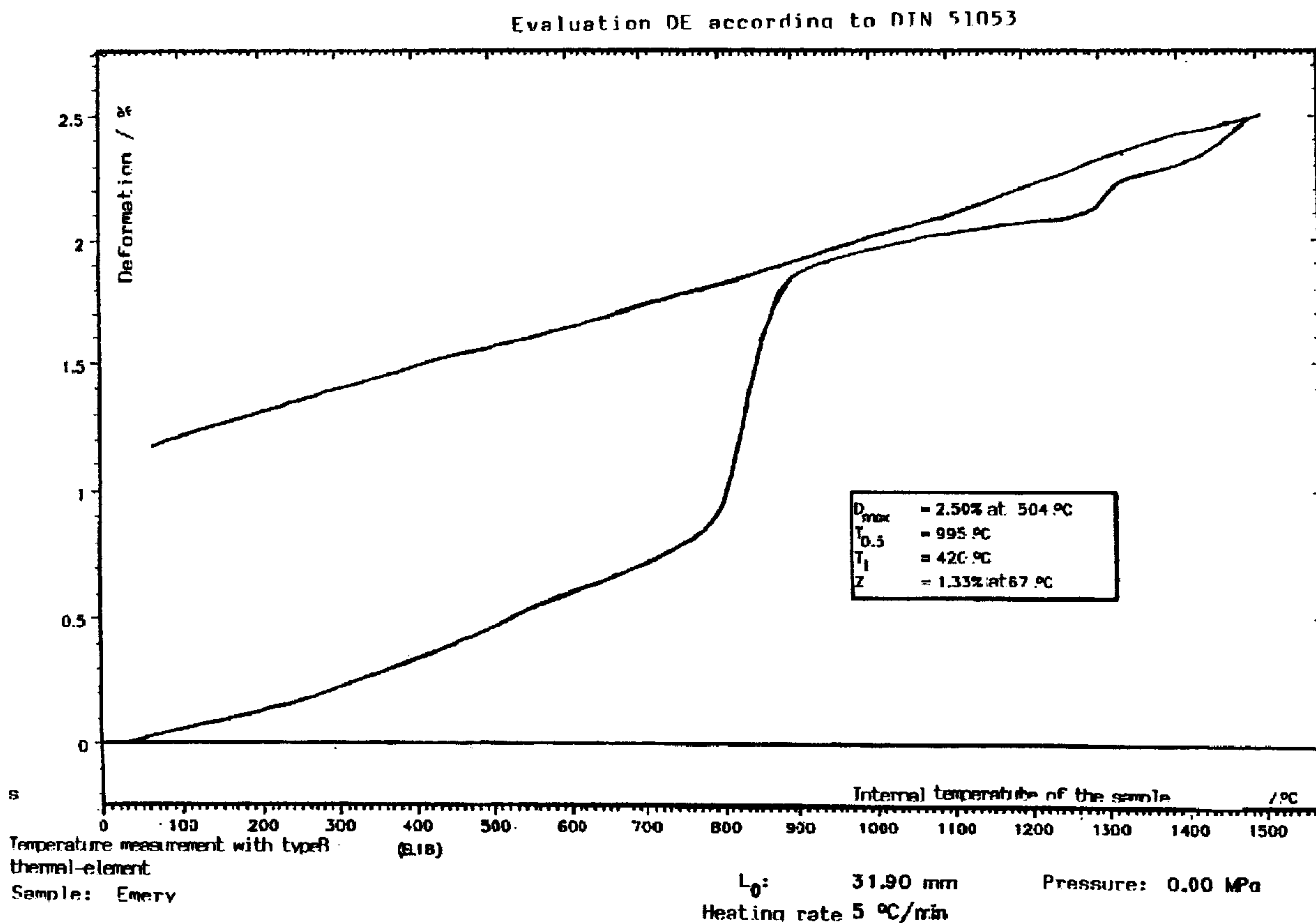




(22) Date de dépôt/Filing Date: 2002/04/02
 (41) Mise à la disp. pub./Open to Public Insp.: 2002/10/05
 (45) Date de délivrance/Issue Date: 2011/03/15
 (30) Priorité/Priority: 2001/04/05 (DE101 17 026.2)

(51) Cl.Int./Int.Cl. *C09K 21/02* (2006.01),
C04B 35/043 (2006.01), *C04B 35/06* (2006.01),
C04B 35/101 (2006.01), *C04B 35/63* (2006.01)
 (72) Inventeur/Inventor:
 BARTHA, PETER, DE
 (73) Propriétaire/Owner:
 REFRASTECHNIK HOLDING GMBH, DE
 (74) Agent: SMART & BIGGAR

(54) Titre : MELANGE IGNIFUGE, AGENT D'ELASTICITE UTILISE DANS CE MELANGE ET METHODE DE PRODUCTION DUDIT MELANGE
 (54) Title: REFRACTORY MIXTURE AND ELASTIFIER FOR THE SAME AND METHOD FOR ITS PRODUCTION



(57) Abrégé/Abstract:

The invention relates to a refractory mixture, in particular for the production of refractory moulded bodies, the mixture comprising a refractory metal oxidic main component in an amount ranging from 80 wt. % to 99.5 wt. %, and a granular elastifying component

(57) **Abrégé(suite)/Abstract(continued):**

comprising a mineral emery, the mineral emery substantially comprising Fe_2O_3 and Al_2O_3 . The mixture may further comprise a binding component such as lignin sulphonate. The invention further relates to a method for producing and using the refractory mixture.

ABSTRACT

The invention relates to a refractory mixture, in particular for the production of refractory moulded bodies, the mixture comprising a refractory metal oxidic main component in an amount ranging from 80 wt. % to 99.5 wt. %, and a granular elastifying component comprising a mineral emery, the mineral emery substantially comprising Fe_2O_3 and Al_2O_3 . The mixture may further comprise a binding component such as lignin sulphonate. The invention further relates to a method for producing and using the refractory mixture.

REFRACTORY MIXTURE AND ELASTIFIER FOR THE SAME AND METHOD FOR ITS PRODUCTION

The invention relates to a refractory mixture, in particular on the basis of magnesia, as well as an elastifier therefor and a method for producing the mixture and a moulded body thereof.

Hereinafter, the carrier of the refractory quality and thus customarily also the main component of a refractory moulded body or of refractory masses is termed a resistor. This resistor can, in the most general case, be a metallic oxide, mineral, refractory substance such as MgO, Al₂O₃, doloma or similar.

Hereinafter, the term elastifier is used to designate minerals which lead to an increase of the thermal fatigue resistance of a mixture of resistor and elastifier as opposed to a pure resistor as a result of an inherent, relatively high refractory quality, but an extension under temperature different from the resistor, through formation of micro-fissures and further effects.

Refractory moulded bodies, in particular basic refractory materials on the basis of magnesia, doloma, chromite and/or spinel (MgAl₂O₄), are used in all high-temperature processes with basic slag attacks, such as cement, lime, dolomite, iron and steel production and also in production of non-ferrous metals and in the glass industry as lining materials for furnaces, vessels and treatment systems. With high refractory quality and good chemical resistances, the materials and moulded bodies are however highly brittle, i.e. have a high module of elasticity, thus resulting in negative influences on the service life with regard to the heat extension, stresses, mechanical load and the thermal fatigue resistance.

In addition, it is known that refractory moulded bodies are also produced on the basis of Al₂O₃, with in particular bauxite, tabular oxide of aluminium or fused corundum being used as the raw material. The main fields of application for such stones are electrical furnace lids and kettles in the steel industry as well as cement kilns and furnaces in the glass industry.

It is known that the high thermal expansion stresses of basic refractory products or moulded bodies are reduced by laying the refractory stones with a mortar joint, metallic inserts such as sheets perforated sheets or nets arranged between them.

Further, numerous measures have been taken in the past in order to improve the thermal fatigue resistance, in particular at basic refractory materials. Harders/Kienow, "Feuerfestkunde, Herstellung, Eigenschaften und Verwendung feuerfester Baustoffe, Springer Verlag", 1960, Chapter 5.5, pages 754 and 755, states that the thermal fatigue resistance can be distinctly improved by the addition of chrome ore (magnesium chromite) and by a so-called mixture gap, i.e. minimisation of the share of medium grains (0.2 to 0.6 mm). However, a decisive disadvantage of the mixture gap is, on the one hand, that its effect is only sufficiently high in combination with a thermal fatigue resistance component such as magnesia or chrome ore in magnesia chrome stones if, on the other hand, no optimum grain packing density can be achieved in use of the mixture gap, as is required to achieve a high infiltration resistance against slags. Further, the quantity of chrome ore and the optimum grain fraction of the chrome ores has been defined with a view to the addition of chrome ore (e.g. Harders/Kienow, page 754). In order to achieve a satisfactory thermal fatigue resistance, quantities of chrome ore between 15 and 30 % by weight have been recognised as being suitable. The elastifying effect of the chrome ore in moulded bodies on the basis of magnesia has been unsurpassed up to now. Decisive disadvantages of the use of chrome ore as an elastifier (thermal fatigue resistance component) are however that material fatigue takes place in a change of the furnace atmosphere and that the trivalent chrome oxide in the chrome ore is converted into toxic hexavalent chrome oxide by oxidation under the effect of alkalis, with all the problems connected with this from a work-hygiene and disposal point of view.

Attempts were made at an early stage (AT-PS 158208) to add aluminium oxide, corundum and aluminium powder to magnesia stones in order to improve the thermal fatigue resistance, with spinel ($MgAl_3O_4$) being formed when the stones are burnt in situ. The spinel formed in this way is concentrated in the matrix, which means that the matrix decisive for the strength is preferably destroyed in the attack of such stones by slags. In addition, the improvement of the thermal fatigue resistance which can be achieved is limited, as the share of Al_2O_3 necessary for a decisive improvement would have to be way

above 8% by weight. However, this is not possible due to the excessive growth of the stones as a result of an increase in volume in the matrix, as otherwise dimensional accuracy and mechanical strength become too low and the porosity too high. A considerable improvement of both the heating fatigue resistance and also the chemical resistance of magnesia stones was only achieved by the addition of pre-synthesised magnesium aluminium spinel in the form of sintered or fused spinel, with the customary added quantities being between 15 and 25% by weight.

DE 41 19 251 A1 manifests that a spinel clinker of the magnesium oxide/aluminium oxide type, containing Fe_2O_3 and TiO_2 on the borders between the crystal grains, is used in a chamotte slab.

Further, DE 44 03 869 manifests a refractory ceramic mixture essentially containing MgO sinter as the carrier of the refractory quality, with a spinel of the hercynite type being used as an elastifier.

The thing common to all the attempts to replace the chrome ore with its outstanding elastification property for in particular basic refractory products by materials with less reservations with regard to environmental hygiene is that, although elastification effects can be achieved, they are inferior to those of the chrome ore. A further disadvantage is that the elastifiers used, such as hercynite, fused or sintered spinel or molten zirconium oxide are synthetic raw materials which are considerably more expensive than the natural material chrome ore.

Refractory moulded bodies and thus also the elastifying components are increasingly burdened in use, for example by greater thermal loads and thus increasing mechanical forming in industrial kilns (cement kilns, rotary lime kilns, steel casting ladles etc.) or by the increasing use of secondary combustion materials, which have a negative influence on the annexing property otherwise required, for example in rotary cement kilns, and lead to an undesired change of temperature with the accompanying destruction of the stones due to a reduced formation of annexing or flaking of annexing.

The task of the invention is to provide a mixture for refractory moulded bodies and an

elastifier, the elastification effect of which is very high and which is free of reservations as regards environmental hygiene and is reasonably priced in addition.

This task is solved with a mixture, in particular for refractory moulded bodies, comprising: a refractory metal oxidic main component, an elastifying component manifesting the mineral emery, with the mineral emery essentially comprising Fe_2O_3 and Al_2O_3 , and if need be, a binding component such as lignin sulphonate.

In various embodiments, the elastifying component in the mixture is the natural mineral emery, a synthetic material with the composition of emery, or a mixture of natural and a synthetic mineral with the composition of emery.

In various embodiments, the elastifying component in the mixture contains bauxites rich in iron. In various embodiments, the elastifying component essentially contains Fe_2O_3 and Al_2O_3 .

In various embodiments, the elastifying component is contained in the mixture in quantities of 0.5 to 15 wt. %.

In various embodiments, the elastifying component exists in a grain of 0 to 10 mm, in particular 0.5 to 4 mm. In various embodiments, the elastifier (elastifying component) manifests a grain distribution corresponding to a Fuller curve.

In various embodiments, the refractory metal oxidic main component is contained in the mixture in quantities of 80 to 99.5 wt. %.

In various embodiments, the refractory metal oxidic main component contains fused magnesia and/or sintered magnesia, oxide aluminium or CaO. In various embodiments, the refractory metal oxidic main component is essentially made of MgO , Al_2O_3 , or doloma.

In various embodiments, the refractory metal oxidic main component exists in a grain of 0 to 10 mm, in particular 0 to 5 mm. In various embodiments, the refractory metal oxidic main component manifests a grain distribution corresponding to a Fuller curve.

In various embodiments, the mixture may contain subsidiary components such as anti-oxidants, pressing aids as well as, if need be, further customary subsidiary components.

In various embodiments, the mixture may be used for the production of moulded bodies, refractory injection, vibration, ramming or casting masses.

The task is further to create a method for the production of the mixture described above, making use of the elastifier. This task is solved with a method for the production of the mixture described above by combining the refractory metal oxidic main component with the elastifying component manifesting the mineral emery, and mixing the components. In various embodiments, the method may further comprise mixing, if need be, the binding component such as lignin sulphonate.

In various embodiments, the method may further comprise combining and mixing other elastifiers, and the resultant mixture may be used to reduce the primary elastification with identical secondary elastification.

In various embodiments, the method may further comprise increasing the share of emery in the elastifying component at the cost of the other elastifiers in order to increase the primary elastification effect.

In various embodiments, the method as described above wherein the elastifying component is the natural mineral emery, a natural mineral or mixture of natural minerals, a synthetic material or a mixture of synthetic materials, or a mixture of natural and synthetic materials is used as the elastifying component.

In various embodiments, the method as described above wherein the elastifying component containing bauxites rich in iron is used.

In various embodiments, the method as described above wherein the elastifying component is used in quantities of 0.5 to 15 % by weight.

In various embodiments, the method as described above wherein the refractory metal oxidic main component is added in shares of 80 to 99.5 % by weight.

In various embodiments, the method as described above wherein the refractory metal oxidic main component containing fused magnesia and/or sintered magnesia is used.

In various embodiments, the method as described above wherein the refractory metal oxidic main component containing oxide of aluminium is used.

In various embodiments, the method as described above wherein the refractory metal oxidic main component essentially made of MgO, oxide of aluminium, doloma is used.

In various embodiments, the method as described above wherein the refractory metal oxidic main component with a grain of 0 to 10 mm, in particular 0 to 5 mm, is used.

In various embodiments, the method as described above wherein the refractory metal oxidic main component is used with a grain distribution corresponding to a Fuller curve.

In various embodiments, the method as described above wherein the elastifying component with a grain from 0 to 10 mm, in particular 0.5 to 4 mm is used.

In various embodiments, the method as described above wherein the elastifying component with a grain distribution corresponding to a Fuller curve is used.

In various embodiments, the method may further comprise combining, if need be, any further customary subsidiary components, and mixing to homogeneity, if need, be with the addition of the binding component.

In various embodiments, the method may further comprise selecting a required grain belt of various fractions of one or more components and combining for mixing.

In various embodiments, the method may further comprise portioning the mixture, and pressing to make moulded bodies at a pressure of >50, in particular 80 to 200 MPa,

preferably 130 MPa.

In various embodiments, the method may further comprise drying the pressed mixture at temperatures above 100°C, in particular at 120 to 150°C.

In various embodiments, the method may further comprise firing (burning) the mixture above the formation temperature of the mixed spinel forming following pressing and drying.

In various embodiments, the method may further comprise firing (burning) the pressed, dried mixture is burnt at 1000 to 1700°C, in particular 1200 to 1600°C.

In various embodiments, emery may be used as the elastifier (elastifying component) for refractory moulded bodies or masses.

In the invention, the natural mineral emery leads to an elastification considerably exceeding the elastification performances of known elastifiers reached up to now.

The mineral emery, for example of grained, black-brown or brown emery stone, which has resulted in a contact or regionally metamorphous way (for example Turkey, Naxos, Ural, Massachusetts, Eastern Steiermark), manifests a chemical composition comprising approximately 5.5% SiO₂, 64.7% Al₂O₃, 25.1% Fe₂O₃, 3% TiO₂, 0.5% CaO and 0.4 MgO, the rest being impurities. The composition has been registered for example in the FeO-Al₂O₃/TiO₂—SiO₂ pseudo three-material system (Fig. 2). As it is a natural mineral, the individual shares of the above mentioned chemical compounds in emery can deviate, with the result that 25 to 30% Fe₂O₃ and 62 to 75% Al₂O₃ are contained in the most general form. The remaining percentages are distributed amongst SiO₂, TiO₂, CaO and MgO.

The following Table 1 contains elastifiers used up to now. The examples entail 4 typical mixtures of refractory, basic moulded bodies with the G modules which can typically be achieved up to now (% figures as % by weight). The added quantities of the elastifiers spinel, chrome ore, hercynite and zirconium oxide known up to now correspond to amounts typical in the trade.

Table 1

	V1	V2	V3	V4
Magnesia	82%	80%	95%	95%
Spinel	18%			
Chrome ore		20%		
Hercynite			5%	
Zirconium oxide				5%
G module	8—12 GPa	8—12 GPa	15—20 GPa	15—20 GPa

It can be seen from the table that the G module, which can in fact be achieved in order to bring about satisfactory results in thermo-mechanically burdened systems, for example rotary cement kilns, by addition of comparatively high amounts of spinels or chrome ore, is comparatively high in the case of hercynite or zirconium oxide. Here, an impairment of the behaviour in use with a high mechanical load is to be expected, as can be calculated from known relevant equations, for example that by Meedom (ZKG 29 (1976), no. 12, pp. 568-571).

Products such as those shown in the table are currently in use with more or less success.

The invention is explained in an exemplary way on the basis of a diagram, showing:

Fig. 1 a heat expansion curve of emery

Fig. 2 the position of the emery in the $\text{Fe}_2\text{O}_3\text{-Al}_2\text{O}_3/\text{TiO}_2\text{-SiO}_2$ composition triangle.

Surprisingly, the elastification in a moulded body of a magnesia sinter and the mineral emery is considerably higher than with the elastifiers stated in the table. The specifically selected natural material emery essentially comprises the oxides Al_2O_3 and Fe_2O_3 as well as the subsidiary phase SiO_2 . The effect of the emery is surprising; a module of elasticity distinctly below the figures which can be achieved with the elastifiers customary up to now, such as synthetic spinel, synthetic zirconium oxide, synthetic hercynite and even natural chrome ore, can be achieved.

A further surprise is that the natural mineral emery has a course of heat expansion favourable for use as an elastifier, and a simultaneous high refractory quality and in addition high resistance against slags and alkalis, in particular at extremely high application temperatures, can be guaranteed.

Fig. 1 shows the heat expansion graph of the natural mineral emery selected as an elastifier in the invention. As can be seen from Fig. 1, the emery manifests an anomaly in heat expansion in the first heating up with a larger phase commencing around 750°C and ending around 1000°C. After this, the heat expansion is approximately constant up to 1250°C, at which point a further slight phase is formed again. In the subsequent cooling, one sees that the deformation becomes linear and constantly less, with a remaining expansion of 1.2% linear remains after the initial temperature has been reached.

With the first heat expansion phase and the small, second heat expansion phase, a primary elastification in the structure can be generated, leading to successful elastification of the moulded body during the first burning of the same. Possible causes for the elastification and disturbances of the structures such as stresses, micro-fissures and other effects, which lead to stresses brought in from the outside being broken down. Although micro-fissures can be “healed” by solid-state reactions (sintering), the elastifying effect of the emery is so high, even after the primary elastification, that a new formation of micro-fissures is imaginable and the micro-fissure system or other disturbances in the structure caused in the primary elastification can be renewed again and again (secondary elastification). This could be what the surprising elastification performance of the emery is to be put down to. Such micro-fissures are used in particular along the grain borders.

In comparison with this, the “pure” minerals corundum and hematite, of which emery is theoretically composed, manifest other coefficients of thermal expansion, with the coefficient of thermal expansion of corundum being $6.2 \times 10^{-6} \text{ K}^{-1}$ and that of hematite $7.6 \times 10^{-6} \text{ K}^{-1}$. The coefficient of thermal expansion of the periclasite (MgO) representing the resistor is $13.5 \times 10^{-6} \text{ K}^{-1}$, with that of the MA-spinel elastifier frequently used being $8.5 \times 10^{-6} \text{ K}^{-1}$. The courses of the expansion graphs of the above mentioned minerals are constant, unlike that of emery. The behaviour of the emery, i.e. its lack of constancy in

thermal expansion, cannot be explained on the basis of the constant expansion graphs for a corresponding mixture of corundum and hematite.

Naturally, emery can also be used as an elastifier in combination with other elastifiers. For example, joint use with hercynite or MA-spinel is possible. In addition, the emery can also be combined with bauxites used as elastifiers. If required, the share of primary elastification can be lowered with a per se constant secondary elastification as a result of the combination. Further, not only the use of the natural mineral emery, but also the use of a synthesised mineral with the composition of the emery is also possible in its place.

This synthetic mineral can, for example, be produced by sintering or fusing the initial substances ferric oxide (calculated as Fe_2O_3) and magnesium oxide.

The invention is explained below on the basis of an example.

A fused magnesia with a maximum grain of 4 mm and a grain distribution corresponding to a typical Fuller curve is mixed with the natural mineral emery in a grain distribution of 0.5 to 4 mm. In order to bind the dry mixture, a necessary quantity of lignin sulphonate is added and the homogenised mixture fed to a hydraulic press customary for the refractory area. The combination or the mixture is pressed at a pressure of 130 Megapascal. The moulded bodies obtained in this way are dried in a drying step at above 100°C . After this, the moulded bodies are burnt at 1470°C . This sintering temperature is above the formation temperature of the mixed spinel which forms.

The following table portrays the thermo-mechanical properties achieved as a function of the amount of emery added. For this, 3 exemplary mixtures were produced according to the example above, with the share of emery being increased from 2 to 10 % at the cost of the share of magnesia.

Table 2

	V5	V6	V7
Magnesia	98%	95%	90%
Emery	2%	5%	10%
G module	10.4 GPa	7.5 GPa	2.7 GPa

As can be seen from the table, the elasticity, characterized by the G module, can be varied within wide limits and is a function of the amount of the natural mineral emery added in accordance with the invention within these limits. It is surprising that even small amounts of only 2% of emery lead to elastic modules like those also observed for elastifiers known up to now. Under the peripheral condition of a strength of refractory stones necessary for the use in order to counteract the stresses occurring, specifically bending stresses, for which ceramic products are most sensitive in general, with a figure of about 3 Megapascal, the G module can be reduced to a figure of 2.7 Gigapascal. Such a low figure has not yet been achieved in any case for refractory stones. The mechanism which leads to the dramatic reduction of the G module is not yet known. It is presumably the formation of micro-fissures between the resistor and the added emery already described, caused by the primary and secondary elastification, or it is disturbances caused by differing thermal expansion coefficients.

The moulded bodies produced in accordance with the invention can be used beneficially wherever high changes in temperature occur and mechanical and thermo-mechanical stresses occur. For example, this can be sinter and transition zones of cylindrical rotary kilns in the stones and soils industry, in the ferrous and non-ferrous metal industry as well as fusion and treatment vessels in the ferrous and non-ferrous metal industry.

A benefit in the mixture and the moulded body according to the invention is that an elastification of the moulded body is achieved by the addition of the emery which is clearly above the elastification by chrome ore achieved up to now.

A further benefit is that the elastifier used in accordance with the invention is by no means toxic and can thus be used completely free of reservations, both with regard to industrial hygiene and also disposal.

Yet another advantage is the fact that it is a raw material occurring in natural deposits and in quantities worth mining. No large amounts of energy are necessary for its treatment or production, such as, for example, in the production of synthetic raw materials like fused spinel. Another benefit is the fact that this natural raw material produces a higher elastification performance in moulded bodies with considerably lower quantities than the synthetic elastifiers and is thus more favourable in price in this regard.

CLAIMS:

1. A refractory mixture, the mixture comprising:
a refractory metal oxidic main component in an amount ranging from 80 wt. % to 99.5 wt. %; and
a granular elastifying component comprising a mineral emery, the mineral emery substantially comprising Fe_2O_3 and Al_2O_3 .
2. The mixture according to claim 1 further comprising a binding component.
3. The mixture according to claim 2 wherein the binding component comprises lignin sulphonate.
4. The mixture according to any one of claims 1 to 3 wherein the granular elastifying component is a natural mineral emery.
5. The mixture according to any one of claims 1 to 3 wherein the granular elastifying component is a synthetic material having a composition of emery.
6. The mixture according to any one of claims 1 to 3 wherein the granular elastifying component is a mixture of a natural mineral emery and a synthetic mineral having a composition of emery.
7. The mixture according to any one of claims 1 to 6 wherein the granular elastifying component further comprises a bauxite rich in iron.
8. The mixture according to any one of claims 1 to 7 wherein the granular elastifying component essentially contains Fe_2O_3 and Al_2O_3 .
9. The mixture according to any one of claims 1 to 8 wherein the granular elastifying component is in an amount ranging from 0.5 wt. % to 15 wt. %.
10. The mixture according to any one of claims 1 to 9 wherein the refractory metal oxidic main component comprises fused magnesia, sintered magnesia, or a combination

thereof.

11. The mixture according to any one of claims 1 to 10 wherein the refractory metal oxidic main component comprises an oxide of aluminium.
12. The mixture according to any one of claims 1 to 11 wherein the refractory metal oxidic main component is essentially made of MgO.
13. The mixture according to any one of claims 1 to 11, wherein the refractory metal oxidic main component is essentially made of Al₂O₃.
14. The mixture according to any one of claims 1 to 11, wherein the refractory metal oxidic main component comprises CaO.
15. The mixture according to any one of claims 1 to 11 or claim 14 wherein the refractory metal oxidic main component is essentially made of doloma.
16. The mixture according to any one of claims 1 to 15 wherein the refractory metal oxidic main component comprises a grain size of 0 to 10 mm.
17. The mixture according to any one of claims 1 to 15 wherein the refractory metal oxidic main component comprises a grain size of 0 to 5 mm.
18. The mixture according to any one of claims 1 to 17 wherein the refractory metal oxidic main component comprises a grain size distribution corresponding to a Fuller curve.
19. The mixture according to any one of claims 1 to 18 wherein the granular elastifying component comprises a grain size of 0 to 10 mm.
20. The mixture according to any one of claims 1 to 18 wherein the granular elastifying component comprises a grain size of 0.5 to 4 mm.
21. The mixture according to any one of claims 1 to 20 wherein the granular elastifying

component comprises a grain size distribution corresponding to a Fuller curve.

22. The mixture according to any one of claims 1 to 21 further comprising a subsidiary component comprising an anti-oxidant, a pressing aid, or a combination thereof.
23. The mixture according to claim 22 further comprising a standard subsidiary component.
24. Use of the mixture according to any one of claims 1 to 23 for producing a moulded body.
25. Use of the mixture according to any one of claims 1 to 23 for producing a refractory injection mass, a refractory vibration mass, a refractory ramming mass, or a refractory casting mass.
26. A method for producing a refractory mixture, the method comprising:

combining a refractory metal oxidic main component in an amount ranging from 80 wt. % to 99.5 wt. % with a granular elastifying component comprising a mineral emery, the mineral emery comprising Fe_2O_3 and Al_2O_3 to form the refractory mixture.
27. The method according to claim 26 further comprising combining a binding component.
28. The method according to claim 27 wherein the binding component comprises lignin sulphonate.
29. The method according to any one of claims 26 to 28, wherein the mineral emery in the granular elastifying component reduces a primary elastification property of the refractory mixture while maintaining a secondary elastification property of the refractory mixture as it was.
30. The method according to claim 29 further comprising combining at least one

further elastifying component wherein the mineral emery and the at least one further elastifying component reduce the primary elastification property of the refractory mixture while maintaining the secondary elastification property of the refractory mixture as it was.

31. The method according to any one of claims 26 to 30 wherein a content of the mineral emery in the granular elastifying component is higher than a content of the at least one further elastifying component such that the primary elastification property of the refractory mixture is increased.
32. The method according to any one of claims 26 to 31 wherein the granular elastifying component comprises a natural mineral or a mixture of natural minerals.
33. The method according to any one of claims 26 to 32 wherein the at least one further elastifying component comprises at least one synthetic material.
34. The method according to any one of claims 26 to 32 wherein the at least one further elastifying component comprises a mixture of a natural material and a synthetic material.
35. The method according to any one of claims 26 to 34 wherein the granular elastifying component is a natural mineral emery.
36. The method according to any one of claims 26 to 35 wherein the granular elastifying component further comprises a bauxite rich in iron.
37. The method according to any one of claims 26 to 36 wherein the granular elastifying component is in an amount ranging from 0.5 wt. % to 15 wt. %.
38. The method according to any one of claims 26 to 37 wherein the refractory metal oxidic main component comprises fused magnesia, sintered magnesia or a combination thereof.
39. The method according to any one of claims 26 to 38 wherein the refractory metal

oxidic main component comprises an oxide of aluminium.

40. The method according to any one of claims 26 to 39 wherein the refractory metal oxidic main component is essentially made of MgO.
41. The method according to any one of claims 26 to 40 wherein the refractory metal oxidic main component is essentially made of an oxide of aluminium.
42. The method according to any one of claims 26 to 41 wherein the refractory metal oxidic main component is essentially made of doloma.
43. The method according to any one of claims 26 to 42 wherein the refractory metal oxidic main component comprises a grain size of 0 to 10 mm.
44. The method according to any one of claims 26 to 43 wherein the refractory metal oxidic main component comprises a grain size of 0 to 5 mm.
45. The method according to any one of claims 26 to 44 wherein the refractory metal oxidic main component comprises a grain size distribution corresponding to a Fuller curve.
46. The method according to any one of claims 26 to 45 wherein the granular elastifying component comprises a grain size from 0 to 10 mm.
47. The method according to any one of claims 26 to 46 wherein the granular elastifying component comprises a grain size from 0.5 to 4 mm.
48. The method according to any one of claims 26 to 47 wherein the granular elastifying component comprises a grain size distribution corresponding to a Fuller curve.
49. The method according to any one of claims 26 to 48 further comprising combining to homogeneity a standard subsidiary component.
50. The method according to any one of claims 26 to 49 further comprising selecting a

grain size range of the refractory metal oxidic main component, the granular elastifying component or a combination thereof prior to combining.

51. The method according to any one of claims 26 to 50 further comprising portioning the refractory mixture into suitable portions and pressing the refractory mixture at a pressure greater than 50 MPa to form a moulded body.
52. The method according to any one of claims 26 to 50 further comprising portioning the refractory mixture into suitable portions and pressing the refractory mixture at a pressure of 80 to 200 MPa to form a moulded body.
53. The method according to any one of claims 26 to 50 further comprising portioning the refractory mixture into suitable portions and pressing the refractory mixture at a pressure of 130 MPa to form a moulded body.
54. The method according to any one of claims 51 to 53 further comprising drying the moulded body at a temperature above 100°C to form a dried moulded body.
55. The method according to any one of claims 51 to 53 further comprising drying the moulded body at a temperature above 120 to 150°C to form a dried moulded body.
56. The method according to claim 54 or 55 further comprising firing the dried moulded body above a temperature required for forming a mixed spinel to obtain a fired moulded body.
57. The method according to claim 56 further comprising drying the fired moulded body at a temperature ranging from 1000 to 1700°C.
58. The method according to claim 56 further comprising drying the fired moulded body at a temperature ranging from 1200 to 1600°C.
59. Use of emery as an elastifier for a refractory moulded body.
60. Use of emery as an elastifier for a refractory mass.

61. Use of a granular elastifying component comprising a mineral emery, the mineral emery substantially comprising Fe_2O_3 and Al_2O_3 for reducing a primary elastification property of a refractory mixture while maintaining a secondary elastification property of the refractory mixture as it was, the refractory mixture comprising a refractory metal oxidic main component in an amount ranging from 80 wt. % to 99.5 wt. % and the granular elastifying component.
62. The use according to claim 61 wherein the refractory mixture further comprises at least one further elastifying component for reducing the primary elastification property of the refractory mixture while maintaining the secondary elastification property of the refractory mixture as it was.
63. A granular elastifying component comprising a mineral emery, the mineral emery substantially comprising Fe_2O_3 and Al_2O_3 for use in reducing a primary elastification property of a refractory mixture while maintaining a secondary elastification property of the refractory mixture as it was, the refractory mixture comprising a refractory metal oxidic main component in an amount ranging from 80 wt. % to 99.5 wt. % and the granular elastifying component.
64. The granular elastifying component according to claim 63 wherein the refractory mixture further comprises at least one further elastifying component for reducing the primary elastification property of the refractory mixture while maintaining the secondary elastification property of the refractory mixture as it was.

Evaluation DE according to DIN 51053

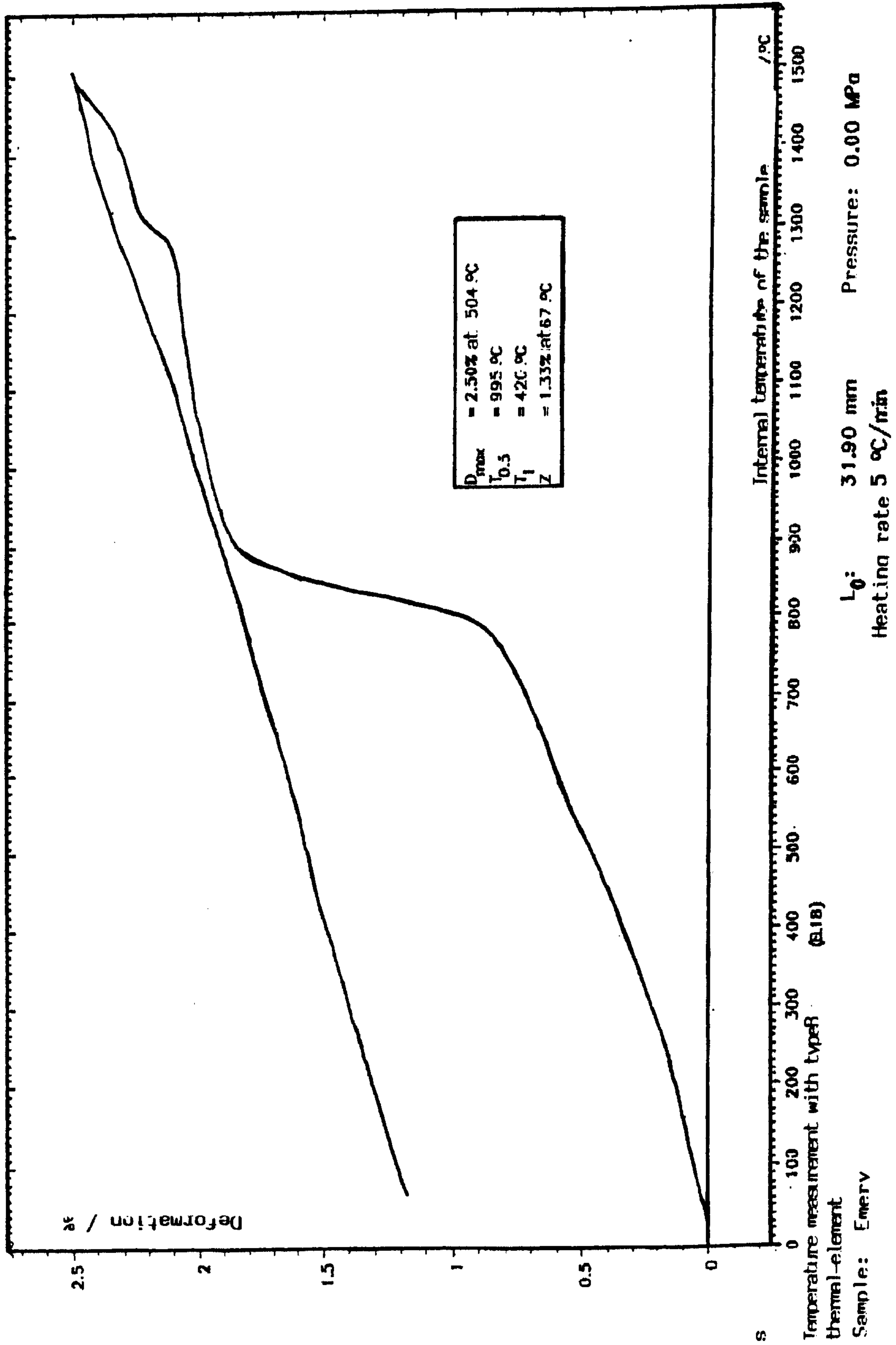


Fig. 1

COMPOSITION
OF EMERY

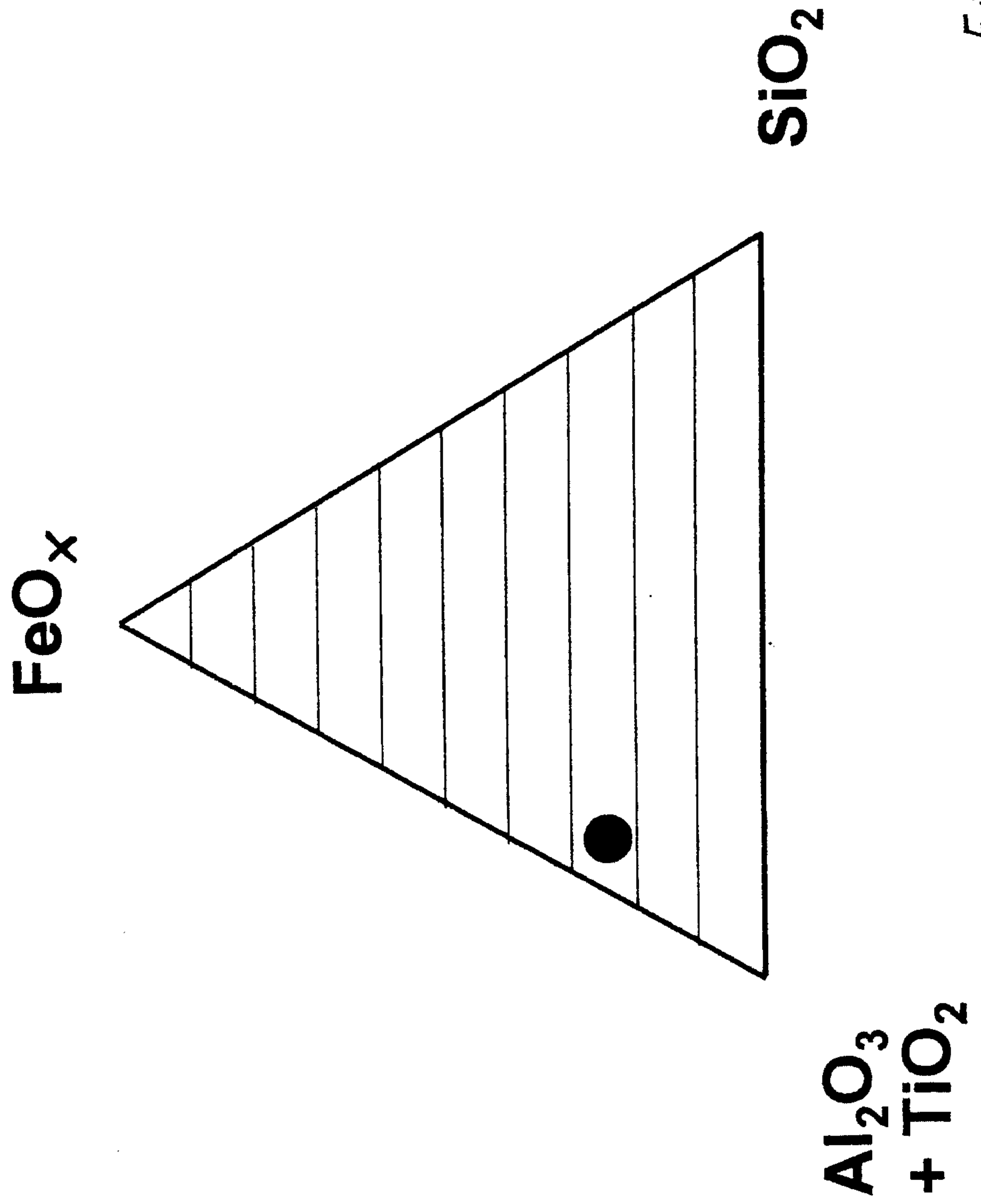


Fig. 2

Evaluation DE according to DIN 51053

