. Advancing of the carrier is again illustrated on the vertical axis, and time is illustrated on the horizontal axis.

25 **Figure 8** is a graphic illustration of still another process of the invention indicating the position of the carrier in relation to the build surface or plate, where both advancing of the carrier and irradiation of the build region is carried out stepwise, the dead zone and gradient of polymerization are maintained, and a reciprocating step is introduced between irradiation steps to enhance the flow of polymerizable liquid into the build region. Advancing of the carrier is again illustrated on the vertical axis, and time is illustrated on the horizontal axis.

30 **Figure 9** is a detailed illustration of a reciprocation step of Figure 8, showing a period of acceleration occurring during the upstroke (*i.e.*, a gradual start of the upstroke) and a period of deceleration occurring during the downstroke (*i.e.*, a gradual end to the downstroke).

Figure 10 schematically illustrates the movement of the carrier (z) over time (t) in the course of fabricating a three-dimensional object by processes of the present invention through a first base (or “adhesion”) zone, a second transition zone, and a third body zone.

Figure 11A schematically illustrates the movement of the carrier (z) over time (t) in the course of fabricating a three-dimensional object by continuous advancing and continuous exposure.

Figure 11B illustrates the fabrication of a three-dimensional object in a manner similar to Figure 11A, except that illumination is now in an intermittent (or “strobe”) pattern.

Figure 12A schematically illustrates the movement of the carrier (z) over time (t) in the course of fabricating a three-dimensional object by intermittent (or “stepped”) advancing and intermittent exposure.

Figure 12B illustrates the fabrication of a three-dimensional object in a manner similar to Figure 12A, except that illumination is now in a shortened intermittent (or “strobe”) pattern.

Figure 13A schematically illustrates the movement of the carrier (z) over time (t) in the course of fabricating a three-dimensional object by oscillatory advancing and intermittent exposure.

Figure 13B illustrates the fabrication of a three-dimensional object in a manner similar to Figure 13A, except that illumination is now in a shortened intermittent (or “strobe”) pattern.

Figure 14A schematically illustrates one segment of a “strobe” pattern of fabrication, where the duration of the static portion of the carrier has been shortened to near the duration of the “strobe” exposure

Figure 14B is a schematic illustration of a segment of a strobe pattern of fabrication similar to Figure 14A, except that the carrier is now moving slowly upward during the period of strobe illumination.

Figure 15A is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 13A, except that the body segment is fabricated in two contiguous segments, with the first segment carried out in an oscillatory operating mode, and the second segment carried out in a continuous operating mode.

Figure 15B is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 15A, except that oscillatory operating modes are replaced with stepped operating modes.

Figure 16A is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 11A, except that the body segment is fabricated in three contiguous segments, with the first and third segments carried out in a continuous operating mode, and the second segment carried out in oscillatory operating mode.

5 **Figure 16B** is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 16A, except that the oscillatory operating mode is replaced with a stepped operating mode.

Figure 17A is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 16A, except that the base zone, transition zone, and first segment of the
10 body zone are carried out in a strobe continuous operating mode, the second segment of the body zone is fabricated in an oscillatory operating mode, and the third segment of the body zone is fabricated in a continuous operating mode.

Figure 17B is similar to Figure 17A, except that the second segment of the body zone is fabricated in a stepped operating mode.

15 **Figure 18A** is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 11A, except that light intensity is varied in the course of fabricating the base and transition zones, and both light intensity and rate of advancing are varied in the course of fabricating the body zone.

Figure 18B is a schematic illustration of the fabrication of a three-dimensional object
20 similar to Figure 17A, except that light is interrupted in an intermittent fashion (dashed line representing light intensity during interrupted segments is for comparison to Figure 17A only).

Figure 19 is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 11A, except that the mode of operation during fabrication of the body
25 segment is changed multiple times for continuous, to reciprocal, and back.

Figure 20 schematically illustrates parameters that may be varied within a reciprocal or step-wise operating mode.

Figure 21A schematically illustrates a method of the invention carried out in a continuous operating mode, with constant slice thickness and constant carrier speed.

30 **Figure 21B** schematically illustrates a method of the invention carried out in a continuous operating mode, with variable slice thickness with constant carrier speed.

Figure 21C schematically illustrates a method of the invention carried out in a continuous operating mode, with constant slice thickness and variable carrier speed.

Figure 21D schematically illustrates a method of the invention carried out in continuous operating mode, mode with variable slice thickness and variable carrier speed.

Figure 21E schematically illustrates a method of the invention carried out in reciprocal operating mode, with constant slice thickness.

5 **Figure 21F** schematically illustrates a method of the invention carried out in reciprocal operating mode, with variable slice thickness.

Detailed Description of Illustrative Embodiments

10 The present invention is now described more fully hereinafter with reference to the accompanying drawings, in which embodiments of the invention are shown. This invention may, however, be embodied in many different forms and should not be construed as limited to the embodiments set forth herein; rather these embodiments are provided so that this disclosure will be thorough and complete and will fully convey the scope of the invention to those skilled in the art.

15 Like numbers refer to like elements throughout. In the figures, the thickness of certain lines, layers, components, elements or features may be exaggerated for clarity. Where used, broken lines illustrate optional features or operations unless specified otherwise.

20 The terminology used herein is for the purpose of describing particular embodiments only and is not intended to be limiting of the invention. As used herein, the singular forms "a," "an" and "the" are intended to include plural forms as well, unless the context clearly indicates otherwise. It will be further understood that the terms "comprises" or "comprising," when used in this specification, specify the presence of stated features, integers, steps, operations, elements components and/or groups or combinations thereof, but do not preclude the presence or addition of one or more other features, integers, steps, operations, elements,
25 components and/or groups or combinations thereof.

As used herein, the term "and/or" includes any and all possible combinations or one or more of the associated listed items, as well as the lack of combinations when interpreted in the alternative ("or").

30 Unless otherwise defined, all terms (including technical and scientific terms) used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this invention belongs. It will be further understood that terms, such as those defined in commonly used dictionaries, should be interpreted as having a meaning that is consistent with their meaning in the context of the specification and claims and should not be

interpreted in an idealized or overly formal sense unless expressly so defined herein. Well-known functions or constructions may not be described in detail for brevity and/or clarity.

It will be understood that when an element is referred to as being “on,” “attached” to, “connected” to, “coupled” with, “contacting,” etc., another element, it can be directly on, attached to, connected to, coupled with and/or contacting the other element or intervening elements can also be present. In contrast, when an element is referred to as being, for example, “directly on,” “directly attached” to, “directly connected” to, “directly coupled” with or “directly contacting” another element, there are no intervening elements present. It will also be appreciated by those of skill in the art that references to a structure or feature that is disposed “adjacent” another feature can have portions that overlap or underlie the adjacent feature.

Spatially relative terms, such as “under,” “below,” “lower,” “over,” “upper” and the like, may be used herein for ease of description to describe an element’s or feature’s relationship to another element(s) or feature(s) as illustrated in the figures. It will be understood that the spatially relative terms are intended to encompass different orientations of the device in use or operation in addition to the orientation depicted in the figures. For example, if the device in the figures is inverted, elements described as “under” or “beneath” other elements or features would then be oriented “over” the other elements or features. Thus the exemplary term “under” can encompass both an orientation of over and under. The device may otherwise be oriented (rotated 90 degrees or at other orientations) and the spatially relative descriptors used herein interpreted accordingly. Similarly, the terms “upwardly,” “downwardly,” “vertical,” “horizontal” and the like are used herein for the purpose of explanation only, unless specifically indicated otherwise.

It will be understood that, although the terms first, second, etc., may be used herein to describe various elements, components, regions, layers and/or sections, these elements, components, regions, layers and/or sections should not be limited by these terms. Rather, these terms are only used to distinguish one element, component, region, layer and/or section, from another element, component, region, layer and/or section. Thus, a first element, component, region, layer or section discussed herein could be termed a second element, component, region, layer or section without departing from the teachings of the present invention. The sequence of operations (or steps) is not limited to the order presented in the claims or figures unless specifically indicated otherwise.

1. Polymerizable liquids/part A components.

Any suitable polymerizable liquid can be used to enable the present invention. In some embodiments, the polymerizable liquid comprises, in addition to a first component (or “part A”) such as described in this section, a second component (or “part B”) such as described in the “Dual Hardening” section below. The liquid (sometimes also referred to as “liquid resin” “ink,” or simply “resin” herein) can include a monomer, particularly photopolymerizable and/or free radical polymerizable monomers, and a suitable initiator such as a free radical initiator, and combinations thereof. Examples include, but are not limited to, acrylics, methacrylics, acrylamides, styrenics, olefins, halogenated olefins, cyclic alkenes, maleic anhydride, alkenes, alkynes, carbon monoxide, functionalized oligomers, multifunctional cure site monomers, functionalized PEGs, etc., including combinations thereof. Examples of liquid resins, monomers and initiators include but are not limited to those set forth in US Patents Nos. 8,232,043; 8,119,214; 7,935,476; 7,767,728; 7,649,029; WO 2012129968 A1; CN 102715751 A; JP 2012210408 A.

Acid catalyzed polymerizable liquids. While in some embodiments as noted above the polymerizable liquid comprises a free radical polymerizable liquid (in which case an inhibitor may be oxygen as described below), in other embodiments the polymerizable liquid comprises an acid catalyzed, or cationically polymerized, polymerizable liquid. In such embodiments the polymerizable liquid comprises monomers contain groups suitable for acid catalysis, such as epoxide groups, vinyl ether groups, etc. Thus suitable monomers include olefins such as methoxyethene, 4-methoxystyrene, styrene, 2-methylprop-1-ene, 1,3-butadiene, etc.; heterocyclic monomers (including lactones, lactams, and cyclic amines) such as oxirane, thietane, tetrahydrofuran, oxazoline, 1,3, dioxepane, oxetan-2-one, etc., and combinations thereof. A suitable (generally ionic or non-ionic) photoacid generator (PAG) is included in the acid catalyzed polymerizable liquid, examples of which include, but are not limited to onium salts, sulfonium and iodonium salts, etc., such as diphenyl iodide hexafluorophosphate, diphenyl iodide hexafluoroarsenate, diphenyl iodide hexafluoroantimonate, diphenyl p-methoxyphenyl triflate, diphenyl p-toluenyl triflate, diphenyl p-isobutylphenyl triflate, diphenyl p-tert-butylphenyl triflate, triphenylsulfonium hexafluorophosphate, triphenylsulfonium hexafluoroarsenate, triphenylsulfonium hexafluoroantimonate, triphenylsulfonium triflate, dibutylnaphthylsulfonium triflate, etc., including mixtures thereof. See, e.g., US Patents Nos. 7,824,839; 7,550,246; 7,534,844;

6,692,891; 5,374,500; and 5,017,461; see also *Photoacid Generator Selection Guide for the electronics industry and energy curable coatings* (BASF 2010).

Hydrogels. In some embodiments suitable resins includes photocurable hydrogels like poly(ethylene glycols) (PEG) and gelatins. PEG hydrogels have been used to deliver a variety of biologicals, including Growth factors; however, a great challenge facing PEG hydrogels crosslinked by chain growth polymerizations is the potential for irreversible protein damage. Conditions to maximize release of the biologicals from photopolymerized PEG diacrylate hydrogels can be enhanced by inclusion of affinity binding peptide sequences in the monomer resin solutions, prior to photopolymerization allowing sustained delivery. Gelatin is a biopolymer frequently used in food, cosmetic, pharmaceutical and photographic industries. It is obtained by thermal denaturation or chemical and physical degradation of collagen. There are three kinds of gelatin, including those found in animals, fish and humans. Gelatin from the skin of cold water fish is considered safe to use in pharmaceutical applications. UV or visible light can be used to crosslink appropriately modified gelatin. Methods for crosslinking gelatin include cure derivatives from dyes such as Rose Bengal.

Photocurable silicone resins. A suitable resin includes photocurable silicones. UV cure silicone rubber, such as Silopren™ UV Cure Silicone Rubber can be used as can LOCTITE™ Cure Silicone adhesives sealants. Applications include optical instruments, medical and surgical equipment, exterior lighting and enclosures, electrical connectors / sensors, fiber optics and gaskets.

Biodegradable resins. Biodegradable resins are particularly important for implantable devices to deliver drugs or for temporary performance applications, like biodegradable screws and stents (US patents 7,919,162; 6,932,930). Biodegradable copolymers of lactic acid and glycolic acid (PLGA) can be dissolved in PEG dimethacrylate to yield a transparent resin suitable for use. Polycaprolactone and PLGA oligomers can be functionalized with acrylic or methacrylic groups to allow them to be effective resins for use.

Photocurable polyurethanes. A particularly useful resin is photocurable polyurethanes. A photopolymerizable polyurethane composition comprising (1) a polyurethane based on an aliphatic diisocyanate, poly(hexamethylene isophthalate glycol) and, optionally, 1,4-butanediol; (2) a polyfunctional acrylic ester; (3) a photoinitiator; and (4) an anti-oxidant, can be formulated so that it provides a hard, abrasion-resistant, and stain-resistant material (US Patent 4,337,130). Photocurable thermoplastic polyurethane elastomers incorporate photoreactive diacetylene diols as chain extenders.

High performance resins. In some embodiments, high performance resins are used. Such high performance resins may sometimes require the use of heating to melt and/or reduce the viscosity thereof, as noted above and discussed further below. Examples of such resins include, but are not limited to, resins for those materials sometimes referred to as liquid crystalline polymers of esters, ester-imide, and ester-amide oligomers, as described in US Patents Nos. 7,507,784; 6,939,940. Since such resins are sometimes employed as high-temperature thermoset resins, in the present invention they further comprise a suitable photoinitiator such as benzophenone, anthraquinone, and fluorenone initiators (including derivatives thereof), to initiate cross-linking on irradiation, as discussed further below.

Additional example resins. Particularly useful resins for dental applications include EnvisionTEC's Clear Guide, EnvisionTEC's E-Denstone Material. Particularly useful resins for hearing aid industries include EnvisionTEC's e-Shell 300 Series of resins. Particularly useful resins include EnvisionTEC's HTM140IV High Temperature Mold Material for use directly with vulcanized rubber in molding / casting applications. A particularly useful material for making tough and stiff parts includes EnvisionTEC's RC31 resin. A particularly useful resin for investment casting applications includes EnvisionTEC's Easy Cast EC500.

Additional resin ingredients. The liquid resin or polymerizable material can have solid particles suspended or dispersed therein. Any suitable solid particle can be used, depending upon the end product being fabricated. The particles can be metallic, organic/polymeric, inorganic, or composites or mixtures thereof. The particles can be nonconductive, semi-conductive, or conductive (including metallic and non-metallic or polymer conductors); and the particles can be magnetic, ferromagnetic, paramagnetic, or nonmagnetic. The particles can be of any suitable shape, including spherical, elliptical, cylindrical, etc. The particles can comprise an active agent or detectable compound as described below, though these may also be provided dissolved solubilized in the liquid resin as also discussed below. For example, magnetic or paramagnetic particles or nanoparticles can be employed. The resin or polymerizable material may contain a dispersing agent, such as an ionic surfactant, a non-ionic surfactant, a block copolymer, or the like.

The liquid resin can have additional ingredients solubilized therein, including pigments, dyes, active compounds or pharmaceutical compounds, detectable compounds (e.g., fluorescent, phosphorescent, radioactive), etc., again depending upon the particular purpose of the product being fabricated. Examples of such additional ingredients include, but are not limited to, proteins, peptides, nucleic acids (DNA, RNA) such as siRNA, sugars,

small organic compounds (drugs and drug-like compounds), etc., including combinations thereof.

Inhibitors of polymerization. Inhibitors or polymerization inhibitors for use in the present invention may be in the form of a liquid or a gas. In some embodiments, gas inhibitors are preferred. The specific inhibitor will depend upon the monomer being polymerized and the polymerization reaction. For free radical polymerization monomers, the inhibitor can conveniently be oxygen, which can be provided in the form of a gas such as air, a gas enriched in oxygen (optionally but in some embodiments preferably containing additional inert gases to reduce combustibility thereof), or in some embodiments pure oxygen gas. In alternate embodiments, such as where the monomer is polymerized by photoacid generator initiator, the inhibitor can be a base such as ammonia, trace amines (e.g. methyl amine, ethyl amine, di and trialkyl amines such as dimethyl amine, diethyl amine, trimethyl amine, triethyl amine, etc.), or carbon dioxide, including mixtures or combinations thereof.

Polymerizable liquids carrying live cells. In some embodiments, the polymerizable liquid may carry live cells as “particles” therein. Such polymerizable liquids are generally aqueous, and may be oxygenated, and may be considered as “emulsions” where the live cells are the discrete phase. Suitable live cells may be plant cells (e.g., monocot, dicot), animal cells (e.g., mammalian, avian, amphibian, reptile cells), microbial cells (e.g., prokaryote, eukaryote, protozoal, etc.), etc. The cells may be of differentiated cells from or corresponding to any type of tissue (e.g., blood, cartilage, bone, muscle, endocrine gland, exocrine gland, epithelial, endothelial, etc.), or may be undifferentiated cells such as stem cells or progenitor cells. In such embodiments the polymerizable liquid can be one that forms a hydrogel, including but not limited to those described in US Patents Nos. 7,651,683; 7,651,682; 7,556,490; 6,602,975; 5,836,313; etc.

2. Apparatus.

A non-limiting embodiment of an apparatus of the invention is shown in **Figure 2**. It comprises a radiation source **11** such as a digital light processor (DLP) providing electromagnetic radiation **12** which through reflective mirror **13** illuminates a build chamber defined by wall **14** and a rigid build plate **15** forming the bottom of the build chamber, which build chamber is filled with liquid resin **16**. The bottom of the chamber **15** is constructed of build plate comprising a semipermeable member as discussed further below. The top of the

object under construction 17 is attached to a carrier 18. The carrier is driven in the vertical direction by linear stage 19, although alternate structures can be used as discussed below.

A liquid resin reservoir, tubing, pumps liquid level sensors and/or valves can be included to replenish the pool of liquid resin in the build chamber (not shown for clarity) though in some embodiments a simple gravity feed may be employed. Drives/actuators for the carrier or linear stage, along with associated wiring, can be included in accordance with known techniques (again not shown for clarity). The drives/actuators, radiation source, and in some embodiments pumps and liquid level sensors can all be operatively associated with a suitable controller, again in accordance with known techniques.

Build plates 15 used to carry out the present invention generally comprise or consist of a (typically rigid or solid, stationary, and/or fixed) semipermeable (or gas permeable) member, alone or in combination with one or more additional supporting substrates (e.g., clamps and tensioning members to rigidify an otherwise flexible semipermeable material). The semipermeable member can be made of any suitable material that is optically transparent at the relevant wavelengths (or otherwise transparent to the radiation source, whether or not it is visually transparent as perceived by the human eye—*i.e.*, an optically transparent window may in some embodiments be visually opaque), including but not limited to porous or microporous glass, and the rigid gas permeable polymers used for the manufacture of rigid gas permeable contact lenses. *See, e.g.*, Norman G. Gaylord, US Patent No. RE31,406; see also US Patents Nos. 7,862,176; 7,344,731; 7,097,302; 5,349,394; 5,310,571; 5,162,469; 5,141,665; 5,070,170; 4,923,906; and 4,845,089. In some embodiments such materials are characterized as glassy and/or amorphous polymers and/or substantially crosslinked that they are essentially non-swellaable. Preferably the semipermeable member is formed of a material that does not swell when contacted to the liquid resin or material to be polymerized (*i.e.*, is “non-swellaable”). Suitable materials for the semipermeable member include amorphous fluoropolymers, such as those described in US Patent Nos. 5,308,685 and 5,051,115. For example, such fluoropolymers are particularly useful over silicones that would potentially swell when used in conjunction with organic liquid resin inks to be polymerized. For some liquid resin inks, such as more aqueous-based monomeric systems and / or some polymeric resin ink systems that have low swelling tendencies, silicone based window materials maybe suitable. The solubility or permeability of organic liquid resin inks can be dramatically decreased by a number of known parameters including increasing the crosslink density of the window material or increasing the molecular weight of the liquid resin ink. In some

embodiments the build plate may be formed from a thin film or sheet of material which is flexible when separated from the apparatus of the invention, but which is clamped and tensioned when installed in the apparatus (*e.g.*, with a tensioning ring) so that it is rendered fixed or rigid in the apparatus. Particular materials include TEFLON AF® fluoropolymers, commercially available from DuPont. Additional materials include perfluoropolyether polymers such as described in US Patents Nos. 8,268,446; 8,263,129; 8,158,728; and 7,435,495.

It will be appreciated that essentially all solid materials, and most of those described above, have some inherent “flex” even though they may be considered “rigid,” depending on factors such as the shape and thickness thereof and environmental factors such as the pressure and temperature to which they are subjected. In addition, the terms “stationary” or “fixed” with respect to the build plate is intended to mean that no mechanical interruption of the process occurs, or no mechanism or structure for mechanical interruption of the process (as in a layer-by-layer method or apparatus) is provided, even if a mechanism for incremental adjustment of the build plate (for example, adjustment that does not lead to or cause collapse of the gradient of polymerization zone) is provided), or if the build surface contributes to reciprocation to aid feeding of the polymerizable liquid, as described further below.

The semipermeable member typically comprises a top surface portion, a bottom surface portion, and an edge surface portion. The build surface is on the top surface portion; and the feed surface may be on one, two, or all three of the top surface portion, the bottom surface portion, and/or the edge surface portion. In the embodiment illustrated in **Figure 2** the feed surface is on the bottom surface portion, but alternate configurations where the feed surface is provided on an edge, and/or on the top surface portion (close to but separate or spaced away from the build surface) can be implemented with routine skill.

The semipermeable member has, in some embodiments, a thickness of from 0.01, 0.1 or 1 millimeters to 10 or 100 millimeters, or more (depending upon the size of the item being fabricated, whether or not it is laminated to or in contact with an additional supporting plate such as glass, etc., as discussed further below.

The permeability of the semipermeable member to the polymerization inhibitor will depend upon conditions such as the pressure of the atmosphere and/or inhibitor, the choice of inhibitor, the rate or speed of fabrication, etc. In general, when the inhibitor is oxygen, the permeability of the semipermeable member to oxygen may be from 10 or 20 Barrers, up to 1000 or 2000 Barrers, or more. For example, a semipermeable member with a permeability

of 10 Barrers used with a pure oxygen, or highly enriched oxygen, atmosphere under a pressure of 150 PSI may perform substantially the same as a semipermeable member with a permeability of 500 Barrers when the oxygen is supplied from the ambient atmosphere under atmospheric conditions.

5 Thus, the semipermeable member may comprise a flexible polymer film (having any suitable thickness, *e.g.*, from 0.001, 0.01, 0.05, 0.1 or 1 millimeters to 1, 5, 10, or 100 millimeters, or more), and the build plate may further comprise a tensioning member (*e.g.*, a peripheral clamp and an operatively associated strain member or stretching member, as in a “drum head”; a plurality of peripheral clamps, etc., including combinations thereof)
10 connected to the polymer film and to fix and rigidify the film (*e.g.*, at least sufficiently so that the film does not stick to the object as the object is advanced and resiliently or elastically rebound therefrom). The film has a top surface and a bottom surface, with the build surface on the top surface and the feed surface preferably on the bottom surface. In other embodiments, the semipermeable member comprises: (i) a polymer film layer (having any
15 suitable thickness, *e.g.*, from 0.001, 0.01, 0.1 or 1 millimeters to 5, 10 or 100 millimeters, or more), having a top surface positioned for contacting said polymerizable liquid and a bottom surface, and (ii) a rigid, gas permeable, optically transparent supporting member (having any suitable thickness, *e.g.*, from 0.01, 0.1 or 1 millimeters to 10, 100, or 200 millimeters, or more), contacting said film layer bottom surface. The supporting member has a top surface
20 contacting the film layer bottom surface, and the supporting member has a bottom surface which may serve as the feed surface for the polymerization inhibitor. Any suitable materials that are semipermeable (that is, permeable to the polymerization inhibitor) may be used. For example, the polymer film or polymer film layer may, for example, be a fluoropolymer film, such as an amorphous thermoplastic fluoropolymer like TEFLON AF 1600™ or TEFLON
25 AF 2400™ fluoropolymer films, or perfluoropolyether (PFPE), particularly a crosslinked PFPE film, or a crosslinked silicone polymer film. The supporting member comprises a silicone or crosslinked silicone polymer member such as a polydimethylsiloxane member, a rigid gas permeable polymer member, or a porous or microporous glass member. Films can be laminated or clamped directly to the rigid supporting member without adhesive (*e.g.*, using
30 PFPE and PDMS materials), or silane coupling agents that react with the upper surface of a PDMS layer can be utilized to adhere to the first polymer film layer. UV-curable, acrylate-functional silicones can also be used as a tie layer between UV-curable PFPEs and rigid PDMS supporting layers.

When configured for placement in the apparatus, the carrier defines a “build region” on the build surface, within the total area of the build surface. Because lateral “throw” (*e.g.*, in the X and/or Y directions) is not required in the present invention to break adhesion between successive layers, as in the Joyce and Chen devices noted previously, the area of the build region within the build surface may be maximized (or conversely, the area of the build surface not devoted to the build region may be minimized). Hence in some embodiments, the total surface area of the build region can occupy at least fifty, sixty, seventy, eighty, or ninety percent of the total surface area of the build surface.

As shown in **Figure 2**, the various components are mounted on a support or frame assembly **20**. While the particular design of the support or frame assembly is not critical and can assume numerous configurations, in the illustrated embodiment it is comprised of a base **21** to which the radiation source **11** is securely or rigidly attached, a vertical member **22** to which the linear stage is operatively associated, and a horizontal table **23** to which wall **14** is removably or securely attached (or on which the wall is placed), and with the build plate rigidly fixed, either permanently or removably, to form the build chamber as described above.

As noted above, the build plate can consist of a single unitary and integral piece of a rigid semipermeable member, or can comprise additional materials. For example, a porous or microporous glass can be laminated or fixed to a rigid semipermeable material. Or, a semipermeable member as an upper portion can be fixed to a transparent lower member having purging channels formed therein for feeding gas carrying the polymerization inhibitor to the semipermeable member (through which it passes to the build surface to facilitate the formation of a release layer of unpolymerized liquid material, as noted above and below). Such purge channels may extend fully or partially through the base plate: For example, the purge channels may extend partially into the base plate, but then end in the region directly underlying the build surface to avoid introduction of distortion. Specific geometries will depend upon whether the feed surface for the inhibitor into the semipermeable member is located on the same side or opposite side as the build surface, on an edge portion thereof, or a combination of several thereof.

Any suitable radiation source (or combination of sources) can be used, depending upon the particular resin employed, including electron beam and ionizing radiation sources. In a preferred embodiment the radiation source is an actinic radiation source, such as one or more light sources, and in particular one or more ultraviolet light sources. Any suitable light source can be used, such as incandescent lights, fluorescent lights, phosphorescent or luminescent

lights, a laser, light-emitting diode, etc., including arrays thereof. The light source preferably includes a pattern-forming element operatively associated with a controller, as noted above. In some embodiments, the light source or pattern forming element comprises a digital (or deformable) micromirror device (DMD) with digital light processing (DLP), a spatial modulator (SLM), or a microelectromechanical system (MEMS) mirror array, a mask (aka a reticle), a silhouette, or a combination thereof. See, US Patent No. 7,902,526. Preferably the light source comprises a spatial light modulation array such as a liquid crystal light valve array or micromirror array or DMD (*e.g.*, with an operatively associated digital light processor, typically in turn under the control of a suitable controller), configured to carry out exposure or irradiation of the polymerizable liquid without a mask, *e.g.*, by maskless photolithography. See, *e.g.*, US Patents Nos. 6,312,134; 6,248,509; 6,238,852; and 5,691,541.

In some embodiments, as discussed further below, there may be movement in the X and/or Y directions concurrently with movement in the Z direction, with the movement in the X and/or Y direction hence occurring during polymerization of the polymerizable liquid (this is in contrast to the movement described in Y. Chen et al., or M. Joyce, *supra*, which is movement between prior and subsequent polymerization steps for the purpose of replenishing polymerizable liquid). In the present invention such movement may be carried out for purposes such as reducing “burn in” or fouling in a particular zone of the build surface.

Because an advantage of some embodiments of the present invention is that the size of the build surface on the semipermeable member (*i.e.*, the build plate or window) may be reduced due to the absence of a requirement for extensive lateral “throw” as in the Joyce or Chen devices noted above, in the methods, systems and apparatus of the present invention lateral movement (including movement in the X and/or Y direction or combination thereof) of the carrier and object (if such lateral movement is present) is preferably not more than, or less than, 80, 70, 60, 50, 40, 30, 20, or even 10 percent of the width (in the direction of that lateral movement) of the build region.

While in some embodiments the carrier is mounted on an elevator to advance up and away from a stationary build plate, on other embodiments the converse arrangement may be used: That is, the carrier may be fixed and the build plate lowered to thereby advance the carrier away therefrom. Numerous different mechanical configurations will be apparent to those skilled in the art to achieve the same result.

Depending on the choice of material from which the carrier is fabricated, and the choice of polymer or resin from which the article is made, adhesion of the article to the carrier may

sometimes be insufficient to retain the article on the carrier through to completion of the finished article or "build." For example, an aluminum carrier may have lower adhesion than a poly(vinyl chloride) (or "PVC") carrier. Hence one solution is to employ a carrier comprising a PVC on the surface to which the article being fabricated is polymerized. If this promotes too great an adhesion to conveniently separate the finished part from the carrier, then any of a variety of techniques can be used to further secure the article to a less adhesive carrier, including but not limited to the application of adhesive tape such as "Greener Masking Tape for Basic Painting #2025 High adhesion" to further secure the article to the carrier during fabrication.

10

3. Controller and process control.

The methods and apparatus of the invention can include process steps and apparatus features to implement process control, including feedback and feed-forward control, to, for example, enhance the speed and/or reliability of the method.

15

A controller for use in carrying out the present invention may be implemented as hardware circuitry, software, or a combination thereof. In one embodiment, the controller is a general purpose computer that runs software, operatively associated with monitors, drives, pumps, and other components through suitable interface hardware and/or software. Suitable software for the control of a three-dimensional printing or fabrication method and apparatus as described herein includes, but is not limited to, the ReplicatorG open source 3d printing program, 3DPrint™ controller software from 3D systems, Slic3r, Skeinforge, KISSlicer, Repetier-Host, PrintRun, Cura, etc., including combinations thereof.

20

Process parameters to directly or indirectly monitor, continuously or intermittently, during the process(*e.g.*, during one, some or all of said filling, irradiating and advancing steps) include, but are not limited to, irradiation intensity, temperature of carrier, polymerizable liquid in the build zone, temperature of growing product, temperature of build plate, pressure, speed of advance, pressure, force (*e.g.*, exerted on the build plate through the carrier and product being fabricated), strain (*e.g.*, exerted on the carrier by the growing product being fabricated), thickness of release layer, etc.

25

Known parameters that may be used in feedback and/or feed-forward control systems include, but are not limited to, expected consumption of polymerizable liquid (*e.g.*, from the known geometry or volume of the article being fabricated), degradation temperature of the polymer being formed from the polymerizable liquid, etc.

30

Process conditions to directly or indirectly control, continuously or step-wise, in response to a monitored parameter, and/or known parameters (*e.g.*, during any or all of the process steps noted above), include, but are not limited to, rate of supply of polymerizable liquid, temperature, pressure, rate or speed of advance of carrier, intensity of irradiation, duration of irradiation (*e.g.* for each “slice”), etc.

For example, the temperature of the polymerizable liquid in the build zone, or the temperature of the build plate, can be monitored, directly or indirectly with an appropriate thermocouple, non-contact temperature sensor (*e.g.*, an infrared temperature sensor), or other suitable temperature sensor, to determine whether the temperature exceeds the degradation temperature of the polymerized product. If so, a process parameter may be adjusted through a controller to reduce the temperature in the build zone and/or of the build plate. Suitable process parameters for such adjustment may include: decreasing temperature with a cooler, decreasing the rate of advance of the carrier, decreasing intensity of the irradiation, decreasing duration of radiation exposure, etc.

In addition, the intensity of the irradiation source (*e.g.*, an ultraviolet light source such as a mercury lamp) may be monitored with a photodetector to detect a decrease of intensity from the irradiation source (*e.g.*, through routine degradation thereof during use). If detected, a process parameter may be adjusted through a controller to accommodate the loss of intensity. Suitable process parameters for such adjustment may include: increasing temperature with a heater, decreasing the rate of advance of the carrier, increasing power to the light source, etc.

As another example, control of temperature and/or pressure to enhance fabrication time may be achieved with heaters and coolers (individually, or in combination with one another and separately responsive to a controller), and/or with a pressure supply (*e.g.*, pump, pressure vessel, valves and combinations thereof) and/or a pressure release mechanism such as a controllable valve (individually, or in combination with one another and separately responsive to a controller).

In some embodiments the controller is configured to maintain the gradient of polymerization zone described herein (*see, e.g.*, **Figure 1**) throughout the fabrication of some or all of the final product. The specific configuration (*e.g.*, times, rate or speed of advancing, radiation intensity, temperature, etc.) will depend upon factors such as the nature of the specific polymerizable liquid and the product being created. Configuration to maintain the gradient of polymerization zone may be carried out empirically, by entering a set of process

parameters or instructions previously determined, or determined through a series of test runs or “trial and error”; configuration may be provided through pre-determined instructions; configuration may be achieved by suitable monitoring and feedback (as discussed above), combinations thereof, or in any other suitable manner.

5 In some embodiments, a method and apparatus as described above may be controlled by a software program running in a general purpose computer with suitable interface hardware between that computer and the apparatus described above. Numerous alternatives are commercially available. Non-limiting examples of one combination of components is shown in **Figures 3 to 5**, where “Microcontroller” is Parallax Propeller, the Stepper Motor
10 Driver is Sparkfun EasyDriver, the LED Driver is a Luxeon Single LED Driver, the USB to Serial is a Parallax USB to Serial converter, and the DLP System is a Texas Instruments LightCrafter system.

4. General Methods.

15 As noted above, the present invention provides a method of forming a three-dimensional object, comprising the steps of: (a) providing a carrier and a build plate, said build plate comprising a semipermeable member, said semipermeable member comprising a build surface and a feed surface separate from said build surface, with said build surface and said carrier defining a build region therebetween, and with said feed surface in fluid contact
20 with a polymerization inhibitor; then (concurrently and/or sequentially) (b) filing said build region with a polymerizable liquid, said polymerizable liquid contacting said build segment, (c) irradiating said build region through said build plate to produce a solid polymerized region in said build region, with a liquid film release layer comprised of said polymerizable liquid formed between said solid polymerized region and said build surface, the
25 polymerization of which liquid film is inhibited by said polymerization inhibitor; and (d) advancing said carrier with said polymerized region adhered thereto away from said build surface on said stationary build plate to create a subsequent build region between said polymerized region and said top zone. In general the method includes (e) continuing and/or
30 repeating steps (b) through (d) to produce a subsequent polymerized region adhered to a previous polymerized region until the continued or repeated deposition of polymerized regions adhered to one another forms said three-dimensional object.

Since no mechanical release of a release layer is required, or no mechanical movement of a build surface to replenish oxygen is required, the method can be carried out in

a continuous fashion, though it will be appreciated that the individual steps noted above may be carried out sequentially, concurrently, or a combination thereof. Indeed, the rate of steps can be varied over time depending upon factors such as the density and/or complexity of the region under fabrication.

5 Also, since mechanical release from a window or from a release layer generally requires that the carrier be advanced a greater distance from the build plate than desired for the next irradiation step, which enables the window to be recoated, and then return of the carrier back closer to the build plate (*e.g.*, a “two steps forward one step back” operation), the present invention in some embodiments permits elimination of this “back-up” step and allows
10 the carrier to be advanced unidirectionally, or in a single direction, without intervening movement of the window for re-coating, or “snapping” of a pre-formed elastic release-layer. However, in other embodiments of the invention, reciprocation is utilized not for the purpose of obtaining release, but for the purpose of more rapidly filling or pumping polymerizable liquid into the build region.

15 In some embodiments, the advancing step is carried out sequentially in uniform increments (*e.g.*, of from 0.1 or 1 microns, up to 10 or 100 microns, or more) for each step or increment. In some embodiments, the advancing step is carried out sequentially in variable increments (*e.g.*, each increment ranging from 0.1 or 1 microns, up to 10 or 100 microns, or more) for each step or increment. The size of the increment, along with the rate of
20 advancing, will depend in part upon factors such as temperature, pressure, structure of the article being produced (*e.g.*, size, density, complexity, configuration, etc.)

In other embodiments of the invention, the advancing step is carried out continuously, at a uniform or variable rate.

In some embodiments, the rate of advance (whether carried out sequentially or
25 continuously) is from about 0.1, 1, or 10 microns per second, up to about 100, 1,000, or 10,000 microns per second, again depending again depending on factors such as temperature, pressure, structure of the article being produced, intensity of radiation, etc

As described further below, in some embodiments the filling step is carried out by forcing said polymerizable liquid into said build region under pressure. In such a case, the
30 advancing step or steps may be carried out at a rate or cumulative or average rate of at least 0.1, 1, 10, 50, 100, 500 or 1000 microns per second, or more. In general, the pressure may be whatever is sufficient to increase the rate of said advancing step(s) at least 2, 4, 6, 8 or 10 times as compared to the maximum rate of repetition of said advancing steps in the absence

of said pressure. Where the pressure is provided by enclosing an apparatus such as described above in a pressure vessel and carrying the process out in a pressurized atmosphere (*e.g.*, of air, air enriched with oxygen, a blend of gasses, pure oxygen, etc.) a pressure of 10, 20, 30 or 40 pounds per square inch (PSI) up to, 200, 300, 400 or 500 PSI or more, may be used. For
5 fabrication of large irregular objects higher pressures may be less preferred as compared to slower fabrication times due to the cost of a large high pressure vessel. In such an embodiment, both the feed surface and the polymerizable liquid can be in fluid contact with the same compressed gas (*e.g.*, one comprising from 20 to 95 percent by volume of oxygen, the oxygen serving as the polymerization inhibitor.

10 On the other hand, when smaller items are fabricated, or a rod or fiber is fabricated that can be removed or exited from the pressure vessel as it is produced through a port or orifice therein, then the size of the pressure vessel can be kept smaller relative to the size of the product being fabricated and higher pressures can (if desired) be more readily utilized.

As noted above, the irradiating step is in some embodiments carried out with
15 patterned irradiation. The patterned irradiation may be a fixed pattern or may be a variable pattern created by a pattern generator (*e.g.*, a DLP) as discussed above, depending upon the particular item being fabricated.

When the patterned irradiation is a variable pattern rather than a pattern that is held constant over time, then each irradiating step may be any suitable time or duration depending
20 on factors such as the intensity of the irradiation, the presence or absence of dyes in the polymerizable material, the rate of growth, etc. Thus in some embodiments each irradiating step can be from 0.001, 0.01, 0.1, 1 or 10 microseconds, up to 1, 10, or 100 minutes, or more, in duration. The interval between each irradiating step is in some embodiments preferably as brief as possible, *e.g.*, from 0.001, 0.01, 0.1, or 1 microseconds up to 0.1, 1, or 10 seconds.

25 While the dead zone and the gradient of polymerization zone do not have a strict boundary therebetween (in those locations where the two meet), the thickness of the gradient of polymerization zone is in some embodiments at least as great as the thickness of the dead zone. Thus, in some embodiments, the dead zone has a thickness of from 0.01, 0.1, 1, 2, or 10 microns up to 100, 200 or 400 microns, or more, and/or said gradient of polymerization zone
30 and said dead zone together have a thickness of from 1 or 2 microns up to 400, 600, or 1000 microns, or more. Thus the gradient of polymerization zone may be thick or thin depending on the particular process conditions at that time. Where the gradient of polymerization zone is thin, it may also be described as an active surface on the bottom of the growing three-

dimensional object, with which monomers can react and continue to form growing polymer chains therewith. In some embodiments, the gradient of polymerization zone, or active surface, is maintained (while polymerizing steps continue) for a time of at least 5, 10, 15, 20 or 30 seconds, up to 5, 10, 15 or 20 minutes or more, or until completion of the three-dimensional product.

The method may further comprise the step of disrupting said gradient of polymerization zone/active surface, for a time sufficient to form a cleavage line in said three-dimensional object (*e.g.*, at a predetermined desired location for intentional cleavage, or at a location in said object where prevention of cleavage or reduction of cleavage is non-critical), and then reinstating said gradient of polymerization zone (*e.g.* by pausing, and resuming, the advancing step, increasing, then decreasing, the intensity of irradiation, and combinations thereof

In some embodiments the build surface is flat; in other the build surface is irregular such as convexly or concavely curved, or has walls or trenches formed therein. In either case the build surface may be smooth or textured.

Curved and/or irregular build plates or build surfaces can be used in fiber or rod formation, to provide different materials to a single object being fabricated (that is, different polymerizable liquids to the same build surface through channels or trenches formed in the build surface, each associated with a separate liquid supply, etc.

Carrier Feed Channels for Polymerizable liquid. While polymerizable liquid may be provided directly to the build plate from a liquid conduit and reservoir system, in some embodiments the carrier include one or more feed channels therein. The carrier feed channels are in fluid communication with the polymerizable liquid supply, for example a reservoir and associated pump. Different carrier feed channels may be in fluid communication with the same supply and operate simultaneously with one another, or different carrier feed channels may be separately controllable from one another (for example, through the provision of a pump and/or valve for each). Separately controllable feed channels may be in fluid communication with a reservoir containing the same polymerizable liquid, or may be in fluid communication with a reservoir containing different polymerizable liquids. Through the use of valve assemblies, different polymerizable liquids may in some embodiments be alternately fed through the same feed channel, if desired.

5. Reciprocating feed of polymerizable liquid.

In an embodiment of the present invention, the carrier is vertically reciprocated (or oscillated) with respect to the build surface (that is, the two are vertically reciprocated with respect to one another) to enhance or speed the refilling of the build region with the polymerizable liquid. Such reciprocations or oscillations (these two terms being used interchangeably herein) may be of any suitable configuration, including uniform and non-uniform, and/or periodic or non-periodic, with respect to one another, so long as they are configured to enhance feed of the polymerizable liquid to the build surface.

In some embodiments, the vertically reciprocating step, which comprises an upstroke and a downstroke, is carried out with the distance of travel of the upstroke being greater than the distance of travel of the downstroke, to thereby concurrently carry out the advancing step (that is, driving the carrier away from the build plate in the Z dimension) in part or in whole.

In some embodiments, the speed of the upstroke gradually accelerates (that is, there is provided a gradual start and/or gradual acceleration of the upstroke, over a period of at least 20, 30, 40, or 50 percent of the total time of the upstroke, until the conclusion of the upstroke, or the change of direction which represents the beginning of the downstroke. Stated differently, the upstroke begins, or starts, gently or gradually.

In some embodiments, the speed of the downstroke gradually decelerates (that is, there is provided a gradual termination and/or gradual deceleration of the downstroke, over a period of at least 20, 30, 40, or 50 percent of the total time of the downstroke. Stated differently, the downstroke concludes, or ends, gently or gradually.

While in some embodiments there is an abrupt end, or abrupt deceleration, of the upstroke, and an abrupt beginning or acceleration of the downstroke (*e.g.*, a rapid change in vector or direction of travel from upstroke to downstroke), it will be appreciated that gradual transitions may be introduced here as well (*e.g.*, through introduction of a "plateau" or pause in travel between the upstroke and downstroke). It will also be appreciated that, while each reciprocating step may be consist of a single upstroke and downstroke, the reciprocation step may comprise a plurality of 2, 3, 4 or 5 or more linked set of reciprocations, which may be the same or different in frequent and/or amplitude

In some embodiments, the vertically reciprocating step is carried out over a total time of from 0.01 or 0.1 seconds up to 1 or 10 seconds (*e.g.*, per cycle of an upstroke and a downstroke).

In some embodiments, the upstroke distance of travel is from 0.02 or 0.2 millimeters (or 20 or 200 microns) to 1 or 10 millimeters (or 1000 to 10,000 microns). The distance of

travel of the downstroke may be the same as, or less than, the distance of travel of the upstroke, where a lesser distance of travel for the downstroke serves to achieve the advancing of the carrier away from the build surface as the three-dimensional object is gradually formed. Where a reciprocation step comprises multiple linked reciprocations, the sum distance of travel of all upstrokes in that set is preferably greater than the sum distance of travel of all downstrokes in that set, to achieve the advancing of the carrier away from the build surface as the three-dimensional object is gradually formed.

Preferably the vertically reciprocating step, and particularly the upstroke thereof, does not cause the formation of gas bubbles or a gas pocket in the build region, but instead the build region remains filled with the polymerizable liquid throughout the reciprocation steps, and the gradient of polymerization zone or region remains in contact with the “dead zone” and with the growing object being fabricated throughout the reciprocation steps. As will be appreciated, a purpose of the reciprocation is to speed or enhance the refilling of the build region, particularly where larger build regions are to be refilled with polymerizable liquid, as compared to the speed at which the build region could be refilled without the reciprocation step.

In some embodiments, the advancing step is carried out intermittently at a rate of 1, 2, 5 or 10 individual advances per minute up to 300, 600, or 1000 individual advances per minute, each followed by a pause during which an irradiating step is carried out. It will be appreciated that one or more reciprocation steps (*e.g.*, upstroke plus downstroke) may be carried out within each advancing step. Stated differently, the reciprocating steps may be nested within the advancing steps.

In some embodiments, the individual advances are carried out over an average distance of travel for each advance of from 10 or 50 microns to 100 or 200 microns (optionally including the total distance of travel for each vertically reciprocating step, *e.g.*, the sum of the upstroke distance minus the downstroke distance).

Apparatus for carrying out the invention in which the reciprocation steps described herein are implemented substantially as described above, with the drive associated with the carrier, and/or with an additional drive operatively associated with the transparent member, and with the controller operatively associated with either or both thereof and configured to reciprocate the carrier and transparent member with respect to one another as described above.

In the alternative, vertical reciprocation may be carried out by configuring the build surface (and corresponding build plate) so that it may have a limited range of movement up and down in the vertical or "Z" dimension, while the carrier advances (*e.g.*, continuously or step-wise) away from the build plate in the vertical or "Z" dimension. In some embodiments, such limited range of movement may be passively imparted, such as with upward motion achieved by partial adhesion of the build plate to the growing object through a viscous polymerizable liquid, followed by downward motion achieved by the weight, resiliency, etc. of the build plate (optionally including springs, buffers, shock absorbers or the like, configured to influence either upward or downward motion of the build plate and build surface). In another embodiment, such motion of the build surface may be actively achieved, by operatively associating a separate drive system with the build plate, which drive system is also operatively associated with the controller, to separately achieve vertical reciprocation. In still another embodiment, vertical reciprocation may be carried out by configuring the build plate, and/or the build surface, so that it flexes upward and downward, with the upward motion thereof being achieved by partial adhesion of the build surface to the growing object through a viscous polymerizable liquid, followed by downward motion achieved by the inherent stiffness of the build surface biasing it or causing it to return to a prior position.

It will be appreciated that illumination or irradiation steps, when intermittent, may be carried out in a manner synchronized with vertical reciprocation, or not synchronized with vertical reciprocation, depending on factors such as whether the reciprocation is achieved actively or passively.

It will also be appreciated that vertical reciprocation may be carried out between the carrier and all regions of the build surface simultaneously (*e.g.*, where the build surface is rigid), or may be carried out between the carrier and different regions of the build surface at different times (*e.g.*, where the build surface is of a flexible material, such as a tensioned polymer film).

6. Increased speed of fabrication by increasing light intensity.

In general, it has been observed that speed of fabrication can increase with increased light intensity. In some embodiments, the light is concentrated or "focused" at the build region to increase the speed of fabrication. This may be accomplished using an optical device such as an objective lens.

The speed of fabrication may be generally proportional to the light intensity. For example, the build speed in millimeters per hour may be calculated by multiplying the light intensity in milliWatts per square centimeter and a multiplier. The multiplier may depend on a variety of factors, including those discussed below. A range of multipliers, from low to high, may be employed. On the low end of the range, the multiplier may be about 10, 15, 20 or 30. On the high end of the multiplier range, the multiplier may be about 150, 300, 400 or more.

The relationships described above are, in general, contemplated for light intensities of from 1, 5 or 10 milliWatts per square centimeter, up to 20 or 50 milliWatts per square centimeter.

Certain optical characteristics of the light may be selected to facilitate increased speed of fabrication. By way of example, a band pass filter may be used with a mercury bulb light source to provide 365 ± 10 nm light measured at Full Width Half Maximum (FWHM). By way of further example, a band pass filter may be used with an LED light source to provide 375 ± 15 nm light measured at FWHM.

As noted above, polymerizable liquids used in such processes are, in general, free radical polymerizable liquids with oxygen as the inhibitor, or acid-catalyzed or cationically polymerizable liquids with a base as the inhibitor. Some specific polymerizable liquids will of course cure more rapidly or efficiently than others and hence be more amenable to higher speeds, though this may be offset at least in part by further increasing light intensity.

At higher light intensities and speeds, the "dead zone" may become thinner as inhibitor is consumed. If the dead zone is lost then the process will be disrupted. In such case, the supply of inhibitor may be enhanced by any suitable means, including providing an enriched and/or pressurized atmosphere of inhibitor, a more porous semipermeable member, a stronger or more powerful inhibitor (particularly where a base is employed), etc.

In general, lower viscosity polymerizable liquids are more amenable to higher speeds, particularly for fabrication of articles with a large and/or dense cross section (although this can be offset at least in part by increasing light intensity). Polymerizable liquids with viscosities in the range of 50 or 100 centipoise, up to 600, 800 or 1000 centipoise or more (as measured at room temperature and atmospheric pressure with a suitable device such as a HYDRAMOTION REACTAVISC™ Viscometer (available from Hydramotion Ltd, 1 York Road Business Park, Malton, York YO17 6YA England). In some embodiments, where necessary, the viscosity of the polymerizable liquid can advantageously be reduced by heating the polymerizable liquid, as described above.

In some embodiments, such as fabrication of articles with a large and/or dense cross-section, speed of fabrication can be enhanced by introducing reciprocation to “pump” the polymerizable liquid, as described above, and/or the use of feeding the polymerizable liquid through the carrier, as also described above, and/or heating and/or pressurizing the polymerizable liquid, as also described above.

7. Tiling.

It may be desirable to use more than one light engine to preserve resolution and light intensity for larger build sizes. Each light engine may be configured to project an image (e.g., an array of pixels) into the build region such that a plurality of "tiled" images are projected into the build region. As used herein, the term "light engine" can mean an assembly including a light source, a DLP device such as a digital micromirror device and an optical device such as an objective lens. The "light engine" may also include electronics such as a controller that is operatively associated with one or more of the other components.

In some embodiments, a configuration with the overlapped images is employed with some form of "blending" or "smoothing" of the overlapped regions as generally discussed in, for example, U.S. Patent Nos. 7,292,207, 8,102,332, 8,427,391, 8,446,431 and U.S. Patent Application Publication Nos. 2013/0269882, 2013/0278840 and 2013/0321475, the disclosures of which are incorporated herein in their entireties.

The tiled images can allow for larger build areas without sacrificing light intensity, and therefore can facilitate faster build speeds for larger objects. It will be understood that more than two light engine assemblies (and corresponding tiled images) may be employed. Various embodiments of the invention employ at least 4, 8, 16, 32, 64, 128 or more tiled images.

8. Fabrication in multiple zones.

As noted above, embodiments of the invention may carry out the formation of the three-dimensional object through multiple zones or segments of operation. Such a method generally comprises:

- (a) providing a carrier and an optically transparent member having a build surface, the carrier and the build surface defining a build region therebetween, with the carrier positioned adjacent and spaced apart from the build surface at a start position; then
- (b) forming an adhesion segment of the three-dimensional object by:

(i) filling the build region with a polymerizable liquid,
(ii) irradiating the build region with light through the optically transparent member (e.g., by a single exposure), while

(iii) maintaining the carrier stationary or advancing the carrier away from the build surface at a first cumulative rate of advance, to thereby form from the polymerizable liquid a solid polymer adhesion segment of the object adhered to the carrier; then

(c) optionally but preferably forming a transition segment of the three dimensional object by

(i) filling the build region with a polymerizable liquid,
(ii) continuously or intermittently irradiating the build region with light through the optically transparent member, and

(iii) continuously or intermittently advancing (e.g., sequentially or concurrently with the irradiating step) the carrier away from the build surface at a second cumulative rate of advance to thereby form from the polymerizable liquid a transition segment of the object between the adhesion segment and the build surface;

wherein the second cumulative rate of advance is greater than the first cumulative rate of advance; and then

(d) forming a body segment of the three dimensional object by:

(i) filling the build region with a polymerizable liquid,
(ii) continuously or intermittently irradiating the build region with light through the optically transparent, and

(iii) continuously or intermittently advancing (e.g., sequentially or concurrently with the irradiating step) the carrier away from the build surface at a third cumulative rate of advance, to thereby form from the polymerizable liquid a body segment of the object between the transition segment and the build surface;

wherein the third cumulative rate of advance is greater than the first and/or the second cumulative rate of advance.

Note that the start position can be any position among a range of positions (e.g., a range of up to 5 or 10 millimeters or more), and the irradiating step (b)(ii) is carried out at an intensity sufficient to adhere the solid polymer to the carrier when the carrier is at any position within that range of positions. This advantageously reduces the possibility of failure of adhesion of the three-dimensional object to the carrier due to variations in uniformity of

the carrier and/or build surfaces, variations inherent in drive systems in positioning the carrier adjacent the build surface, etc.

9. Fabrication with Intermittent (or Strobe) illumination.

5 As noted above, in some embodiments the invention may be carried out with the illumination in intermittent periods or burst. In one embodiment, such a method comprises:

providing a carrier and an optically transparent member having a build surface, the carrier and the build surface defining a build region therebetween;

filling the build region with a polymerizable liquid,

10 intermittently irradiating the build region with light through the optically transparent member to form a solid polymer from the polymerizable liquid,

continuously advancing the carrier away from the build surface to form the three-dimensional object from the solid polymer.

Another embodiment of such a mode of operation comprises:

15 providing a carrier and an optically transparent member having a build surface, the carrier and the build surface defining a build region therebetween;

filling the build region with a polymerizable liquid,

intermittently irradiating the build region with light through the optically transparent member to form a solid polymer from the polymerizable liquid,

20 continuously or intermittently advancing (*e.g.*, sequentially or concurrently with the irradiating step) the carrier away from the build surface to form the three-dimensional object from the solid polymer.

In some embodiments, the intermittently irradiating comprises alternating periods of active and inactive illumination, where the average duration of the periods of active
25 illumination is less than the average duration of the periods of inactive illumination (*e.g.*, is not more than 50, 60, or 80 percent thereof).

In other embodiments, the intermittently irradiating comprises alternating periods of active and inactive illumination, where the average duration of the periods of active
30 illumination is the same as or greater than the average duration of the periods of inactive illumination (*e.g.*, is at least 100, 120, 160, or 180 percent thereof).

Examples of such modes of operation are given further below. These features may be combined with any of the other features and operating steps or parameters described herein.

10. Fabrication of body segment by multiple operating modes.

Operating modes (that is, the pattern defining the manner of irradiating and advancing) may be changed in the course of fabricating a three dimensional object (*i.e.*, the major portion, or “body portion”, thereof), to best suit the particular geometry of each contiguous segment of that three-dimensional object, particularly as that geometry changes during the course of fabrication.

In general, base and transition zones may still be fabricated as described above, as the preferred foundation for the body of that object during fabrication thereof.

Horizontal portions of the three, dimensional object, abrupt changes in cross section, and converging or diverging elements of the three dimensional object, may be fabricated in a reciprocal or oscillatory operating mode, for example, to eliminate surface defects, such as pitting, and speed or enhance resin replenishment to the build region.

Vertical and thin-walled sections of the three dimensional object, and fragile elements or fine features thereof, can be fabricated in a continuous operating mode. In some embodiments, continuous mode is least concussive of the various operating modes, and hence is better suited to fabricating segments of three-dimensional objects with complex or delicate geometries (though this may be influenced by the choice of materials for the build surface—that is, rigid vs. flexible).

Feathering, or gradual transitioning of operating mode parameters, may be included in the course of changing operating modes (that is, between one operating mode and a subsequent operating mode). For example, in an intra-oscillatory build: oscillatory parameters are driven by enabling resin flow and allow time for the resin level in the build area to equilibrate--for thinner cross-sections, one can use a lower oscillation height, faster oscillation speeds, and/or smaller delay time to replenish resin, while the opposite is true for thicker cross-sections.

In feathering from an reciprocal (or oscillatory) to continuous operating mode: A pause following oscillatory mode, ramp in continuous speed from 10 mm/hr to standard continuous speed as analog to transition zone, effective dosage to initial slices drops from "over-exposed" (allowing proper adhesion) to the recommended dosage.

In feathering from continuous to oscillatory: initial oscillation displacement following transition accounts for area of last exposed continuous frame, e.g. high oscillation displacement for large cross-section and vice versa. Dosage for initial frames can be constant or ramped from high to low.

In an alternative to changing operating modes (or in combination with changing operating modes), the parameters of an operating mode can be changed during formation of the three-dimensional object. Examples of parameters that can be changed include, for example, frequency of irradiating, intensity of irradiating, duration of irradiating, duty cycle of irradiating, rate of advancing, lead time prior to irradiating, lag time following irradiating, step height, pump height, step or pump duration, or frequency of step-wise or reciprocal advancing. For example:

greater pump height may be preferred for fabricating a dense portion or segments of an object (such as a completely solid portion, or a dense foam or lattice portion);

greater pump speed may be preferred for a sparse (or less dense) segment or portion of an object, such as a hollow, mesh-filled, open foam or open lattice portion of an object; and

decreased lead and lag times may be preferred when overall speed or rate of formation is increased.

Additional reasons for varying such parameters are indicated above and below.

It will be appreciated that the pattern of exposure may be changed in the course of fabrication, *e.g.*, from slice to slice, to alter the geometry of external surfaces of the three-dimensional object, to alter the geometry of internal surfaces of the three dimensional object for structural purposes, to alter the geometry of internal surfaces of the object to change micro-structure or material properties of the object (*e.g.*, in the formation of a regular or irregular mesh, lattice, or foam (including open and closed cell foams), to maintain or alter flow of the polymerizable liquid to the build region, etc. In addition, in the present invention, slice thickness may advantageously be varied, as discussed further below.

11. Varying slice thickness.

As noted above, the methods and processes described herein advantageously accommodate input in varying slice thickness, rather than a fixed slice thickness, during formation of a three-dimensional object, allowing the operation of the methods and apparatus to be simplified, and particularly for electronic or computer-generated instructions to the apparatus for carrying out the method to be simplified. For example, for an object that includes both finely detailed portions as well as less detailed portions, or relatively constant portions, slice thickness can be thinner for the detailed portions, and thicker for the relatively constant portions.

The number of times slice thickness is changed will depend upon factors such as the object material and properties, geometry, tensile or other material properties, tolerances, etc. There are no particular limits, and hence in some embodiments, slice thickness may be changed at least 2, 4, 8 or 10 times during formation of the object or object body body portion (and optionally up to 100 or 1000 times, or more). Note that every change may not be to a different slice thickness, but may in some instances be a reversion to a previous (but not the immediately previous) slice thickness.

For example, in some embodiments, changing may be between: at least one slice having a thickness of less than 2 or 4 microns; optionally at least one slice having a thickness between 40 and 80 microns; and at least one slice having a thickness of more than 200, 400 or 600 microns.

In some embodiments, changing may be between: at least one slice having a thickness of less than 2 or 4 microns; and at least one slice having a thickness of more than 40 or 80 microns.

In some embodiments, the changing may be between at least one slice having a thickness of less than 20 or 40 microns; optionally at least one slice having a thickness between 60 and 80 microns; and at least one slice having a thickness of more than 200, 400, or 600 microns.

In some embodiments, the changing may be between at least a first thin slice and a second thicker slice, wherein said second slice has a thickness at least 5, 10, 15 or 20 times greater than said first slice.

In some embodiments, the changing is between at least a first plurality (*e.g.*, at least 2, 5, 10 or 20) of contiguous thin slices and a second thicker slice, wherein each of said thin slices is different from one another, and wherein said second thicker slice has a thickness at least 5, 10, 15, or 20 times greater than each of said plurality of thin slices.

Variation of slice thickness may be implemented in any operating mode, as discussed further below, and in combination with changing operating modes in the course of fabricating a particular three-dimensional object, as also discussed further below.

12. DUAL HARDENING POLYMERIZABLE LIQUIDS: PART B.

As noted above, in some embodiments of the invention, the polymerizable liquid comprises a first light polymerizable component (sometimes referred to as "Part A" herein) and a second component that solidifies by another mechanism, or in a different manner from,

the first component (sometimes referred to as “Part B” herein), typically by further reacting, polymerizing, or chain extending. Numerous embodiments thereof may be carried out. In the following, note that, where particular acrylates such as methacrylates are described, other acrylates may also be used.

5 **Part A chemistry.** As noted above, in some embodiments of the present invention, a resin will have a first component, termed “Part A.” Part A comprises or consists of a mix of monomers and/or prepolymers that can be polymerized by exposure to actinic radiation or light. This resin can have a functionality of 2 or higher (though a resin with a functionality of 1 can also be used when the polymer does not dissolve in its monomer). A purpose of Part A
10 is to “lock” the shape of the object being formed or create a scaffold for the one or more additional components (*e.g.*, Part B). Importantly, Part A is present at or above the minimum quantity needed to maintain the shape of the object being formed after the initial solidification. In some embodiments, this amount corresponds to less than ten, twenty, or thirty percent by weight of the total resin (polymerizable liquid) composition.

15 In some embodiments, Part A can react to form a cross-linked polymer network or a solid homopolymer.

 Examples of suitable reactive end groups suitable for Part A constituents, monomers, or prepolymers include, but are not limited to: acrylates, methacrylates, α -olefins, N-vinyls, acrylamides, methacrylamides, styrenics, epoxides, thiols, 1,3-dienes, vinyl halides,
20 acrylonitriles, vinyl esters, maleimides, and vinyl ethers.

 An aspect of the solidification of Part A is that it provides a scaffold in which a second reactive resin component, termed “Part B,” can solidify during a second step (which may occur concurrently with or following the solidification of Part A). This secondary reaction preferably occurs without significantly distorting the original shape defined during
25 the solidification of Part A. Alternative approaches would lead to a distortion in the original shape in a desired manner.

 In particular embodiments, when used in the methods and apparatus described herein, the solidification of Part A is continuously inhibited during printing within a certain region, by oxygen or amines or other reactive species, to form a liquid interface between the
30 solidified part and an inhibitor-permeable film or window (*e.g.*, is carried out by continuous liquid interphase/interface printing).

Part B chemistry. Part B may comprise, consist of or consist essentially of a mix of monomers and/or prepolymers that possess reactive end groups that participate in a second

solidification reaction after the Part A solidification reaction. In some embodiments, Part B could be added simultaneously to Part A so it is present during the exposure to actinide radiation, or Part B could be infused into the object made during the 3D printing process in a subsequent step. Examples of methods used to solidify Part B include, but are not limited to, contacting the object or scaffold to heat, water or water vapor, light at a different wavelength than that at which Part A is cured, catalysts, (with or without additional heat), evaporation of a solvent from the polymerizable liquid (e.g., using heat, vacuum, or a combination thereof), microwave irradiation, etc., including combinations thereof.

Examples of suitable reactive end group pairs suitable for Part B constituents, monomers or prepolymers include, but are not limited to: epoxy/amine, epoxy/hydroxyl, oxetane/amine, oxetane/alcohol, isocyanate*/hydroxyl, Isocyanate*/amine, isocyanate/carboxylic acid, anhydride/amine, amine/carboxylic acid, amine/ester, hydroxyl/carboxylic acid, hydroxyl/acid chloride, amine/acid chloride, vinyl/Si-H (hydrosilylation), Si-Cl /hydroxyl, Si-Cl/amine, hydroxyl/aldehyde, amine/aldehyde, hydroxymethyl or alkoxymethyl amide/alcohol, aminoplast, alkyne/Azide (also known as one embodiment of "Click Chemistry," along with additional reactions including thiolene, Michael additions, Diels-Alder reactions, nucleophilic substitution reactions, etc.), alkene/Sulfur (polybutadiene vulcanization), alkene/peroxide, alkene/thiol, alkyne/thiol, hydroxyl/halide, isocyanate*/water (polyurethane foams), Si-OH/hydroxyl, Si-OH/water, Si-OH/Si-H (tin catalyzed silicone), Si-OH/Si-OH (tin catalyzed silicone), Perfluorovinyl (coupling to form perfluorocyclobutane), etc., where *Isocyanates include protected isocyanates (e.g. oximes)), diene/dienophiles for Diels-Alder reactions, olefin metathesis polymerization, olefin polymerization using Ziegler-Natta catalysis, ring-opening polymerization (including ring-opening olefin metathesis polymerization, lactams, lactones, Siloxanes, epoxides, cyclic ethers, imines, cyclic acetals, etc.), etc.

Other reactive chemistries suitable for Part B will be recognizable by those skilled in the art. Part B components useful for the formation of polymers described in "Concise Polymeric Materials Encyclopedia" and the "Encyclopedia of Polymer Science and Technology" are hereby incorporated by reference.

Organic peroxides. In some embodiments, an organic peroxide may be included in the polymerizable liquid or resin, for example to facilitate the reaction of potentially unreacted double bonds during heat and/or microwave irradiation curing. Such organic peroxides may be included in the resin or polymerizable liquid in any suitable amount, such

as from 0.001 or 0.01 or 0.1 percent by weight, up to 1, 2, or 3 percent by weight. Examples of suitable organic peroxides include, but are not limited to, 2,5-bis(tert-butylperoxy)-2,5-dimethylhexane (*e.g.*, LUPEROX 101™), dilauroyl peroxide (*e.g.* LUPEROX LP™), benzoyl peroxide (*e.g.*, LUPEROX A98™), and bis(tert-butylldioxyisopropyl)benzene (*e.g.*, VulCUP R™), etc., including combinations thereof. Such organic peroxides are available from a variety of sources, including but not limited to Arkema (420 rue d'Estienne d'Orves, 92705 Colombes Cedex, France).

Elastomers. A particularly useful embodiment for implementing the invention is for the formation of elastomers. Tough, high-elongation elastomers are difficult to achieve using only liquid UV-curable precursors. However, there exist many thermally cured materials (polyurethanes, silicones, natural rubber) that result in tough, high-elongation elastomers after curing. These thermally curable elastomers on their own are generally incompatible with most 3D printing techniques.

In embodiments of the current invention, small amounts (*e.g.*, less than 20 percent by weight) of a low-viscosity UV curable material (Part A) are blended with thermally-curable precursors to form (preferably tough) elastomers (*e.g.* polyurethanes, polyureas, or copolymers thereof (*e.g.*, poly(urethane-urea)), and silicones) (Part B). The UV curable component is used to solidify an object into the desired shape using 3D printing as described herein and a scaffold for the elastomer precursors in the polymerizable liquid. The object can then be heated after printing, thereby activating the second component, resulting in an object comprising the elastomer.

Adhesion of formed objects. In some embodiments, it may be useful to define the shapes of multiple objects using the solidification of Part A, align those objects in a particular configuration, such that there is a hermetic seal between the objects, then activate the secondary solidification of Part B. In this manner, strong adhesion between parts can be achieved during production. A particularly useful example may be in the formation and adhesion of sneaker components.

Fusion of particles as Part B. In some embodiments, "Part B" may simply consist of small particles of a pre-formed polymer. After the solidification of Part A, the object may be heated above the glass transition temperature of Part B in order to fuse the entrapped polymeric particles.

Evaporation of solvent as Part B. In some embodiments, "Part B" may consist of a pre-formed polymer dissolved in a solvent. After the solidification of Part A into the desired

object, the object is subjected to a process (e.g. heat + vacuum) that allows for evaporation of the solvent for Part B, thereby solidifying Part B.

Thermally cleavable end groups. In some embodiments, the reactive chemistries in Part A can be thermally cleaved to generate a new reactive species after the solidification of Part A. The newly formed reactive species can further react with Part B in a secondary solidification. An exemplary system is described by Velankar, Pezos and Cooper, *Journal of Applied Polymer Science*, **62**, 1361-1376 (1996). Here, after UV-curing, the acrylate/methacrylate groups in the formed object are thermally cleaved to generate diisocyanate prepolymers that further react with blended chain-extender to give high molecular weight polyurethanes/polyureas within the original cured material or scaffold. Such systems are, in general, dual-hardening systems that employ blocked or reactive blocked prepolymers, as discussed in greater detail below. It may be noted that later work indicates that the thermal cleavage above is actually a displacement reaction of the chain extender (usually a diamine) with the hindered urea, giving the final polyurethanes/polyureas without generating isocyanate intermediates.

Methods of mixing components. In some embodiments, the components may be mixed in a continuous manner prior to being introduced to the printer build plate. This may be done using multi-barrel syringes and mixing nozzles. For example, Part A may comprise or consist of a UV-curable di(meth)acrylate resin, Part B may comprise or consist of a diisocyanate prepolymer and a polyol mixture. The polyol can be blended together in one barrel with Part A and remain unreacted. A second syringe barrel would contain the diisocyanate of Part B. In this manner, the material can be stored without worry of "Part B" solidifying prematurely. Additionally, when the resin is introduced to the printer in this fashion, a constant time is defined between mixing of all components and solidification of Part A.

Additional examples of "dual cure" polymerizable liquids (or "resins"), and methods that may be used in carrying out the present invention include, but are not limited to, those set forth in J. Rolland et al., *Method of Producing Polyurethane Three-Dimensional Objects from Materials having Multiple Mechanisms of Hardening*, PCT Publication No. WO 2015/200179 (published 30 Dec. 2015); J. Rolland et al., *Methods of Producing Three-Dimensional Objects from Materials Having Multiple Mechanisms of Hardening*, PCT Publication No. WO 2015/200173 (published 30 Dec. 2015); J. Rolland et al., *Three-Dimensional Objects Produced from Materials Having Multiple Mechanisms of Hardening*,

PCT Publication No. WO/2015/200189 (published 30 Dec. 2015); J. Rolland et al., *Polyurethane Resins Having Multiple Mechanisms of Hardening for Use in Producing Three-Dimensional Objects* published 30 Dec. 2015); and

J. Rolland et al., *Method of Producing Three-Dimensional Objects from Materials having Multiple Mechanisms of Hardening*, US Patent Application No. 14/977,822 (filed 22 Dec. 2015); J. Rolland et al., *Method of Producing Polyurethane Three-Dimensional Objects from Materials having Multiple Mechanisms of Hardening*, US Patent Application No. 14/977,876 (filed 22 Dec. 2015), J. Rolland et al., *Three-Dimensional Objects Produced from Materials having Multiple Mechanisms of Hardening*, US Patent Application No. 14/977,938 (filed 22 Dec. 2015), and J. Rolland et al., *Polyurethane Resins having Multiple Mechanisms of Hardening for Use in Producing Three-Dimensional Objects*, US Patent Application No. 14/977,974 (filed 22 Dec. 2015);

the disclosures of all of which are incorporated by reference herein in their entirety.

15 **13. Fabrication products.**

Three-dimensional products produced by the methods and processes of the present invention may be final, finished or substantially finished products, or may be intermediate products subject to further manufacturing steps such as surface treatment, laser cutting, electric discharge machining, etc., is intended. Intermediate products include products for which further additive manufacturing, in the same or a different apparatus, may be carried out). For example, a fault or cleavage line may be introduced deliberately into an ongoing “build” by disrupting, and then reinstating, the gradient of polymerization zone, to terminate one region of the finished product, or simply because a particular region of the finished product or “build” is less fragile than others.

25 Numerous different products can be made by the methods and apparatus of the present invention, including both large-scale models or prototypes, small custom products, miniature or microminiature products or devices, etc. Examples include, but are not limited to, medical devices and implantable medical devices such as stents, drug delivery depots, functional structures, microneedle arrays, fibers and rods such as waveguides, 30 micromechanical devices, microfluidic devices, etc.

Thus in some embodiments the product can have a height of from 0.1 or 1 millimeters up to 10 or 100 millimeters, or more, and/or a maximum width of from 0.1 or 1 millimeters up to 10 or 100 millimeters, or more. In other embodiments, the product can have a height of

from 10 or 100 nanometers up to 10 or 100 microns, or more, and/or a maximum width of from 10 or 100 nanometers up to 10 or 100 microns, or more. These are examples only: Maximum size and width depends on the architecture of the particular device and the resolution of the light source and can be adjusted depending upon the particular goal of the embodiment or article being fabricated.

In some embodiments, the ratio of height to width of the product is at least 2:1, 10:1, 50:1, or 100:1, or more, or a width to height ratio of 1:1, 10:1, 50:1, or 100:1, or more.

In some embodiments, the product has at least one, or a plurality of, pores or channels formed therein, as discussed further below.

The processes described herein can produce products with a variety of different properties. Hence in some embodiments the products are rigid; in other embodiments the products are flexible or resilient. In some embodiments, the products are a solid; in other embodiments, the products are a gel such as a hydrogel. In some embodiments, the products have a shape memory (that is, return substantially to a previous shape after being deformed, so long as they are not deformed to the point of structural failure). In some embodiments, the products are unitary (that is, formed of a single polymerizable liquid); in some embodiments, the products are composites (that is, formed of two or more different polymerizable liquids). Particular properties will be determined by factors such as the choice of polymerizable liquid(s) employed.

In some embodiments, the product or article made has at least one overhanging feature (or “overhang”), such as a bridging element between two supporting bodies, or a cantilevered element projecting from one substantially vertical support body. Because of the unidirectional, continuous nature of some embodiments of the present processes, the problem of fault or cleavage lines that form between layers when each layer is polymerized to substantial completion and a substantial time interval occurs before the next pattern is exposed, is substantially reduced. Hence, in some embodiments the methods are particularly advantageous in reducing, or eliminating, the number of support structures for such overhangs that are fabricated concurrently with the article.

14. Additional and alternate methods and apparatus.

Additional examples of apparatus, polymerizable liquids (or “resins”), and methods that may be used in carrying out the present invention include, but are not limited to, those set forth in J. DeSimone et al., *Three-Dimensional Printing Using Tiled Light Engines*, PCT

Publication No. WO/2015/195909 (published 23 Dec. 2015); J. DeSimone et al., *Three-Dimensional Printing Method Using Increased Light Intensity and Apparatus Therefore*, PCT Publication No. WO/2015/195920 (published 23 Dec. 2015), A. Ermoshkin et al., *Three-Dimensional Printing with Reciprocal Feeding of Polymerizable Liquid*, PCT Publication No. WO/2015/195924 (published 23 Dec. 2015); J. Rolland et al., *Method of Producing Polyurethane Three-Dimensional Objects from Materials having Multiple Mechanisms of Hardening*, PCT Publication No. WO 2015/200179 (published 30 Dec. 2015); J. Rolland et al., *Methods of Producing Three-Dimensional Objects from Materials Having Multiple Mechanisms of Hardening*, PCT Publication No. WO 2015/200173 (published 30 Dec. 2015); J. Rolland et al., *Three-Dimensional Objects Produced from Materials Having Multiple Mechanisms of Hardening*, PCT Publication No. WO/2015/200189 (published 30 Dec. 2015); J. Rolland et al., *Polyurethane Resins Having Multiple Mechanisms of Hardening for Use in Producing Three-Dimensional Objects* published 30 Dec. 2015); and J. DeSimone et al., *Methods and Apparatus for Continuous Liquid Interface Production with Rotation*, PCT Publication No. WO/2016/007495, the disclosures of which are incorporated by reference herein in their entirety.

In an alternate embodiment of the invention, the methods may be carried out with a method and apparatus as described in Hull, US Patent No. 5,236,637, at Figure 4, where the polymerizable liquid is floated on top of an immiscible liquid layer (said to be “non-wetting” therein). Here, the immiscible liquid layer serves as the build surface. If so implemented, the immiscible liquid (which may be aqueous or non-aqueous) preferably: (i) has a density greater than the polymerizable liquid, (ii) is immiscible with the polymerizable liquid, and (iii) is wettable with the polymerizable liquid. Ingredients such as surfactants, wetting agents, viscosity-enhancing agents, pigments, and particles may optionally be included in either or both of the polymerizable liquid or immiscible liquid.

While the present invention is preferably carried out by continuous liquid interphase polymerization, as described in detail above, in some embodiments alternate methods and apparatus for bottom-up three-dimension fabrication may be used, including layer-by-layer fabrication. Examples of such methods and apparatus include, but are not limited to, those described U.S. Patents No. 7,438,846 to John and U.S. Patent No. 8,110,135 to El-Siblani, and in U.S. Patent Application Publication Nos. 2013/0292862 to Joyce and 2013/0295212 to Chen et al. The disclosures of these patents and applications are incorporated by reference herein in their entirety.

The present invention is explained in greater detail in the following non-limiting Examples.

EXAMPLE 1

5 Continuous Fabrication with Intermittent Irradiation and Advancing

A process of the present invention is illustrated in **Figure 6**, where the vertical axis illustrates the movement of the carrier away from the build surface. In this embodiment, the vertical movement or advancing step (which can be achieved by driving either the carrier or the build surface, preferably the carrier), is continuous and unidirectional, and the irradiating step is carried out continuously. Polymerization of the article being fabricated occurs from a gradient of polymerization or active surface, and hence creation of “layer by layer” fault lines within the article is minimized.

An alternate embodiment of the present invention is illustrated in **Figure 7**. In this embodiment, the advancing step is carried out in a step-by-step manner, with pauses introduced between active advancing of the carrier and build surface away from one another. In addition, the irradiating step is carried out intermittently, in this case during the pauses in the advancing step. We find that, as long as the inhibitor of polymerization is supplied to the dead zone in an amount sufficient to maintain the dead zone and the adjacent gradient of polymerization or active surface during the pauses in irradiation and/or advancing, the gradient of polymerization is maintained, and the formation of layers within the article of manufacture is minimized or avoided. Stated differently, the polymerization is continuous, even though the irradiating and advancing steps are not. Sufficient inhibitor can be supplied by any of a variety of techniques, including but not limited to: utilizing a transparent member that is sufficiently permeable to the inhibitor, enriching the inhibitor (*e.g.*, feeding the inhibitor from an inhibitor-enriched and/or pressurized atmosphere), etc. In general, the more rapid the fabrication of the three-dimensional object (that is, the more rapid the cumulative rate of advancing), the more inhibitor will be required to maintain the dead zone and the adjacent gradient of polymerization.

EXAMPLE 2

30 Continuous Fabrication with Reciprocation During Advancing to Enhance Filling of Build Region with Polymerizable Liquid

A still further embodiment of the present invention is illustrated in **Figure 8**. As in Example 10 above, this embodiment, the advancing step is carried out in a step-by-step manner, with pauses introduced between active advancing of the carrier and build surface away from one another. Also as in Example 1 above, the irradiating step is carried out intermittently, again during the pauses in the advancing step. In this example, however, the ability to maintain the dead zone and gradient of polymerization during the pauses in advancing and irradiating is taken advantage of by introducing a vertical reciprocation during the pauses in irradiation.

We find that vertical reciprocation (driving the carrier and build surface away from and then back towards one another), particularly during pauses in irradiation, serves to enhance the filling of the build region with the polymerizable liquid, apparently by pulling polymerizable liquid into the build region. This is advantageous when larger areas are irradiated or larger parts are fabricated, and filling the central portion of the build region may be rate-limiting to an otherwise rapid fabrication.

Reciprocation in the vertical or Z axis can be carried out at any suitable speed in both directions (and the speed need not be the same in both directions), although it is preferred that the speed when reciprocating away is insufficient to cause the formation of gas bubbles in the build region.

While a single cycle of reciprocation is shown during each pause in irradiation in Figure 8, it will be appreciated that multiple cycles (which may be the same as or different from one another) may be introduced during each pause.

As in Example 1 above, as long as the inhibitor of polymerization is supplied to the dead zone in an amount sufficient to maintain the dead zone and the adjacent gradient of polymerization during the reciprocation, the gradient of polymerization is maintained, the formation of layers within the article of manufacture is minimized or avoided, and the polymerization/fabrication remains continuous, even though the irradiating and advancing steps are not.

EXAMPLE 3

Acceleration during Reciprocation Upstroke and Deceleration during Reciprocation Downstroke to Enhance Part Quality

We observe that there is a limiting speed of upstroke, and corresponding downstroke, which if exceeded causes a deterioration of quality of the part or object being fabricated

(possibly due to degradation of soft regions within the gradient of polymerization caused by lateral shear forces a resin flow). To reduce these shear forces and/or enhance the quality of the part being fabricated, we introduce variable rates within the upstroke and downstroke, with gradual acceleration occurring during the upstroke and gradual deceleration occurring during the downstroke, as schematically illustrated in **Figure 9**.

EXAMPLE 4

Fabrication in Multiple Zones

Figure 10 schematically illustrates the movement of the carrier (z) over time (t) in the course of fabricating a three-dimensional object by methods as described above, through a first base (or “adhesion”) zone, an optional second transition zone, and a third body zone. The overall process of forming the three-dimensional object is thus divided into three (or two) immediately sequential segments or zones. The zones are preferably carried out in a continuous sequence without pause substantial delay (*e.g.*, greater than 5 or 10 seconds) between the three zones, preferably so that the gradient of polymerization is not disrupted between the zones.

The first base (or “adhesion”) zone includes an initial light or irradiation exposure at a higher dose (longer duration and/or greater intensity) than used in the subsequent transition and/or body zones. This is to obviate the problem of the carrier not being perfectly aligned with the build surface, and/or the problem of variation in the positioning of the carrier from the build surface, at the start of the process, by insuring that the resin is securely polymerized to the carrier. Note an optional reciprocation step (for initial distributing or pumping of the polymerizable liquid in or into the build region) is shown before the carrier is positioned in its initial, start, position. Note that a release layer (not shown) such as a soluble release layer may still be included between the carrier and the initial polymerized material, if desired. In general, a small or minor portion of the three-dimensional object is produced during this base zone (*e.g.*, less than 1, 2 or 5 percent by volume). Similarly, the duration of this base zone is, in general, a small or minor portion of the sum of the durations of the base zone, the optional transition zone, and the body zone (*e.g.*, less than 1, 2 or 5 percent).

Immediately following the first base zone of the process, there is optionally (but preferably) a transition zone. In this embodiment, the duration and/or intensity of the illumination is less, and the displacement of the oscillatory step less, compared to that employed in the base zone as described above. The transition zone may (in the illustrated

embodiment) proceed through from 2 or 5, up to 50 or more oscillatory steps and their corresponding illuminations. In general, an intermediate portion (greater than that formed during the base zone, but less than that formed of during the body zone), of the three dimensional object is produced during the transition zone (*e.g.*, from 1, 2 or 5 percent to 10, 20 or 40 percent by volume). Similarly, the duration of this transition zone is, in general, greater than that of the base zone, but less than that of the body zone (*e.g.*, a duration of from 1, 2 or 5 percent to 10, 20 or 40 percent that of the sum of the durations of the base zone, the transition zone, and the body zone (*e.g.*, less than 1, 2 or 5 percent).

Immediately following the transition zone of the process (or, if no transition zone is included, immediately following the base zone of the process), there is a body zone, during which the remainder of the three-dimensional object is formed. In the illustrated embodiment, the body zone is carried out with illumination at a lower dose than the base zone (and, if present, preferably at a lower dose than that in the transition zone), and the reciprocation steps are (optionally but in some embodiments preferably) carried out at a smaller displacement than that in the base zone (and, if present, optionally but preferably at a lower displacement than in the transition zone). In general, a major portion, typically greater than 60, 80, or 90 percent by volume, of the three-dimensional object is produced during the transition zone. Similarly, the duration of this body zone is, in general, greater than that of the base zone and/or transition zone (*e.g.*, a duration of at least 60, 80, or 90 percent that of the sum of the durations of the base zone, the transition zone, and the body zone).

Note that, in this example, the multiple zones are illustrated in connection with an oscillating mode of fabrication, but the multiple zone fabrication technique described herein may also be implemented with other modes of fabrication as illustrated further in the examples below (with the transition zone illustrated as included, but again being optional).

EXAMPLE 5

Fabrication with Intermittent (or “Strobe”) Illumination

The purpose of a “strobe” mode of operation is to reduce the amount of time that the light or radiation source is on or active (*e.g.*, to not more than 80, 70, 60, 50, 40, or 30 percent of the total time required to complete the fabrication of the three-dimensional object), and increase the intensity thereof (as compared to the intensity required when advancing is carried out at the same cumulative rate of speed without such reduced time of active illumination or radiation), so that the overall dosage of light or radiation otherwise remains

substantially the same. This allows more time for resin to flow into the build region without trying to cure it at the same time. The strobe mode technique can be applied to any of the existing general modes of operation described herein above, including continuous, stepped, and oscillatory modes, as discussed further below.

5 **Figure 11A** schematically illustrates one embodiment of **continuous mode**. In the conventional continuous mode, an image is projected and the carrier starts to move upwards. The image is changed at intervals to represent the cross section of the three-dimensional object being produced corresponding to the height of the build platform. The speed of the motion of the build platform can vary for a number of reasons. As illustrated, often there is a
10 base zone where the primary goal is to adhere the object to the build platform, a body zone which has a speed which is suitable for the whole object being produced, and a transition zone which is a gradual transition from the speed and/or dosages of the base zone to the speeds and/or dosages of the body zone. Note that cure is still carried out so that a gradient of polymerization, which prevents the formation of layer-by-layer fault lines, in the
15 polymerizable liquid in the build region, is preferably retained, and with the carrier (or growing object) remaining in liquid contact with the polymerizable liquid, as discussed above.

Figure 11B schematically illustrates one embodiment of **strobe continuous mode**. In strobe continuous the light intensity is increased but the image is projected in short flashes or
20 intermittent segments. The increased intensity allows the resin to cure more quickly so that the amount of flow during cure is minimal. The time between flashes lets resin flow without being cured at the same time. This can reduce problems caused by trying to cure moving resin, such as pitting.

 In addition, the reduced duty cycle on the light source which is achieved in strobe
25 mode can allow for use of increased intermittent power. For example: If the intensity for the conventional continuous mode was $5\text{mW}/\text{cm}^2$ the intensity could be doubled to $10\text{mW}/\text{cm}^2$ and the time that the image is projected could be reduced to half of the time, or the intensity could be increased 5-fold to $25\text{mW}/\text{cm}^2$ and the time could be reduced to $1/5^{\text{th}}$ of the previous light on time.

30 **Figure 12A** schematically illustrates one embodiment of **stepped mode**: In the conventional stepped mode an image is projected while the build platform is stationary (or moving slowly as compared to more rapid movement in between illumination). When one height increment is sufficiently exposed the image is turned off and the build platform is

moved upwards by some increment. This motion can be at one speed or the speed can vary such as by accelerating from a slow speed when the thickness of uncured resin is thin to faster as the thickness of the uncured resin is thicker. Once the build platform is in the new position the image of the next cross section is projected to sufficiently expose the next height increment.

Figure 12B schematically illustrates one embodiment of **strobe stepped mode**: In the strobe stepped mode the light intensity is increased and the amount of time that the image is projected is reduced. This allows more time for resin flow so the overall speed of the print can be reduced or the speed of movement can be reduced. For example: If the intensity for the conventional stepped mode was 5mW/cm^2 and the build platform moves in increments of 100um in 1 second and the image is projected for 1 second the intensity could be doubled to 10mW/cm^2 , the time that the image is projected could be reduced to 0.5 seconds, and the speed of movement could be reduced to 50um/second, or the time that the stage is moving could be reduced to 0.5 seconds. The increased intensity could be as much as 5 fold or more allowing the time allotted for image projection to be reduced to $1/5^{\text{th}}$ or less.

Figure 13A schematically illustrates one embodiment of **oscillatory mode**: In the oscillatory mode an image is again projected while the build platform is stationary (or moving slowly as compared to more rapid movement in-between illuminations). When one height increment is cured the image is turned off and the build platform is moved upwards to pull additional resin into the build zone and then moved back down to the next height increment above the last cured height. This motion can be at one speed or the speed can vary such as by accelerating from a slow speed when the thickness of uncured resin is thin to faster as the thickness of the uncured resin is thicker. Once the build platform is in the new position the image of the next cross section is projected to cure the next height increment.

Figure 13B illustrates one embodiment of **strobe oscillatory mode**. In the strobe oscillatory mode the light intensity is increased and the amount of time that the image is projected is reduced. This allows more time for resin flow so the overall speed of the print can be reduced or the speed of movement can be reduced. For example: If the intensity for the conventional oscillatory mode was 5mW/cm^2 and the build platform moves up by 1mm and back down to an increment of 100um above the previous height in 1 second and the image is projected for 1 second the intensity could be doubled to 10mW/cm^2 , the time that the image is projected could be reduced to 0.5 seconds, and the speed of movement could be reduced to by half or the time that the stage is moving could be reduced to 0.5 seconds. The

increased intensity could be as much as 5 fold or more allowing the time allotted for image projection to be reduced to 1/5th or less. Segment "A" of Figure 13 is discussed further below.

Figure 14A illustrates a segment of a fabrication method operated in another embodiment of strobe oscillatory mode. In this embodiment, the duration of the segment during which the carrier is static is shortened to close that of the duration of the strobe illumination, so that the duration of the oscillatory segment may—if desired—be lengthened without changing the cumulative rate of advance and the speed of fabrication.

Figure 14B illustrates a segment of another embodiment of strobe oscillatory mode, similar to that of Figure 14A, except that the carrier is now advancing during the illumination segment (relatively slowly, as compared to the upstroke of the oscillatory segment).

EXAMPLE 6

Varying of Process Parameters During Fabrication

In the methods of the Examples above, the operating conditions during the body zone are shown as constant throughout that zone. However, various parameters can be altered or modified in the course of the body zone or segment, as discussed further below.

A primary reason for altering a parameter during production would be variations in the cross section geometry of the three-dimensional object; that is, smaller (easier to fill), and larger (harder to fill) segments or portions of the same three-dimensional object. For easier to fill segments (*e.g.*, 1-5mm diameter equivalents), the speed of upwards movement could be quick (up to 50-1000m/hr) and/or the pump height could be minimal (*e.g.*, as little at 100 to 300um). For larger cross sectional segments (*e.g.*, 5-500mm diameter equivalents) the speed of upward movement can be slower (*e.g.*, 1-50 mm/hr) and/or the pump height can be larger (*e.g.*, 500 to 5000um). Particular parameters will, of course, vary depending on factors such as illumination intensity, the particular polymerizable liquid (including constituents thereof such as dye and filler concentrations), the particular build surface employed, etc.

In some embodiments, the overall light dosage (determined by time and intensity) may be reduced as the "bulk" of the cross section being illuminated increases. Said another way, small points of light may need higher per unit dosage than larger areas of light. Without wishing to be bound to any specific theory, this may relate to the chemical kinematics of the polymerizable liquid. This effect could cause us to *increase* the overall light dosage for *smaller* cross sectional diameter equivalents.

In some embodiments, vary the thickness of each height increment between steps or pumps can be varied. This could be to increase speed with decreased resolution requirements (that is, fabricating a portion that requires less precision or permits more variability, versus a portion of the object that requires greater precision or requires more precise or narrow tolerances). For example, one could change from 100um increments to 200um or 400um increments and group all the curing for the increased thickness into one time period. This time period may be shorter, the same or longer than the combined time for the equivalent smaller increments.

In some embodiments, the light dosage (time and/or intensity) delivered could be varied in particular cross sections (vertical regions of the object) or even in different areas within the same cross section or vertical region. This could be to vary the stiffness or density of particular geometries. This can, for example, be achieved by changing the dosage at different height increments, or changing the grayscale percentage of different zones of each height increment illumination.

Examples of body portion fabrication through multiple zones are given in **Figures 15A-19**.

Figure 15A is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 13A, except that the body segment is fabricated in two contiguous segments, with the first segment carried out in an oscillatory operating mode, and the second segment carried out in a continuous operating mode. **Figure 16A** is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 11A, except that the body segment is fabricated in three contiguous segments, with the first and third segments carried out in a continuous operating mode, and the second segment carried out in oscillatory operating mode. **Figure 17A** is a schematic illustration of the fabrication of a three-dimensional object similar to Figure 16A, except that the base zone, transition zone, and first segment of the body zone are carried out in a strobe continuous operating mode, the second segment of the body zone is fabricated in an oscillatory operating mode, and the third segment of the body zone is fabricated in a continuous operating mode.

Figure 15B, 16B, and 17B are similar to the foregoing, except that stepped or step-wise mode is used in place of oscillatory, or "reciprocal" mode. In general, reciprocal or oscillatory mode is preferred over stepped mode, with reciprocation being achieved entirely through motion of the carrier, or the combined motion of the carrier and a flexible, or movable, build surface.

Figure 18A is a schematic illustration of the fabrication of a three-dimensional object similar to **Figure 11A**, except that light intensity is varied in the course of fabricating the base and transition zones, and both light intensity and rate of advancing are varied in the course of fabricating the body zone. **Figure 18B** is a schematic illustration of the fabrication of a three-dimensional object similar to **Figure 17A**, except that light is interrupted in an intermittent fashion (dashed line representing light intensity during interrupted segments is for comparison to **Figure 17A** only).

Figure 19 is a schematic illustration of the fabrication of a three-dimensional object similar to **Figure 11A**, except that the mode of operation during fabrication of the body segment is changed multiple times for continuous, to reciprocal, and back. This may be employed not only to accommodate changes in geometry of the three-dimensional object during fabrication, but a relatively constant geometry where the part is hollow, to facilitate replenishment of polymerizable liquid in the build region.

Figure 20 schematically illustrates parameters that may be varied within a reciprocal (also referred to as “oscillatory”) operating mode (solid line throughout) or a step operating mode (solid line horizontal lines and dashed lines). Note the parameters that may be varied in these two modes are similar, except for the absence of a pump height parameter in step mode.

EXAMPLE 7

Varying of Slice Thickness During Fabrication

In the methods of the present invention, slice thickness may be held constant or varied in any of the operating modes. Examples are given in **Figures 21A to 21F**, where horizontal dashed lines represent the transition from each contiguous slice (corresponding to different exposure or illumination frames or patterns) during the formation of the three-dimensional object.

Figure 21A schematically illustrates a method of the invention carried out in a continuous operating mode, with constant slice thickness and constant carrier speed, while **Figure 21B** schematically illustrates a method of the invention carried out in a continuous operating mode, with variable slice thickness with constant carrier speed. In both cases, illumination or exposure is continuous, with slices changing over time. Slice thickness could likewise be varied in an intermittent exposure mode of operation (including strobe mode).

Figure 21C schematically illustrates a method of the invention carried out in a continuous operating mode, with constant slice thickness and variable carrier speed, while

Figure 21D schematically illustrates a method of the invention carried out in continuous operating mode, mode with variable slice thickness and variable carrier speed. Again in both cases, illumination or exposure is continuous with the slices changing over time, but slice thickness could likewise be varied in an intermittent exposure mode of operation.

5 **Figure 21E** schematically illustrates a method of the invention carried out in reciprocal operating mode, with constant slice thickness, while **Figure 21F** schematically illustrates a method of the invention carried out in reciprocal operating mode, with variable slice thickness. Bold diagonal hash patterns during the exposure periods are to emphasize slice thickness, and variability thereof in Figure 21F. In both cases, a step-wise mode of
10 operation could be used in place of a reciprocal mode of operation (see, for example, Figure 20).

The foregoing is illustrative of the present invention, and is not to be construed as limiting thereof. The invention is defined by the following claims, with equivalents of the claims to be included therein.

WE CLAIM:

1. In a method of forming the body portion of a three-dimensional object from a polymerizable liquid by the process of continuous liquid interface printing, the body portion having a plurality of contiguous segments, and the process including advancing a carrier for the object away from a build surface while irradiating a build region between the carrier and build surface in a pattern of advancing and irradiating defined by an operating mode, the improvement comprising:

changing operating mode at least once during the formation of said body portion for different contiguous segments of said body portion.

2. The method of claim 1, comprising:

providing a carrier and an optically transparent member having a build surface, said carrier and said build surface defining a build region therebetween,

wherein said body portion is formed by: (i) filling said build region with a polymerizable liquid, (ii) continuously or intermittently irradiating said build region with light through said optically transparent member, and (iii) continuously or intermittently advancing (e.g., sequentially or concurrently with said irradiating step) said carrier away from said build surface to thereby form from said polymerizable liquid a solid polymer body portion of said object.

3. The method of claim 2, wherein said filling step, said irradiating step, and said advancing step are carried out while also concurrently: (i) continuously maintaining a dead zone of polymerizable liquid in contact with said build surface, and (ii) continuously maintaining a gradient of polymerization zone or active surface between said dead zone and said solid polymer and in contact with each thereof, said gradient of polymerization zone comprising said polymerizable liquid in partially cured form.

4. The method of claim 1 to 3, wherein said operating mode is selected from the group consisting of:

- (a) continuous advancing with continuous exposure;
- (b) continuous advancing with intermittent exposure;
- (c) step-wise advancing with intermittent exposure; and
- (d) reciprocal advancing with intermittent exposure.

5. The method of claim 4, wherein said intermittent exposure is a strobe mode exposure.

6. The method of claim 4 or 5, wherein said reciprocal advancing is carried out through carrier motion, or by combination of carrier and window motion (e.g., as imparted by a flexible window).

7. The method of claim 1 to 6, wherein said step of changing operating modes includes the step of feathering (or gradually transitioning) from one operating mode to a subsequent operating mode.

8. The method of claim 1 to 7, wherein said step of changing operating modes is carried out sequentially at least five or ten times during the formation of said body portion.

9. The method of claim 1 to 8, further comprising changing at least one parameter of an operating mode at least once during formation of said body portion.

10. The method of claim 9, wherein said at least one parameter is slice thickness, frequency of irradiating, intensity of irradiating, duration of irradiating, duty cycle of irradiating, rate of advancing, lead time prior to irradiating, lag time following irradiating, step height, pump height, step or pump duration, or frequency of step-wise or reciprocal advancing.

11. In a method of forming the body portion of a three-dimensional object from a polymerizable liquid by the process of continuous liquid interface printing, the process including advancing a carrier for the object away from a build surface while irradiating a build region between the carrier and build surface in a pattern of advancing and irradiating defined by an operating mode, with the body portion having a plurality of contiguous segments, the improvement comprising:

changing at least one parameter of an operating mode at least once during the formation of said body portion for fabrication of different contiguous segments of said body portion, where said operating mode is: (i) continuous advancing with intermittent exposure;

(ii) step-wise advancing with intermittent exposure; or (iii) reciprocal advancing with intermittent exposure.

12. The method of claim 11, comprising:

providing a carrier and an optically transparent member having a build surface, said carrier and said build surface defining a build region therebetween,

wherein said body segment is formed by: (i) filling said build region with a polymerizable liquid, (ii) continuously or intermittently irradiating said build region with light through said optically transparent member, and (iii) continuously or intermittently advancing (e.g., sequentially or concurrently with said irradiating step) said carrier away from said build surface at a third cumulative rate of advance, to thereby form from said polymerizable liquid a body segment of said object between said transition segment and said build surface.

13. The method of claim 11 or 12, wherein said filling step, said irradiating step, and said advancing step are carried out while also concurrently: (i) continuously maintaining a dead zone of polymerizable liquid in contact with said build surface, and (ii) continuously maintaining a gradient of polymerization zone or active surface between said dead zone and said solid polymer and in contact with each thereof, said gradient of polymerization zone comprising said polymerizable liquid in partially cured form.

14. The method of claim 1 to 13, wherein said at least one parameter is slice thickness, frequency of irradiating, intensity of irradiating, duration of irradiating, duty cycle of irradiating, rate of advancing, lead time prior to irradiating, lag time following irradiating, step height, pump height, step or pump duration, or frequency of step-wise or reciprocal advancing.

15. The method of claim 11 to 13, wherein said changing at least one parameter comprises concurrently or simultaneously changing at least two or three parameters.

16. The method of claim 11 to 15, wherein said step of changing at least one operating parameter is carried out sequentially at least five or ten times during the formation of said body portion.

17. The method of any preceding claim, wherein said plurality of contiguous segments are geometrically distinct from one another.

18. The method of any preceding claim, wherein said dead zone, and/or said gradient of polymerization or said active surface, are maintained through said changing steps.

19. The method of any preceding claim, wherein said build surface is fixed and stationary in the lateral (*e.g.*, X and Y) dimensions.

20. The method of any preceding claim, wherein said advancing is carried out at a cumulative rate (*e.g.*, through all zones) of at least 0.1, 1, 10, 100 or 1000 microns per second.

21. The method of any preceding claim, wherein said optically transparent member comprises a semipermeable member, and said continuously maintaining a dead zone is carried out by feeding an inhibitor of polymerization through said optically transparent member in an amount sufficient to maintain said dead zone and said gradient of polymerization.

22. The method of any preceding claim, wherein said optically transparent member is comprised of a semipermeable polymer (*e.g.*, a fluoropolymer).

23. The method of any preceding claim, wherein said gradient of polymerization zone and said dead zone together have a thickness of from 1 to 1000 microns.

24. The method of any preceding claim, wherein said gradient of polymerization zone is maintained for a time of at least 5, 10, 20, or 30 seconds, or at least 1 or 2 minutes.

25. The method of any preceding claim, further comprising the step of heating said polymerizable liquid to reduce the viscosity thereof in said build region.

26. The method of any preceding claim, wherein said irradiating step is carried out by maskless photolithography.

27. The method of any preceding claim, wherein:
said polymerizable liquid comprises a free radical polymerizable liquid and said inhibitor comprises oxygen; or
said polymerizable liquid comprises an acid-catalyzed or cationically polymerizable liquid, and said inhibitor comprises a base.

28. A method of any preceding claim, wherein:
said polymerizable liquid comprises a mixture of (i) a light polymerizable liquid first component, and (ii) a second solidifiable component that is different from said first component,
said method further comprising:
concurrently with or following the forming of said three dimensional object, solidifying and/or curing said second solidifiable component in said three-dimensional object.

29. The method of claim 28, wherein said second component comprises a polymerizable liquid solubilized in or suspended in said first component.

30. The method of claim 28, wherein said second component comprises:
(i) a polymerizable solid suspended in said first component;
(ii) a polymerizable solid solubilized in said first component; or
(iii) a polymer solubilized in said first component.

31. The method of claim 28, wherein said three-dimensional intermediate is collapsible or compressible.

32. The method of claim 28, wherein said three-dimensional object comprises a polymer blend, interpenetrating polymer network, semi-interpenetrating polymer network, or sequential interpenetrating polymer network formed from said first component and said second component.

33. The method of claim 28, wherein said polymerizable liquid comprises:
from 1 or 10 percent by weight to 40, 90 or 99 percent by weight of said first component; and
from 1, 10 or 60 percent by weight to 90 or 99 percent by weight of said second component.

34. The method of claim 28, wherein said solidifying and/or curing step (*d*) is carried out concurrently with said irradiating step (*c*) and:

- (i) said solidifying and/or curing step is carried out by precipitation; or
- (ii) said irradiating step generates heat from the polymerization of said first component in an amount sufficient to thermally solidify or polymerize said second component.

35. The method of claim 28, wherein said solidifying and/or curing step (*d*) is carried out subsequent to said irradiating step (*c*) and is carried out by:

- (i) heating said second solidifiable component;
- (ii) irradiating said second solidifiable component with light at a wavelength different from that of the light in said irradiating step (*c*);
- (iii) contacting said second polymerizable component to water; and/or
- (iv) contacting said second polymerizable component to a catalyst.

36. The method of claim 28, wherein: said second component comprises the precursors to a polyurethane, polyurea, or copolymer thereof, a silicone resin, an epoxy resin, a cyanate ester resin, or a natural rubber; and said solidifying step is carried out by heating and/or microwave irradiating.

37. The method of claim 28, wherein:
said second component comprises the precursors to a polyurethane, polyurea, or copolymer thereof, and
said solidifying and/or curing step is carried out by contacting said second component to water.

38. The method of claim 28, wherein:

said solidifying and/or curing step (d) is carried out subsequent to said irradiating step; and

said solidifying and/or curing step (d) is carried out under conditions in which said solid polymer scaffold degrades and forms a constituent necessary for the polymerization of said second component.

39. The method of claim 28, wherein:

said second component comprises precursors to a polyurethane, polyurea, or copolymer thereof, a silicone resin, a ring-opening metathesis polymerization resin, or a click chemistry resin, a cyanate ester resin, and

said solidifying and/or curing step is carried out by contacting said second component to a polymerization catalyst.

40. The method of claim 28, wherein said polymerizable liquid comprises a first component (Part A) and at least one additional component (Part B),

said first component comprising monomers and/or prepolymers that can be polymerized by exposure to actinic radiation or light;

said second component solidifiable on contacting to heat, water, water vapor, light at a different wavelength than that at which said first component is polymerized, catalysts, evaporation of a solvent from the polymerizable liquid, exposure to microwave irradiation, and combinations thereof.

41. The method of claim 40, said first component monomers and/or prepolymers comprising reactive end groups selected from the group consisting of acrylates, methacrylates, α -olefins, N-vinyls, acrylamides, methacrylamides, styrenics, epoxides, thiols, 1,3-dienes, vinyl halides, acrylonitriles, vinyl esters, maleimides, and vinyl ethers.

42. The method of claim 40, said additional component comprising monomers and/or prepolymers comprising reactive end groups selected from the group consisting of: epoxy/amine, epoxy/hydroxyl, oxetane/amine, oxetane/alcohol, isocyanate/hydroxyl, isocyanate/amine, isocyanate/carboxylic acid, cyanate ester, anhydride/amine, amine/carboxylic acid, amine/ester, hydroxyl/carboxylic acid, hydroxyl/acid chloride, amine/acid chloride, vinyl/Si-H, Si-Cl/hydroxyl, Si-Cl/amine, hydroxyl/aldehyde,

amine/aldehyde, hydroxymethyl or alkoxymethyl amide/alcohol, aminoplast, alkyne/azide, click chemistry reactive groups, alkene/sulfur, alkene/thiol, alkyne/thiol, hydroxyl/halide, isocyanate/water, Si-OH/hydroxyl, Si-OH/water, Si-OH/Si-H, Si-OH/Si-OH, perfluorovinyl, diene/dienophiles, olefin metathesis polymerization groups, olefin polymerization groups for Ziegler-Natta catalysis, and ring-opening polymerization groups and mixtures thereof.

43. The method of claim 28, wherein said three-dimensional object comprises an interpenetrating polymer network (IPN), said interpenetrating polymer network comprising a sol-gel composition, a hydrophobic-hydrophilic IPN, a phenolic resin, a polyimide, a conductive polymer, a natural product-based IPN, a sequential IPN, a polyolefin, or a combination thereof.

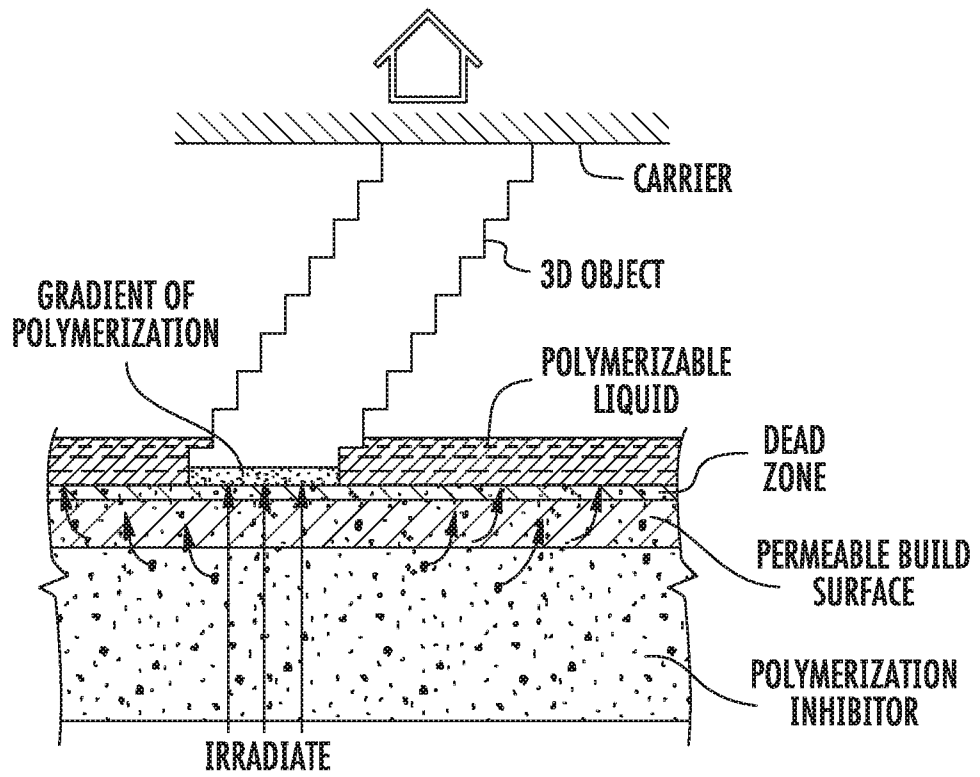


FIG. 1

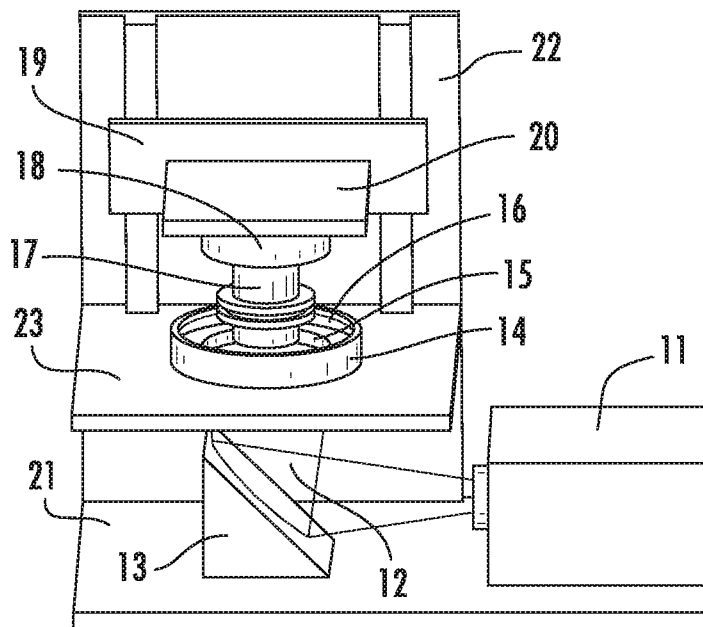


FIG. 2

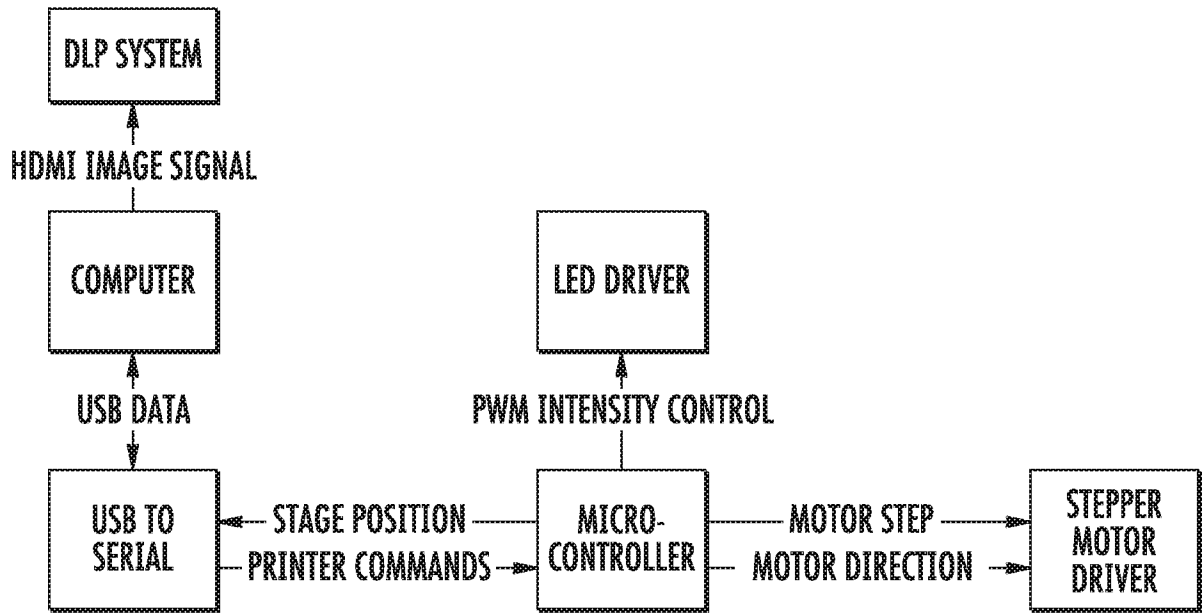


FIG. 3

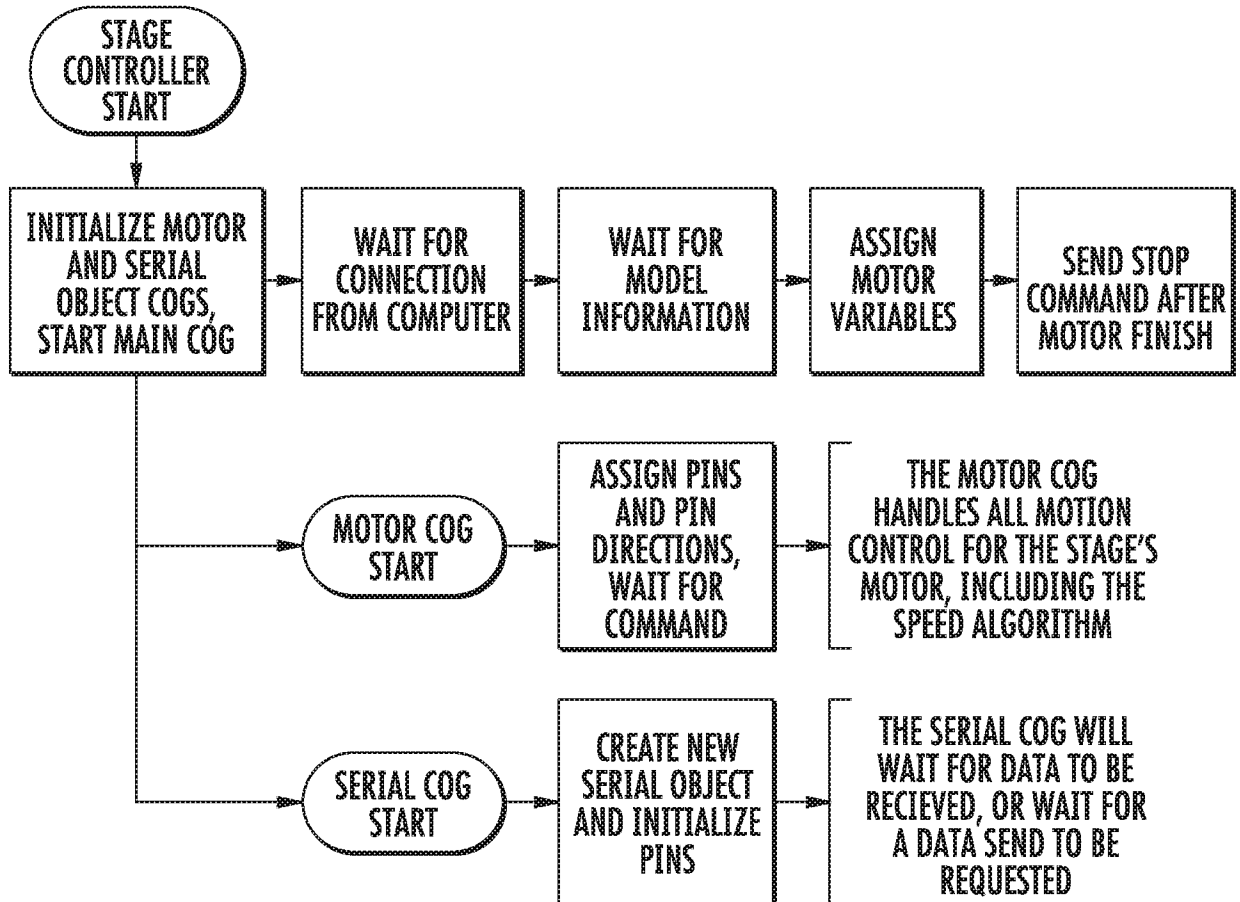


FIG. 4

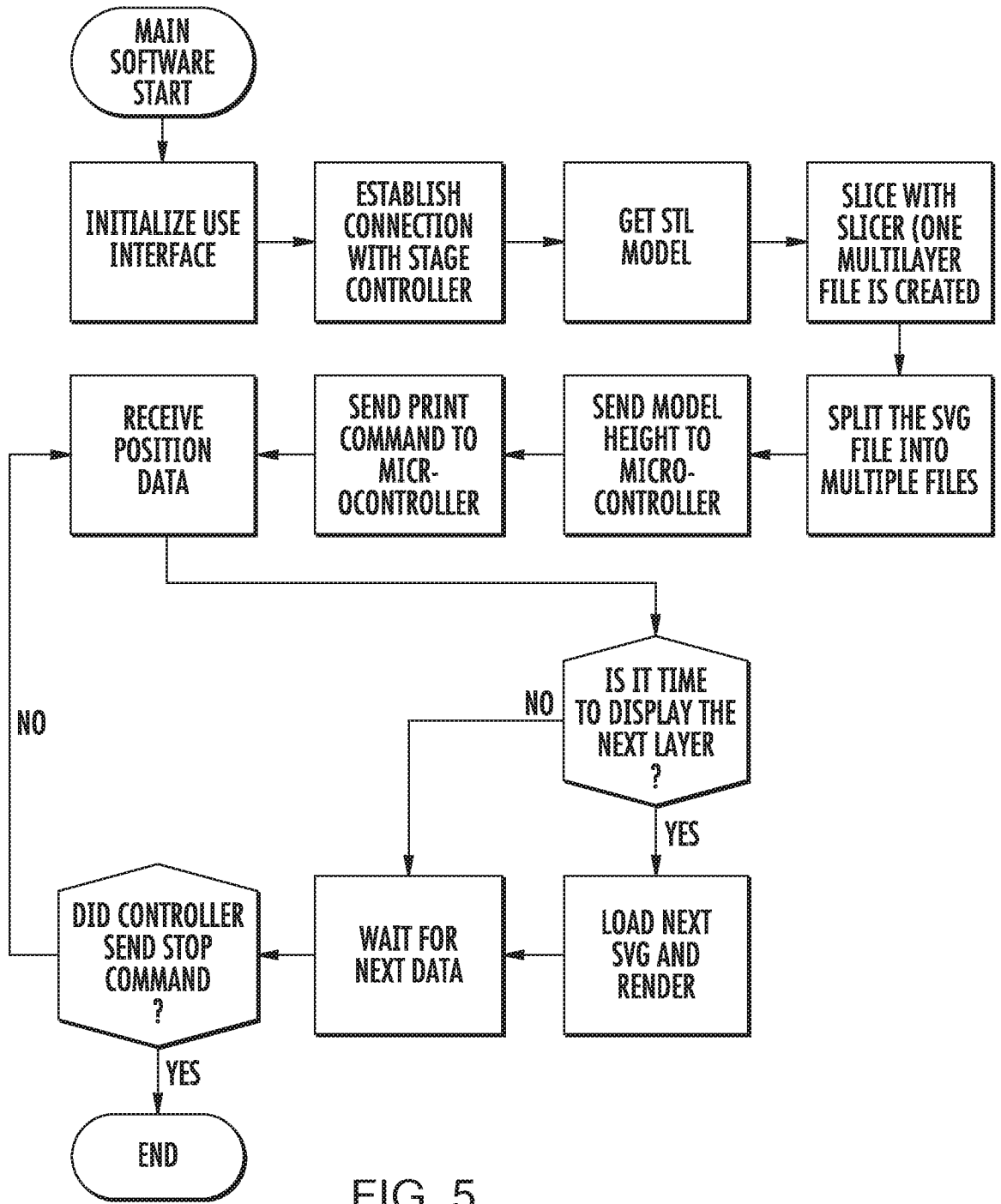


FIG. 5

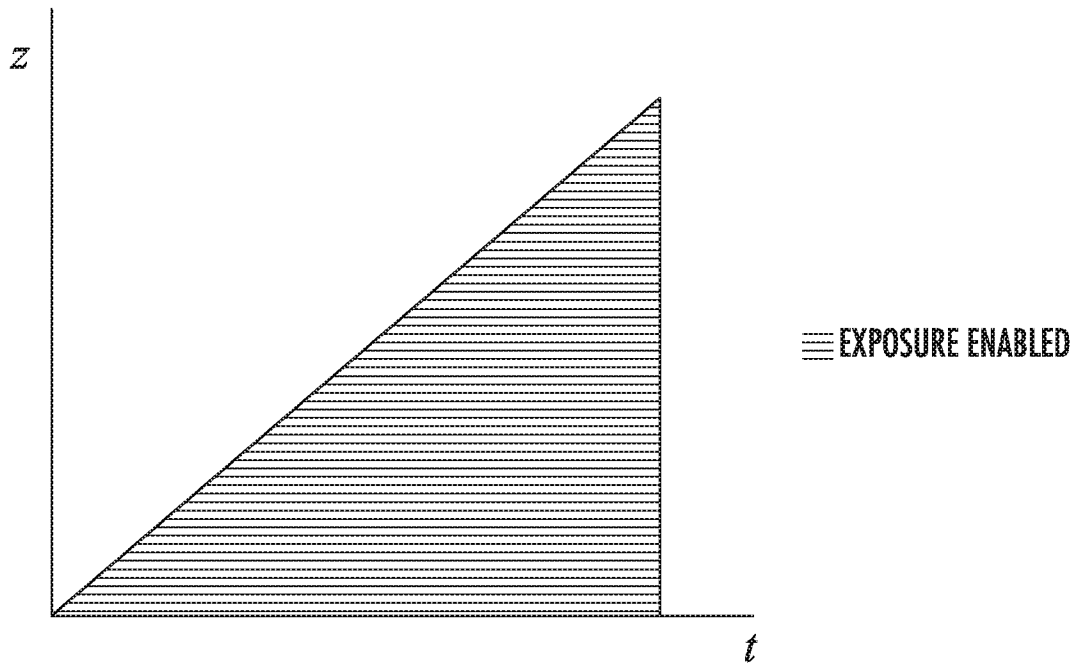


FIG. 6

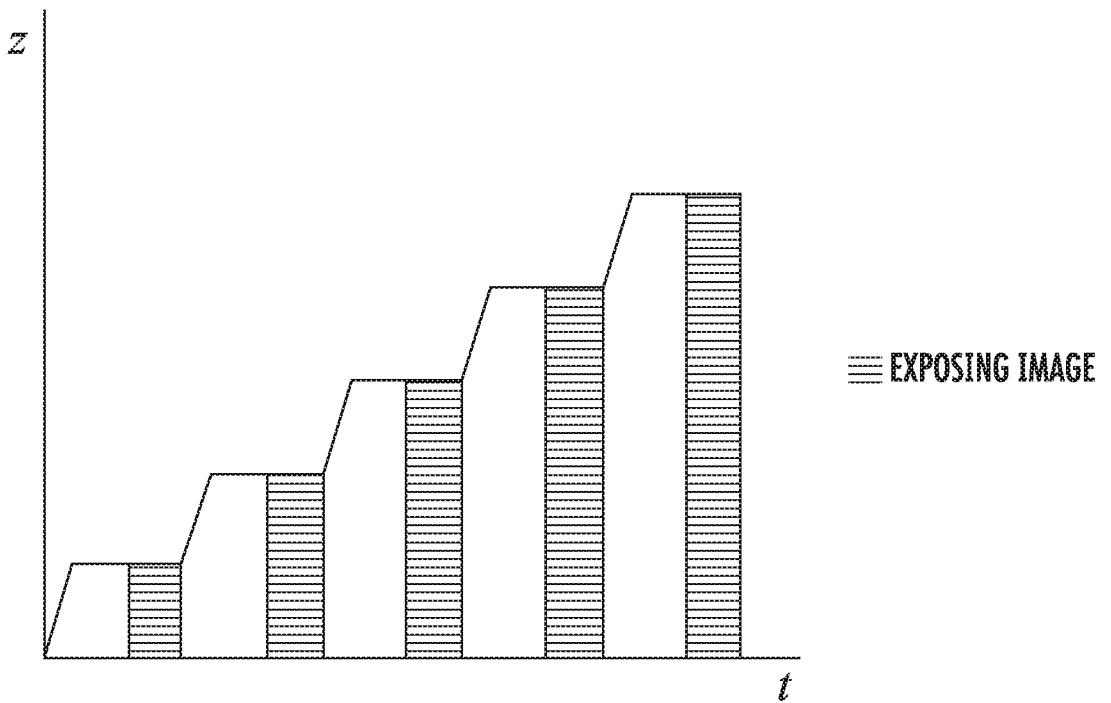


FIG. 7

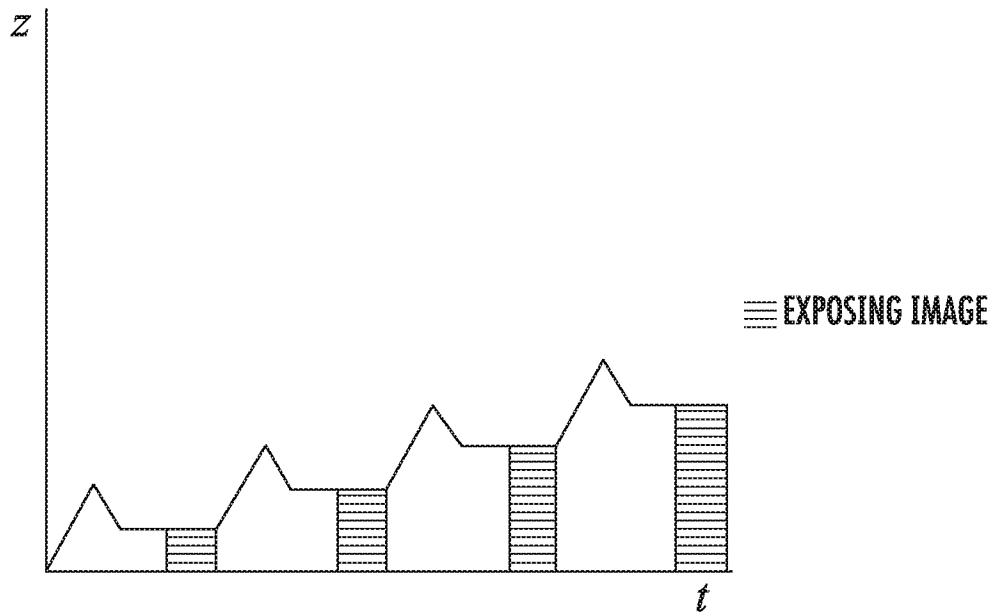


FIG. 8

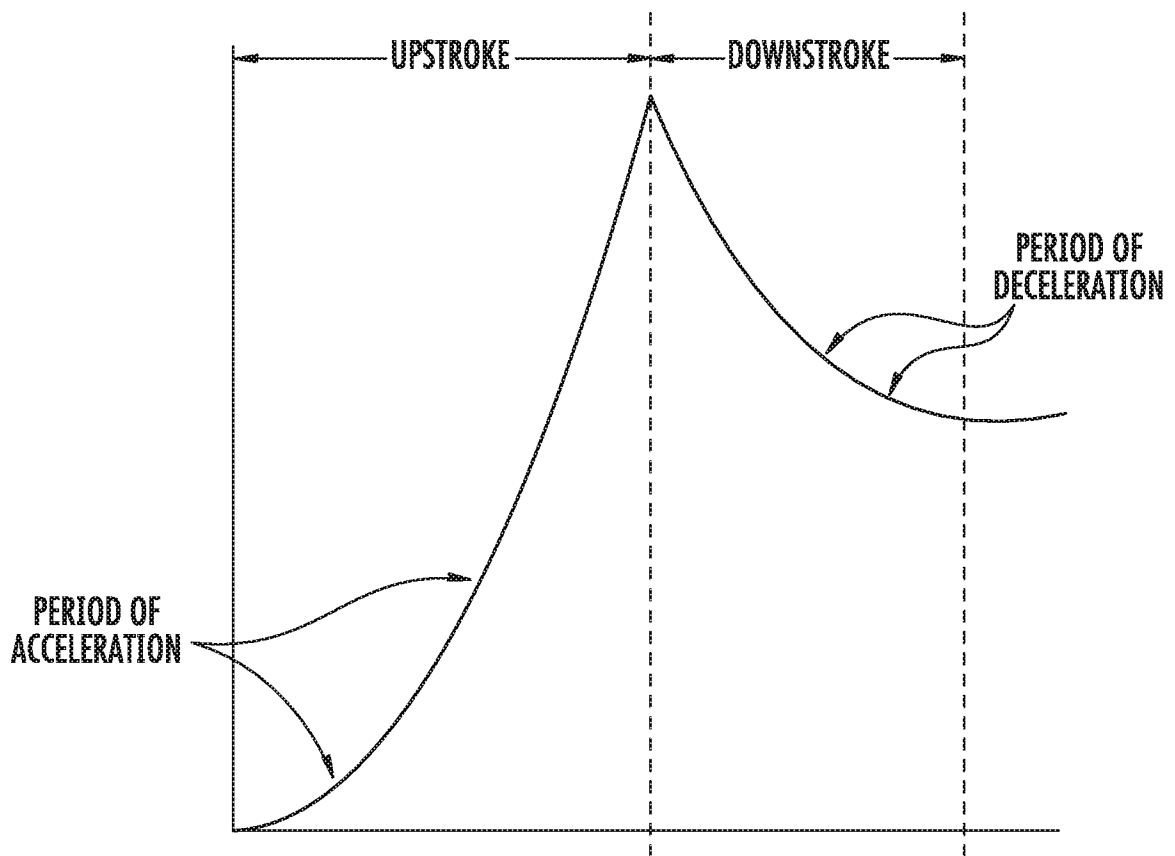


FIG. 9

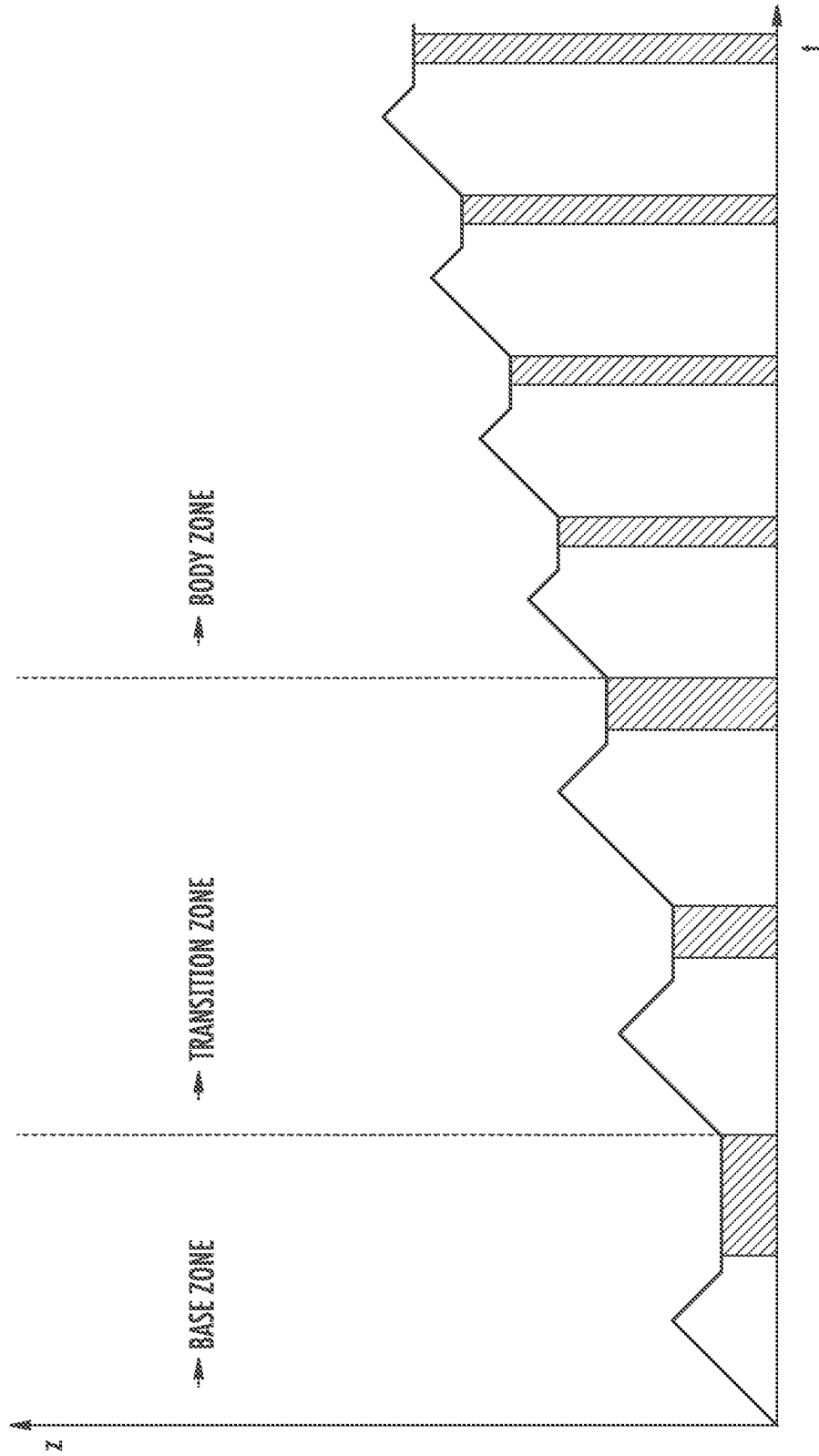


FIG. 10

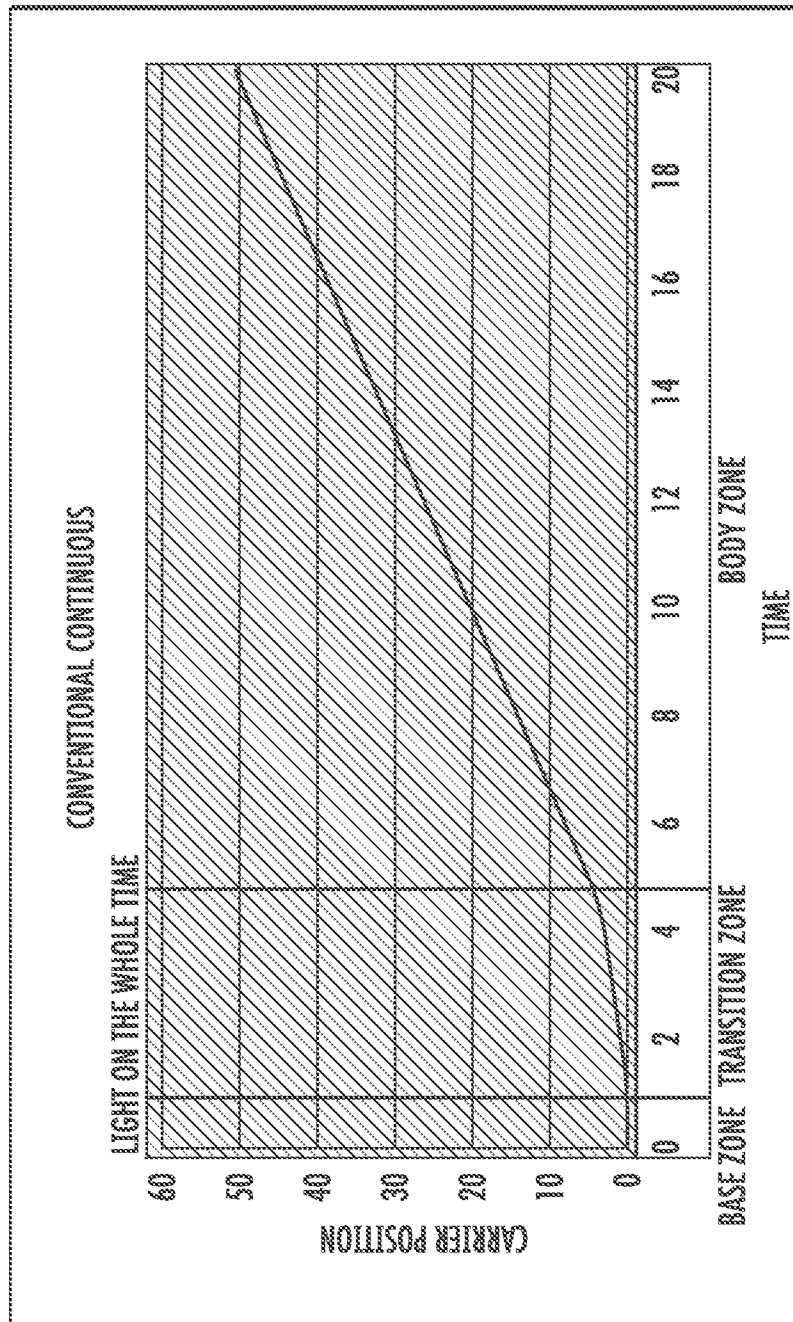


FIG. 11A

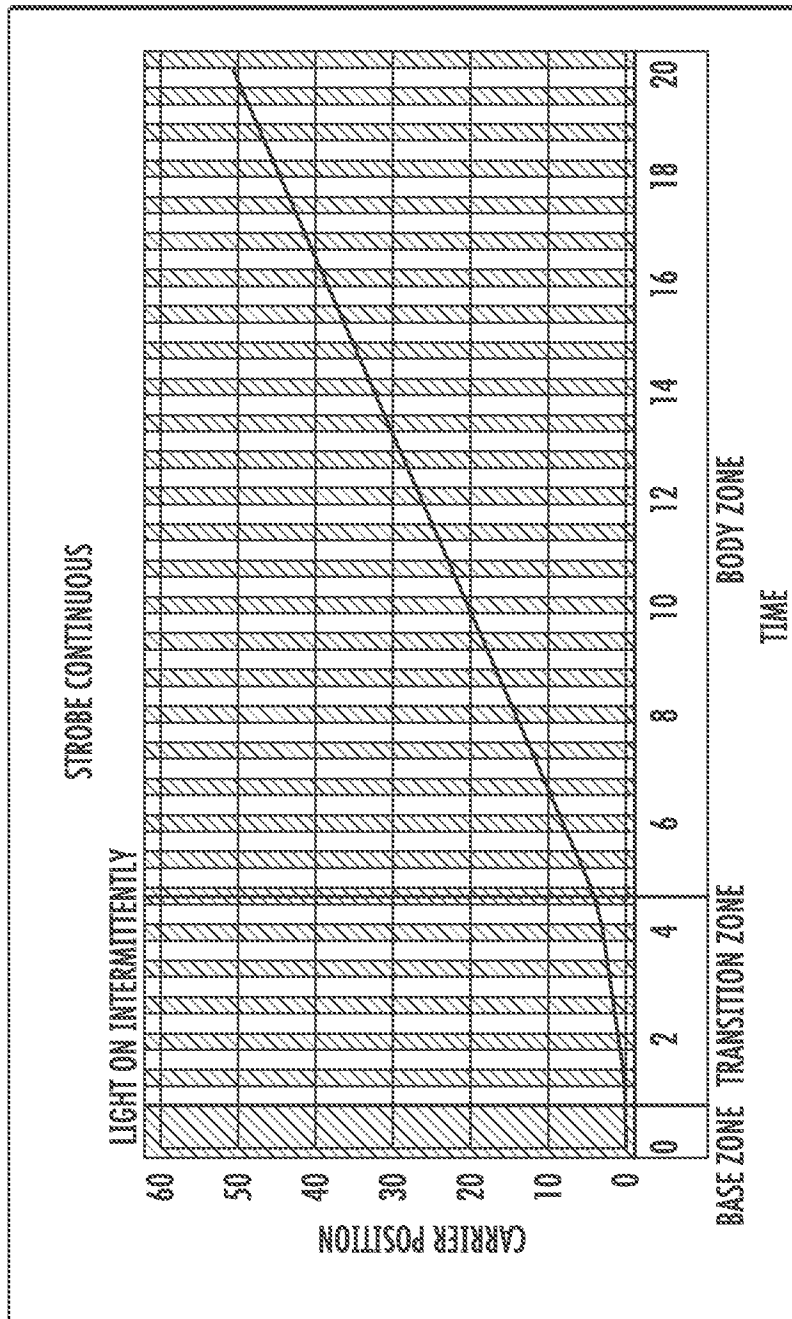


FIG. 11B

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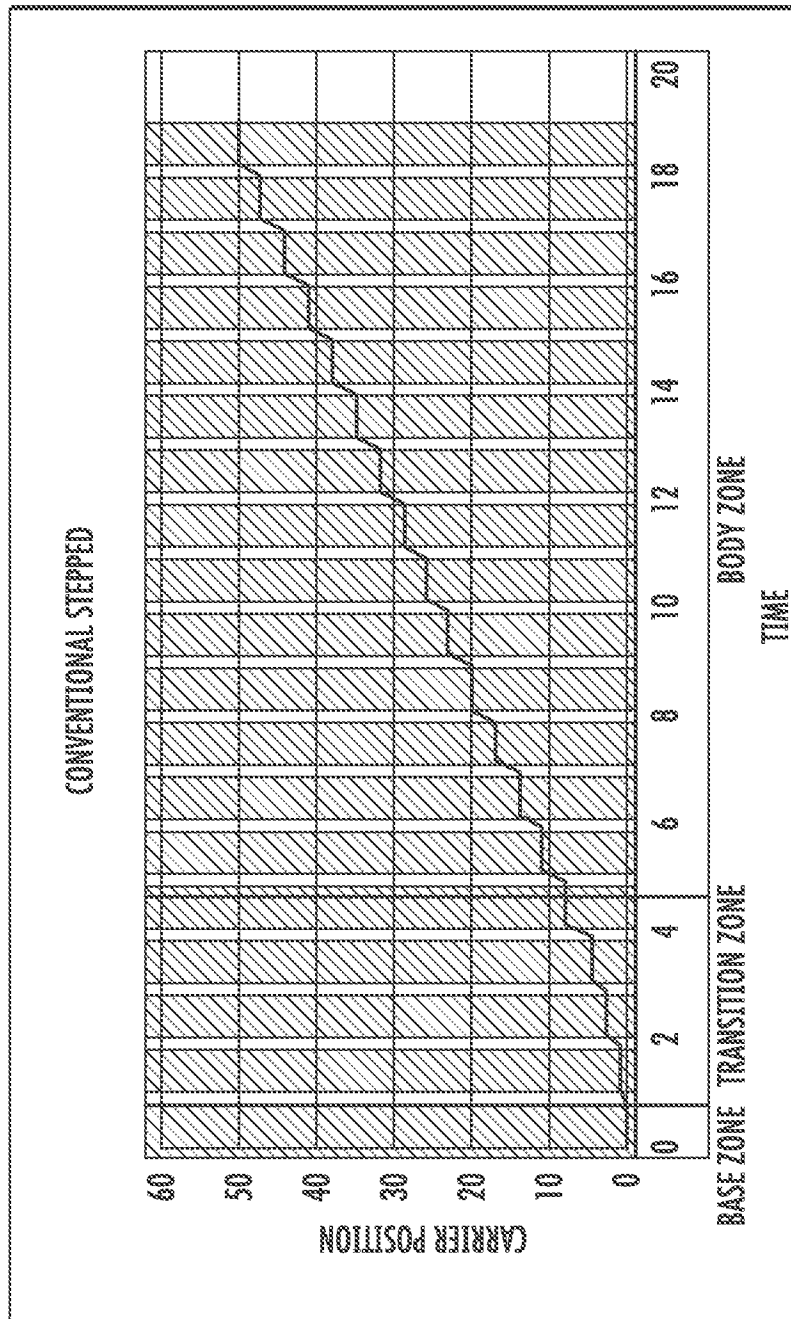


FIG. 12A

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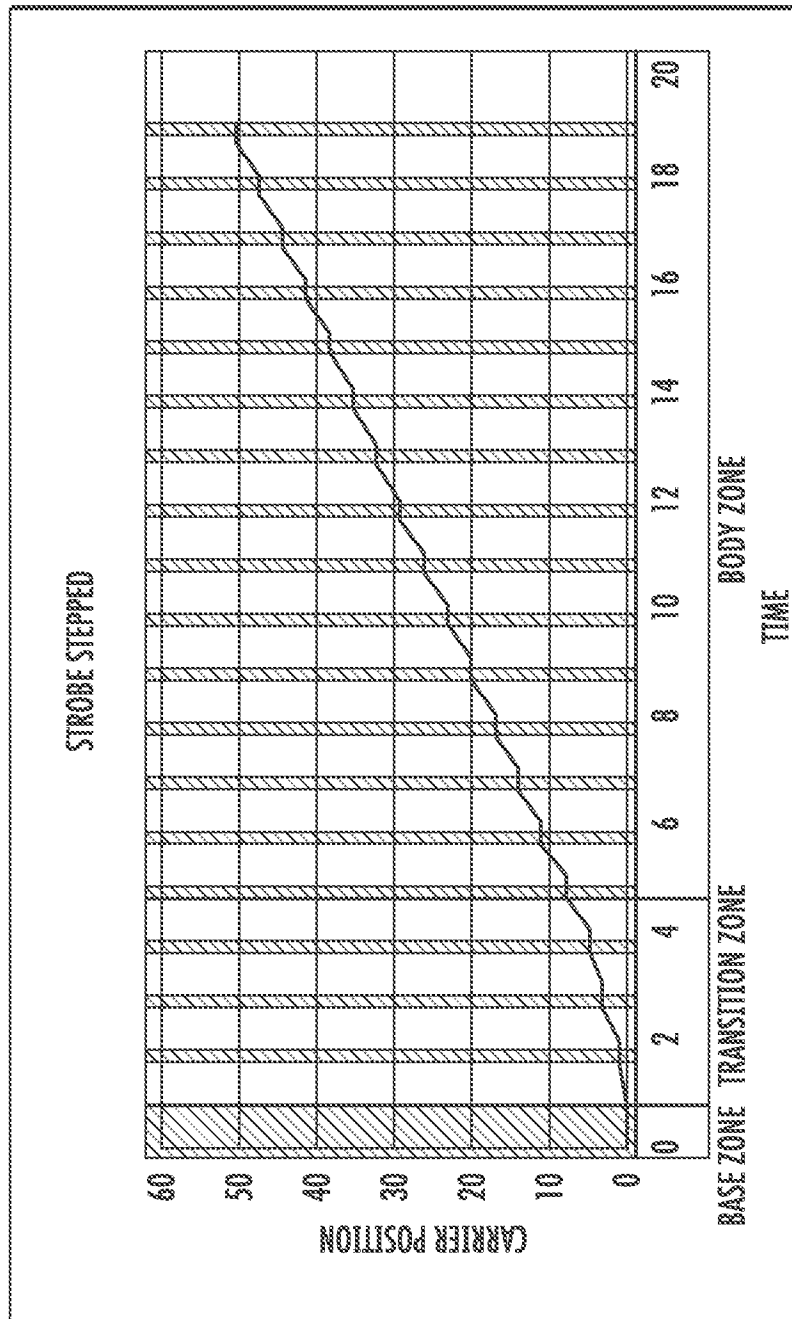


FIG. 12B

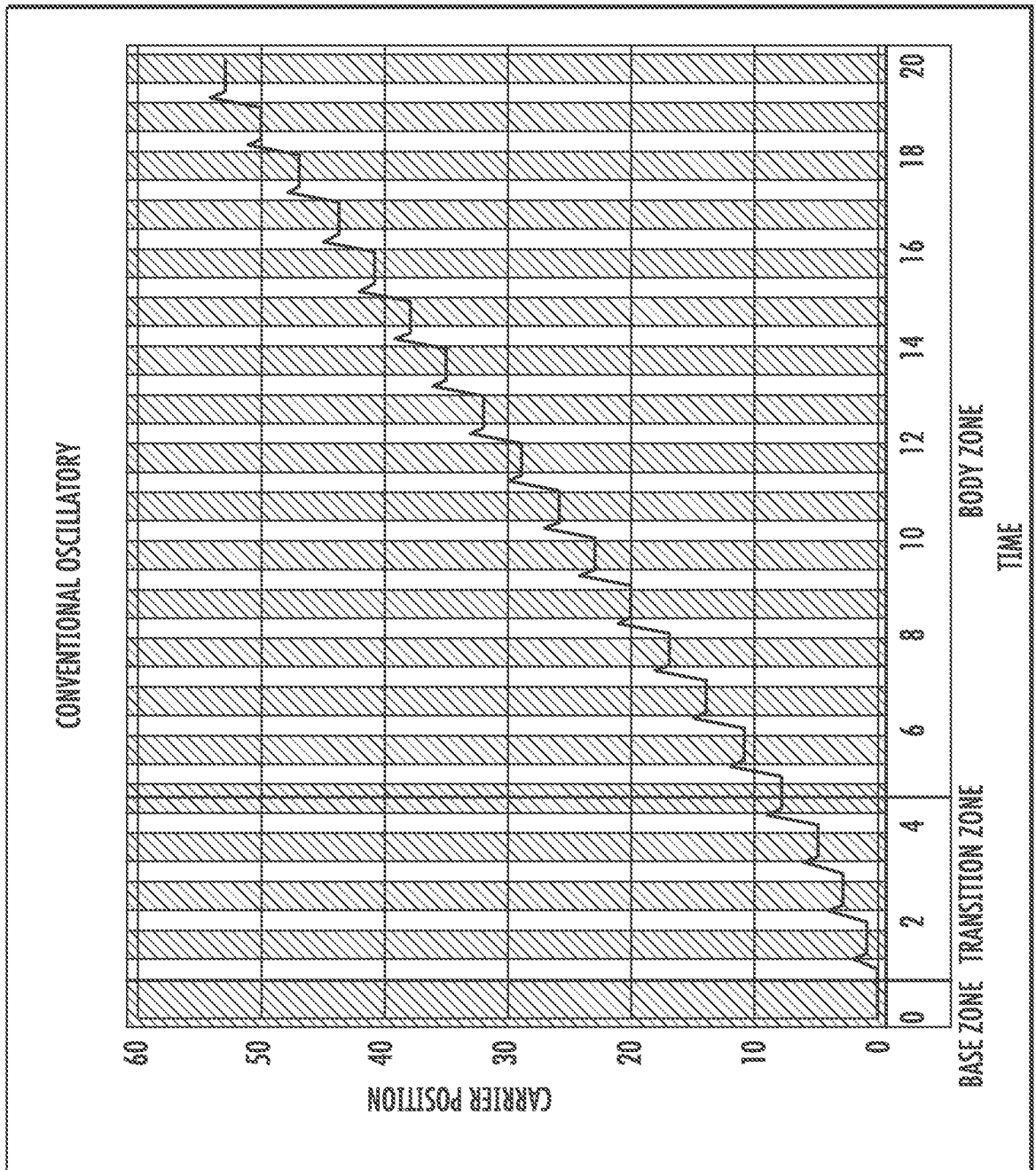


FIG. 13A

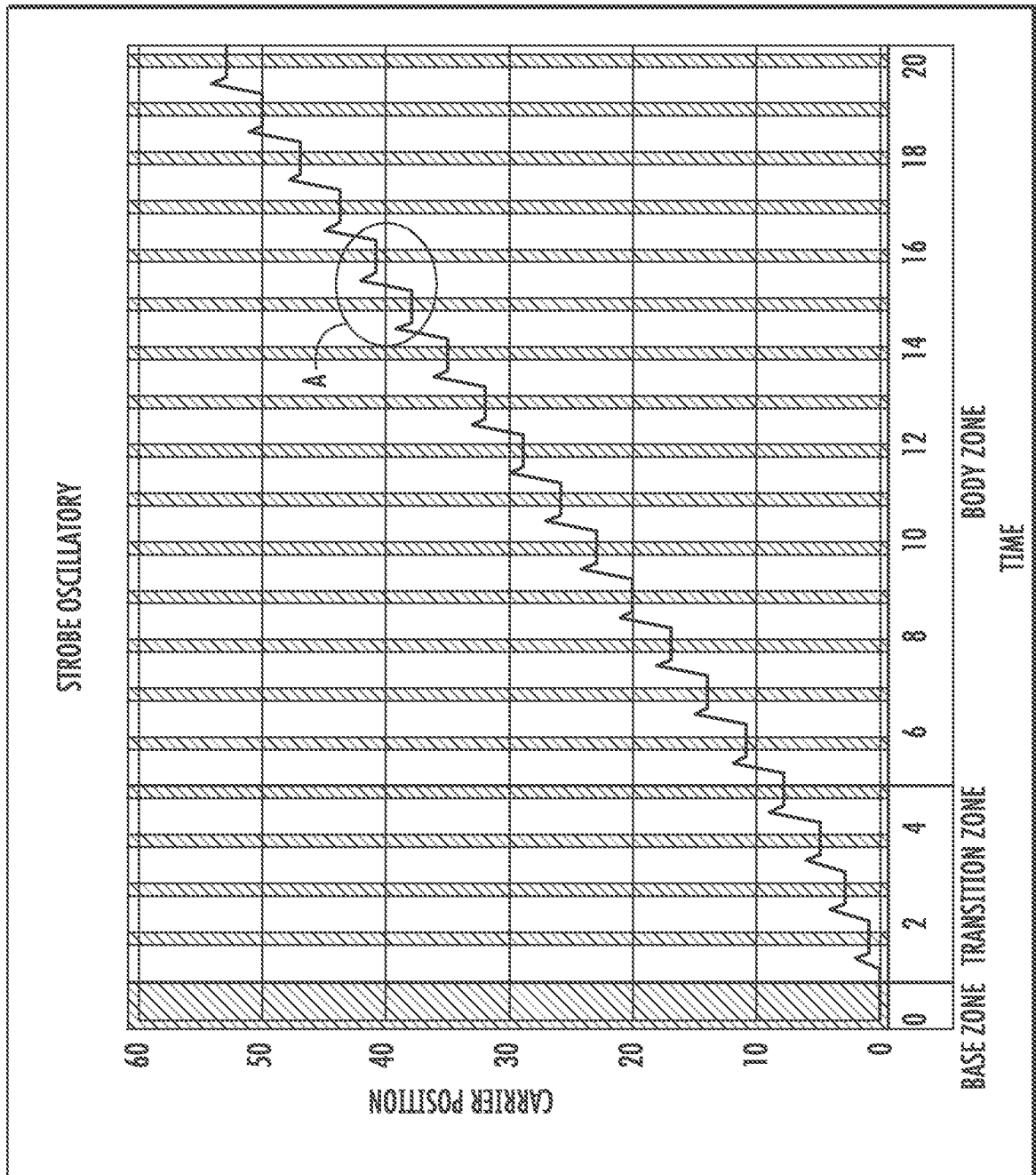


FIG. 13B

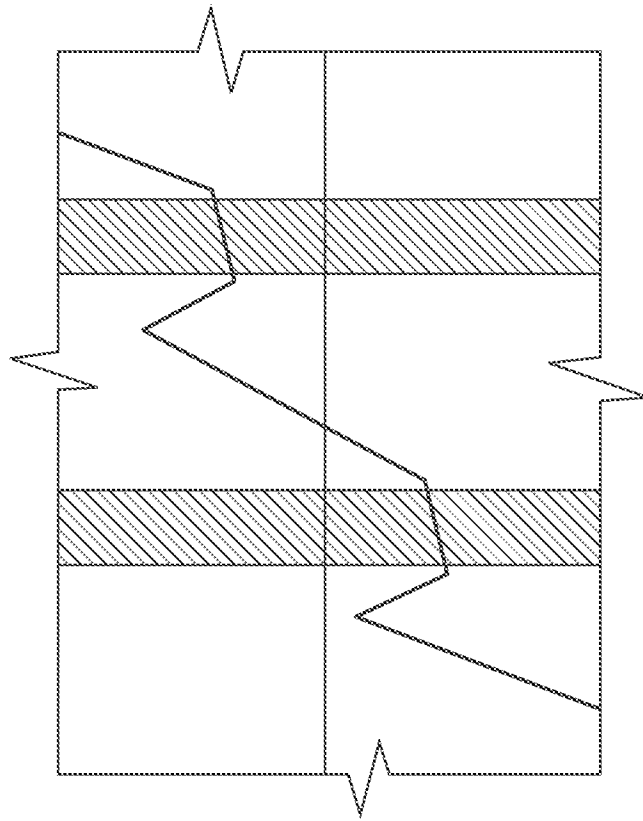


FIG. 14B

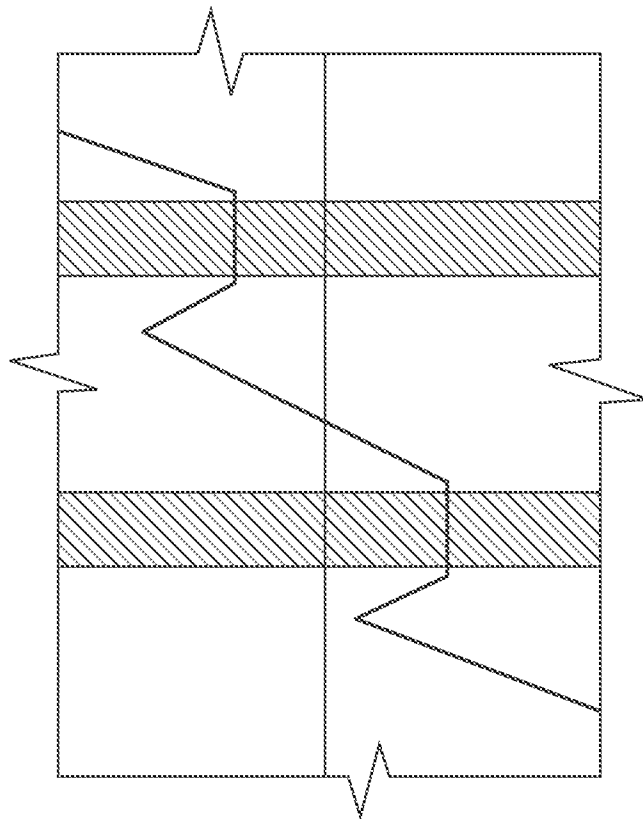


FIG. 14A

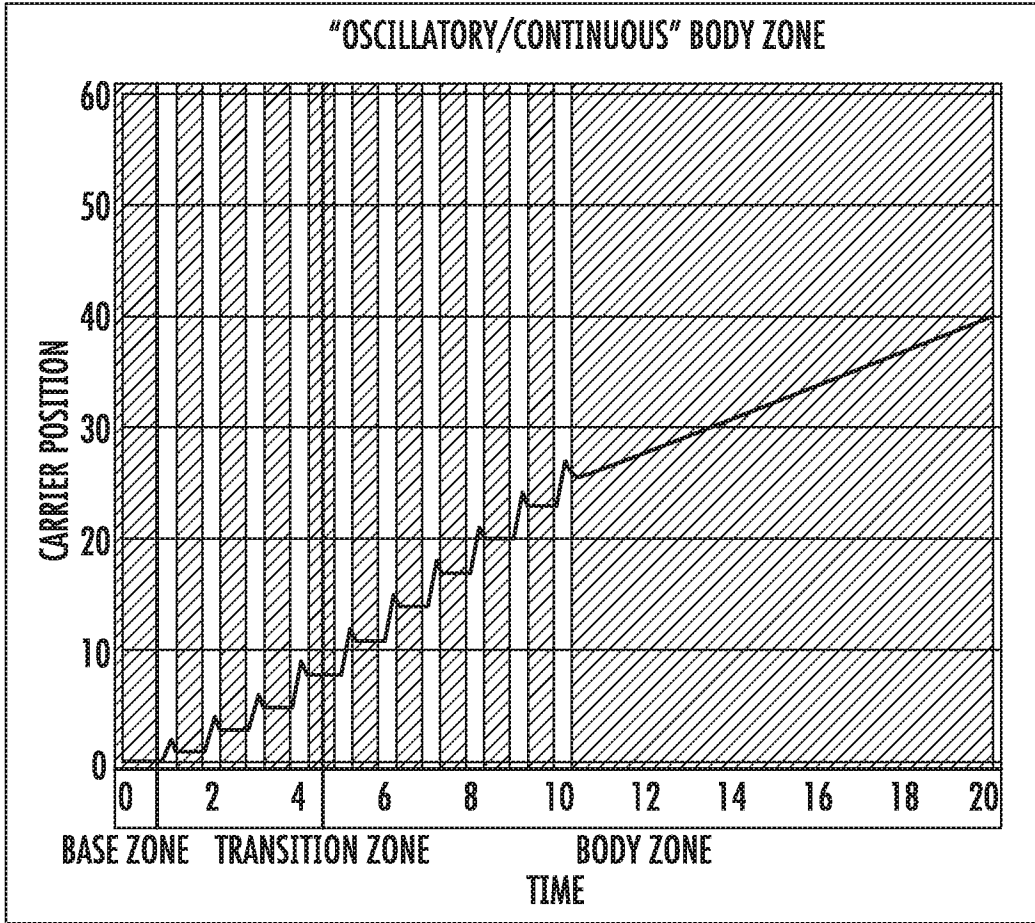


FIG. 15A

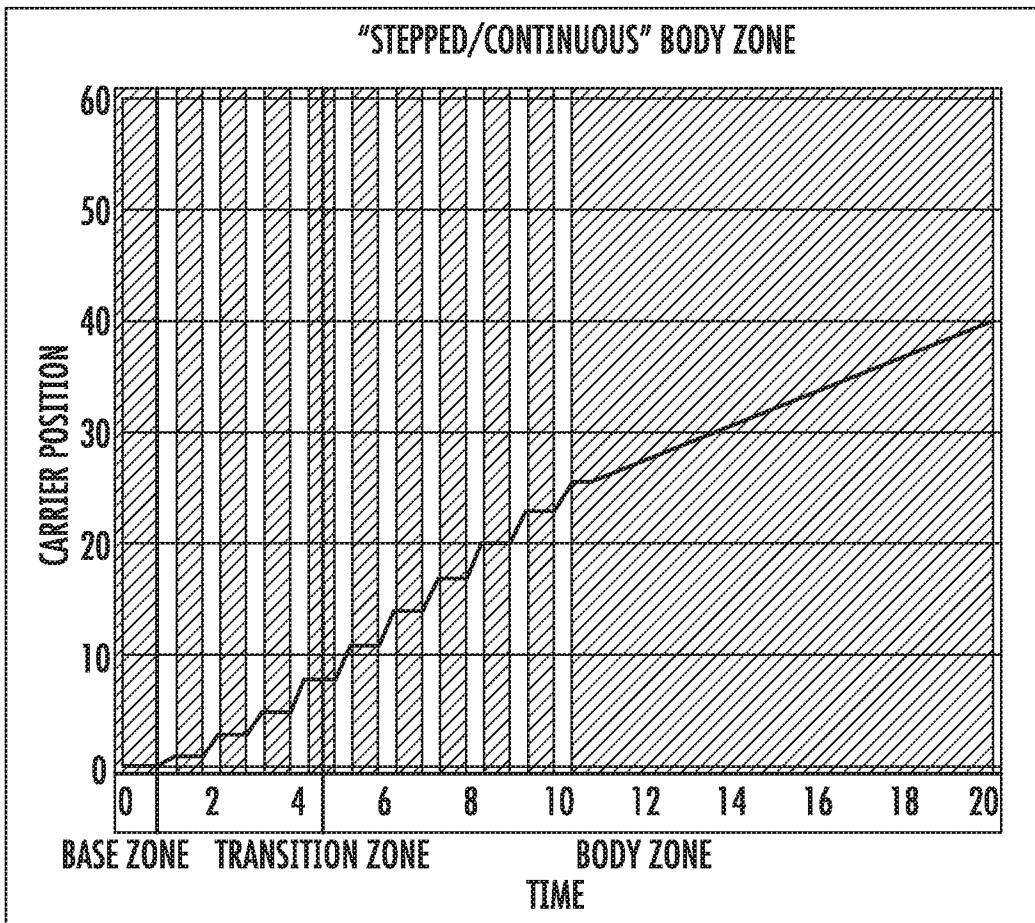


FIG. 15B

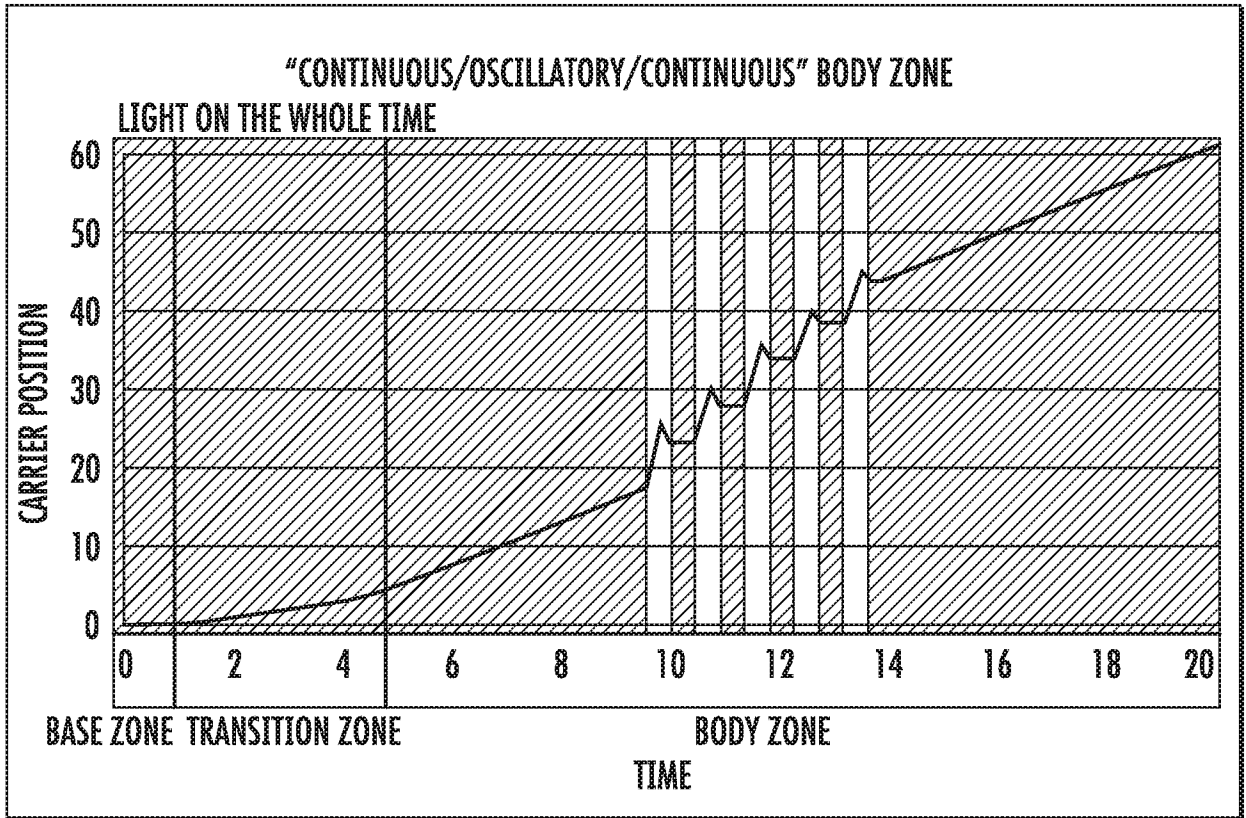


FIG. 16A

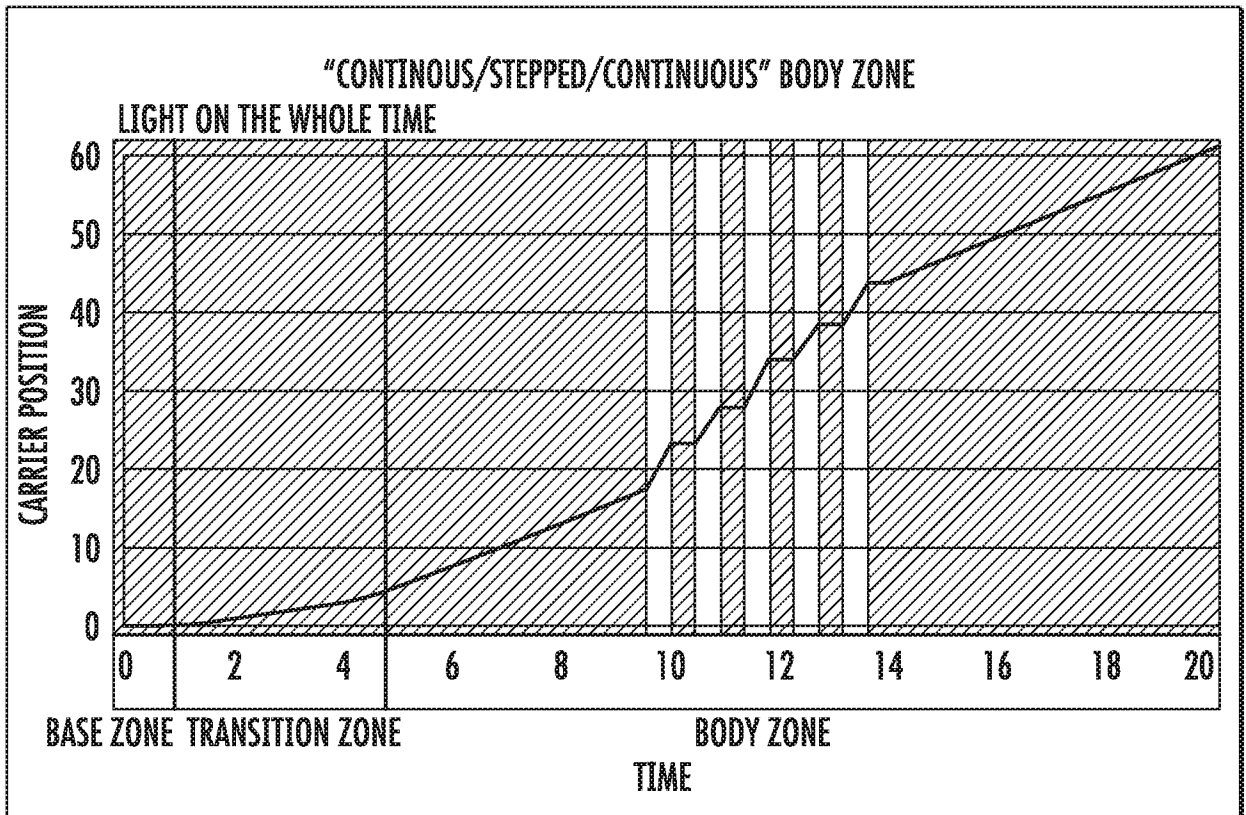


FIG. 16B

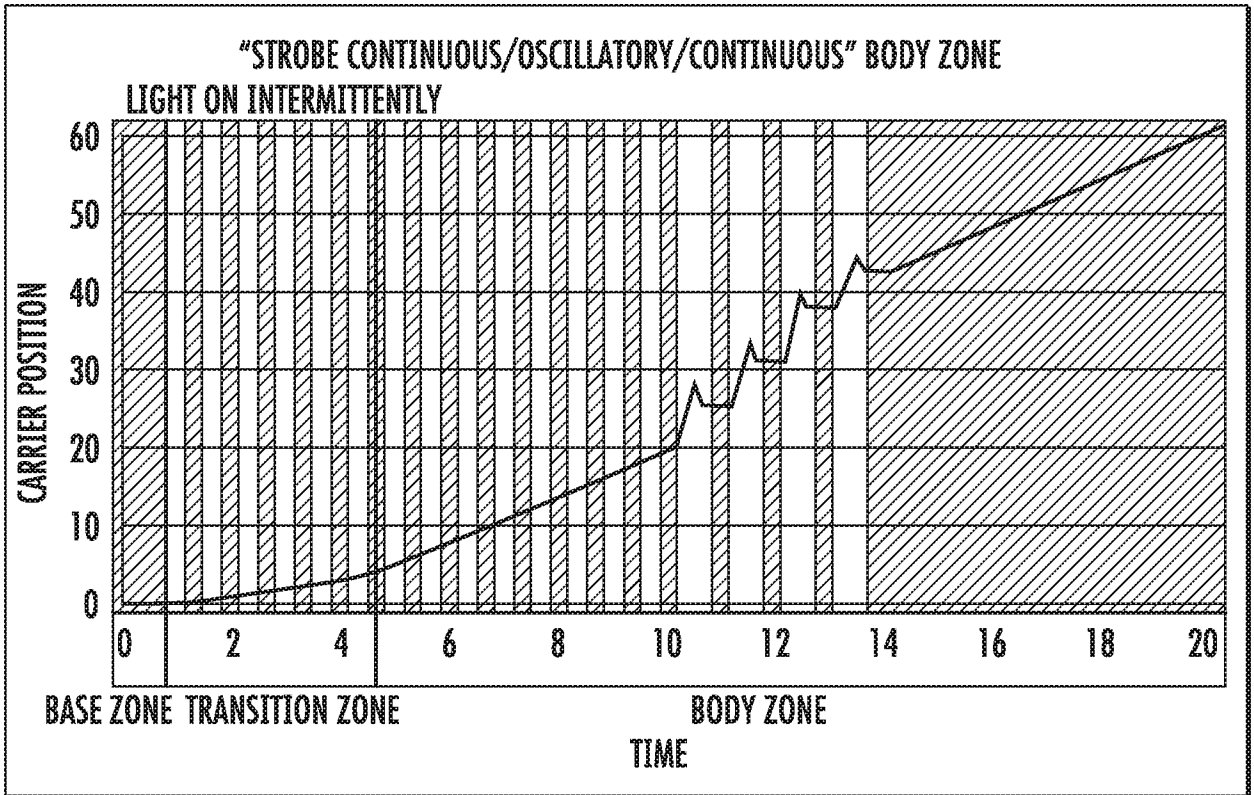


FIG. 17A

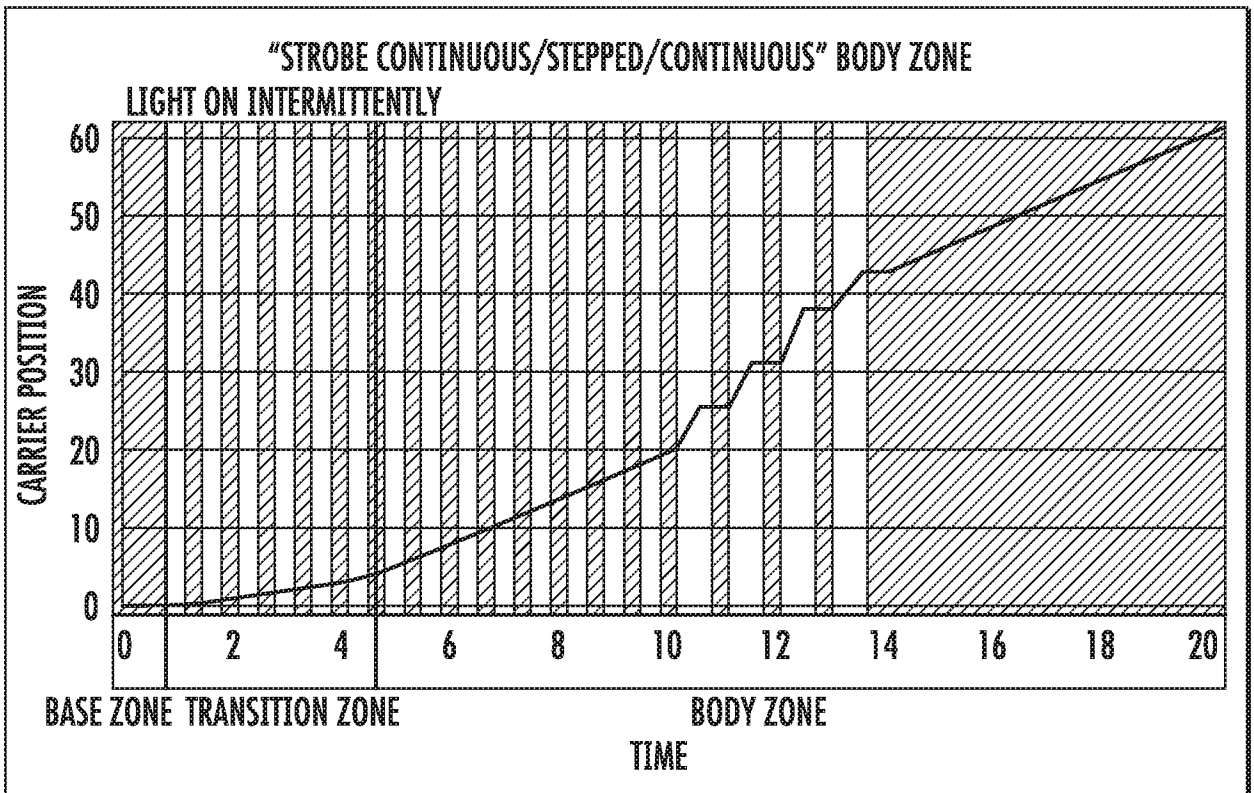


FIG. 17B

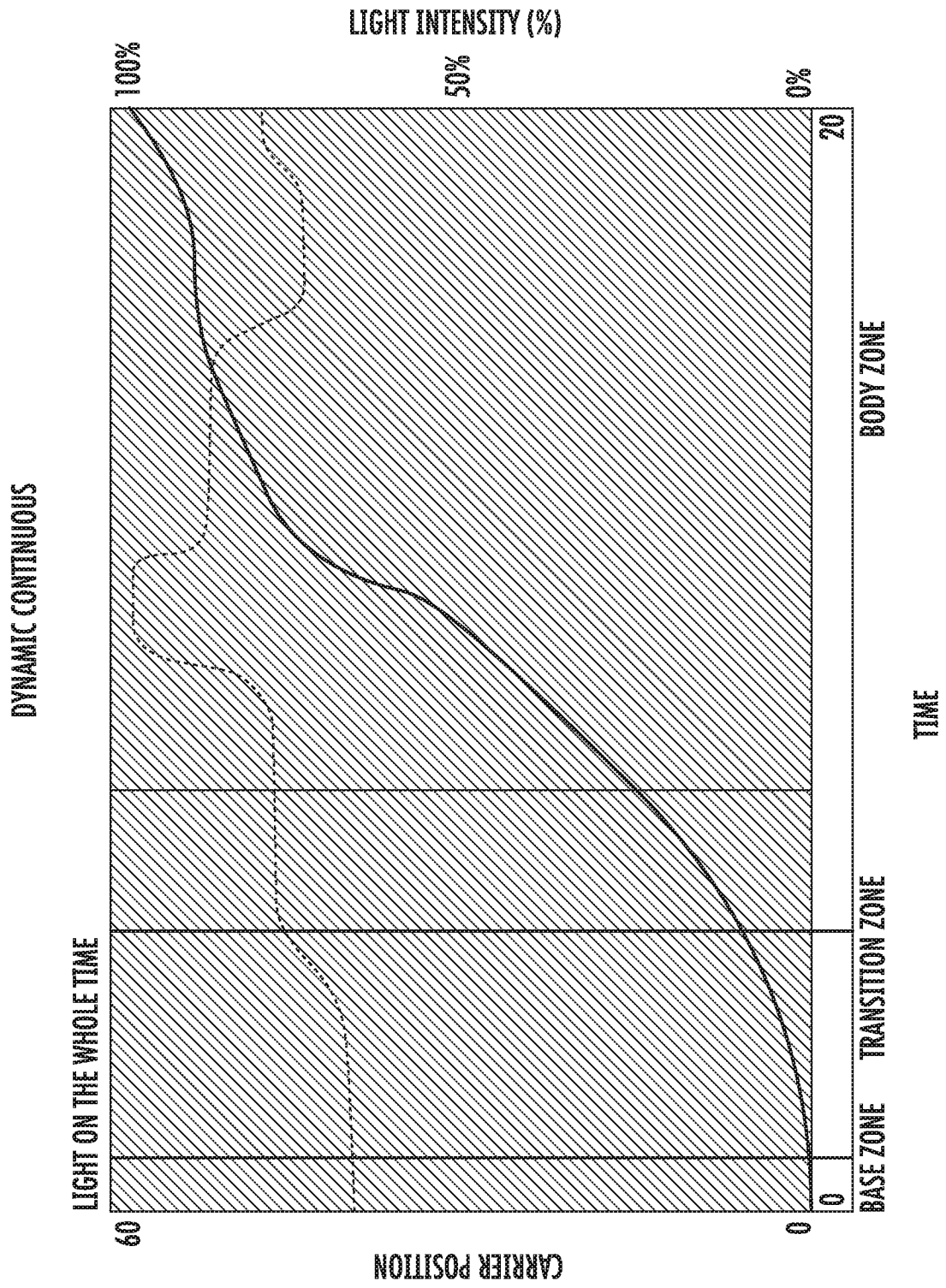


FIG. 18A

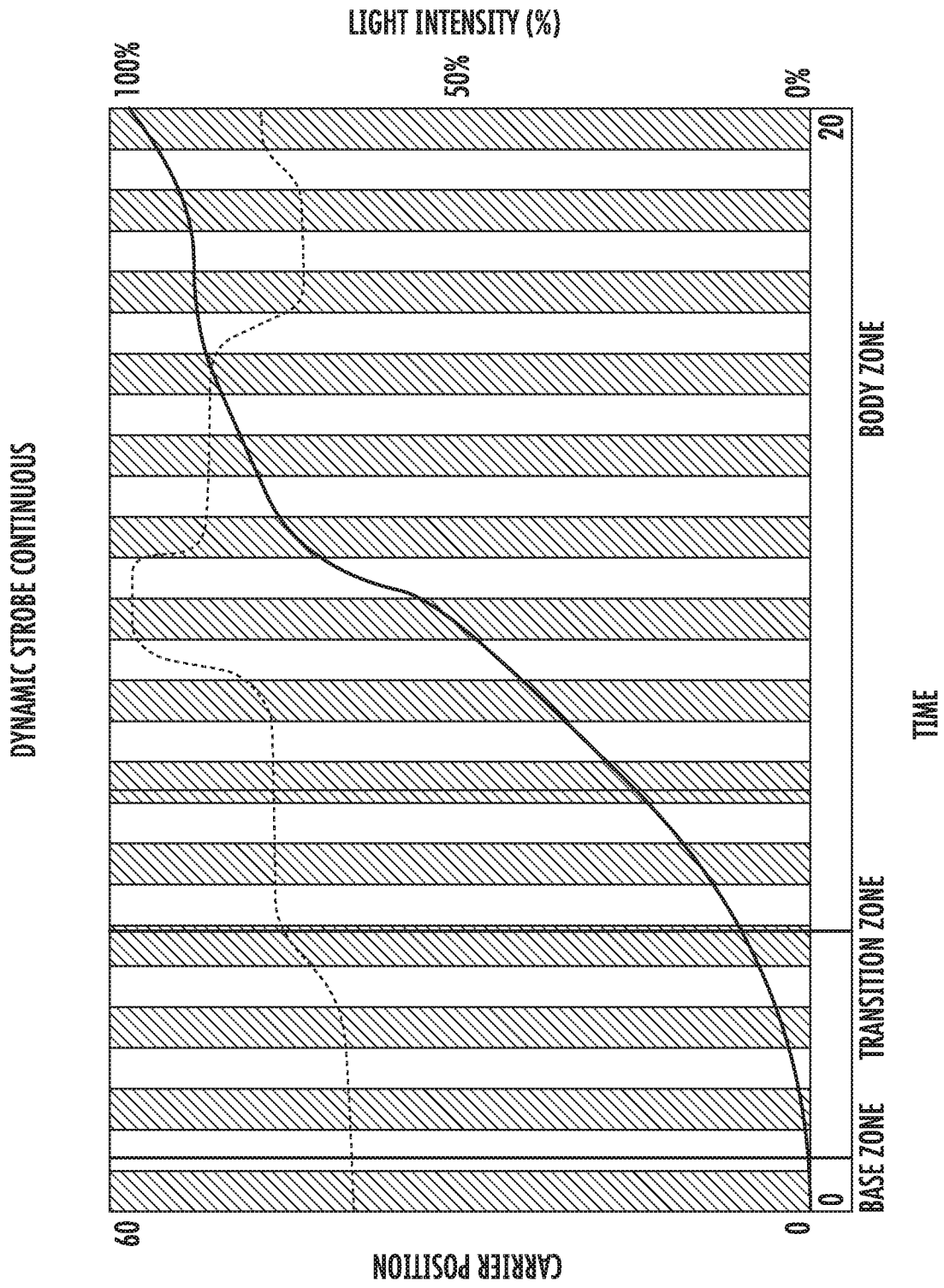


FIG. 18B

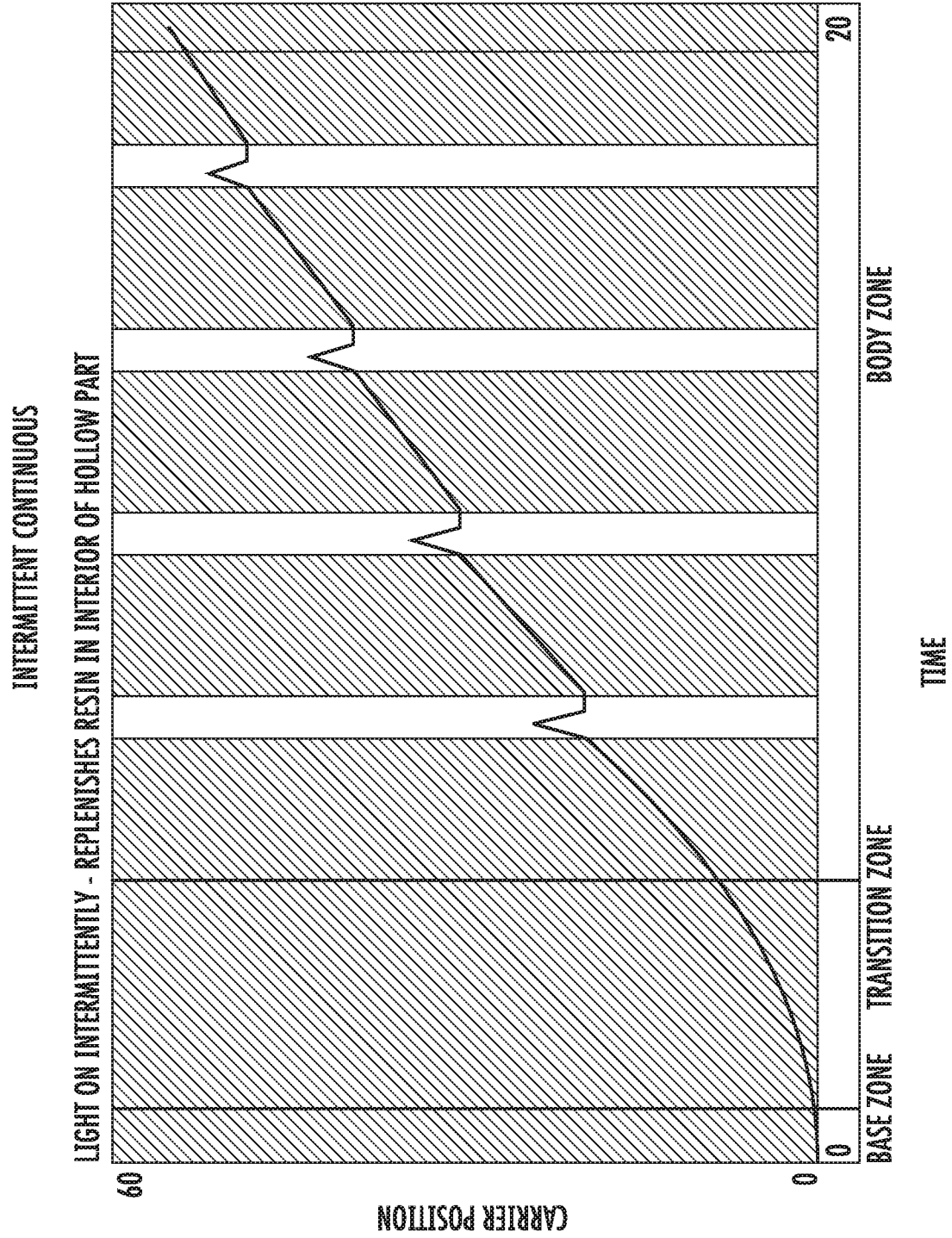


FIG. 19

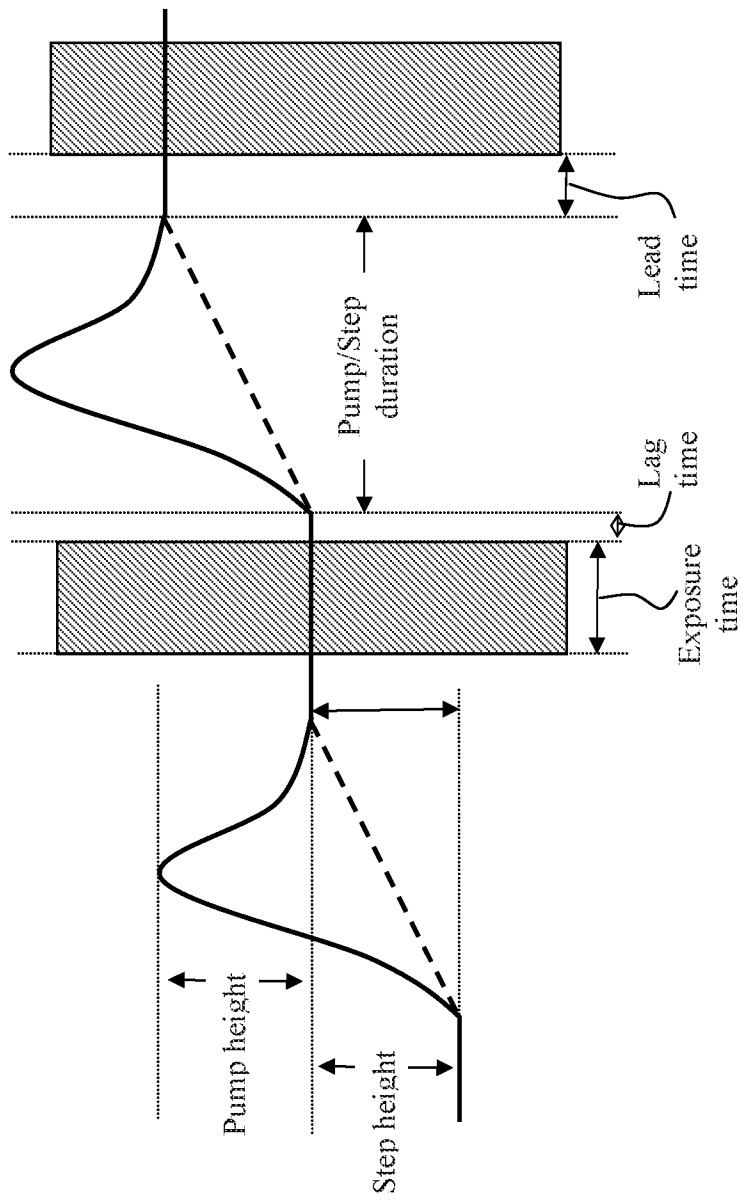


Figure 20
Reciprocal and Step Mode Parameters

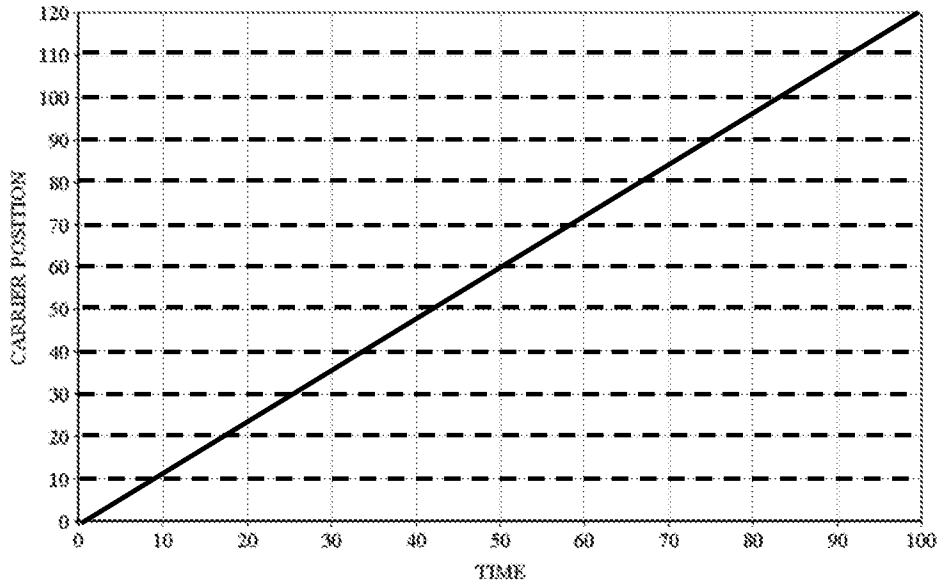


FIGURE 21A
Constant Slice Thickness with Constant Carrier Speed

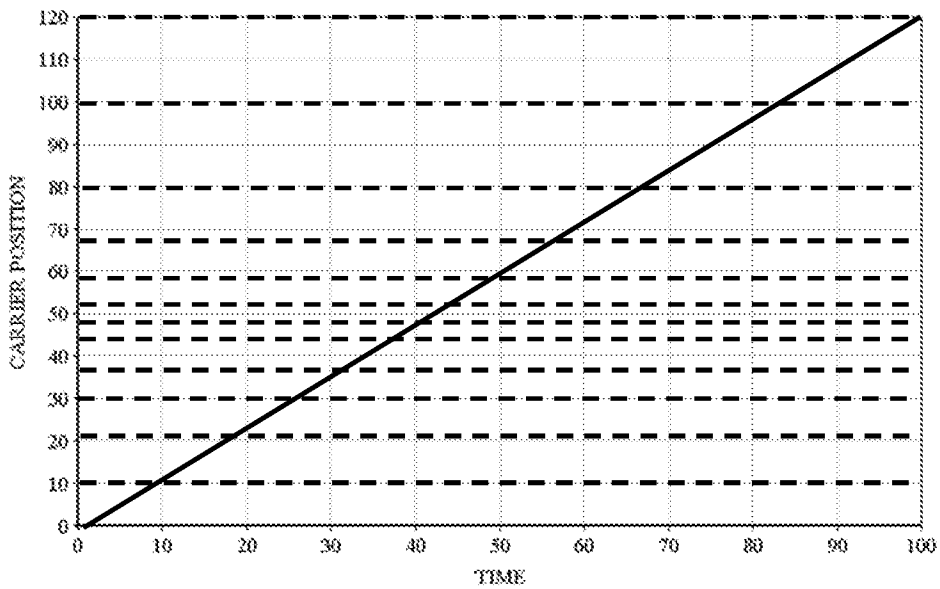


FIGURE 21B
Variable Slice Thickness with Constant Carrier Speed

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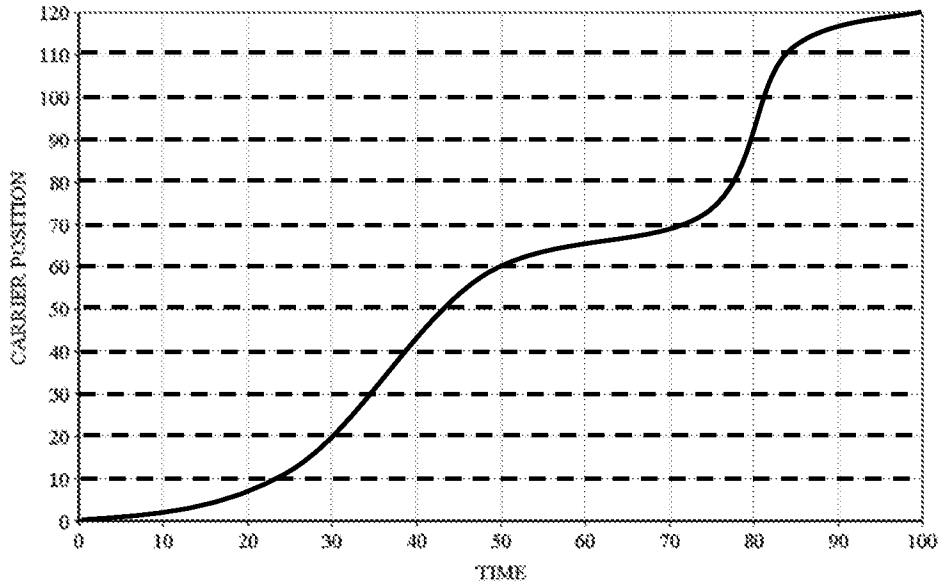


FIGURE 21C
Constant Slice Thickness with Variable Carrier Speed

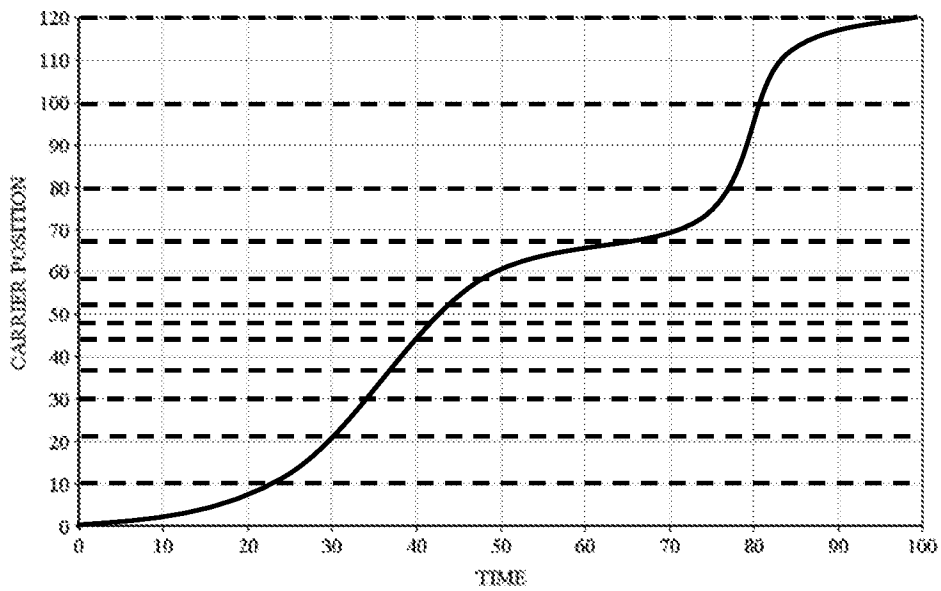


FIGURE 21D
Variable Slice Thickness with Variable Carrier Speed

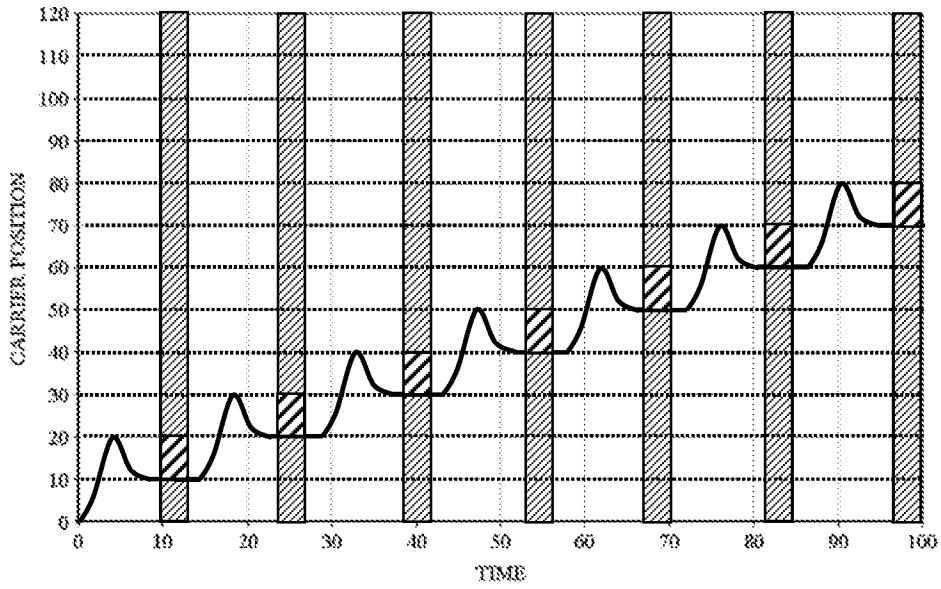


FIGURE 21E
Constant Slice Thickness in Reciprocal Mode

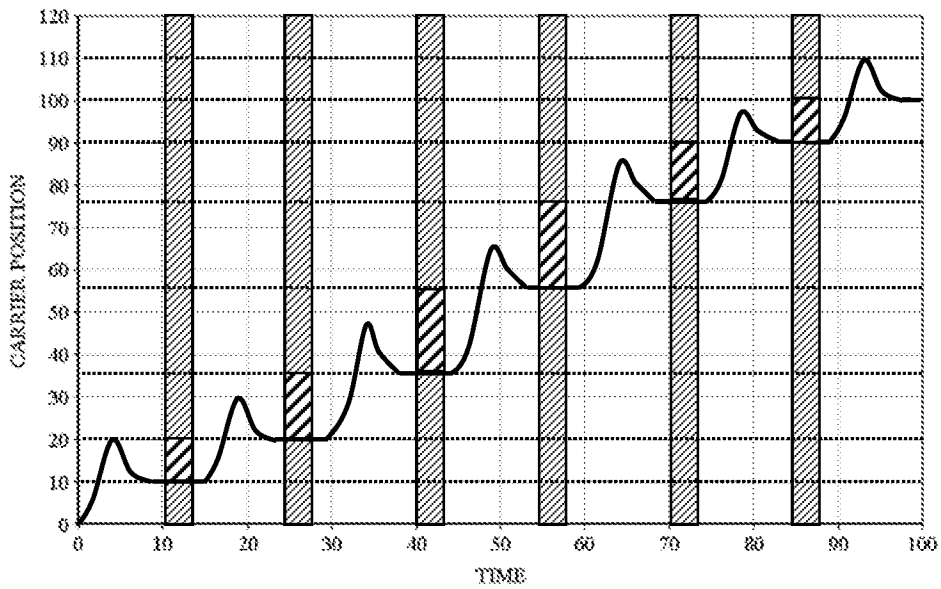


FIGURE 21F
Variable Slice Thickness in Reciprocal Mode

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2016/019839

A. CLASSIFICATION OF SUBJECT MATTER
INV. B29C67/00
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED
Minimum documentation searched (classification system followed by classification symbols)
B29C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 2014/126830 A2 (EIPi SYSTEMS INC [US]) 21 August 2014 (2014-08-21) claims page 1, line 8 - page 30, line 30 -----	1-43
X	US 2008/113293 A1 (SHKOLNIK ALEXANDR [US] ET AL) 15 May 2008 (2008-05-15) claims -----	1-43

Further documents are listed in the continuation of Box C.

See patent family annex.

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- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
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Date of the actual completion of the international search

6 May 2016

Date of mailing of the international search report

17/05/2016

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Whelan, Natalie

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/US2016/019839

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