

AUSTRALIA

Patents Act 1990

NOTICE OF ENTITLEMENT

We, GEC ALSTHOM LIMITED of Mill Road, Rugby, Warwickshire, CV21 1TB, United Kingdom, being the applicant in respect of Application No. 11367/95 state the following:-

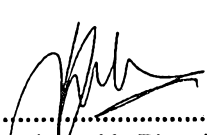
The Person nominated for the grant of the patent has entitlement from the actual inventor by an assignment.

The person nominated for the grant of the patent is the applicant of the basic application listed on the patent request form.

The basic application listed on the request form is the first application made in a Convention country in respect of the invention.

GEC ALSTHOM LIMITED

By our Patent Attorneys,
WATERMARK PATENT & TRADEMARK ATTORNEYS


.....
Stephen K. Plymin
Registered Patent Attorney

.....
10 October 1997

AUSTRALIA

Patents Act 1990

PATENT REQUEST: STANDARD PATENT/PATENT OF ADDITION

We, being the persons identified below as the Applicant, request the grant of a patent to the person identified below as the Nominated Person, for an invention described in the accompanying standard complete specification.

Full application details follow.

[71] Applicant: GEC ALSTHOM LIMITED
Address: MILL ROAD, RUGBY, WARWICKSHIRE, CV21 1TB, UNITED KINGDOM

[70] Nominated Person: GEC ALSTHOM LIMITED
Address: MILL ROAD, RUGBY, WARWICKSHIRE, CV21 1TB, UNITED KINGDOM

[54] Invention Title: A METHOD OF LOCATING THE POSITION OF A FAULT ON A POWER TRANSMISSION LINE

[72] Name(s) of actual inventor(s): ALLAN THOMAS JOHNS

[74] Address for service in Australia: c/o WATERMARK PATENT & TRADEMARK ATTORNEYS, of
290 Burwood Road, Hawthorn, Victoria 3122, Australia Attorney Code: WM

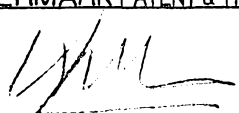
BASIC CONVENTION APPLICATION(S) DETAILS

[31] Application Number	[33] Country	Country Code	[32] Date of Application
9401467.7	UNITED KINGDOM	GB	26 JANUARY 1994

Basic Applicant(s): GEC ALSTROM LIMITED

Drawing number recommended to accompany the abstract

By our Patent Attorneys,
WATERMARK PATENT & TRADEMARK ATTORNEYS


.....
Stephen K. Plymin

Registered Patent Attorney**DATED** this 24th day of January 1995.

14064420 240195



AU9511367

(12) PATENT ABRIDGMENT (11) Document No. AU-B-11367/95
(19) AUSTRALIAN PATENT OFFICE (10) Acceptance No. 685887

- (54) Title
A METHOD OF LOCATING THE POSITION OF A FAULT ON A POWER TRANSMISSION LINE
- (51)⁵ International Patent Classification(s)
G01R 027/16 G01R 031/3193
- (21) Application No. : 11367/95 (22) Application Date : 24.01.95
- (30) Priority Data
- (31) Number (32) Date (33) Country
9401467 26.01.94 GB UNITED KINGDOM
- (43) Publication Date : 03.08.95
- (44) Publication Date of Accepted Application : 29.01.98
- (71) Applicant(s)
GEC ALSTHOM LIMITED
- (72) Inventor(s)
ALLAN THOMAS JOHNS
- (74) Attorney or Agent
WATERMARK PATENT & TRADEMARK ATTORNEYS , Locked Bag 5, HAWTHORN VIC 3122
- (56) Prior Art Documents
GB 2036478
EP 106790
- (57) Claim

1. A method of locating the position of a fault on a power transmission line between first and second ends of the line, the method comprising the steps of:
- (a) calculating the complex fault impedance at each of a plurality of assumed fault positions along the length of the line, the fault impedance at each assumed position being calculated utilising:
- (i) a measurement before and after fault occurrence of the voltage and current at said first end of the line,
 - (ii) parameters of the line, and
 - (iii) a source impedance of said second end of the line, and
- (b) selecting as the actual fault position the assumed fault position of said plurality of assumed fault positions for which the argument of the complex fault impedance most closely equals zero.

2. A method according to Claim 1 wherein said fault impedance at each said assumed position is calculated utilising the equation:

$$Z_f = (V_f + V_{fss}) / I_f,$$

where Z_f is the fault impedance, V_f is the difference between the fault point voltage before and after fault occurrence, V_{fss} is the fault point voltage before fault occurrence, and I_f is the fault current, and where

$$V_f = A_x \cdot V_L - B_x \cdot I_L$$

$$V_{fss} = A_x \cdot V_{Lss} - B_x \cdot I_{Lss}, \text{ and}$$

$$I_f = -(C_x + [C_y \cdot Z_{sR} + D_y] \cdot [A_y \cdot Z_{sR} + B_y]^{-1} \cdot A_x) \cdot V_L \\ + (D_x + [C_y \cdot Z_{sR} + D_y] \cdot [A_y \cdot Z_{sR} + B_y]^{-1} \cdot B_x) \cdot I_L,$$

where A_x , B_x , C_x and D_x are four parameters describing a two-port network representing the transmission line between said first end and the fault, A_y , B_y , C_y and D_y are four parameters describing the two-port network representing the transmission line between said second end and the fault, V_L is the difference between the voltage at said first end before and after fault occurrence, I_L is the difference between the current at said first end before and after fault occurrence, V_{Lss} is the voltage at said first end before fault occurrence, I_{Lss} is the current at said first end before fault occurrence, and Z_{sR} is the impedance at said second end.

4. A method according to Claim 1 wherein: said power transmission line is a multi-phase power transmission line; said step of calculating the complex fault impedance is carried out in respect of each complex impedance of each of a plurality of forms of fault network assumed to be at each of said plurality of assumed fault positions, each complex impedance of each network at each position being calculated utilising the measurement before and after fault occurrence in respect of each phase of the line of the voltage and current at said first end of the line, parameters of the line, and the impedance at said second end of the line; said method further comprises the step of analysing the variation of each complex impedance of each assumed fault network over said plurality of assumed fault positions to determine the assumed fault network for which the argument of each complex impedance most closely equals zero at the same assumed fault position of the plurality of assumed fault positions; and said step of selecting as the actual fault position comprises selecting as the actual fault position that same assumed fault position.

AUSTRALIA

Patents Act 1990

ORIGINAL
COMPLETE SPECIFICATION
STANDARD PATENT

Application Number:

Lodged:

Invention Title:

A METHOD OF LOCATING THE POSITION OF A FAULT ON A POWER
TRANSMISSION LINE

The following statement is a full description of this invention, including the
best method of performing it known to us :-

MTR/4596 A01

A method of locating the position of a
fault on a power transmission line

This invention relates to a method of locating the position of a fault on a power transmission line, be it a single or multi-phase line. In another aspect the invention relates to a method of determining the form of impedance network at a fault on a multi-phase power transmission line.

It is important that a method of locating the position of a fault on a power transmission line provides an accurate estimate of the distance to the fault. Accuracy is required so that the fault can be located quickly and repairs begun. Hence the power is cut off for less time and less revenue lost to the power utility.

At present, fault location methods providing the required accuracy require measurements to be made at both ends, as opposed to only one end, of the line, and communicated to a single location. Such methods are more complicated, and hence more expensive, to implement than those that require measurements to be made at only one end.

It is an object of the present invention to provide a method of locating the position of a fault on a power transmission line which provides an accurate

estimate of the distance to the fault yet requires measurements to be made at only one end of the line.

According to a first aspect of the present invention there is provided a method of locating the position of a fault on a power transmission line between first and second ends of the line comprising: calculating the complex fault impedance at each of a plurality of assumed fault positions along the length of the line, the fault impedance at each assumed position being calculated utilising the measurement before and after fault occurrence of the voltage and current at said first end of the line, parameters of the line, and the impedance at said second end of the line; and selecting as the actual fault position the assumed fault position of said plurality of assumed fault positions for which the argument of the complex fault impedance most closely equals zero.

In one particular method according to the first aspect of the present invention where said power transmission line is a multi-phase power transmission line: said step of calculating the complex fault impedance is carried out in respect of each complex impedance of each of a plurality of forms of fault network assumed to be at each of said plurality of assumed fault positions, each complex impedance of each network at each position being calculated utilising the measurement before and after fault occurrence in respect of each phase of the line of the voltage and current at said first end of the line, parameters of the line, and the impedance at said second end of the line; said method further comprises the step of analysing the variation of each complex impedance of each assumed fault network over said plurality of assumed fault positions to determine the assumed fault network for which the argument of each complex impedance most closely

equals zero at the same assumed fault position of the plurality of assumed fault positions; and said step of selecting as the actual fault position comprises selecting as the actual fault position that same assumed fault position.

According to a second aspect of the present invention there is provided a method of determining the form of impedance network at a fault on a multi-phase power transmission line between first and second ends of the line comprising: calculating the complex impedances of each of a plurality of assumed forms of fault impedance network at each of a plurality of assumed fault positions along the length of the line, each complex impedance of each network at each position being calculated utilizing the measurement before and after fault occurrence in respect of each phase of the line of the voltage and current at said first end of the line, parameters of the line, and the impedance at said second end of the line; analysing the variation of each complex impedance of each assumed fault network over said plurality of assumed fault positions to determine the assumed fault network for which the argument of each complex impedance most closely equals zero at the same assumed fault position of the plurality of assumed fault positions; and selecting as the form of the actual fault impedance network the form of that determined assumed fault network.

The invention will now be further explained, and methods in accordance with the first and second aspects of the invention described, by way of example, with reference to the accompanying drawings in which:

Figure 1 illustrates single-ended fault location on a single-circuit double-end fed power network;

Figure 2 illustrates overall unfaulted and faulted system models for

a single-phase single-circuit double-end fed network;

Figure 3 illustrates an analysis of the faulted system model of Figure 2 by decomposition into pre-fault and superimposed component circuits;

Figure 4 illustrates measured, assumed and unknown values in the pre-fault and superimposed circuits of Figure 3; and

Figures 5 and 6 illustrate a method in accordance with the first aspect of the invention;

Figure 7 illustrates methods in accordance with the first and second aspects of the invention;

Figure 8 illustrates in more detail that illustrated in Figure 3; and

Figures 9 and 10 illustrate respectively circuits and the two-port representations thereof used in the calculation of fault impedance as occurs in the methods according to the first and second aspects of the invention.

The following symbols are used in the explanation and description.

L - Local-end busbar

R - Remote-end busbar

F - Fault point

EL - Local-end generator driving voltage (phasor) [V]

ER - Remote-end generator driving voltage (phasor) [V]

ZsL - Local-end source impedance (phasor) [ohm]

ZsR - Remote-end source impedance (phasor) [ohm]

Ipre - Pre-fault current at local-end busbar (phasor) [A]

Vpre - Pre-fault voltage at local-end busbar (phasor) [V]

Ipost - Post-fault current at local-end busbar (phasor) [A]

- V_{post} - Post-fault voltage at local-end busbar (phasor) [V]
 I - Superimposed current at local-end busbar (phasor) [A]
 V - Superimposed voltage at local-end busbar (phasor) [V]
 L - Total line length [km]
 Z_L - Line impedance per unit length (phasor) [ohm/km]
 x - Distance to fault from local-end busbar [km]
 R_f - Fault resistance [ohm]
 Z_f - Fault impedance (phasor) [ohm]
 V_{fss} - Pre-fault voltage at fault point (phasor) [V]
 E_f - Superimposed back injecting fault point generator driving voltage (phasor) [V]

The following conventions are used in the explanation and description.

- $\#^m$ - Measured value
 $\#^i$ - Assumed value
 $\#^c$ - Calculated value
 $\#^?$ - Unknown value
 $\#^*$ - Changing value

Referring to Figure 1, measurements are made at the local-end busbar L only and supplied to fault locator 1. Generators 3, 5 feed the local- and remote-ends respectively of the single-circuit power network 7.

A single-phase single-circuit double-end fed network of the form shown in Figure 2a) is taken as the overall unfaulted system model. The source

networks, at the local- and remote-ends, are represented by their thevenin equivalents and the line is represented by a lumped parameter model. Applying a resistive fault to the Figure 2a) system at some distance, x from the local-end busbar, a faulted system model as shown in Figure 2b) is achieved.

Using the law of superposition in linear network theory, the Figure 2b) faulted system model can be analysed by decomposing it into two component circuits : pre-fault and superimposed. This decomposition will now be explained.

A faulted system model, as shown in Figure 3a), can be decomposed into two component circuits : pre-fault and superimposed, as shown in Figures 3b) and 3c). This process of decomposition is shown again, but in an alternative and more detailed form, in Figure 8. Note that the following new symbols have been introduced.

V_f - Superimposed fault point voltage (phasor) [V]

I_f - Fault current (phasor) [I]

E_{fss} - Pre-fault injecting fault point generator driving voltage (phasor) [V]

I_{fss} - Pre-fault fault current (phasor) [I]

Looking at the decomposition of the faulted system model shown in Figure 8, the following points can be made:

(i) The faulted system model (or post-fault circuit) contains two driving voltage sources in the faulted leg on the ground side of the fault resistance. Since, after the fault the ground side of the fault resistance is at zero potential, these driving voltage sources must have equal and opposite driving potentials.

(ii) Applying the superposition theorem, the faulted system model can be seen to decompose easily into the pre-fault and superimposed component circuits shown. One of the fault point driving sources is associated with the pre-fault component circuit and regarded as the pre-fault injecting fault point generator driving voltage, E_{fss} . The other fault point driving source is associated with the superimposed component circuit and regarded as the superimposed injecting fault point generator driving voltage, E_f .

(iii) The pre-fault component circuit represents the situation before the fault occurred. Since before the fault there is an open circuit to ground at the fault point, the pre-fault fault current, I_{fss} equals zero and the pre-fault injecting fault point generator driving voltage, E_{fss} will equal the pre-fault voltage at the fault point, V_{fss} .

(iv) The superimposed component circuit represents the 'fault-caused component' which is superimposed upon the pre-fault circuit.

(v) Based upon what has been said above, it can be seen that the superimposed injecting fault point generator driving voltage, E_f is equal and opposite to the pre-fault voltage at the fault point, V_{fss} , the former being renamed the superimposed back injecting fault point generator driving voltage.

Thus, the decomposition of the faulted system model, as shown in Figure 3, can be understood.

Viewing a faulted network in terms of its pre-fault and superimposed component circuits is known in single-ended fault location, see, for example, Takagi, Yamakoshi, Yamuaura, Kondow, and Matsushima, "Development of a new type fault locator using one-terminal voltage and current data", IEEE Trans., PAS-

101, Aug. 1982, pp.2892-2898. Note that the use of these component circuits has the advantage of taking into account the pre-fault loading and also eliminating the need to know the precise nature of the local-end network.

Having arrived at the pre-fault and superimposed circuits shown in Figure 3, values are inserted as follows. The pre-fault circuit is forced with the measured values for the pre-fault current at local-end busbar, I_{pre} , and the pre-fault voltage at local-end busbar, V_{pre} . The superimposed circuit is forced with values, derived from measured values, for the superimposed current at local-end busbar, $I (= I_{post} - I_{pre})$, and the superimposed voltage at local-end busbar, $V (= V_{post} - V_{pre})$, where I_{post} is the post-fault current measured at local-end busbar, and V_{post} is the post-fault voltage measured at local-end busbar. Here the pre-fault and post-fault current and voltages are the steady-state power-frequency voltage and current phasors, measured at the local-end busbar in the actual system before and after the fault, as illustrated in Figure 2.

Values for the following pre-fault and superimposed circuit parameters are assumed: total line length, L , line impedance per unit length, Z_L , and remote-end source impedance, Z_{sR} . Note that the method of fault location to be described below is insensitive to likely inaccuracies in the foregoing assumed values.

The following values remain as unknown: pre-fault voltage at fault point, V_{fss} (hence superimposed back injecting fault point generator driving voltage, E_f which equals and is opposite to V_{fss}), fault resistance, R_f , and distance to fault from local-end busbar, x . Hence, we have arrived at the situation summarised in Figure 4. Here the circuit values measured, assumed and

remaining unknown are shown.

To this point nothing novel has been described. However, from this point forth a new direction is taken to those taken previously.

The unknown fault resistance, R_f , in the superimposed circuit is replaced with a fault impedance, Z_f . The fault position is assumed at different positions, F' , along the entire line length. That is the fault distance, x' , is assumed for a range of values from zero up to the total line length, L . For each assumed fault position, the fault impedance, Z_f , is calculated. The foregoing is summarised in Figure 5.

The fault impedance Z_f is calculated using steady-state analytical techniques as will now be explained.

The pre-fault and superimposed circuits used to calculate the fault impedance Z_f are shown in Figures 9 and 10. The former shows the actual circuits and the latter the equivalent two-port representation. The calculation of the fault impedance Z_f involves calculating the fault current I_f , the superimposed fault point voltage V_f , the pre-fault fault point voltage V_{fss} and the superimposed back injecting fault point generator driving voltage E_f . The calculation of these values and the subsequent calculation of the fault impedance Z_f is as follows.

In the calculation the following new symbols are used.

I_{Lss} - Pre-fault current at local-end busbar (phasor) [A]

(previously referred to as I_{pre})

V_{Lss} - Pre-fault voltage at local-end busbar (phasor) [V]

(previously referred to as V_{pre})

I_L - Superimposed current at local-end busbar (phasor) [A]

10)

(previously referred to as I)

VL - Superimposed voltage at local-end busbar (phasor) [V]

(previously referred to as V)

IR - Superimposed current at remote-end busbar (phasor) [A]

VR - Superimposed voltage at remote-end busbar (phasor) [V]

IfL - Current fed into fault from local-end source (phasor) [A]

IfR - Current fed into fault from remote-end source (phasor) [A]

Ax - Four parameters describing the two-port network

Bx representing the transmission line

Cx to the left of the fault

Dx (phasor values)

Ay - Four parameters describing the two-port network

By representing the transmission line

Cy to the right of the fault

Dy (phasor values)

y - Distance to fault from remote-end busbar [km]

To derive the fault current If only the superimposed circuit is required. Considering the two-port representation of the superimposed circuit shown in Figure 10b) and applying two-port network theory we can obtain the following equations:

For the transmission line to the left of the fault:

$$V_f = A_x \cdot V_L - B_x \cdot I_L \quad \dots(1)$$

$$I_{fL} = -[C_x \cdot V_L] + D_x \cdot I_L$$

$$I_{fL} = -[C_x \cdot V_L - D_x \cdot I_L] \quad \dots(2)$$

Where for the simple transmission line circuit being employed here,

$$A_x = 1$$

$$B_x = x.Z_L$$

$$C_x = 0$$

$$D_x = 1$$

For the transmission line to the right of the fault:

$$V_f = A_y \cdot V_R + B_y \cdot [-I_R]$$

$$V_f = A_y \cdot V_R - B_y \cdot I_R \quad \dots(3)$$

$$-I_f R = C_y \cdot V_R + D_y \cdot [-I_R]$$

$$I_f R = -[C_y \cdot V_R] + D_y \cdot I_R \quad \dots(4)$$

Where

$$A_y = 1$$

$$B_y = y \cdot Z_L$$

$$C_y = 0$$

$$D_y = 1$$

and

$$y = L - x$$

Considering the superimposed circuit in Figure 9 b) the following equation can be obtained for the remote-end source network:-

$$V_R = -Z_{sR} \cdot I_R \quad \dots(5)$$

Further, from the superimposed model in Figure 9b) it can be seen that

$$I_f = I_{fL} + I_{fR} \quad \dots(6)$$

Combining equations (2) and (4) according to equation (6):

$$I_f = -[C_x \cdot V_L - D_x \cdot I_L] - C_y \cdot V_R + D_y \cdot I_R$$

$$I_f = -C_x \cdot V_L + D_x \cdot I_L - C_y \cdot V_R + D_y \cdot I_R \quad \dots(7)$$

Equating equations (1) and (3)

$$A_x \cdot V_L - B_x \cdot I_L = A_y \cdot V_R - B_y \cdot I_R \quad \dots(8)$$

Substituting (5) into (8)

$$A_x \cdot V_L - B_x \cdot I_L = A_y \cdot [-Z_s R \cdot I_R] - B_y \cdot I_R$$

$$A_x \cdot V_L - B_x \cdot I_L = -[A_y \cdot Z_s R + B_y] \cdot I_R$$

$$I_R = -[A_y \cdot Z_s R + B_y]^{-1} \cdot [A_x \cdot V_L - B_x \cdot I_L] \quad \dots(9)$$

Substituting (9) into (7)

$$I_f = -C_x \cdot V_L + D_x \cdot I_L - C_y \cdot [-Z_s R \cdot I_R] + D_y \cdot I_R$$

$$I_f = -C_x \cdot V_L + D_x \cdot I_L + [C_y \cdot Z_s R + D_y] \cdot I_R \quad \dots(10)$$

Substituting (9) into (10)

$$I_f = -C_x \cdot V_L + D_x \cdot I_L +$$

$$[C_y \cdot Z_s R + D_y] \cdot \{-[A_y \cdot Z_s R + B_y]^{-1} \cdot [A_x \cdot V_L - B_x \cdot I_L]\}$$

$$I_f = -C_x \cdot V_L + D_x \cdot I_L -$$

$$[C_y \cdot Z_s R + D_y] \cdot [A_y \cdot Z_s R + B_y]^{-1} \cdot [A_x \cdot V_L - B_x \cdot I_L]$$

$$I_f = -C_x \cdot V_L - [C_y \cdot Z_s R + D_y] \cdot [A_y \cdot Z_s R + B_y]^{-1} \cdot [A_x \cdot V_L]$$

$$+ D_x \cdot I_L - [C_y \cdot Z_s R + D_y] \cdot [A_y \cdot Z_s R + B_y]^{-1} \cdot [-B_x \cdot I_L] =$$

$$I_f = -\{C_x + [C_y \cdot Z_s R + D_y] \cdot [A_y \cdot Z_s R + B_y]^{-1} \cdot A_x\} \cdot V_L$$

$$+ \{D_x + [C_y \cdot Z_s R + D_y] \cdot [A_y \cdot Z_s R + B_y]^{-1} \cdot B_x\} \cdot I_L$$

Letting functions,

$$M = -\{C_x + [C_y \cdot Z_s R + D_y] \cdot [A_y \cdot Z_s R + B_y]^{-1} \cdot A_x\}$$

$$N = D_x + [C_y \cdot Z_s R + D_y] \cdot [A_y \cdot Z_s R + B_y]^{-1} \cdot B_x$$

Hence, the final equation for fault current, I_f is

$$I_f = M \cdot V_L + N \cdot I_L \quad \dots(11)$$

Where

$$M = - \{ Cx + [Cy. ZsR + Dy]. [Ay. ZsR + By]^{-1} . Ax \}$$

$$N = Dx + [Cy. ZsR + Dy]. [Ay. ZsR + By]^{-1} . Px$$

$$Ax = 1$$

$$Bx = x. ZL$$

$$Cx = 0$$

$$Dx = 1$$

$$Ay = 1$$

$$By = y. ZL$$

$$Cy = 0$$

$$Dy = 1$$

$$y = L - x$$

The superimposed fault point voltage V_f is found using equation (1)

already derived and reshown below:

$$V_f = Ax. VL - Bx. IL \quad \dots(12)$$

Where

$$Ax = 1$$

$$Bx = x.ZL$$

$$Cx = 0$$

$$Dx = 1$$

The pre-fault fault point voltage V_{fss} is found using the pre-fault circuit shown in Figure 9a). Considering the two-port representation of the pre-fault circuit in Figure 10a) and applying two-port network theory we can obtain the following equation:-

$$V_{fss} = Ax. VL_{ss} - Bx. IL_{ss} \quad \dots(13)$$

Where

$$A_x = 1$$

$$B_x = x.Z_L$$

$$C_x = 0$$

$$D_x = 1$$

According to the theory on which these pre-fault and superimposed circuits are based, the superimposed back injecting fault point generator driving voltage E_f is equal and opposite to the pre-fault fault point voltage V_{fss} . Hence

$$E_f = - V_{fss} \quad \dots(14)$$

Looking at the superimposed circuit in Figure 9 b), the fault impedance Z_f is given by the equation:

$$Z_f = (V_f - E_f) / I_f \quad \dots(15)$$

The equations for the terms contained within the above equation for Z_f have already been derived. These are equations (11) to (14) which together with equation (15) enable the fault impedance Z_f to be calculated.

Having calculated the fault impedance Z_f for a range of assumed fault distances x' , the actual fault distance x is identified as that assumed fault distance for which the argument of Z_f equals (or tends towards) zero. This is based on the tested observation that only when the assumed fault position F' is at the actual fault position F does the calculated fault impedance Z_f become a purely real (resistive) value. The complete method, as given here, is summarised in Figure 6.

In a practical system there is more than one phase involved, typically there are three phases. In the case of a multi-phase system the method is the

same as has been applied in the single-phase case, with the exception that the single fault impedance to be calculated has become a network of inter-phase and phase-to-earth fault impedances. Any one of these fault impedances can be calculated and its argument used to pinpoint the fault position. However, since the fault impedance network is not solvable for the general case, the fault type needs to be identified so that one of the fault impedances can be calculated correctly.

Identifying the fault type involves determining the form of the fault point network. To do this a range of fault networks are assumed and the fault impedances, assumed to be involved, calculated. The actual form of the fault network is identified by the calculated fault impedances, involved, sharing the same assumed fault distance at which their arguments tend towards zero. This is basically the same idea as has been employed in the fault location, except it is now applied to fault type identification.

Figure 7 illustrates this method of fault type identification, showing an actual fault point network, two assumed fault point networks, one correct the other incorrect, and the variation of the calculated fault impedance arguments with assumed fault distance for each assumed network.

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

1. A method of locating the position of a fault on a power transmission line between first and second ends of the line, the method comprising the steps of:

(a) calculating the complex fault impedance at each of a plurality of assumed fault positions along the length of the line, the fault impedance at each assumed position being calculated utilising:

- (i) a measurement before and after fault occurrence of the voltage and current at said first end of the line,
- (ii) parameters of the line, and
- (iii) a source impedance of said second end of the line, and

(b) selecting as the actual fault position the assumed fault position of said plurality of assumed fault positions for which the argument of the complex fault impedance most closely equals zero.

2. A method according to Claim 1 wherein said fault impedance at each said assumed position is calculated utilising the equation:

$$Z_f = (V_f + V_{fss}) / I_f,$$

where Z_f is the fault impedance, V_f is the difference between the fault point voltage before and after fault occurrence, V_{fss} is the fault point voltage before fault occurrence, and I_f is the fault current, and where

$$V_f = A_x \cdot V_L - B_x \cdot I_L$$

$$V_{fss} = A_x \cdot V_{Lss} - B_x \cdot I_{Lss}, \text{ and}$$

$$I_f = -(C_x + [C_y \cdot Z_{sR} + D_y] \cdot [A_y \cdot Z_{sR} + B_y]^{-1} \cdot A_x) \cdot V_L \\ + (D_x + [C_y \cdot Z_{sR} + D_y] \cdot [A_y \cdot Z_{sR} + B_y]^{-1} \cdot B_x) \cdot I_L,$$

where A_x , B_x , C_x and D_x are four parameters describing a two-port network representing the transmission line between said first end and the fault, A_y , B_y , C_y and D_y are four parameters describing the two-port network representing the transmission line between said second end and the fault, V_L is the difference

between the voltage at said first end before and after fault occurrence, IL is the difference between the current at said first end before and after fault occurrence, VL_{ss} is the voltage at said first end before fault occurrence, IL_{ss} is the current at said first end before fault occurrence, and Z_{sR} is the impedance at said second end.

3. A method according to Claim 2 wherein $A_x = 1$, $B_x = x.Z_L$, $C_x = 0$, $D_x = 1$, $A_y = 1$, $B_y = y.Z_L$, $C_y = 0$, and $D_y = 1$, where x is the distance to the fault from said first end, Z_L is the transmission line impedance per unit length, and $y = L - x$, where L is the total transmission line length.

4. A method according to Claim 1 wherein: said power transmission line is a multi-phase power transmission line; said step of calculating the complex fault impedance is carried out in respect of each complex impedance of each of a plurality of forms of fault network assumed to be at each of said plurality of assumed fault positions, each complex impedance of each network at each position being calculated utilising the measurement before and after fault occurrence in respect of each phase of the line of the voltage and current at said first end of the line, parameters of the line, and the impedance at said second end of the line; said method further comprises the step of analysing the variation of each complex impedance of each assumed fault network over said plurality of assumed fault positions to determine the assumed fault network for which the argument of each complex impedance most closely equals zero at the same assumed fault position of the plurality of assumed fault positions; and said step of selecting as the actual fault position comprises selecting as the actual fault position that same assumed fault position.

5. A method of determining the form of impedance network at a fault on a multi-phase power transmission line between first and second ends of the line, the method comprising the steps of:

(a) calculating the complex impedances of each of a plurality of assumed forms of fault impedance network at each of a plurality of assumed fault positions along the length of the line, each complex impedance of each network at each position being calculated utilizing:

(i) a measurement before and after fault occurrence, in respect of each phase of the line, of the voltage and current at said first end of the line,

(ii) parameters of the line, and

(iii) a source impedance of said second end of the line,

(b) analysing the variation of each complex impedance of each assumed fault network over said plurality of assumed fault positions to determine the assumed fault network for which the argument of each complex impedance most closely equals zero at the same assumed fault position of the plurality of assumed fault positions, and

(c) selecting as the form of the actual fault impedance network the form of that determined assumed fault network.

6. A method of locating the position of a fault on a single-phase power transmission line between first and second ends of the line substantially as hereinbefore described with reference to Figures 1 to 6 and 8 to 10 of the accompanying drawings.

7. A method of locating the position of a fault on a multi-phase power transmission line between first and second ends of the line substantially as hereinbefore described with reference to the accompanying drawings.

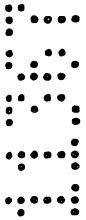


8. A method of determining the form of the impedance network at a fault on a multi-phase power transmission line between first and second ends of the line substantially as hereinbefore described with reference to the accompanying drawings.

DATED this 24th day of January 1995.

GEC ALSTHOM LIMITED

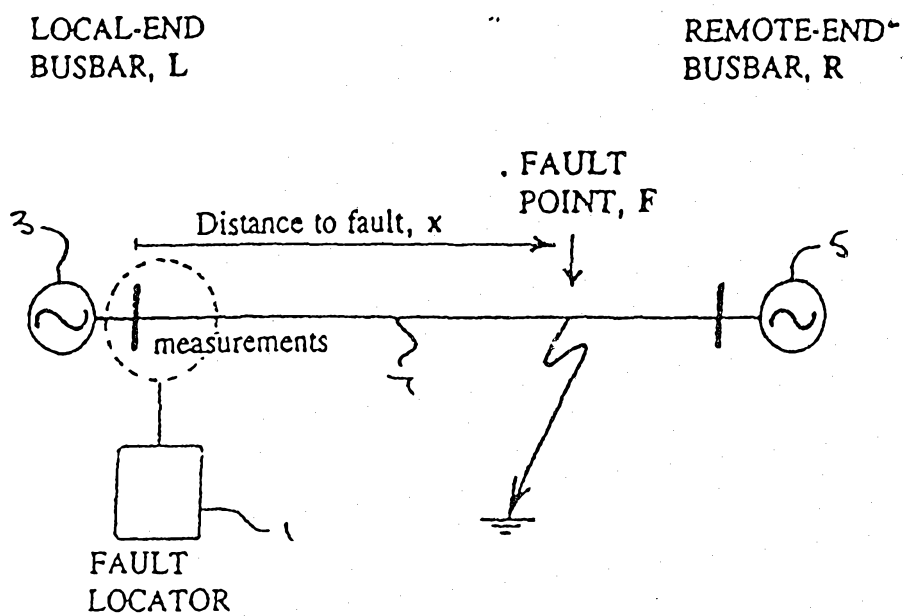
WATERMARK PATENT & TRADEMARK ATTORNEYS
290 BURWOOD ROAD
HAWTHORN. VIC. 3122.



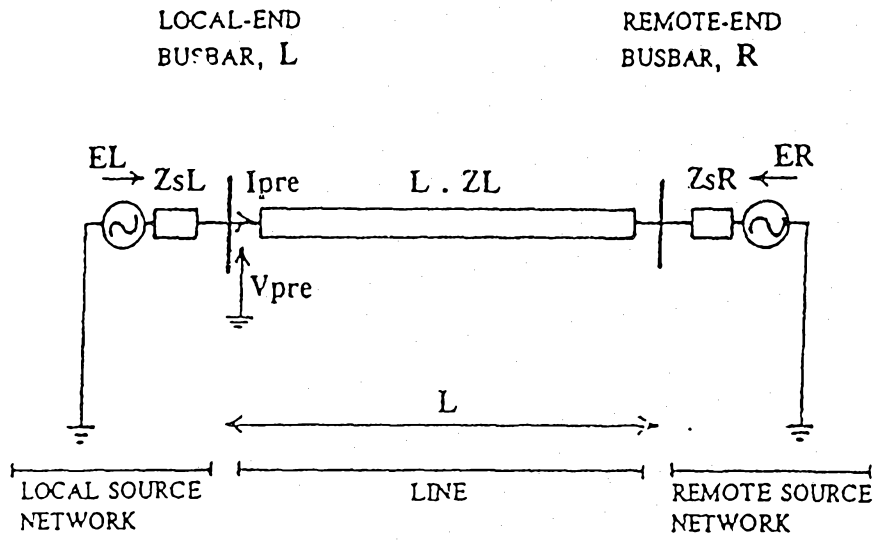
ABSTRACTA method of locating the position of a fault on a power transmission line

A method of locating the position of a fault on a power transmission line between first and second ends of the line comprising: calculating the complex fault impedance at each of a plurality of assumed fault positions along the length of the line, the fault impedance at each assumed position being calculated utilising the measurement before and after fault occurrence of the voltage and current at the first end of the line, parameters of the line, and the impedance at the second end of the line; and selecting as the actual fault position the assumed fault position of the plurality of assumed fault positions for which the argument of the complex fault impedance most closely equals zero. The method may be used with single or multi-phase power transmission lines. There is also disclosed a method of determining the form of impedance network at a fault on a multi-phase power transmission line.

FIG. 1.



a) Unfaulted system model



b) Faulted system model

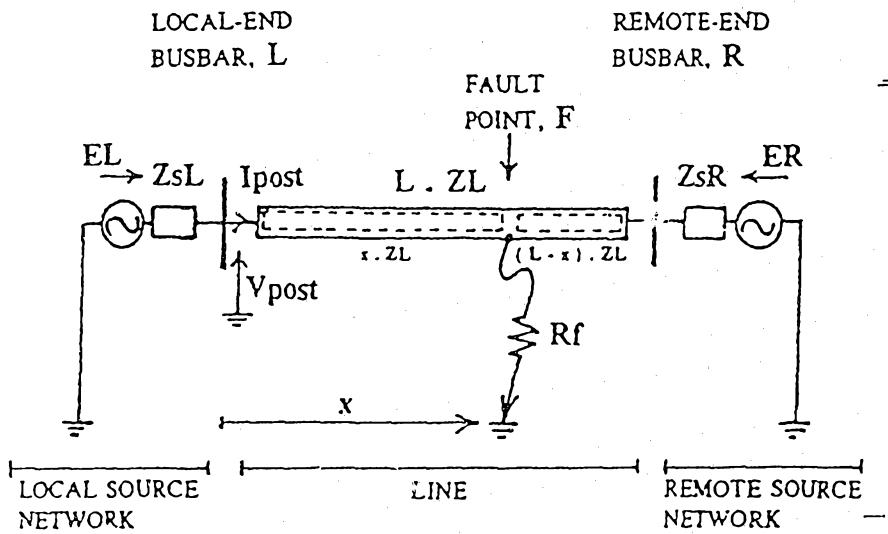
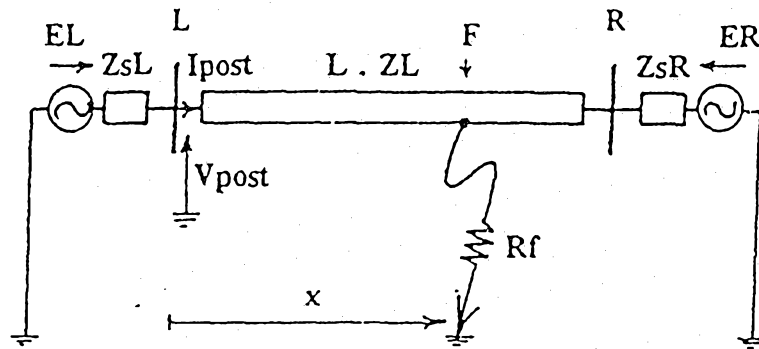
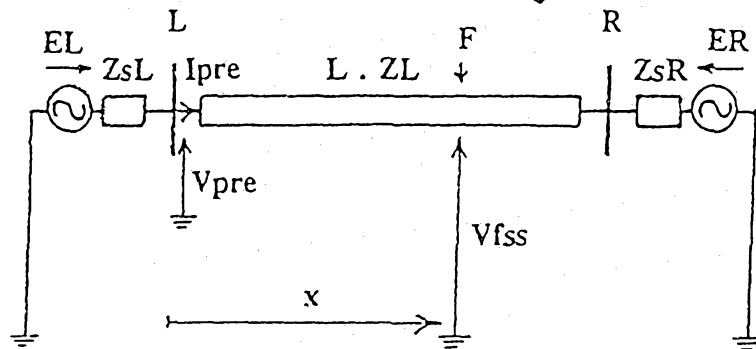


FIG. 3.

a) Faulted system model



b) Pre-fault component circuit



c) Superimposed component circuit

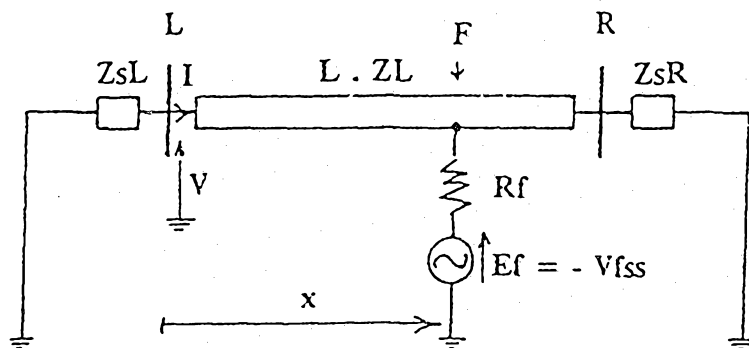
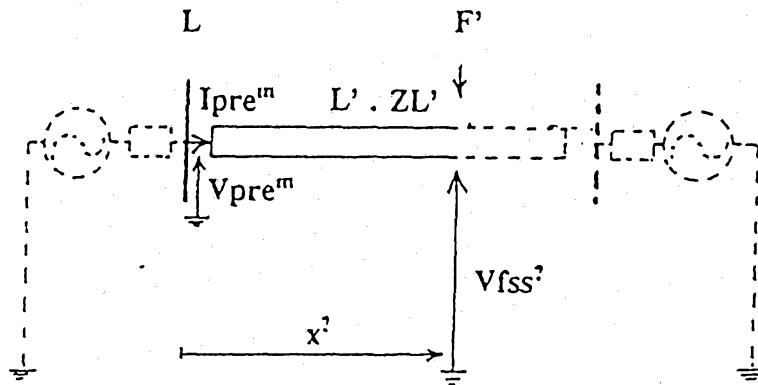
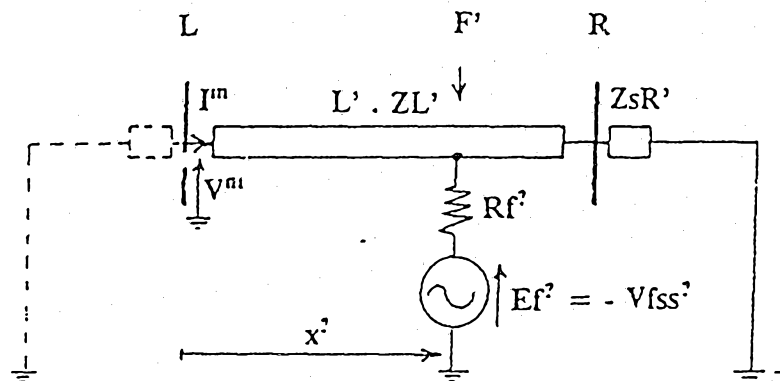


FIG. 4.

a) Pre-fault circuit



b) Superimposed circuit

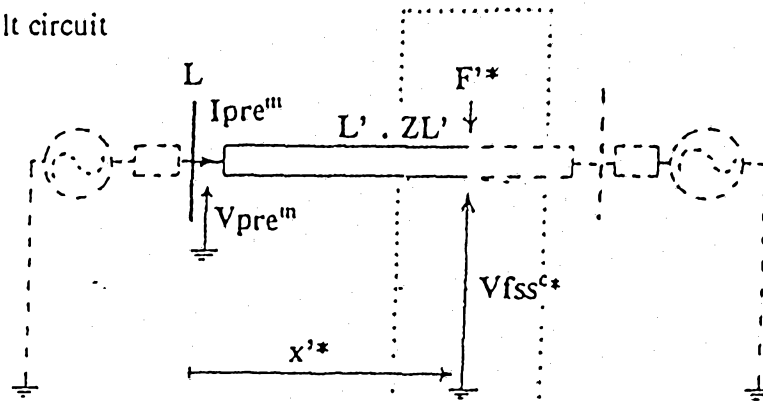


KEY

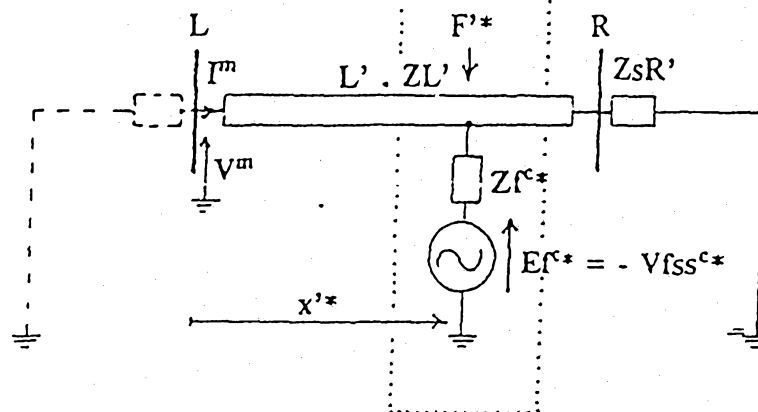
^m	- measured
[']	- assumed
[?]	- unknown

FIG. 5.

a) Pre-fault circuit



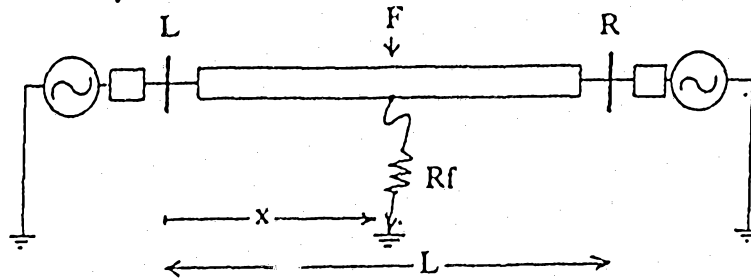
b) Superimposed circuit



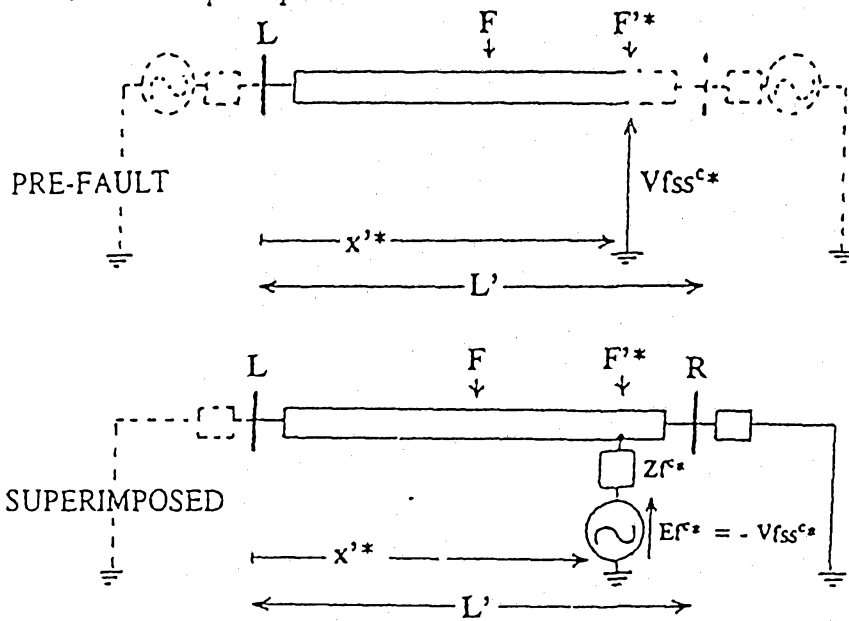
KEY

m	-	measured
$'$	-	assumed
c	-	calculated
$*$	-	changing

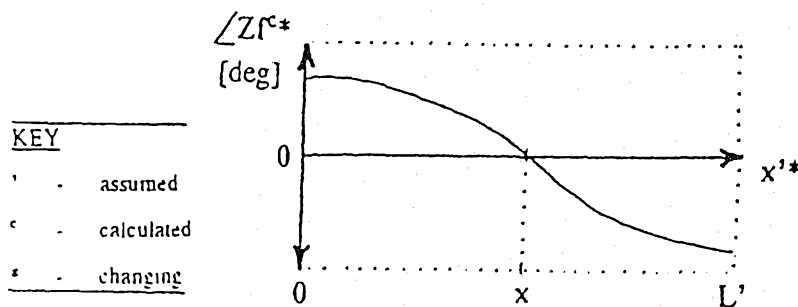
a) Actual faulted system



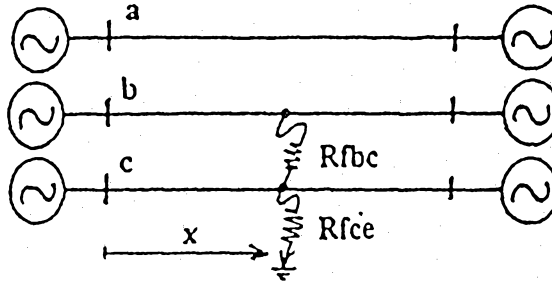
b) Pre-fault and superimposed circuits



c) Argument of calculated fault impedance, $\angle Zf^{c*}$ against assumed fault distance, x'

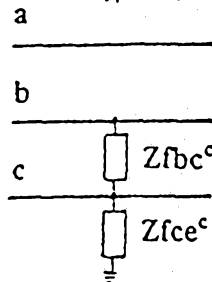


- a) Actual faulted system (showing actual fault point network)
Fault type = (b-c; c-e)

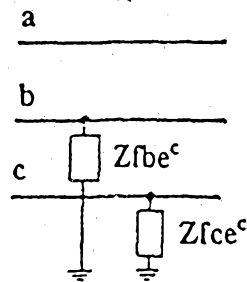


- b) Assumed fault point networks

- i) Correctly assumed case :
fault type = (b-c; c-e)



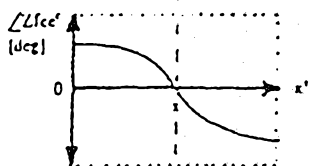
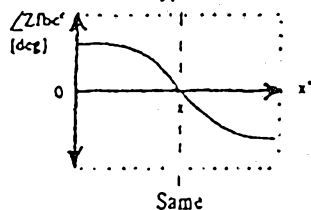
- ii) Incorrectly assumed case :
fault type = (b-e; c-e)



- c) Argument of calculated fault impedance, $\angle Zf^c$ against
assumed fault distance, x' . Done for :

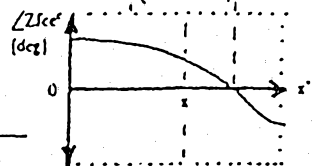
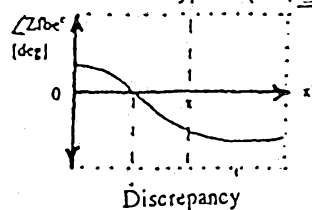
- Each assumed fault point network
- Every fault connection (hence fault impedance) assumed involved

- i) Correctly assumed case :
fault type = (b-c; c-e)



Same

- ii) Incorrectly assumed case :
fault type = (b-e; c-e)



KEY

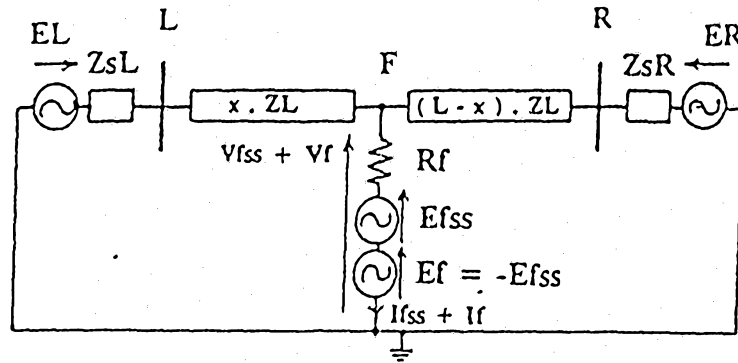
' - assumed

c - calculated

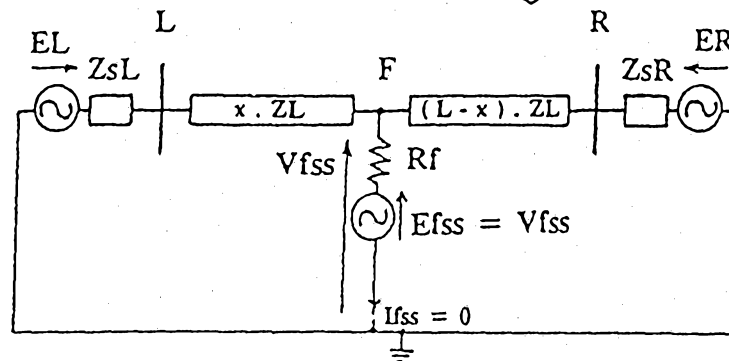
8. (10)

1. 1. 1.

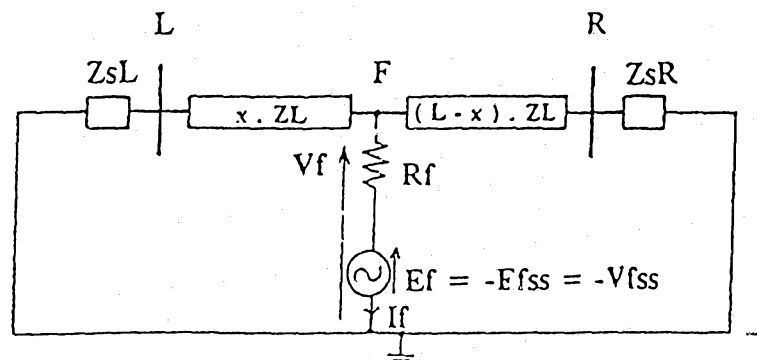
a) Faulted system model (Post-fault circuit)



b) Pre-fault component circuit



c) Superimposed component circuit

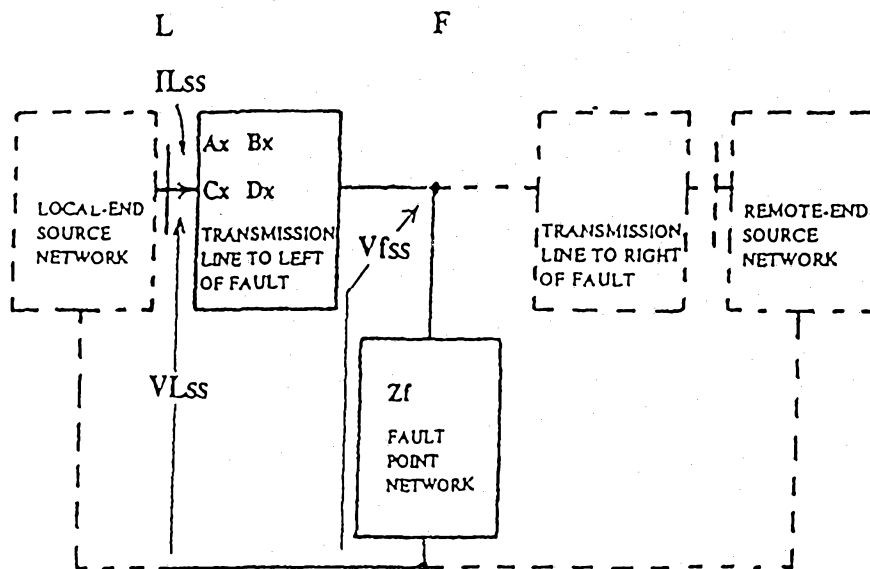


116. 9.

The diagram shows an equivalent circuit for a transmission line section of length x . It consists of a series impedance labeled $x \cdot Z_L$. The input voltage is V_{LSS} and the input current is I_{LSS} . The output voltage is V_{FSS} . The diagram is labeled L and F at the top, and x at the bottom.

FIG. 10.

a) Pre-fault circuit



b) Superimposed circuit

