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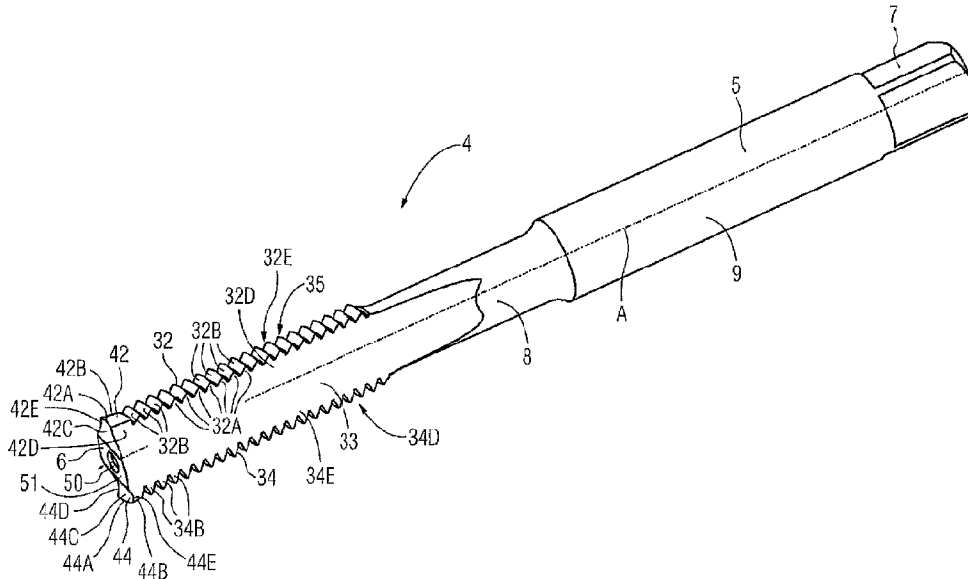
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(57) **Abrégé/Abstract:**

The thread generating tool for producing a thread in a workpiece has the following features:

- a) the tool is rotatable about a tool axis (A),
- b) the tool has a number $n \geq 1$ of groove generating regions (42, 44) for respectively generating a groove in the workpiece and a number $m \geq 1$ of thread generating regions (32, 34) for generating the thread in the workpiece,
- c) each of the m thread generating regions is arranged behind one of the n groove generating regions in an axial projection parallel to the tool axis (A) and has in cross section in the axial projection a smaller extent than this groove generating region.

Abstract

The thread generating tool for producing a thread in a workpiece has the following features:

- a) the tool is rotatable about a tool axis (A),
 - b) the tool has a number $n \geq 1$ of groove generating regions (42, 44) for
5 generating in each case one groove in the workpiece and a number $m \geq 1$
of thread generating regions (32, 34) for generating the thread in the
workpiece,
 - c) each of the m thread generating regions is arranged behind one of the n
10 groove generating regions as viewed in an axial projection parallel to the
tool axis (A), and has a smaller extent than said groove generating region
as viewed in cross section in the axial projection.
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THREAD GENERATING TOOL FOR PRODUCING A THREAD IN A WORKPIECE

The invention relates to a thread generating tool for producing a thread in a workpiece.

For thread generation or thread reworking, both cutting and also non-cutting processes and threading tools are known. Cutting thread generation is based on material removal from the workpiece in the region of the thread flight. Non-cutting thread generation is based on deformation of the workpiece and generation of the thread flight in the workpiece by pressure. An overview of thread generating tools and working methods in use is given in *Handbuch der Gewindetechnik und Frästechnik [Manual of threading practice and milling practice]*, publisher: EMUGE-FRANKEN, publishing firm: Publicis Corporate Publishing, year of publication: 2004 (ISBN 3-89578-232-7), designated below only as "EMUGE manual".

Falling within the scope of cutting thread generation are taps (cf. *EMUGE manual*, chapter 8, pages 181 to 298) and thread milling cutters (cf. *EMUGE manual*, chapter 10, pages 325 to 372) and also, only for external threads, thread-cutting dies (cf. *EMUGE manual*, chapter 11, pages 373 to 404).

A tap is a thread-cutting tool whose cutting edges or thread cutting teeth are arranged along an external thread beneath the thread pitch of the thread to be generated. During the generation of the thread, the tap is moved with a feed motion axially with respect to the tool axis, and whilst being rotated about its tool axis with a rotational speed which is dependent on the axial feed speed in accordance with the thread pitch, into a cylindrical core hole in a workpiece, wherein the tool axis of the tap is oriented coaxially with respect to the central axis of the core hole, and the cutting edges of said tap are permanently in engagement with the workpiece at the core hole wall (continuous cutting), such that a continuous thread flight is generated on the core hole wall.

Falling within the scope of non-cutting thread generating tools are so-called cold-forming taps (cf. *EMUGE manual, chapter 9, pages 299 to 324*) and, only for external threads, thread-rolling tools (cf. *EMUGE manual, chapter 11, pages 373 to 404*).

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Cold-forming taps are threading tools with an approximately spirally or helically encircling thread profile, along which are arranged a plurality of pressing lobes (also referred to as shaping teeth, cold-forming teeth or shaping wedges) which are formed by generally rounded polygon corner regions, which are offset with respect to one another and project further outward, of an approximately polygonal cross section of the cold-forming tap. During the generation of the thread, the cold-forming tap is, similarly to the tap, moved with a feed motion axially with respect to the tool axis and whilst being rotated about its tool axis into a cylindrical core hole in a workpiece, wherein the tool axis of the tap is oriented coaxially with respect to the central axis of the core hole. The rotational speed and axial feed speed are coordinated with one another in accordance with the thread pitch. The pressing lobes of the cold-forming tap are permanently in engagement with the workpiece at the core hole wall, and press the thread flight into the core hole wall by plastic deformation, such that a continuous thread flight is generated on the core hole wall.

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Furthermore, combination tools which operate exclusively by cutting processes and which are composed of drills and thread milling cutters are known, specifically so-called drill thread milling cutters (cf. *EMUGE manual, chapter 10, page 354*) and so-called circular drill thread milling cutters (cf. *EMUGE manual, chapter 10, page 355*), by means of which firstly the core hole for the thread can be generated, and then the thread can be generated in the core hole.

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The tool shank of the specified thread generating tools is generally of at least approximately cylindrical form about its longitudinal axis and/or is received and held with its end facing away from the workpiece in the chuck of a machine tool.

30

The direction of rotation of taps and cold-forming taps during the generation of the thread corresponds to the turning direction of the thread to be generated. The known screws or screw threads screwed into the generated internal thread comprise continuous helical external threads which are complementary to the internal threads.

It is now an object of the invention to specify a novel tool for generating a thread, in particular for generating an internal thread.

- 10 Said object is achieved by means of a tool having the features of claim 1. Advantageous embodiments and refinements of the tool according to the invention emerge from the patent claims which are dependent on patent claim 1.

The tool for generating a thread in a workpiece as claimed in patent claim 1 is rotatable about a tool axis and has at least one groove generating region for generating a groove in the workpiece, and at least one thread generating region for generating the thread in the workpiece. Here, each thread generating region is arranged behind the at least one groove generating region as viewed in an axial projection parallel to the tool axis, and has a smaller extent than said groove generating region, or remains entirely within the projection (or: within the projection shadow) of the groove generating region, as viewed in cross section in the axial projection. In this way, each thread generating region has a spacing to the groove rim, in particular to the groove base, in a projection plane perpendicular to the axial direction, and/or can in the axial direction be freely moved through or introduced into or passed through the groove generated in the workpiece by the groove generating region situated in front as viewed in the projection.

In other words, it is thus the case according to the invention that the tool has a number $n \geq 1$ of groove generating regions for generating in each case one groove in the workpiece and a number $m \geq 1$ of thread generating regions for

It is now an object of the invention to specify a novel tool for generating a thread, in particular for generating an internal thread.

- 5 Said object is achieved by means of a tool having the features described herein. Advantageous embodiments and refinements of the tool are also described herein.

The tool for generating a thread in a workpiece is rotatable about a tool axis and has at least one groove generating region for generating a groove in the workpiece,
10 and at least one thread generating region for generating the thread in the workpiece. Here, each thread generating region is arranged behind the at least one groove generating region as viewed in an axial projection parallel to the tool axis, and has a smaller extent than said groove generating region, or remains entirely within the projection (or: within the projection shadow) of the groove generating
15 region, as viewed in cross section in the axial projection. In this way, each thread generating region has a spacing to the groove rim, in particular to the groove base, in a projection plane perpendicular to the axial direction, and/or can in the axial direction be freely moved through or introduced into or passed through the groove generated in the workpiece by the groove generating region situated in front as
20 viewed in the projection.

In other words, it is thus the case according to the invention that the tool has a number $n \geq 1$ of groove generating regions for generating in each case one groove in the workpiece and a number $m \geq 1$ of thread generating regions for

generating the thread in the workpiece, wherein m is generally at least as large as n , that is to say $m \geq n$, preferably $m = n$. Each of the m thread generating regions is arranged behind one of the n groove generating regions as viewed in an axial projection parallel to the tool axis (or conversely: a groove generating region is situated in front of each thread generating region as viewed in the axial projection) and has a smaller extent than said groove generating region as viewed in cross section in the axial projection.

The tool according to the invention may be used in the following intended manner to produce a thread in a workpiece:

generating a number n of grooves in a wall, which encircles the thread axis, of the workpiece by means of the n groove generating regions of the tool and by means of a movement of the tool substantially axial with respect to the thread axis, wherein each groove generating region of the tool generates an associated groove;

introducing the thread generating regions, which are situated behind the groove generating regions, of the thread generating tool into the generated associated grooves in the wall of the workpiece in a direction along the associated groove, wherein the thread generating region projects, in a direction radial with respect to the thread axis, into the associated groove so as to maintain a radial spacing from the groove base;

generating the thread in each wall sub-region, adjoining the groove(s), of the wall of the workpiece by rotating the thread generating tool about the thread axis by a predefined angle of rotation and with a simultaneous axial feed motion of the thread generating tool coaxially with respect to the tool axis with an axial feed speed adapted to the rotational speed of the rotational movement and to the thread pitch, wherein, during the rotation and the simultaneous axial feed movement, each thread generating region engages into the associated wall sub-region and generates an associated part of a thread flight, and after the rotation projects into the same groove again or into another groove in the wall;

moving the thread generating regions of the thread generating tool out of the associated grooves in a direction along the grooves.

In a preferred variant, at least some of the n groove generating regions are
5 formed as cutting groove generating regions with groove generating cutting edges, wherein the groove generating cutting edges are formed in particular as reaming cutting edges and/or are arranged on a face side of the tool.

At least some of the cutting groove generating regions and/or groove generating
10 cutting edges may have, in an axial direction and/or in a circumferential direction, in each case at least one step or edge which is provided in particular as a chip-splitting step or edge.

In a preferred variant, the or each groove generating region has a groove cutting
15 edge or face cutting edge oriented toward or situated on the face side, wherein said groove cutting edges are generally the radially furthest outward projecting parts of the tool, at least in the front portion thereof.

In one embodiment, the groove cutting edges are of at least approximately circular
20 lar form and/or the outer radius of the groove cutting edges (42A) is greater than the radius of the first thread generating sub-region or of the thread generating region as a whole.

In one embodiment, the or each groove cutting edge is adjoined laterally in a circumferential
25 direction by a side cutting edge, which is at the front in the direction of rotation about the tool axis, and preferably also by a side region which is at the rear in the direction of rotation about the tool axis. During the rotation of the tool in the direction of rotation which takes place for the generation of the thread, the front side cutting edge cuts laterally into the workpiece, wherein
30 there adjoins preferably in a radially inward direction a lateral rake surface. The

rear side region is, by contrast, generally at an obtuse angle, that is to say does not have a cutting action and is preferably of convex form.

5 Axially behind the groove cutting edge there generally adjoins a free surface which preferably slopes downward, in particular in a linear or conical fashion, from the outer radius at the groove cutting edge to a radius which is smaller than the radius of the first pressing lobe or of the first thread generating sub-region.

10 The groove cutting edge is adjoined in a radially inward direction by a face-side rake surface which runs axially rearward in a linear or else concave fashion and on which chips produced during the generation, in particular reaming, of the groove with the groove cutting edge are discharged. The face-side rake surface runs preferably from a lowest point axially forward again to a planar central region oriented perpendicular to the tool axis, which central region surrounds a
15 central opening of a central duct of the tool, by which central duct coolant and/or lubricant can be supplied.

In a further embodiment, at least some of the n groove generating regions are formed as groove generating regions which operate in a non-cutting manner
20 and/or which operate by plastic deformation or impression of the workpiece material. Each groove generating region preferably has a shaping spine (or: shaping ridge, pressing ridge) which runs substantially in a circumferential direction around the tool axis and which, as viewed in an axial direction, is the radially highest elevation of the groove generating region and/or projects radially furthest
25 outward, and generally also a front surface which is situated in front of the shaping spine in an axial direction and which serves as a run-on surface by means of which the groove generating region presses into the workpiece surface for the first time and with slowly increasing deformation force. The front surface connects a front profile, which is situated radially further inward than the shaping
30 spine and which is arranged in particular on the face side of the tool, to the shaping spine in an axial direction. Axially behind the shaping spine, each groove

generating region has a back surface which slopes downward from the shaping spine in an axial direction and which provides a free space for the flow of work-piece material.

- 5 The shaping spine preferably has a maximum which projects radially furthest outward, and said shaping spine slopes downward radially from the maximum in one flank to a first end point which is situated radially further inward than the maximum, and in a further flank to a second end point which is situated radially further inward than the maximum. It is preferably also the case that one end
10 point is situated radially further inward than the other end point and/or one flank of the shaping spine is shorter than the other flank.

The front profile generally has a similar shape to the shaping spine with a maximum and two flanks sloping downward from the maximum to end points, wherein
15 in this case the front surface preferably connects corresponding points and lines, such as corresponding maxima and/or corresponding end points and/or corresponding flanks of the front profile and of the shaping spine, to one another. The front surface preferably runs between the front profile and the shaping spine in an axial direction in a substantially linear or convexly inwardly or outwardly
20 curved manner, or following an arbitrary continuous function.

In one embodiment, the n groove generating regions are arranged at uniform angular intervals of $360^\circ/n$ relative to one another about the tool axis, that is to say they are uniformly distributed. A non-uniform distribution is however also possible.
25

In one variant of the invention, the angle component of one or each groove generating region and of the thread generating regions, situated therebehind, about the tool axis is between 7.2° and 45° , in particular between 13° and 40° and
30 preferably between 27° and 36° .

The thread generating regions generally project radially further outward than the other outer surfaces of the thread generating tool.

In one variant of the invention, at least one thread generating region is a thread
5 shaping region and generates its part of the thread flight by a shaping and thus
non-cutting process, and/or at least some of the thread generating regions of the
thread generating tool have thread pressing lobes arranged on a helical line,
which corresponds in terms of thread pitch and turning direction to the thread to
be generated, about the tool axis, which thread pressing lobes project radially
10 furthest outward within the thread generating region but project radially outward
to a lesser extent than the one or more groove generating region(s). The thread
generating regions are in this case in particular derived, in terms of function,
from a cold-forming tap.

15 In a preferred embodiment, at least one thread generating region is a thread cut-
ting region and generates its part of the thread flight by a cutting process. At
least some of the thread generating regions of the thread generating tool have
thread cutting teeth arranged on a helical line, which corresponds in terms of
thread pitch and turning direction to the thread to be generated, about the tool
20 axis, which thread cutting teeth project radially furthest outward within the
thread generating region but project radially outward to a lesser extent than the
one or more groove generating region(s), wherein the thread cutting teeth are
joined in a direction opposite to the cutting direction or direction of rotation by
preferably outer free surfaces. The thread cutting teeth have thread cutting edg-
25 es or a cutting profile which reflect or reflects the cross section of the thread
profile of the thread flight to be generated.

In one embodiment, the thread cutting teeth are arranged and formed so as to
cut in the turning direction of the thread to be generated and of the helical line
30 about the tool axis on which the thread cutting teeth are arranged. This means
that, if the thread to be generated is a right-handed thread, the thread cutting

teeth also cut in a right-handed sense or are likewise right-handed, and if the thread to be generated is a left-handed thread, the thread cutting teeth also cut in a left-handed sense or are left-handed.

- 5 A thread is referred to as being a right-handed thread or right-handed if, as viewed in the direction in which it runs into the workpiece or toward the workpiece, that is to say from the outside to the inside, or away from the viewer, it turns clockwise, that is to say if the turning direction is clockwise or corresponds to a right-handed rotation, and is referred to as being a left-handed thread or
10 left-handed if it turns counterclockwise or in a left-handed rotation, that is to say if the turning direction is counterclockwise. The same nomenclature generally applies to a helical line or helix.

The direction of rotation of the tool and of its thread generating regions during
15 the generation of the thread thus corresponds to the turning direction of the thread, or in other words, in the case of an internal thread, the tool is rotated in the same way as a screw being rotated or screwed into the thread, or in the case of an external thread, the tool is rotated in the same way as a nut being rotated or screwed onto the thread.

- 20 In one embodiment, the thread cutting teeth are arranged and formed so as to cut in the turning direction of the thread to be generated and of the helical line about the tool axis on which the thread cutting teeth are arranged. This means that, if the thread to be generated is a right-handed thread, the thread cutting
25 teeth also cut in a right-handed sense or are likewise right-handed, and if the thread to be generated is a left-handed thread, the thread cutting teeth also cut in a left-handed sense or are left-handed. The direction of rotation of the tool and of its thread generating regions during the generation of the thread thus corresponds to the turning direction of the thread, or in other words, in the case of
30 an internal thread, the tool is rotated in the same way as a screw being rotated or screwed into the thread, or in the case of an external thread, the tool is rotated
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ed in the same way as a nut being rotated or screwed onto the thread. This corresponds to the direction of rotation of a known tap.

5 In a special alternative embodiment of the invention, the thread cutting teeth are however arranged and formed so as to cut oppositely to the turning direction of the thread to be generated and of the helical line about the tool axis on which the thread cutting teeth are arranged.

10 This is possible owing to the special form of the tool according to the invention, because the thread cutting teeth can firstly be moved into the workpiece or onto the workpiece through the grooves in the workpiece wall without engaging into the workpiece wall, and can then cut the thread only during the turning-out process, by contrast to known taps which always cut the thread during the turning-in process.

15 This means, therefore, if the thread to be generated is a right-handed thread, the thread cutting teeth cut in a left-handed sense or left-handedly, and if the thread to be generated is left-handed, the thread cutting teeth cut in a right-handed sense or right-handedly. The direction of rotation of the tool and of its thread generating regions during the generation of the thread is therefore specifically
20 opposite to the turning sense of the thread, or in other words, in the case of an internal thread, the tool is rotated in the same way as a screw being screwed out of or unscrewed from the thread, or in the case of an external thread, the tool is rotated in the same way as a nut being screwed off or unscrewed from a thread.

25 An advantage of the tool according to the invention in relation to known thread cutting or thread cold-forming tools consists in that the thread generating tool need no longer have a run-on cone or cut-starting region, such as is conventionally provided in the case of taps or cold-forming taps, in which the maximum radial spacing of the threading teeth or pressing lobes increases along a conical
30 surface proceeding from the end of the tap or cold-forming tap. In this way, even

in the case of a blind hole, it is possible for a complete thread flight to be generated axially along a greater thread length, because the incomplete thread flight which would arise over the length of the cut-starting region or run-on cone is eliminated. Furthermore, the thread generating tools may be designed to be shorter, which, aside from other advantages, has a positive effect in particular in the case of small working heights.

Furthermore, by contrast to the prior art, the tool according to invention can, owing to the (only) axial insertion movement, be guided very quickly from the outside into its working position on the wall of the workpiece, and the thread can then be produced with a significantly smaller angle of rotation or with significantly fewer revolutions, and finally, after the generation of the thread, the threading tool can, owing to the (only) axial removal movement, be guided very quickly to the outside away from the wall of the workpiece. In the case of tapping or thread cold-forming according to the prior art, it is also the case that multiple revolutions of the tap or of the cold-forming tap are required, specifically firstly during the turning-in process and then once again during the turning-back process of the tool. In the case of the tool according to the invention, one revolution, or even only part of one revolution, is sufficient, corresponding to the number and arrangement of the grooves in combination with axial feed and removal movements. Here, the additional time required for the generation of the grooves is generally shorter than the time saving during the thread generation. Furthermore, according to the invention, the thread can be formed accurately in terms of its axial position and with regard to the start of the thread. The grooves constitute defined positions for the thread.

The angle of rotation for the rotation of the thread generating tool may be selected so as to correspond to the angle spacing between two directly adjacent grooves, and/or such that, after the rotation, each thread generating region projects into a groove which is directly adjacent to the groove into which the thread generating region projected before the rotation. In particular, the n grooves are

generated at uniform angular intervals of $360^\circ/n$ relative to one another, and the angle of rotation is $360^\circ/n$ or $720^\circ/n$ or $1080^\circ/n$.

5 The groove(s) runs (run) substantially axially and/or parallel with respect to the thread axis.

10 In a first variant, at least one thread generating region is a thread shaping region and generates its part of the thread flight by a shaping and thus non-cutting process. In particular, at least some of the thread generating regions have thread pressing lobes arranged on a helical line, which corresponds in terms of thread pitch to the thread to be generated, about the tool axis, which thread pressing lobes project radially furthest outward within the thread generating region.

15 In a second variant which can also be combined with the first variant, at least one thread generating region is a thread cutting region and generates its part of the thread flight by a cutting process. In particular, at least some of the thread generating regions of the thread generating tool have thread cutting teeth arranged on a helical line, which corresponds in terms of thread pitch to the thread to be generated, about the tool axis, which thread cutting teeth project radially furthest outward within the thread generating region. The thread cutting teeth are generally adjoined in a direction opposite to the cutting direction or direction of rotation by preferably outer free surfaces.

20 The thread cutting regions of the thread generating tool generally project radially further outward than the other outer surfaces of the thread generating tool.

30 In general, the outer profile of only one thread cutting tooth or thread cold-forming wedge already defines the final thread profile of the thread flight portion generated by said tooth or wedge.

In a special refinement of the tool, each thread generating region is divided into at least two axially offset thread generating sub-regions with different thread outer profiles, wherein in particular any desired thread outer profiles may be combined in any desired sequence. In this way, it is possible in particular to set
5 different clamping forces for the screw, which is screwed into the thread generated by means of said thread generating tool, in the different thread sub-regions which correspond to the different thread generating sub-regions. In particular, it is possible to set a greater clamping action for the screwed-in screw in the thread sub-region with the smaller thread profile.

10

In one advantageous embodiment, a first thread generating sub-region, preferably a front thread generating sub-region, which is situated in front of a rear thread generating sub-region axially or in a direction toward the face side, has a thread outer profile with at least partially smaller dimensions or outer dimensions, in particular at the profile tip but if appropriate also at the profile flanks,
15 than a second thread generating sub-region, preferably the rear thread generating sub-region.

It is then preferably possible for the screw to be screwed initially with a low
20 clamping action, or more loosely, into the rear thread sub-region generated by the rear thread generating sub-region, before said screw is then screwed further into the front thread sub-region, generated by the front thread generating sub-region, with a greater clamping action or more tightly with a firmer fit.

25 In one special refinement, each first thread generating sub-region, in particular front thread generating sub-region has, in its thread outer profile, a flattening at the profile tip and/or each second, in particular rear, thread generating sub-region has a thread outer profile which has a radially further outwardly projecting profile tip than the thread outer profile of the first thread generating sub-region,
30 in particular front thread generating sub-region.

In one advantageous embodiment, the diameter of a thread generating sub-region, in particular of the first thread generating sub-region or of the front thread generating sub-region, is smaller than the diameter of another thread generating sub-region, in particular of the second thread generating sub-region or of the rear thread generating sub-region.

The wall of the workpiece in which the thread is generated is preferably a core hole wall of a core hole, in particular of a blind hole or of a through hole, in the workpiece, such that the thread is an internal thread. The generation of an external thread on an outer wall of the workpiece is however also possible.

The invention will be explained in more detail below on the basis of exemplary embodiments. Here, reference is made to the drawing, in which, in each case schematically:

15

- FIG 1 shows a sectional illustration of a core hole in a workpiece,
FIG 2 shows a sectional illustration of the core hole as per FIG 1 with two grooves generated in a first method step,
FIG 3 shows a sectional illustration of the core hole as per FIG 2 with a threading tool, having two thread generating regions situated in the grooves, inserted in a second method step,
20 FIG 4 shows a partially sectional illustration of the core hole as per FIG 3 with the threading tool inserted therein, which threading tool, in a third method step, is rotated through an angle of rotation and moved with an axial feed motion, wherein the thread generating regions have generated a part of a thread flight,
25 FIG 5 shows a partially sectional illustration of the core hole as per FIGS 3 and 5 with the threading tool inserted therein, which threading

tool, in the third method step, has been rotated through the full angle of rotation and moved with an axial feed motion, wherein the thread generating regions have generated the complete thread flight,

- 5 FIG 6 shows a perspective illustration of a workpiece having a core hole with two grooves and having a finished thread between the grooves,
- FIG 7 shows a plan view of the core hole as per FIG 6, and
- FIG 8 shows a sectional illustration of the core hole as per FIG 7 along
10 the line VIII-VIII in FIG 7,
- FIG 9 shows a thread generating tool which operates in a non-cutting manner and which has two thread generating regions,
- FIG 10 shows a view of the face side of a further thread generating tool which operates in a non-cutting manner,
- 15 FIG 11 shows a perspective view of a thread generating tool having two thread generating regions and, in front thereof, groove generating regions,
- FIG 12 shows a side view of the thread generating tool as per FIG 11,
- FIG 13 shows, in a side view rotated through 90°, the thread generating
20 tool as per FIGs 11 and 12,
- FIG 14 shows a view of the face side of the thread generating tool as per FIGs 11 to 13,
- FIG 15 shows a front part of the thread generating tool as per FIGs 11 to 13 in a longitudinal section along XV-XV in FIG 14,
- 25 FIG 16 shows a front region of the thread generating tool as per FIGs 11 to 15 in a section, inclined obliquely along the thread pitch, through the front thread teeth in a view toward the front along the line XVI in FIG 15,
- FIG 17 shows a perspective illustration of a workpiece with a blind hole
30 having two grooves and having a finished thread between the
-

grooves, wherein the grooves and the thread have been generated by means of a thread generating tool as per FIGs 11 to 16,

FIG 18 shows a plan view of the blind hole as per FIG 17,

FIG 19 shows the blind hole as per FIG 17 in a sectional illustration along the line XIX-XIX in FIG 18,

FIG 20 shows a side view of a further embodiment of a thread generating tool,

FIG 21 shows a perspective illustration of a workpiece having a blind hole in which grooves and a thread have been generated by means of a thread generating tool as per FIG 20,

FIG 22 shows a perspective view of a thread generating tool with two thread generating regions and, in front thereof, non-cutting groove generating regions,

FIG 23 shows a side view of the thread generating tool as per FIG 22,

FIG 24 shows a view of the face side of the thread generating tool as per FIGs 22 and 23, and

FIG 25 shows a side view of a thread generating tool with two thread generating regions and, in front thereof, non-cutting, concave groove generating regions.

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Corresponding parts and dimensions are denoted by the same reference numerals in FIGs 1 to 25.

FIG 1 shows a core hole 20 in a workpiece 2 in a section, wherein the core hole 20 has a cylindrical core hole wall 21 which encircles a central axis M and which has the diameter D. The direction radial with respect to the central axis M is denoted by an arrow and the reference sign r. The core hole 20 is generated preferably by a cutting process, in particular by means of a drilling tool or a milling tool.

30

According to FIG 2, there are then formed in the core hole wall 21 two axial grooves 22 and 24 which are formed and arranged parallel to one another and to the central axis M and on opposite sides diametrically with respect to the central axis M, that is to say so as to be offset by 180° with respect to one another. The
 5 depths of the grooves 22 and 24 measured from the outer diameter or from the original cylindrical core hole wall 21 of the core hole 20 are denoted by t, and are preferably identical in both grooves 22 and 24. The radially outer groove base of the groove 22 is denoted by 22B, and correspondingly, the groove base of the groove 24 is denoted by 24B. A wall sub-region of the core hole wall 21 running
 10 counterclockwise between the grooves 22 and 24 in FIG 2 is denoted by 23, and a wall sub-region situated on the other side between the grooves 22 and 24 is denoted by 25.

To generate the two grooves, use is correspondingly made of two groove generating regions of a thread generating tool 3 not illustrated in FIGs 1 and 2, which
 15 thread generating tool is inserted axially into the core hole 20 with its tool axis A coaxial with respect to the central axis M of the core hole 20. This will be explained in more detail again on the basis of FIGs 9 to 19.

20 The angle component β , corresponding to the circumferential component, of a groove 22 or 24 in relation to the overall circumference of the core hole 20 and the core hole wall thereof, that is to say in relation to 360° , is between 2% and 12.5%, preferably between 7.5% and 10% or, expressed in degrees, between 7.2° and 45° , preferably between 27° and 36° . It is also possible here for the
 25 angle component β of the grooves 22 to be smaller in the case of a cutting thread generating tool, for example a tap, than in the case of a shaping or cold-forming threading tool, such as for example a cold-forming tap. The angle component γ , corresponding to the remaining circumferential component, of each wall sub-region 23 and 25 is then $(360^\circ - 2\beta)/2 = 180^\circ - \beta$.

According to FIG 3, the thread generating tool 3 which is rotatable about its tool axis A is then inserted, with its tool axis A coaxial with respect to the central axis M of the core hole 20, into the core hole 20. The thread generating tool 3 has two thread generating regions 32 and 34 arranged diametrically with respect to the tool axis A or offset with respect to one another by 180°, and has two in particular cylindrical outer surfaces 33 and 35 between the thread generating regions 32 and 34.

The thread generating regions 32 and 34 project radially further outward than the outer surfaces 33 and 35. The diameter of the thread generating tool 3 from the outer surface 33 to the outer surface 35 is denoted by d. The thread generating regions 32 and 34 have thread cutting teeth 32A and 34A (of which in each case only one is visible in section in FIG 2) arranged on a spiral or helical line, which corresponds in terms of thread pitch to the thread to be generated, about the tool axis A, and said thread generating regions have outer free surfaces 32B and 34B which adjoin the thread cutting teeth 32A and 34A. In FIG 2, the thread cutting teeth 32A and 34A are arranged at the front as viewed in a direction of rotation S about the tool axis A, and the free surfaces 32B and 34B run in each case rearward from the thread cutting teeth 32A and 34A. The thread cutting teeth 32A and 34A are the radially furthest outward projecting regions of the thread generating regions 32 and 34 of the thread generating tool 3. The radial height of the thread cutting tooth 32A or 34A in relation to the rest of the outer circumference of the thread generating tool 3, that is to say in particular in relation to the outer surfaces 33 and 35 thereof, is denoted by h, and is preferably identical for both thread generating regions 32 and 34.

The radial spacing of the thread cutting teeth 32A and 34A to the respective groove base 22B and 24B of the respective groove 22 or 24 is denoted by Δr , and is preferably likewise identical for both groups 22 and 24. Said radial spacing Δr is typically between 1/20 and 1/5 of the groove depth t.

The thread generating region 32 projects in a radial direction r into the groove 22, and the thread generating region 34 projects into the groove 24. The following thus applies for the respective dimensions: $d < D$ and $d/2 + h < D/2 + t$.

- 5 The radial spacing or the gap width between the wall sub-region 23 of the core hole wall 21 and the facing outer surface 33 of the thread generating tool 3, and between the wall sub-region 25 of the core hole wall 21 and the facing outer surface 35 of the tool 3 is denoted by g and corresponds to $g = (D - d) / 2$. Said gap width g and also the radial spacing Δr between the free surface 32B or 34B and
10 groove base 22B or 24B respectively are illustrated in each case on an exaggerated scale in order to provide a clearer illustration. The clearance between the thread generating tool 3 on the one hand and the core hole wall 21 of the core hole 20 or the grooves 22 and 24 on the other hand will generally be smaller. It is preferably the case that $0.01 < g/D < 0.1$, though other parameter relationships may also be selected.
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FIG 4 then shows the thread generating tool 3, which has been rotated in the direction of rotation S by an angle α in relation to the position shown in FIG 3, in the core hole 20 of the workpiece 2.

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In addition to the rotational movement in the direction of rotation S , the thread generating tool 3 has been moved inward into the core hole 20 coaxially with respect to the tool axis A and also with respect to the central axis M by means of an axial or linear feed movement, which cannot be seen in the section in FIG 4.

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- The feed speed of said axial feed movement is adapted to the rotational speed of the rotational movement in the direction of rotation S and the desired thread pitch P , in such a way that, in the same amount of time as that taken by the tool 3 to perform one full revolution or rotate through an angle of rotation $\alpha = 360^\circ$,
30 the axial feed or the axial travel corresponds precisely to the thread pitch P . The

axial feed speed thus corresponds to the product of the thread pitch P and the rotational frequency of the tool 3.

As a result of the rotational movement through the angle of rotation α of the
5 thread generating tool 3 with simultaneous axial feed movement by the travel $P \cdot$
 $\alpha/360^\circ$, a part of the thread flight 36 of the thread has been generated in the
core hole wall 21 of the core hole 20, specifically proceeding from the groove 22
in the wall sub-region 25 and proceeding from the groove 24 in the wall sub-
region 23. For illustration, the entire sub-region already generated in a turn of
10 the generated thread flight 36 is also shown in the illustrated section in FIG 4.

The thread generating tool 3 has, axially with respect to its tool axis A in the
thread generating regions 32 and 34, in each case one axial row of thread cutting
teeth 32A and 34A which are arranged axially offset with respect to one another.

15 Corresponding to the number of said thread cutting teeth 32A and 34A in the re-
spective row, during half of one revolution, through $\alpha = 180^\circ$, of the thread gen-
erating tool 3 with a simultaneous feed movement by $P/2$, a number of thread
turns of the thread flight 36 are generated corresponding to the number of thread
20 cutting teeth in an axial row, said thread turns being interrupted in each case by
the grooves 22 and 24. Here, the thread cutting teeth 32A and 34A, which are
situated diametrically opposite one another, are arranged offset in each case by
 $P/2$ in order that the two separately generated half-turns of the thread flight 36
in the wall region 23 and in the wall region 25 then merge into one another, after
25 the groove 22 and 24, along the desired thread profile on the helical line with the
thread pitch P .

Here, the radial height h of the thread cutting tooth 32A or 34A determines the
spacing of the groove base 36B of the thread flight 36 from the core hole wall 21.

Here, a rotation of the tool 3 by the spacing angle, 180° in the example of FIGs 2 to 4, between the grooves 22 and 24 in the core hole 20 as a total angle of rotation α covers the entire wall sub-regions 23 and 25 situated between said grooves, such that the thread flight 36 is fully generated in said wall sub-regions 23 and 25.

The state after half of one revolution is shown in FIG 5.

The thread generating region 32, which previously projected into the groove 22, now projects into the diametrically opposite groove 24, and the thread generating region 34, which previously projected into the groove 24, now projects into the groove 22, in each case with the radial spacing Δr to the groove base 24B and 22B respectively.

As a result, it is then possible in a further step for the thread generating tool 3 to be pulled out of the core hole 20 again axially with respect to the central axis M, since the thread generating regions 32 and 34 can be moved outward axially along the grooves 24 and 22 without damaging the generated thread flight 36.

In the case of, in general, a number $n > 2$ of grooves and in the case of an equidistant or uniform distribution of the grooves in the core hole wall 21, that is to say a spacing angle of $360^\circ/n$, a rotation through $360^\circ/n$ is then sufficient to generate a complete thread flight between the grooves and move the tool out of the core hole again.

In the case of a non-equidistant arrangement or non-uniform distribution of the grooves, a complete rotation through 360° is generally necessary in order to bring the thread generating regions into the grooves again and to be able to pull the tool out, unless axial symmetry is present or n-fold rotational symmetry is present whereby each thread generating region projects into an associated groove again already after a smaller angle of rotation.

One advantage is that the thread generating tool 3, which is ultimately a modified tap, need not have a run-on cone or cut-starting region in which the maximum radial spacing of the thread cutting teeth increases along a cone surface proceeding from the end of the tap in order to attain a corresponding growth of the chip and of the penetration depth of the thread cutting teeth into the workpiece surface and in order to prevent the cut pressure from becoming too high.

In the case of the thread generating tool 3 according to the invention, which engages with its thread generating regions 32 and 34 into the previously generated grooves 22 and 24, the thread flight can moreover be generated uniformly with the full thread profile depth as per the radial height h of the thread cutting teeth 32A and 34A, and, as viewed over the axial thread length of the thread, there is also no loss, even in the case of a blind hole as a core hole 20, of a sub-region with an incomplete thread flight such as would otherwise be generated in the case of conventional taps by the cut-starter or run-on cone of the tap. The thread flight 36 which is generated also over a rotation of only 180° is thus complete, specifically over its entire axial thread length. This is an advantage which can more than compensate for the certain strength disadvantage as a result of the interruptions of the thread flight 36 in the region of the two grooves 22 and 24.

Furthermore, despite the additional step of the generation of the grooves 22 and 24, the actual thread generating process can be performed in a shorter time than is possible with conventional taps in a circular core hole without grooves 22 and 24.

Furthermore, it is advantageously possible for coolant and/or lubricant, in particular in the form of oil or oil aerosol, to be guided or conducted through the grooves 22 and 24 to the location of the thread generation, and said grooves can also be used for the discharge of chips. Furthermore, it is also possible for at least the last chips generated to be introduced by the thread cutting tooth into the respective groove 22 or 24 and discharged there with a relatively large volume with the coolant and/or lubricant.

For the transport of coolant and/or lubricant to and from the thread generating regions 32 and 34 and/or for the discharge of chips from cutting thread generating regions 32 and 34, the thread generating tool 3 may also have outer grooves and/or inner ducts (not illustrated) which run on or to the thread generating regions 32 and 34.

The core hole 20 in FIGs 1 to 5 may be either a through hole or a blind hole. The wall of the workpiece may thus, as illustrated, be the inner wall of a continuous or non-continuous hole in the workpiece for the production of an internal thread. The tool may however likewise be used for producing an external thread, wherein then, the grooves and subsequently the thread are generated in the outer wall of a shank or bolt or the like, and the thread generating regions of the thread generating tool are correspondingly arranged on an inner surface or directed inward and engage from the outside into the outer wall of the workpiece. The thread generating tool is then also of greater diameter than the wall of the workpiece, whereas in the case of an internal thread, said thread generating tool is of smaller diameter.

FIGs 6 to 8 show a thread, generated by means of the tool according to the invention, in a through hole as a core hole 20, with the thread generating tool 3 already having been pulled out.

The thread flight 36 has been fully generated in the wall sub-regions 23 and 25 of the core hole wall 21 of the core hole 20 and is interrupted only in the region of the grooves 22 and 24. The central axis M of the core hole 20 is now the thread axis of the generated thread with the (interrupted) thread flight 36. The
5 thread pitch P of the thread flight 36 is also indicated in FIG 8.

In a further embodiment, as a thread generating tool, instead of a tap modified according to the invention such as is shown in FIGs 3 to 5, there may also be provided a cold-forming tap modified according to the invention, in which the
10 thread generating regions have radially outwardly projecting pressing lobes or cold-forming teeth instead of thread cutting teeth. The pressing lobes or cold-forming teeth generate the thread flight in a non-cutting manner, by plastic impression into the core hole wall 21, during the rotational movement and simultaneous axial feed movement of the thread generating tool. The pressing lobes may
15 in particular be arranged in the center of the thread generating regions, again with a radial spacing to the respective groove base of the grooves.

FIGs 9 and 10 show in each case an exemplary embodiment of such a threading tool 3 according to the invention designed as a cold-forming tap which operates
20 in a non-cutting manner.

The threading tool 3 comprises a shank 5 which has a rear portion 9, which is for example of cylindrical form, and a front portion 8 which is narrowed in diameter adjacent to the rear portion 9 and centrally through which the tool axis A extends. At the end of the rear portion 9 there is formed a polygon 7 or a clamping
25 region of some other form for the clamping of the shank 5 in a clamping means, in particular a chuck or clamping jaw, of a machine tool for driving the threading tool 3, in particular for rotating the latter about the tool axis A.

30 The front portion 8 has, toward the face side 6 which faces away from the rear portion 9 or which is arranged at the front (or: toward the free end), two thread

generating regions 32 and 34 which are in the form of axial rows, running in each case parallel to the tool axis A, of thread generating ridges and which are arranged diametrically with respect to one another on opposite sides of the tool axis A.

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The thread generating ridges run along the thread pitch of the desired thread and are thus inclined by the thread pitch angle relative to a plane orthogonal with respect to the tool axis A, and have in each case one pressing lobe or shaping wedge, which projects radially furthest outward with respect to the tool axis A, for the plastic impression of the thread flight into the workpiece.

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The pressing lobes of the first three thread generating ridges of the thread generating region 32 proceeding from the face side 6 are denoted in FIG 9 by 32-1, 32-2 and 32-3, and those of the thread generating region 34 are denoted by 34-1, 34-2 and 34-3. In FIG 10, only the foremost pressing lobes 32-1 and 34-1 are visible.

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The radii or spacings of the thread generating ridges of the two thread generating regions 32 and 34 from the tool axis A are constant or equal to one another. In this way, even the radii of the shaping wedges or pressing lobes 32-1, 32-2 and 32-3 and 34-1, 34-2 and 34-3 situated furthest forward at the face side 6 are equal to one another. The cold-forming tap or the thread generating tool 3 both as per FIG 9 and also as per FIG 10 thus has no initial-forming cone and thus no increasing radius over the first thread forming wedges. Rather, the radii of the pressing lobes of all of the thread generating ridges in each of the thread generating regions 32 and 34 are equal or constant over the entire axial length. The furthest outward projecting shaping wedges or pressing lobes, including the pressing lobes 32-1, 32-2 and 32-3 of the thread generating ridges, thus lie on a lobe axis B which runs parallel, or with constant radial spacing, to the tool axis A. The same applies to the thread generating ridges with the pressing lobes 34-1 to 34-4 of the thread generating region 34.

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The two thread generating regions 32 and 34 are separated by interposed outer surfaces 33 and 35 which have a smaller radius from the tool axis A or a smaller outer diameter than the thread generating regions 32 and 34, that is to say are
5 recessed radially with respect to said thread generating regions. The thread generating regions 32 and 34 are thus the radially furthest outward projecting parts in the front portion 8 of the thread generating tool 3, and the outer surfaces 33 and 35 form free spaces between the thread generating regions 32 and 34.

10 Here, as shown in FIG 10, the thread generating regions 32 and 34 cover in each case an angle range δ , and the outer surfaces 33 and 35 cover in each case an angle range ε , wherein preferably $\varepsilon < \delta < 2.5 \varepsilon$ and/or, in relation to the grooves (FIG 2), $\delta < \beta$ and $\gamma < \varepsilon$. The pressing lobes 32-1 and 34-1 are situated preferably centrally in or in the middle of the respective angle ranges δ .

15 Each outer surface 33 and 35 of the thread generating tool 3 between the thread generating regions 32 and 34 thereof has a special shape. As per FIG 9, the outer surfaces 33 and 35 initially form concavely inwardly running portions directly adjoining one of the thread generating regions 32 and 34, and then bulge convexly
20 outward into bulges 52 and 54.

In FIG 10, in each case only a convexly outwardly directed bulge 52 and 54 is provided, without concave intermediate portions.

25 Good rigidity is attained as a result of the convex bulges 52 and 54.

The diameters or radii of the thread generating ridges of the two thread generating regions 32 and 34 are constant, that is to say the outer radii of the outwardly projecting shaping wedges 32-1, 32-2 and 32-3 which are situated furthest forward at the face side 6 are in each case identical. The cold-forming tap or the
30 thread generating tool 3 thus has no initial-forming cone or run-on region with an

increasing outer radius over the first thread shaping wedges for the successive deepening or working-in of the thread flight at the thread base. Rather, the radii of all of the thread generating ridges and the shaping wedges thereof in each of the thread generating regions 32 and 34 are identical or constant over the entire axial length, as shown on the basis of the first three thread generating ridges 32-1, 32-2 and 32-3. The furthest outward projecting shaping wedges or pressing lobes of the thread generating ridges thus lie on a lobe axis B which runs parallel or with a uniform radial spacing to the tool axis A. The same applies to the thread generating ridges of the thread generating region 34 (not illustrated in FIG 9). The special shape of the free spaces 52 and 54 and of the thread generating region 32 and 34 permits the use of the thread cold-forming tool 3 as per FIG 9 or FIG 10 for thread generation as per FIGs 1 to 8, wherein the thread generating regions 32 and 34 are inserted axially into the previously generated grooves 22 and 24 in the workpiece 2, and the thread generating tool 3 is then rotated in the described manner until the thread generating regions 32 and 34 come to rest again in the associated grooves or in the opposite grooves 22 and 24 or 24 and 22, whereafter the tool 3 can be pulled axially out of the workpiece 2 again.

FIGs 11 to 16 show various illustrations of a combined tool 4 according to the invention, in which, in the front portion 8 of the tool 4, in addition to two cutting thread generating regions 32 and 34, a groove generating region 42 is also positioned axially in front of the thread generating region 32 on the face side 6 and a groove generating region 44 is positioned axially in front of the thread generating region 34.

Each groove generating region 42 and 44 has a groove cutting edge 42A or 44A which is directed axially forward and situated on the face side 6. The groove cutting edges 42A and 44A are the radially furthest outward projecting regions, and the axially furthest forward situated regions of those regions which are situated radially at the outside, of the tool 3 in the front portion 8 thereof.

The groove cutting edges 42A and 44A may in particular be of at least approximately circular form. As shown in FIG 15, the radius r_0 of the groove cutting edge 42A is greater by a differential radius Δr than the radius r_1 of the first thread generating sub-region 321 and than the radius r_2 , which in FIG 15 is identical to radius r_1 , of the second thread generating sub-region 321.

Each groove cutting edge 42A and 44A is adjoined laterally in a circumferential direction by a side cutting edge 42D and 44D, which is at the front in the direction of rotation S about the tool axis A , and by a side region 42E or 44E which is at the rear in the direction of rotation S about the tool axis A .

During the rotation of the tool 4 in the direction of rotation S which takes place for the generation of the thread, the front side cutting edge 42D and 44D cuts laterally into the workpiece, and said front side cutting edge is correspondingly ground so as to be adjoined in a radially inward direction by a rake surface 42F or 44F for the discharge of chips. The rear side region 42E and 44E is, by contrast, at an obtuse angle and is preferably of convex form, since it merely follows but need not perform any cutting.

Axially behind the groove cutting edge 42A and 44A there adjoins a free surface 42B and 44B which, as shown in FIG 15, slopes downward, in particular in a linear or conical fashion, from the radius r_0 to a radius smaller than the radius r_1 of the first pressing lobe 32-1.

The groove cutting edge 42A is adjoined in a radially inward direction by a face-side rake surface 42C, and the groove cutting edge 44A is correspondingly adjoined in a radially inward direction by a rake surface 44C, which rake surface in each case runs axially rearward in a linear or else concavely curved fashion and on which chips produced during the reaming of the groove with the groove cutting edge 42A or 44A are discharged. The rake surface 42C or 44C runs from a

lowest point axially forward again to a planar central region 51 oriented perpendicular to the tool axis A, which central region surrounds a central opening of a central duct 50 of the tool 4, via which central duct coolant and/or lubricant can be supplied.

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The two thread generating regions 32 and 34 in the combination tool 4 according to FIGs 11 to 16 are preferably designed to impart a cutting action and have a plurality of thread cutting teeth 32A and 34A arranged at the front in the direction of rotation S about the tool axis A, the outer cutting edges of which thread cutting teeth are matched to the shape of the thread profile to be generated. A radially inwardly running rake surface for the chips generated by the thread cutting teeth 32A and 34A is denoted by 32C and 34C respectively. The thread cutting teeth 32A and 34A are adjoined, oppositely to the direction of rotation S, by an outer free surface 32B or 34B which ends at a side region 32E or 34E which is at the rear in the direction of rotation S and which is slightly bulged convexly outward.

As viewed proceeding from the face side 6, the first three thread generating sub-regions of the thread generating region 32 with in each case one thread cutting tooth are denoted 32-1 to 32-3.

The thread cutting teeth 32A and 34A are the radially furthest outward projecting regions of the thread generating regions 32 and 34. As can be clearly seen in FIG 16, the groove generating regions 42 and 44 project radially even further outward than the thread generating regions 32 and 34.

The two thread generating regions 32 and 34 are separated from one another by interposed outer surfaces 33 and 35 of the tool 4, and the groove generating regions 42 and 44, which are situated in front of said thread generating regions, are separated from one another by interposed outer surfaces 43 and 45 of the tool 4. The outer surfaces 33 and 35 and also 43 and 45 have a smaller radius

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from the tool axis A or a smaller outer diameter than the thread generating regions 32 and 34 and the groove generating regions 42 and 44, and form free spaces between the cutting thread generating regions 32 and 34 and the groove generating regions 42 and 44, which free spaces also serve for the discharge of chips.

It is preferable, in particular for reasons of simple production, for the shape and contour of the lateral regions, which are at the front and at the rear in the direction of rotation S, of the thread generating regions 32 and 34 and of the groove generating regions 42 and 44 and of the outer surfaces 33 and 35 and also 43 and 45 to be adapted to one another, in particular situated one above the other or congruent in the perpendicular projection along the tool axis A, that is to say for example the rake surfaces 32C and 42F and the side regions 32E and 42E and the outer surfaces 33 and 43 and also 35 and 45 are adapted to one another, in particular are ground together.

Each outer surface 33 and 43 and also 35 and 45 of the combined tool 3 initially form concavely inwardly running portions directly adjoining the cutting edges, that is to say the groove cutting edges 42D and 44D and the thread cutting teeth 32A and 34A, which portions form the rake surfaces 32C and 34C and 42F and 44F respectively and then bulge convexly outward into bulges 52 and 54, before then running outward on the other side into the convex side regions 32E and 34E and also 42E and 44E. As a result of the convex bulges 52 and 54, good rigidity and stability of the tool with respect to torques is achieved.

During the axial feed movement of the tool 4 and the axial reaming or cutting process, the contours of the groove cutting edges 42D and 44D are reflected in the groove contour of the groove 22 and 24 respectively. The thread cutting teeth 32A and 34A generate the thread flight 36 during the subsequent rotational movement.

In the embodiment illustrated in FIGs 11 to 16, the groove cutting edges 42A and 44A lie in a common plane which is oriented perpendicular to the tool axis A, that is to say are situated axially at the same height. In this way, the back sides of the cutting edges or free surfaces 42B and 44B, situated behind said groove cutting edges, of the groove generating regions 42 and 44 are of different lengths
5 corresponding to the thread pitch. In an embodiment which is not illustrated, the groove cutting edges 42A and 44A may however also be arranged axially offset with respect to one another by the thread pitch in order to permit an equal axial length of the groove generating regions 42 and 44.

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According to the invention, the groove generating regions work the thread in merely by means of a small rotation between one groove (for example 22 or 24) and the next groove (for example 24 or 22), wherein individual thread flight portions are generated which form part of the helix of the thread and which are interrupted or separated from one another by the grooves. Each thread generating
15 region and each thread cutting tooth or thread shaping tooth or wedge therein thus generates an associated individually generated thread flight portion which, during a rotation only to the next groove, that is to say in the case of n grooves, through the angle of rotation $360^\circ/n$, is passed through and generated only once and only by said thread generating region and its thread cutting tooth or thread
20 shaping wedge. During a rotation of each thread generating region to the next but one groove, that is to say a rotation of the tool through $720^\circ/n$, the thread flight portion between two grooves is generally run through and worked in jointly in succession only by two successive thread generating regions and their thread
25 cutting teeth or thread shaping wedges. Considered conversely, each thread generating region and each thread cutting tooth or thread shaping tooth or wedge therein machines the workpiece surface in two successive individual thread flight portions, one between the first groove with $i = 1$ where $1 \leq i \leq n$ and the next groove with $i = 2$ and one between the next groove ($i = 2$) and the next but one
30 groove ($i = 3$ or $i = 1$ again if $n = 2$). In the general case of m $360^\circ/n$ revolutions, where m is a whole number, m thread cutting teeth or thread shaping

wedges situated one behind the other work in the same thread flight portion. Although, in extremely rare situations, m is selected to be greater than 2 or at most 3, $m = 1$ will always suffice.

- 5 The outer profile of only one thread cutting tooth or thread shaping wedge (or at most m thread cutting teeth or thread shaping wedges) thus already defines the final thread profile of the thread flight portion generated by said tooth or wedge.

10 It is thus possible according to the invention for the thread to be composed of individual thread flight portions with practically arbitrarily predefined thread profiles, wherein the thread profile of each thread flight portion is, on its own and independently of the other thread flight portions, reflected by or formed so as to be complementary to the outer profile of the single thread cutting tooth or thread shaping wedge assigned to the thread flight portion during a rotation through
15 $360^\circ/n$ (or, in the case of a rotation through $m \cdot 360^\circ/n$, the at most m associated thread cutting teeth or thread shaping wedges).

In the case of the known taps or cold-forming taps, said individual assignment of tooth to thread flight portion is not possible. Moreover, in the case of said tools
20 according to the prior art, the axially foremost thread cutting tooth or thread shaping tooth situated axially at the front closest to the face side is, during the rotational movement, guided through the entire thread flight over the entire thread length, and in the process generates a pilot thread flight, corresponding in terms of length to the final thread, with a pilot thread profile. Said pilot thread
25 flight and its pilot thread profile is then further worked in or reworked, in particular at the thread base and/or at the thread flanks of the thread profile, by the subsequent thread cutting teeth or thread shaping teeth. For example, the next, second-to-foremost thread cutting tooth or thread shaping tooth runs through the pilot thread flight generated by the foremost thread cutting tooth or thread shaping
30 ing tooth, likewise over at least a length corresponding to the overall length of the pilot thread minus the distance between the foremost thread cutting tooth or

thread shaping tooth and the second-to-foremost thread cutting tooth or thread shaping tooth. The thread profile of the thread flight with thread flanks is worked successively into the workpiece by thread cutting teeth or thread shaping teeth which are arranged along the thread helix and which successively perform work
5 on the same points on the workpiece. This working sequence is particularly pronounced in the run-on region of said known threading tools.

The invention thus permits an axial division of the thread over its thread length, which has hitherto not been possible in the case of a tap or cold-forming tap, into
10 different thread portions in which, in principle, any desired thread profiles may be generated in any desired sequence or combination. Here, it is even possible to generate threads in which first thread flight portions which are situated in front of second thread flight portions in the forward direction of the tool, or in a direction into the thread, have a thread profile with smaller dimensions or outer di-
15 mensions, in particular at the thread base but if appropriate also at the thread flanks, than the second thread flight portions, which would be technically impossible in the case of a known tap or cold-forming tap.

FIG 20 shows, for illustration of such refinements according to the invention, a
20 further exemplary embodiment of a thread generating tool 14 according to the invention, and FIG 21 shows a thread, generated by means of said thread generating tool 14 as per FIG 20, in a blind hole of a workpiece.

In the further embodiment of a thread generating tool 14 shown in FIG 20, taking
25 a thread generating tool 4 as per FIG 12 as a starting point, the thread generating region 32 axially behind the groove generating region 42 and the thread generating region 34 axially behind the groove generating region 44 are divided in each case into two thread generating sub-regions 72 and 82, and 74 and 84, respectively, arranged offset with respect to one another axially with respect to the
30 tool axis A.

In the front thread generating sub-region 72 or 74 arranged toward the face side 6 and directly adjacent to the associated groove generating region 42 or 44, it is now the case, by contrast to FIG 12, that the thread cutting teeth 32A and 34A are provided, in their thread cutting profile or outer profile, with in each case one
5 flattening 32F or 34F in the tooth tip region, which flattening is reflected in the thread base in the complementarily generated thread flight in the workpiece.

By contrast, in the rear thread generating sub-region 82 or 84 facing away from the face side 6 and situated behind the front thread generating sub-region 72 or
10 74, the thread cutting teeth 32A or 34A are provided with a thread cutting profile or outer profile which corresponds to the complete thread profile of the generated thread, and in the example of FIG 20, have a tooth tip 32G which is more pointed or merges into an outer edge or a spine, which tooth tip is reflected in a correspondingly formed thread base of the thread flight in the workpiece.

15 The axial length of the front thread generating sub-regions 72 and 74 is denoted jointly by L1, and that of the rear thread generating sub-regions 82 and 84 is denoted by L2, wherein, strictly speaking, the two thread generating sub-regions 72 and 84 or 82 and 84 offset by 180° are offset axially with respect to one another
20 in each case by half of one thread pitch $P/2$. The thread pitch P is twice the axial spacing of the thread cutting teeth 32A and 34A to one another.

To generate the thread 36 shown in FIG 21, said thread generating tool 14 as per FIG 20 is again initially fed, axially with respect to the central axis M and with its
25 tool axis A coaxial with respect to or coinciding with said central axis, axially into the core hole 20 in the workpiece 2. Here, the groove generating regions 42 and 44 again generate the associated axial grooves 22 and 24 on the core hole wall 21, and, as viewed in the forward direction of the tool toward its face side 6, the thread generating region 32 is now arranged behind the groove generating region
30 42 in the groove 22, and the thread generating region 34 is correspondingly arranged behind the groove generating region 44 in the groove 24.

The tool is then rotated about its tool axis A through 180°, and in the process moves forward (or rearward), or into (or out of) the core hole 20, by half of one thread pitch $P/2$, until the thread generating region 32 is arranged in the groove 24 and the thread generating region 34 is arranged in the groove 22, that is to say said thread generating regions are exactly reversed.

During said working movement, each thread cutting tooth 32A of the front thread generating sub-region 72 generates in each case exactly one associated thread flight portion between the groove 22 and the groove 24 in a thread sub-region 76 of the thread 36, which sub-region 76 is at the front in a forward direction, and
5 each thread cutting tooth 34A of the front thread generating sub-region 74 generates in each case exactly one associated thread flight portion between the groove 24 and the groove 22. Each thread flight portion has a thread profile which corresponds exactly to the outer profile of the associated thread cutting tooth 32A or 34A, in the present example a for example trapezoidal interference-fit thread. The outer flattenings 32F and 34F of the thread cutting tooth 32A or
10 34A are reflected here in a correspondingly flattened or shallower thread base 36F of the thread flight portions. Here, the axial length of the front thread sub-region 76 of the thread 36 corresponds substantially to the length L1 of the thread generating sub-regions 72 and 74 of the thread generating tool 14, and
15 may for example, as illustrated, amount to 16 thread flights or thread pitches P, but is not restricted in terms of length L1 and number of thread pitches P. The diameter of the front thread sub-region 76, measured from thread base 36F to opposite thread base 36F perpendicular to the central axis M, is denoted by E.

20 During the same working movement of the thread generating tool 14, in a thread sub-region 86, which is at the rear with respect to a forward direction, of the thread 36, each thread cutting tooth 32A of the rear thread generating sub-region 82 generates exactly one associated thread flight portion between the groove 22 and the groove 24, and each thread cutting tooth 34A of the rear thread generat-
25 ing sub-region 84 generates in each case exactly one associated thread flight portion between the groove 24 and the groove 22. Again, each thread flight portion has a thread profile which corresponds exactly to the outer profile of the associated thread cutting tooth 32A or 34A, in the present example a metric thread. The ridge-like tooth tips 32G and 34G of the thread cutting tooth 32A or 34A are
30 reflected here in a corresponding thread base 36G of the thread flight portions in the rear thread sub-region 86. The axial length of the rear thread sub-region 76

of the thread 36 corresponds substantially to the length L2 of the rear thread generating sub-regions 82 and 84 of the thread generating tool 14, and may for example, as illustrated, amount to 3 thread flights or three thread pitches P, without this restricting the general nature. The diameter of the rear thread sub-region 86, measured from thread base 36G to diametrically opposite thread base 36G perpendicular to the central axis M, is denoted by F.

All thread flight portions generated in this way in the thread sub-regions 76 and 86 lie on a common thread helix with the thread pitch P.

In the illustrated exemplary embodiment, the diameter E of the front thread sub-region 76 is smaller than the diameter F of the rear thread sub-region 86. In this way, a clamping action for a screw or a threaded bolt can be attained in the front thread sub-region 76, whereas no such clamping action arises in the rear thread sub-region 76 which is formed as a full thread.

By contrast to the illustrated exemplary embodiment, it is possible for a thread with some other, practically arbitrary axial distribution of its thread profile to be generated. For example, it would also be possible for the thread profiles in the front thread sub-region 76 and in the rear thread sub-region 86 to simply be reversed, such that the clamping action arises in the rear thread sub-region 86.

Instead of or in addition to cutting thread generating regions 32 and 34 with thread cutting teeth 32A and 34A, provision may also be made, in all embodiments, of thread generating regions 32 and 34 which impart a shaping action or which press into the workpiece so as to cause plastic deformation of the latter and which have thread pressing lobes, for example as shown in FIG 9 or FIG 10.

Furthermore, it is also possible for more than two, for example three or four, thread generating regions, in each case with a groove generating region situated in front thereof in the case of the combination tool, to be provided, which thread

generating regions may be arranged in a uniformly distributed manner, that is to say at uniform angular intervals, or else with a non-uniform distribution.

In a further embodiment which is not illustrated, it is also possible, as in the case
5 of a known cold-forming tap or tap, for the thread pressing lobes or the thread cutting teeth in a run-on cone region to grow in terms of their radial outer dimension up to the maximum outer dimension corresponding to the final thread depth, in order to generate the depth of the thread flight in successive passes during multiple rotations of the tool. This embodiment is suitable in particular for
10 relatively large thread lengths, and reduces the torque acting on the tool during the thread generation process.

Finally, instead of or in addition to cutting or chip-removing groove generating regions of the tool, it is also possible for groove generating regions to be provided
15 which operate in a non-cutting manner and which work the grooves into the material in particular by plastic deformation or impression.

Two exemplary embodiments of tools 4 with such groove generating regions 42
20 and 44 which operate in a non-cutting manner are illustrated in FIGs 22 to 25.

Each groove generating region 42 and 44 has a central shaping spine (or: shaping ridge, pressing ridge) 42G and 44G which runs substantially in a circumferential direction around the tool axis A and which, as viewed axially with respect to the tool axis A, is the radially highest elevation of the groove generating region 42
25 and 44, that is to say has the greatest radial spacing to the tool axis A or projects radially furthest outward.

Axially in front of the shaping spine 42G or 44G, each groove generating region 42 and 44 has a front surface 42F and 44F which rises axially to the shaping
30 spine 42G or 44G from a front profile 42G' or 44G', situated radially further inward than the shaping spine 42G and 44G, on the face side 6 of the tool 4 and

which forms a run-on surface by means of which the groove generating region 42 and 44 presses into the workpiece surface for the first time and with slowly increasing deformation force.

- 5 Behind the shaping spine 42G or 44G there adjoins, in an axial direction, a back surface 42H or 44H of the groove generating region 42 and 44, which back surface slopes downward from the shaping spine 42G or 44G in an axial direction.

The shaping spine 42G or 44G itself has, as viewed in a circumferential direction,
 10 an elevation which projects radially furthest outward, specifically a maximum 42I or 44I, and said shaping spine slopes downward radially from the maximum 42I or 44I in both circumferential directions, specifically in one flank 42J or 44J to a rear end point 42L or 44L which is situated radially further inward than the maximum 42I or 44I, and in a further flank 42K or 44K to a front end point 42M or
 15 44M which is situated radially further inward than the maximum 42I or 44I. In the example of FIG 24, the end point 42M or 44M is situated radially further inward than the end point 42L or 44L, and the flank 42J or 44J is shorter than the flank 42K or 44K, that is to say the maximum 42I or 44I is situated closer to the rear side region 42E or 44E and the rear end point 42L or 44L of the groove generating
 20 region 42 and 44. This asymmetrical shape of the groove generating regions 42 and 44 leads to greater rigidity of the tool during the shaping of the grooves and/or is adapted to the subsequent thread generating regions 32 and 34. A symmetrical design is also possible.

- 25 The front profile 42G' or 44G' has a similar shape to the shaping spine 42G or 44G with a maximum 42I' or 44I' and two flanks 42J' or 44J', or 42K' or 44K', respectively, sloping downward from the maximum to end points 42L' or 44L', or 42M' or 44M', respectively. The front surface 42F or 44F connects corresponding maxima 42I and 42I' and also 44I and 44I', and corresponding end points 42L
 30 and 42L' and also 44L and 44L', and self-evidently the interposed flanks 42J and 42J' and also 44J and 44J' and 42K and 42K' and 44K and 44K'.
-

In the exemplary embodiment of FIGs 22 to 24, the front surface 42F or 44F runs between the front profile and the shaping spine in an axial direction in a substantially linear manner, or by contrast in a convexly inwardly curved manner in the
5 exemplary embodiment of FIG 25. These and numerous other different shapes of the front surface 42F or 44F are possible depending on the desired growth or axial gradients of the deformation force.

The wedge-like shape, sloping downward in both circumferential directions, of the
10 shaping spine 42G or 44G and of the front surface 42F or 44F permits a flow of the workpiece material also to the side or in a circumferential direction when the groove generating region 42 or 44 is moved axially into the workpiece.

The thread generating regions 32 and 34 of the tool 4 are, in these exemplary
15 embodiments as per FIGs 22 to 25, designed to impart a cutting action as in FIGs 11 to 14, though may also be of some other design, for example as in FIG 20, or else so as to operate in a non-cutting manner as in FIG 9.

Preferred materials for the workpiece are metals, in particular aluminum alloys
20 and magnesium alloys and other light metals, though the invention is not restricted to these materials. Furthermore, as workpieces, use may be made of both thick-walled or solid workpieces or also thin-walled components or metal sheets, composed in particular of steel or other materials.

List of reference signs

2	Workpiece
3	Thread generating tool
4	Thread generating tool
5	Shank
6	Face side
7	Polygon
8	Front portion
9	Rear portion
14	Thread generating tool
20	Core hole
21	Core hole wall
22, 24	Groove
22B, 24B	Groove base
23, 25	Wall region
32, 34	Thread generating region
32-1, 32-2	Pressing lobe
32-3	Pressing lobe
32A, 34A	Thread-cutting tooth
32B, 34B	Free surface
32C, 34C	Rake surface
32E, 34E	Side region
32F, 34F	Flattening
32G, 34G	Tooth tip
33, 35	Outer surface
36	Thread flight
36F	Thread base
42, 44	Groove generating region
42A, 44A	Groove cutting edge
42B, 44B	Free surface
42C, 44C	Rake surface
42D, 44D	Front side cutting edge
42E, 44E	Rear side region
42F, 44F	Front surface

42G, 44G	Shaping spine
42G', 44G'	Front profile
42H, 44H	Back surface
42I, 44I	Maximum
42I', 44I'	Maximum
42J, 44J	Flank
42J', 44J'	Flank
42K, 44K	Flank
42K', 44K'	Flank
42L, 44L	End point
42L', 44L'	End point
42M, 44M	End point
42M', 44M'	End point
43, 45	Outer surface
50	Duct
51	Central region
52, 54	Bulge
55	Drilled region
56	Cut region
62, 64	Bulge
72, 82	Thread generating sub-region
74, 84	Thread generating sub-region
76, 86	Thread sub-region
321, 322	Thread generating sub-region
A	Tool axis
B	Lobe axis
D	Core hole diameter
E,F	Thread diameter
d	Tool diameter
g	Gap width
S	Direction of rotation
M	Central axis
P	Thread pitch
t	Groove depth
r	Radius

r_0, r_1, r_2	Radius
h	Radial height
Δr	Radial spacing
L_1, L_2	Axial length
α	Angle of rotation
β, γ	Angle
δ, ε	Angle

Claims:

1. A thread generating tool for producing a thread in a workpiece, having the features:
 - a) the tool is rotatable about a tool axis (A),
 - b) the tool has n groove generating regions for generating in each case one groove in the workpiece, wherein $n \geq 1$, and m thread generating regions for generating the thread in the workpiece, wherein $m \geq 1$,
 - c) each of the m thread generating regions is arranged behind one of the n groove generating regions as viewed in an axial projection parallel to the tool axis (A), and has a smaller extent than said groove generating region as viewed in cross section in the axial projection,
 - d) wherein at least some of the n groove generating regions are formed as cutting groove generating regions with groove generating cutting edges,
 - e) wherein each groove generating region has a groove cutting edge oriented toward or situated on the face side,
 - f) wherein the groove cutting edges are the radially furthest outward projecting regions of the tool, at least in the front portion thereof,
 - g) wherein the or each groove cutting edge is adjoined laterally in a circumferential direction by a side cutting edge, which is at the front in the direction of rotation (S) about the tool axis (A),
 - h) wherein during the rotation of the tool in the direction of rotation (S) which takes place for the generation of the thread, the front side cutting edge cuts laterally into the workpiece.
2. The tool as claimed in claim 1, in which the groove generating cutting edges are arranged on a face side of the tool, wherein at least some of the cutting groove generating regions or groove generating cutting edges have, in an axial direction or in a circumferential direction, in each case at least one step or edge which is provided as a chip-splitting step or edge.

3. The tool as claimed in claimed in claim 1, wherein
the n groove generating regions are arranged at uniform angular intervals of $360^\circ/n$ relative to one another about the tool axis.
4. The tool as claimed in claimed in claim 1, wherein
an angle component β of one or each groove generating region and of the thread generating regions, situated therebehind, about the tool axis (A) is between 7.2° and 45° .
5. The tool as claimed in claimed in claim 1, wherein
the thread generating regions project radially further outward than the other outer surfaces of the thread generating tool.
6. The tool as claimed in claimed in claim 1, wherein
at least one thread generating region is a thread shaping region and generates its part of the thread flight by a shaping and thus non-cutting process.
7. The tool as claimed in claimed in claim 1, wherein
at least some of the thread generating regions of the thread generating tool have thread pressing lobes arranged on a helical line, which corresponds in terms of thread pitch and turning direction to the thread to be generated, about the tool axis (A), which thread pressing lobes project radially furthest outward within the thread generating region but project radially outward to a lesser extent than the one or more groove generating region(s).
8. The tool as claimed in claimed in claim 1, wherein
at least one thread generating region is a thread cutting region and generates its part of the thread flight by a cutting process.
9. The tool as claimed in claimed in claim 1, wherein
at least some of the thread generating regions of the thread generating tool have thread cutting teeth arranged on a helical line, which corresponds in terms of thread pitch and turning direction to the thread to be generated, about the tool axis

(A), which thread cutting teeth project radially furthest outward within the thread generating region but project radially outward to a lesser extent than the one or more groove generating region(s), wherein the thread cutting teeth are joined in a direction opposite to the cutting direction or direction of rotation by outer free surfaces.

10. The tool as claimed in claim 9, wherein:

the thread cutting teeth are arranged and formed so as to cut in the turning direction of the thread to be generated and of the helical line about the tool axis

(A) on which the thread cutting teeth are arranged,

or

the thread cutting teeth are arranged and formed so as to cut oppositely to the turning direction of the thread to be generated and of the helical line about the tool axis (A) on which the thread cutting teeth are arranged.

11. The tool as claimed in claimed in claim 1, wherein

the groove generating regions or the thread generating regions are fastened detachably or exchangeably to a tool carrier.

12. The tool as claimed in claimed in claim 1, wherein

the groove cutting edges are of at least approximately circular form.

13. The tool as claimed in claimed in claim 1, wherein

the groove cutting edges are of a radius (r_0) that is greater by a differential radius (Δr) than a radius (r_1) of a first thread generating sub-region of the m thread generating regions, the or each groove cutting edge is adjoined laterally in a circumferential direction by a rear side region which is at the rear in the direction of rotation (S) about the tool axis (A), wherein there adjoins in a radially inward direction a lateral rake surface to the front side cutting edge.

14. The tool as claimed in claimed in claim 13, wherein

the rear side region is, by contrast, at an obtuse angle, that is to say does

not have cutting action and is of convex form.

15. The tool as claimed in claim 13, wherein
axially behind the groove cutting edge there adjoins a free surface which slopes downward, in a linear or conical fashion, from the radius (r_0) to a radius smaller than the radius (r_1) of a first pressing lobe or of the first thread generating sub-region.
16. The tool as claimed in claim 1, wherein
the groove cutting edge is adjoined in a radially inward direction by a face-side rake surface which runs axially rearward in a linear or concavely curved fashion and on which chips produced during the generation or reaming of the groove with the groove cutting edge are discharged.
17. The tool as claimed in claim 16, wherein
the face-side rake surface runs from a lowest point axially forward again to a planar central region oriented perpendicular to the tool axis A, which central region surrounds a central opening of a central duct of the tool, via which central duct coolant or lubricant can be supplied.
18. The tool as claimed in any one of claims 6 and 7, wherein
the tool comprises a shank which has a rear portion, which is of cylindrical form, and a front portion which is narrowed in diameter adjacent to the rear portion and centrally through which the tool axis (A) extends.
19. The tool as claimed in claim 18, wherein
at the end of the rear portion there is formed a clamping region for the clamping of the shank.
20. The tool as claimed in any one of claim 18 and 19, wherein
the front portion has, toward the face side which faces away from the rear portion or which is arranged at the front, the m thread generating regions.

21. The tool as claimed in any one of claims 6 and 7, wherein
the m thread generating regions are in the form of axial rows, running in each case parallel to the tool axis (A), of thread generating ridges which, in the case of $m = 2$, are arranged diametrically with respect to one another on opposite sides of the tool axis (A), and wherein
the thread generating ridges run along the thread pitch of the desired thread and each have one thread pressing lobe, which projects radially furthest outward in relation to the tool axis (A), for a plastic impression of the thread flight into the workpiece, and
the outer radii of different thread generating ridges or the thread pressing lobes of two thread generating regions are equal to one another over the entire axial length.
22. The tool as claimed in any one of claims 6 and 7, wherein
the m thread generating regions are in the form of axial rows, running in each case parallel to the tool axis (A), of thread generating ridges which, in the case of $m = 2$, are arranged diametrically with respect to one another on opposite sides of the tool axis (A), and
the thread generating ridges run along the thread pitch of the desired thread and have in each case one thread pressing lobe, which projects radially furthest outward in relation to the tool axis (A), for plastic impression of the thread flight into the workpiece.
23. The tool as claimed in any one of claims 6 and 7, wherein
the m thread generating regions are in the form of axial rows, running in each case parallel to the tool axis (A), of thread generating ridges which, in the case of $m = 2$, are arranged diametrically with respect to one another on opposite sides of the tool axis (A).
24. The tool as claimed in any one of claims 6 and 7, wherein
the thread generating regions are separated by interposed outer surfaces which have a smaller outer radius than the thread generating regions, such that the interposed outer surfaces are recessed radially with respect to said thread

generating regions, or form free spaces between the thread generating regions.

25. The tool as claimed in any one of claims 6 and 7, wherein
the thread generating regions cover in each case a first angle range (δ) and
the outer surfaces cover in each case a second angle range (ϵ), wherein the first
angle range (δ) lies in an interval from one to 2.5 times the second angle range (ϵ)
or wherein the pressing lobes are situated centrally in the respective angle ranges.
26. The tool as claimed in any one of claims 24 and 25, wherein
the outer surfaces initially form concavely inwardly running portions directly
adjoining one of the thread generating regions and then bulge convexly outward
into bulges, or have only a convex outwardly directed bulge.
27. The tool as claimed in claimed in claim 1, wherein
the thread generating regions are divided into axially offset thread
generating sub-regions with different thread outer profiles, wherein any desired
thread outer profiles may be combined in any desired sequence.
28. The tool as claimed in claimed in claim 1, wherein
a first thread generating sub-region, the first thread generating sub-region
being a front thread generating sub-region, which is situated in front of a rear
thread generating sub-region axially or in a direction toward the face side, has a
thread outer profile with at least partially smaller dimensions or outer dimensions,
at the profile tip and at the profile flanks, than a second thread generating sub-
region, the second thread generating sub-region being the rear thread generating
sub-region.
29. The tool as claimed in claimed in claim 28, wherein
the front thread generating sub-region has, in its thread outer profile, a
flattening at the profile tip.
30. The tool as claimed in claimed in claim 28, wherein
the rear thread generating sub-region has an outer profile which has a

radially further outwardly projecting profile tip than the front thread generating sub-region.

31. The tool as claimed in claim 28, wherein
the diameter (E) of the front thread generating sub-region, is smaller than
the diameter (F) of the rear thread generating sub-region.

32. A method for producing a thread in a blind hole in a workpiece,
comprising the following method steps:

generating a number n of grooves in a wall, which encircles a thread axis,
of the workpiece by means of n groove generating regions of a tool and by means
of a movement of the tool substantially axial with respect to the thread axis,
wherein each groove generating region of the tool generates an associated groove;

introducing thread generating regions, which are situated behind the groove
generating regions, of the tool into the generated associated grooves in the wall of
the workpiece in a direction along the associated groove,

generating the thread in each wall sub-region, adjoining the groove(s), of
the wall of the workpiece by rotating the tool about the thread axis and with a
simultaneous axial feed motion of the thread generating tool coaxially with respect
to the thread axis with an

axial feed speed adapted to the rotational speed of the rotational movement
and to the thread pitch, wherein, during the rotation and the simultaneous axial
feed movement, each thread generating region engages into the associated wall
sub-region and generates an associated part of a thread flight, and after the
rotation projects into the same groove again

or into another groove in the wall;

moving the thread generating regions of the thread generating tool out of
the associated grooves in a direction along the grooves,

wherein the tool is used to perform the method, the tool comprising a
thread generating tool for producing the thread in the workpiece, the tool having
the following features:

- a) the tool is rotatable about a tool axis (A);
- b) the number of groove generating regions for generating in each

case one groove in the workpiece is $n \geq 1$ and the number of thread generating regions for generating the thread in the workpiece is $m \geq 1$;

c) each of the m thread generating regions is arranged behind one of the n groove generating regions as viewed in an axial projection parallel to the tool axis (A), and has a smaller extent than said groove generating region as viewed in cross section in the axial projection;

d) wherein at least some of the n groove generating regions are formed as cutting groove generating regions with groove generating cutting edges;

e) wherein each groove generating region has a groove cutting edge oriented toward or situated on the face side;

f) wherein the groove cutting edges are the radially furthest outward projecting regions of the tool, at least in the front portion thereof;

g) wherein the or each groove cutting edge is adjoined laterally in a circumferential direction by a side cutting edge, which is at the front in the direction of rotation (S) about the tool axis (A); and

h) wherein during the rotation of the tool in the direction of rotation (S) which takes place for the generation of the thread, the front side cutting edge cuts laterally into the workpiece.

33. The method as claimed in claim 32, wherein, during the introduction of the thread generating regions of the tool into the generated associated grooves, each thread generating region projects, in a direction radial with respect to the thread axis, into the associated groove so as to maintain a radial spacing from the groove base.

34. The method as claimed in claim 32, wherein, during the generation of the thread, the tool is rotated about the thread axis by a predefined angle of rotation.

35. A thread generating tool for producing a thread in a workpiece, having the features:

a) the tool is rotatable about a tool axis (A),

- b) the tool has a number $n \geq 1$ of groove generating regions for generating in each case one groove in the workpiece and a number $m \geq 1$ of thread generating regions for generating the thread in the workpiece,
- c) each of the m thread generating regions is arranged behind one of the n groove generating regions as viewed in an axial projection parallel to the tool axis (A), and has a smaller extent than said groove generating region as viewed in cross section in the axial projection,
- d) wherein at least some of the n groove generating regions are formed as groove generating regions which operate by plastic deformation or impression of the workpiece material,
- e) each groove generating region has a shaping spine which runs substantially in a circumferential direction around the tool axis (A) and which, as viewed in an axial direction, is the radially highest elevation of the groove generating region or projects radially furthest outward,
- f) in front of the shaping spine in an axial direction, each groove generating region has a front surface,
- g) wherein the front surface rises in an axial direction from a front profile, which is situated radially further inward than the shaping spine to the shaping spine,
- h) the front surface forming a run-on surface by means of which the groove generating region presses into the workpiece surface for the first time and with slowly increasing deformation force,
- i) wherein behind the shaping spine in an axial direction, each groove generating region has a back surface which slopes downward from the shaping spine in an axial direction and provides a free space for the flows of workpiece material.

36. The tool as claimed in claimed in any of claims 3 to 5, wherein the angle component β of one or each groove generating region and of the thread generating regions, situated therebehind, about the tool axis (A) is between 13° and 40° .

37. The tool as claimed in claimed in any of claims 3 to 5, wherein the

angle component β of one or each groove generating region and of the thread generating regions, situated therebehind, about the tool axis (A) is between 27° and 36° .

38. The tool as claimed in claimed in claim 35, wherein
the n groove generating regions are arranged at uniform angular intervals of $360^\circ/n$ relative to one another about the tool axis.
39. The tool as claimed in claimed in claim 35, wherein
an angle component β of one or each groove generating region and of the thread generating regions, situated therebehind, about the tool axis (A) is between 7.2° and 45° .
40. The tool as claimed in claimed in claim 35, wherein
the thread generating regions project radially further outward than the other outer surfaces of the thread generating tool.
41. The tool as claimed in claimed in claim 35, wherein:
at least one thread generating region is a thread shaping region and generates its part of the thread flight by a shaping and thus non-cutting process.
42. The tool as claimed in claimed in claim 35, wherein
at least some of the thread generating regions of the thread generating tool have thread pressing lobes arranged on a helical line, which corresponds in terms of thread pitch and turning direction to the thread to be generated, about the tool axis (A), which thread pressing lobes project radially furthest outward within the thread generating region but project radially outward to a lesser extent than the one or more groove generating region(s).
43. The tool as claimed in claimed in claim 35, wherein
at least one thread generating region is a thread cutting region and generates its part of the thread flight by a cutting process.

44. The tool as claimed in claim 35, wherein
at least some of the thread generating regions of the thread generating tool have thread cutting teeth arranged on a helical line, which corresponds in terms of thread pitch and turning direction to the thread to be generated, about the tool axis (A), which thread cutting teeth project radially furthest outward within the thread generating region but project radially outward to a lesser extent than the one or more groove generating region(s), wherein the thread cutting teeth are joined in a direction opposite to the cutting direction or direction of rotation by outer free surfaces.
45. The tool as claimed in claim 43 or 44, wherein:
the thread cutting teeth are arranged and formed so as to cut in the turning direction of the thread to be generated and of the helical line about the tool axis (A) on which the thread cutting teeth are arranged,
or
the thread cutting teeth are arranged and formed so as to cut oppositely to the turning direction of the thread to be generated and of the helical line about the tool axis (A) on which the thread cutting teeth are arranged.
46. The tool as claimed in claim 35, wherein
the groove generating regions or the thread generating regions are fastened detachably or exchangeably to a tool carrier.
47. The tool as claimed in claim 35, wherein
groove cutting edges of the groove generating regions are of at least approximately circular form.
48. The tool as claimed in claim 35, wherein
a radius (r_0) of groove cutting edges of the groove generating regions is greater by a differential radius (Δr) than a radius (r_1) of the first thread generating sub-region, the or each groove cutting edge is adjoined laterally in a

circumferential direction by a side region which is at the rear in the direction of rotation (S) about the tool axis (A), wherein there adjoins in a radially inward direction a lateral rake surface to a front side cutting edge.

49. The tool as claimed in claimed in claim 35, wherein
a rear side region adjoining a groove cutting edge is, by contrast, at an obtuse angle, hence with no cutting action, and is of convex form.
50. The tool as claimed in claimed in claim 35, wherein
axially behind a groove cutting edge of the groove generating region there adjoins a free surface which slopes downward, in a linear or conical fashion, from the radius (r_0) to a radius smaller than the radius (r_1) of the first pressing lobe or of the first thread generating sub-region.
51. The tool as claimed in claimed in claim 35, wherein
a groove cutting edge of the groove generating region is adjoined in a radially inward direction by a face-side rake surface which runs axially rearward in a linear or concavely curved fashion and on which chips produced during the generation or reaming of the groove with the groove cutting edge are discharged.
52. The tool as claimed in claimed in claim 35, wherein
a face-side rake surface runs from a lowest point axially forward again to a planar central region oriented perpendicular to the tool axis A, which central region surrounds a central opening of a central duct of the tool, via which central duct coolant or lubricant can be supplied.
53. The tool as claimed in claim 41 or 42, wherein
the tool comprises a shank which has a rear portion, which is of cylindrical form, and a front portion which is narrowed in diameter adjacent to the rear portion and centrally through which the tool axis (A) extends.
54. The tool as claimed in claim 41 or 42, wherein
at the end of the rear portion there is formed a clamping region for the

clamping of the shank.

55. The tool as claimed in claim 41 or 42, wherein
the front portion has, toward the face side which faces away from the rear portion or which is arranged at the front, the m thread generating regions.
56. The tool as claimed in claim 41 or 42, wherein
the m thread generating regions are in the form of axial rows, running in each case parallel to the tool axis (A), of thread generating ridges which, in the case of $m = 2$, are arranged diametrically with respect to one another on opposite sides of the tool axis (A), and
the thread generating ridges run along the thread pitch of the desired thread and have in each case one pressing lobe, which projects radially furthest outward in relation to the tool axis (A), for the plastic impression of the thread flight into the workpiece, and
the outer radii of the thread generating ridges or pressing lobes of the thread generating regions are equal to one another over the entire axial length.
57. The tool as claimed in claim 41 or 42, wherein
the m thread generating regions are in the form of axial rows, running in each case parallel to the tool axis (A), of thread generating ridges which, in the case of $m = 2$, are arranged diametrically with respect to one another on opposite sides of the tool axis (A), and
the thread generating ridges run along the thread pitch of the desired thread and have in each case one pressing lobe, which projects radially furthest outward in relation to the tool axis (A), for the plastic impression of the thread flight into the workpiece.
58. The tool as claimed in claim 41 or 42, wherein
the m thread generating regions are in the form of axial rows, running in each case parallel to the tool axis (A), of thread generating ridges which, in the case of $m = 2$, are arranged diametrically with respect to one another on opposite sides of the tool axis (A).

59. The tool as claimed in claim 41 or 42, wherein
the thread generating regions are separated by interposed outer surfaces
which have a smaller outer radius than the thread generating regions, that is to say
are recessed radially with respect to said thread generating regions, or form free
spaces between the thread generating regions.
60. The tool as claimed in claim 41 or 42, wherein
the thread generating regions cover in each case a first angle range (δ) and
the outer surfaces cover in each case a second angle range (ϵ), wherein the first
angle range (δ) lies in an interval from one to 2.5 times the second angle range (ϵ)
or wherein the pressing lobes are situated centrally in the respective angle ranges.
61. The tool as claimed in claim 41 or 42, wherein
the outer surfaces initially form concavely inwardly running portions directly
adjoining one of the thread generating regions and then bulge convexly outward
into bulges, or have only a convex outwardly directed bulge.
62. The tool as claimed in claimed in claim 35, wherein
the thread generating regions are divided into axially offset thread
generating sub-regions with different thread outer profiles, wherein any desired
thread outer profiles may be combined in any desired sequence.
63. The tool as claimed in claimed in claim 35, wherein
a first thread generating sub-region, the first thread generating sub-region
being a front thread generating sub-region, which is situated in front of a rear
thread generating sub-region axially or in a direction toward the face side, has a
thread outer profile with at least partially smaller dimensions or outer dimensions,
at the profile tip but also at the profile flanks, than a second thread generating
sub-region, the second thread generating sub-region being the rear thread
generating sub-region.
64. The tool as claimed in claimed in claim 35, wherein

the front thread generating sub-region has, in its thread outer profile, a flattening at the profile tip.

65. The tool as claimed in claim 35, wherein
the rear thread generating sub-region has an outer profile which has a radially further outwardly projecting profile tip than the front thread generating sub-region.
66. The tool as claimed in claim 35, wherein
the diameter (E) of the front thread generating sub-region, is smaller than the diameter (F) of the rear thread generating sub-region.
67. A method for producing a thread in a blind hole in a workpiece, comprising the following method steps:
generating a number n of grooves in a wall, which encircles a thread axis, of the workpiece by means of n groove generating regions of a tool and by means of a movement of the tool substantially axial with respect to the thread axis, wherein each groove generating region of the tool generates an associated groove;
introducing thread generating regions, which are situated behind the groove generating regions, of the tool into the generated associated grooves in the wall of the workpiece in a direction along the associated groove,
generating the thread in sub-regions of the wall, adjoining the groove(s), of the wall of the workpiece by rotating the tool about the thread axis and with a simultaneous axial feed motion of the thread generating tool coaxially with respect to the thread axis with an
axial feed speed adapted to the rotational speed of the rotational movement and to the thread pitch, wherein, during the rotation and the simultaneous axial feed movement, each thread generating region engages into an associated sub-region of the sub-regions of the wall and generates an associated part of a thread flight, and after the rotation projects into the same groove again
or into another groove in the wall;
moving the thread generating regions of the thread generating tool out of the associated grooves in a direction along the grooves,

wherein the tool comprising the thread generating tool is used to perform the above method steps, the tool having the following features:

- a) the tool is rotatable about a tool axis (A),
- b) the tool has the n groove generating regions for generating in each case one groove in the workpiece, wherein $n \geq 1$, and the tool has a number m of the thread generating regions, wherein $m \geq 1$, for generating the thread in the workpiece,
- c) each of the m thread generating regions is arranged behind one of the n groove generating regions as viewed in an axial projection parallel to the tool axis (A), and has a smaller extent than said groove generating region as viewed in cross section in the axial projection,
- d) wherein at least some of the n groove generating regions are formed as groove generating regions which operate by plastic deformation or impression of the workpiece material,
- e) each of the n groove generating regions has a shaping spine which runs substantially in a circumferential direction around the tool axis (A) and which, as viewed in an axial direction, is the radially highest elevation of the groove generating region or projects radially furthest outward,
- f) in front of the shaping spine in an axial direction, each groove generating region has a front surface,
- g) wherein the front surface rises in an axial direction from a front profile, which is situated radially further inward than the shaping spine to the shaping spine,
- h) the front surface forming a run-on surface by means of which the groove generating region presses into the workpiece surface for the first time and with slowly increasing deformation force;
- i) wherein behind the shaping spine in an axial direction, each groove generating region has a back surface which slopes downward from the shaping spine in an axial direction and provides a free space for the flows of workpiece material.

68. The method as claimed in claim 67, wherein, during the introduction of the thread generating regions of the tool into the generated associated

grooves, each thread generating region projects, in a direction radial with respect to the thread axis, into the associated groove so as to maintain a radial spacing from the groove base.

69. The method as claimed in claim 67, wherein, during the generation of the thread, the tool is rotated about the thread axis by a predefined angle of rotation.

70. The tool as claimed in claim 35, wherein the shaping spine has a maximum which projects radially furthest outward, and said shaping spine slopes downward radially from the maximum in one circumferential direction in one flank to a first end point which is situated radially further inward than the maximum, and in the other circumferential direction in a further flank to a second end point which is situated radially further inward than the maximum, and

one end point of the first or second end points is situated radially further inward than the other end point of the first or second end points or one of the flanks of the shaping spine is shorter than the other flank of the shaping spine, and

the front profile has a similar shape to the shaping spine with a maximum and two flanks sloping downward from the maximum to end points.

71. The tool as claimed in claim 35, wherein the shaping spine has a maximum which projects radially furthest outward, and said shaping spine slopes downward radially from the maximum in one circumferential direction in one flank to a first end point which is situated radially further inward than the maximum, and in the other circumferential direction in a further flank to a second end point which is situated radially further inward than the maximum, and

one end point is situated radially further inward than the other end point or one flank is shorter than the other flank.

72. The tool as claimed in claim 35, wherein the shaping spine has a maximum which projects radially furthest outward, and said shaping spine

slopes downward radially from the maximum in one circumferential direction in one flank to a first end point which is situated radially further inward than the maximum, and in the other circumferential direction in a further flank to a second end point which is situated radially further inward than the maximum.

73. The tool as claimed in claim 35, wherein the front surface connects corresponding maxima of the shaping spine and front profile or corresponding end points or corresponding flanks.

74. The tool as claimed in claim 35, wherein the front surface runs between the front profile and the shaping spine in an axial direction in a substantially linear or convexly inwardly curved manner or following an arbitrary continuous radial function.

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FIG 1

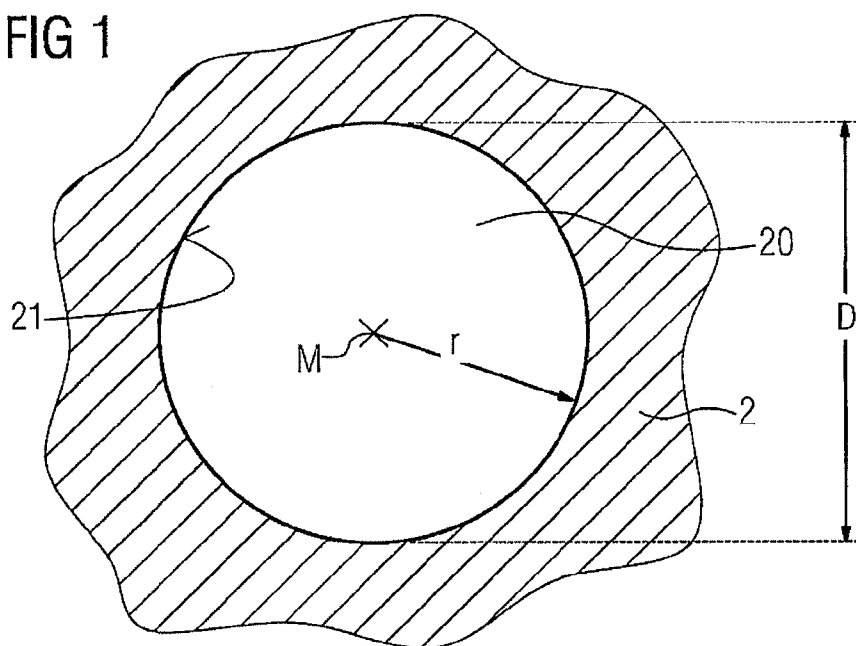


FIG 2

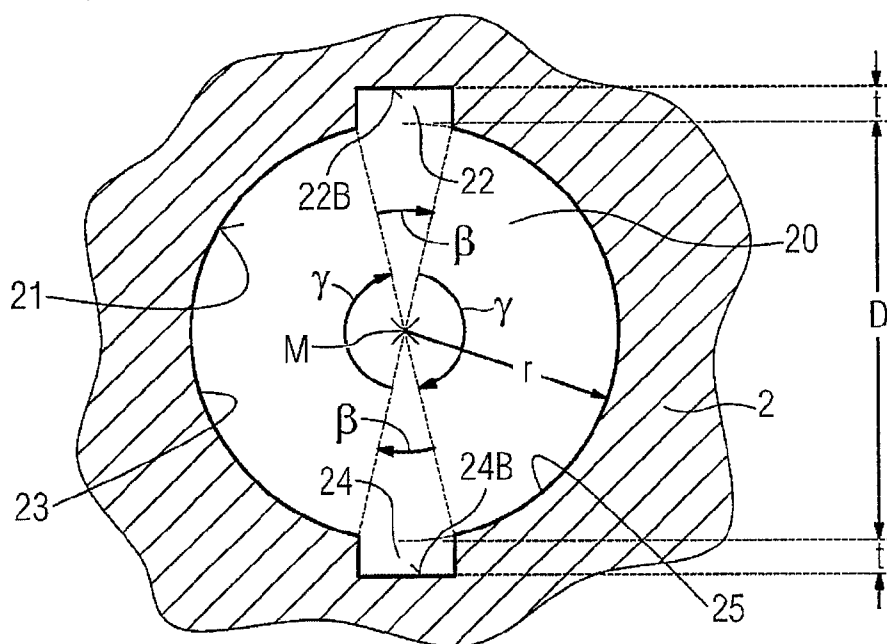


FIG 3

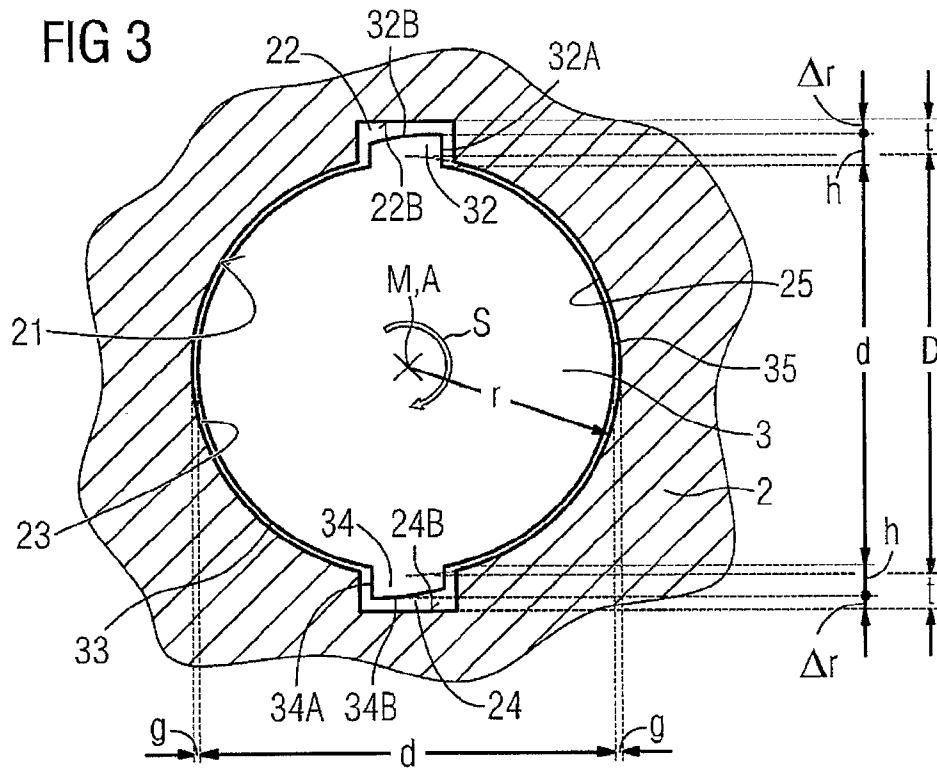
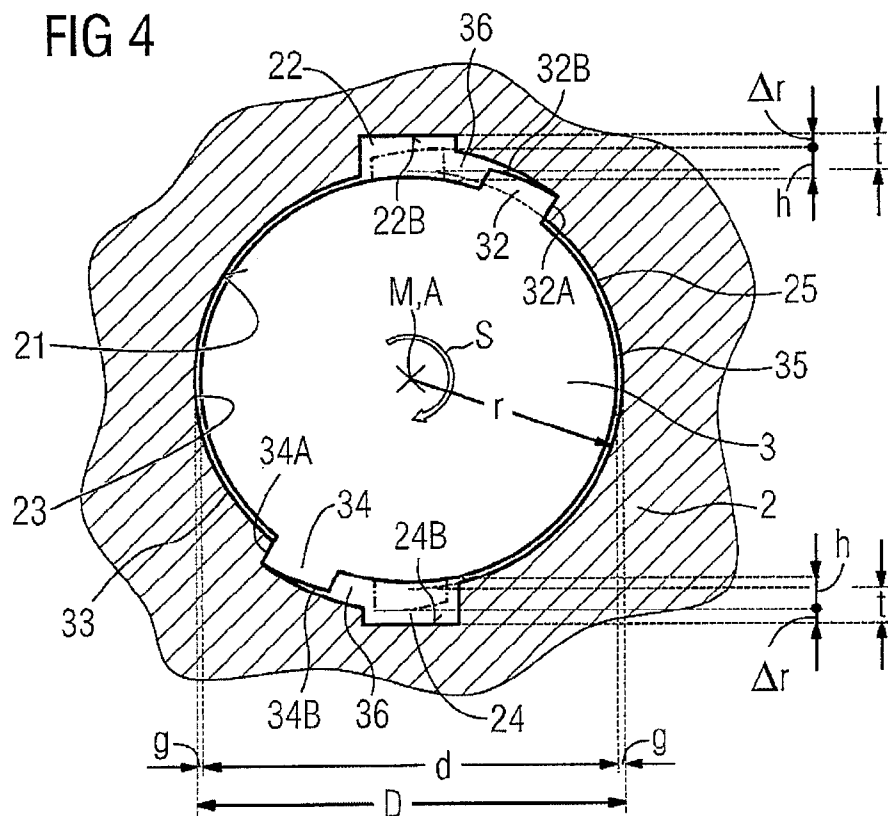
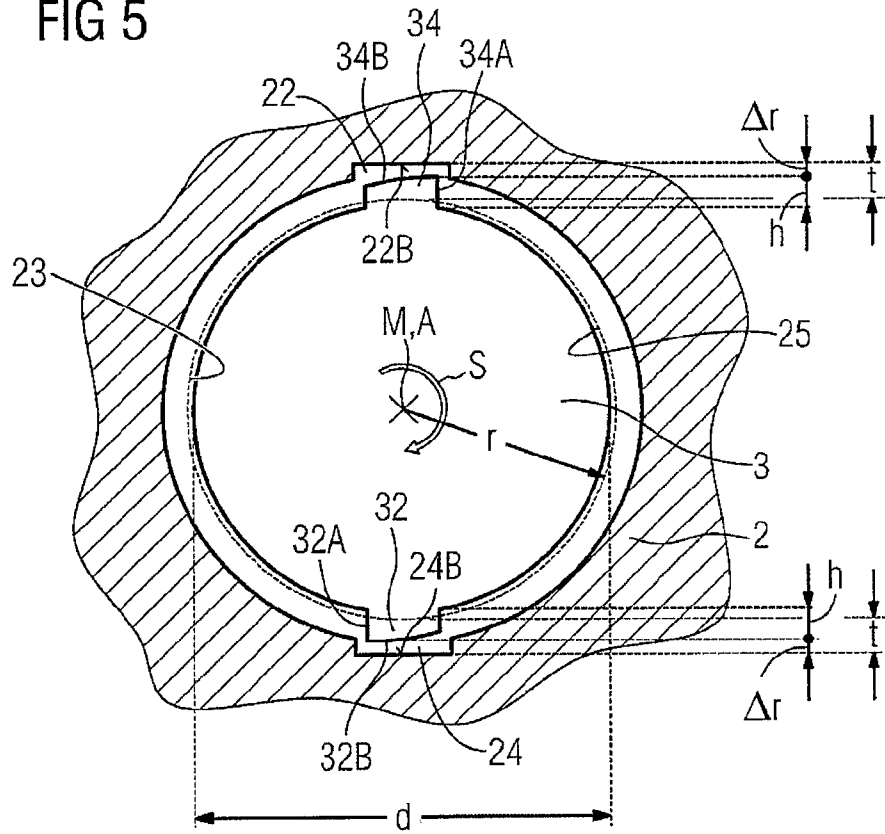


FIG 4



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FIG 5



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FIG 6

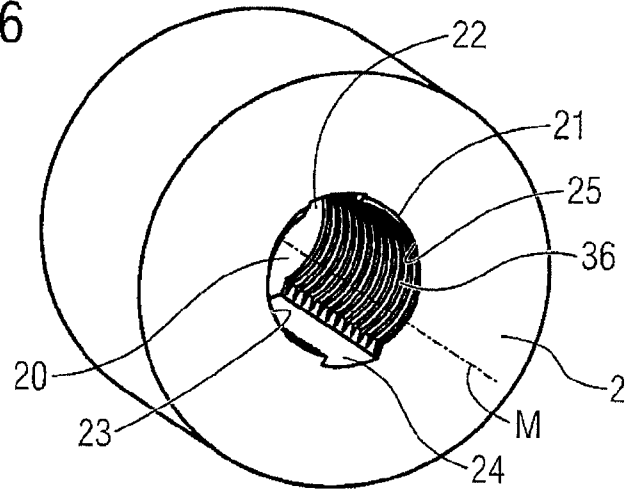


FIG 7

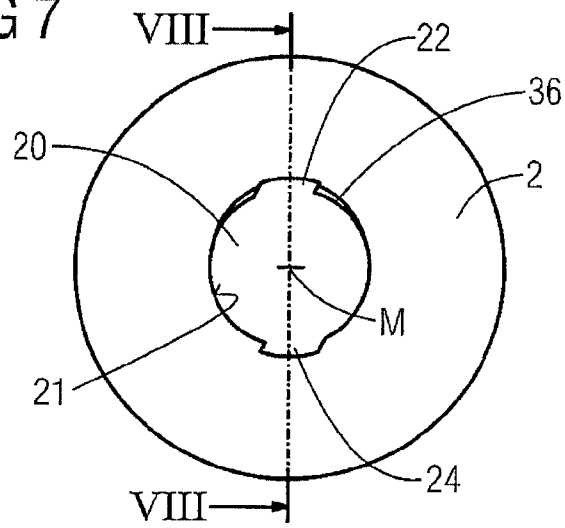
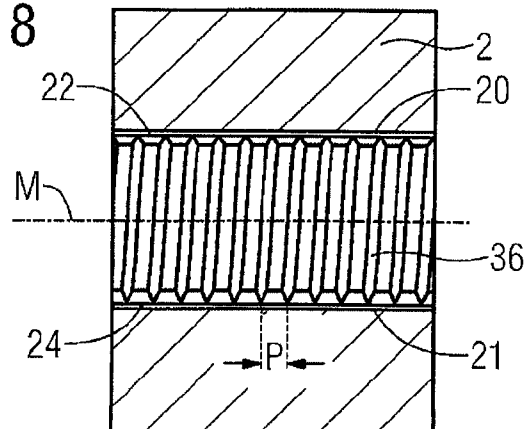
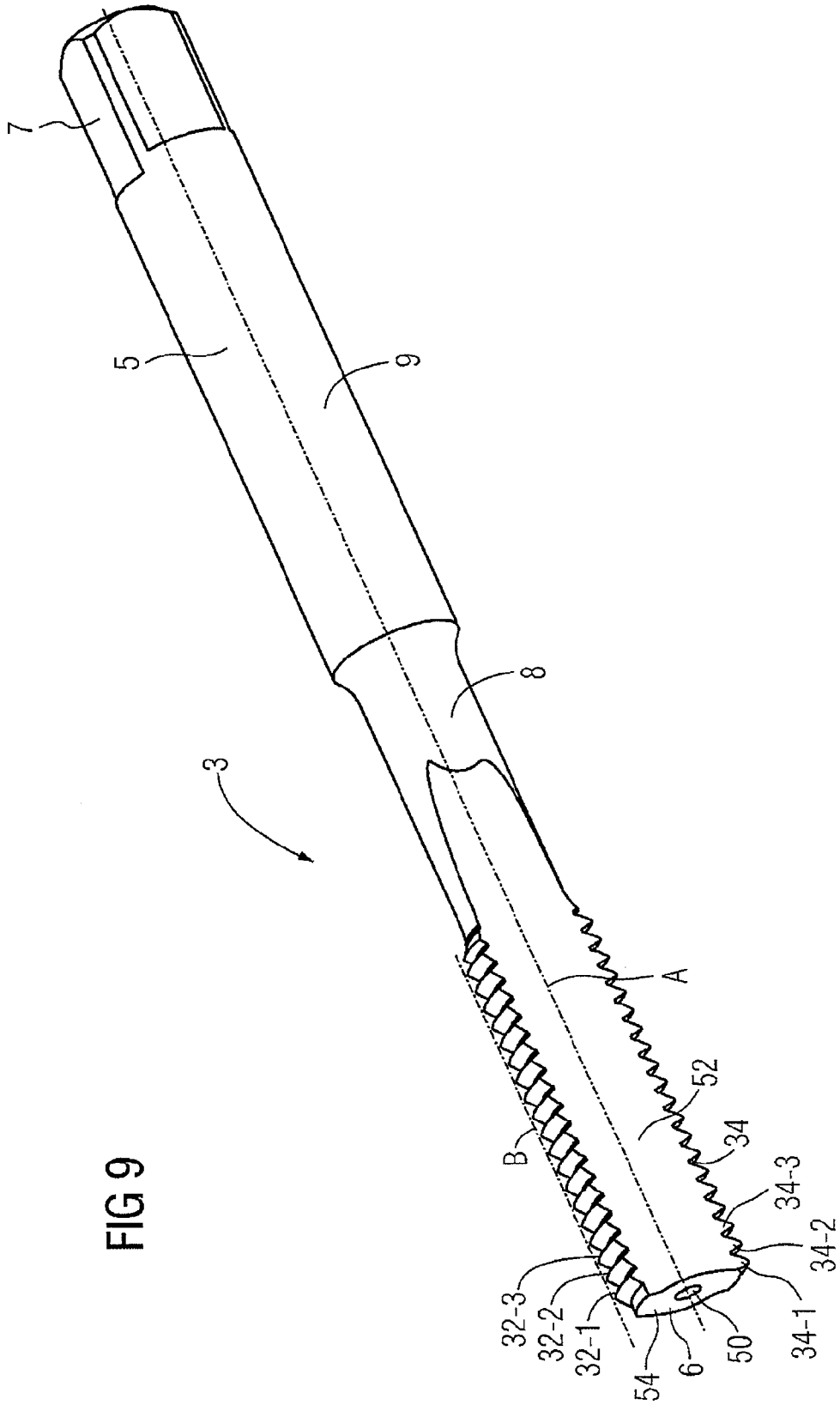


FIG 8

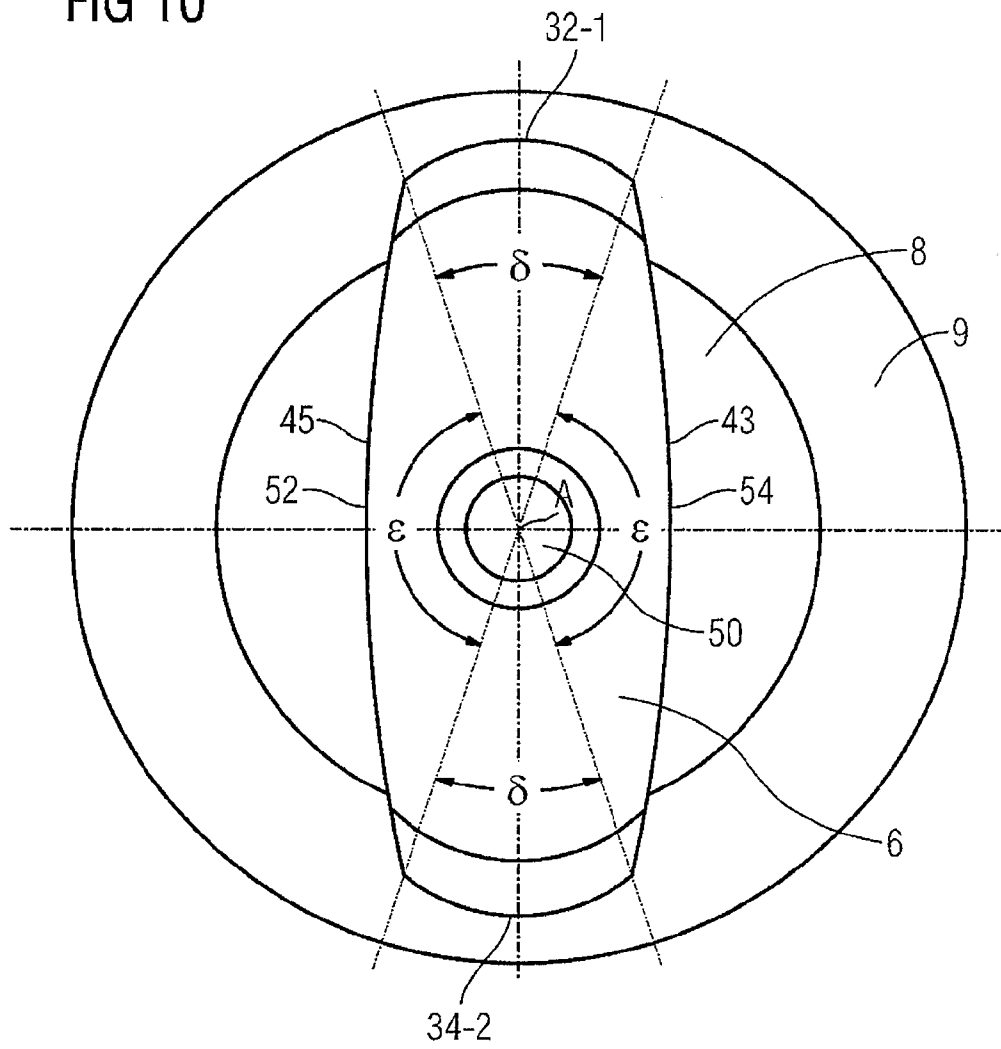


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FIG 10



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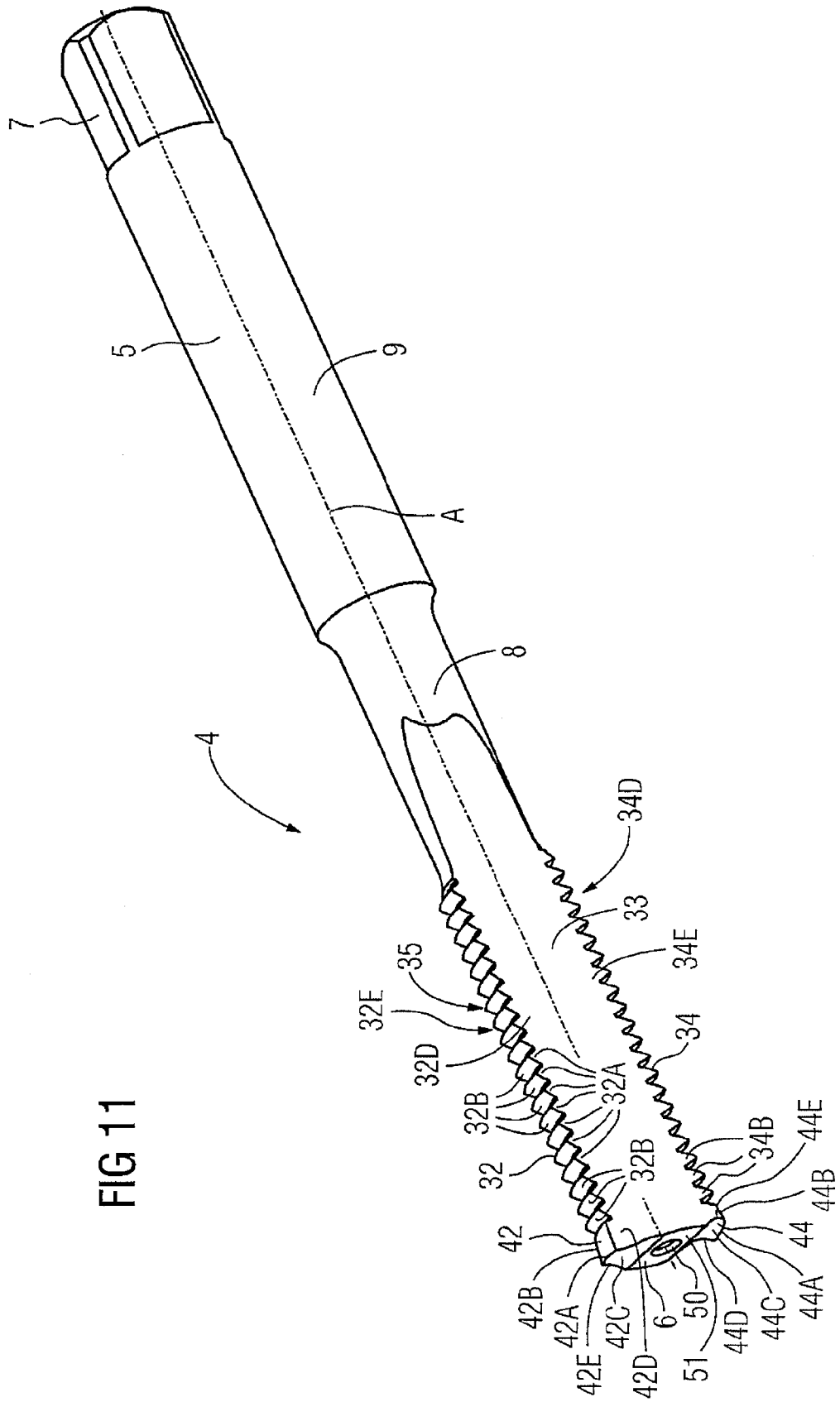


FIG 12

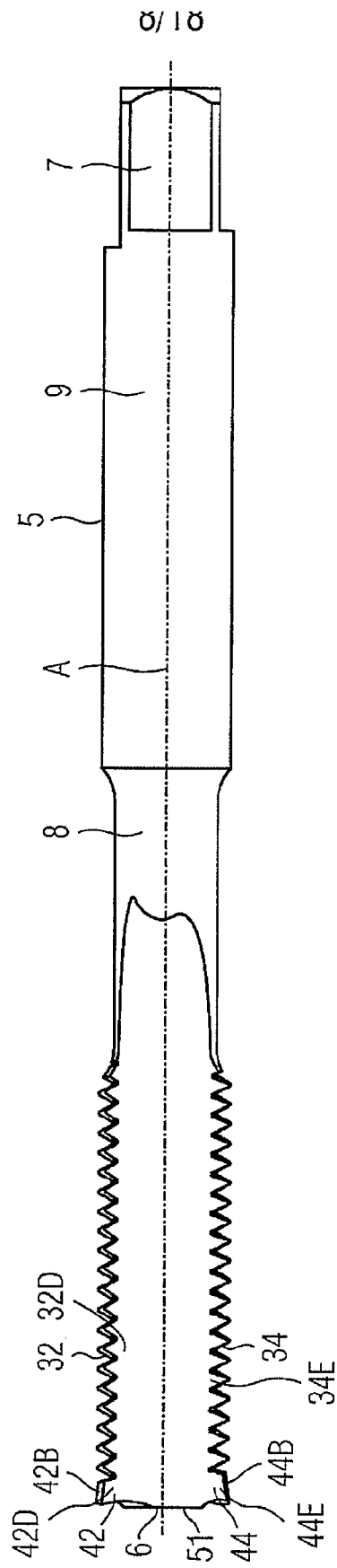
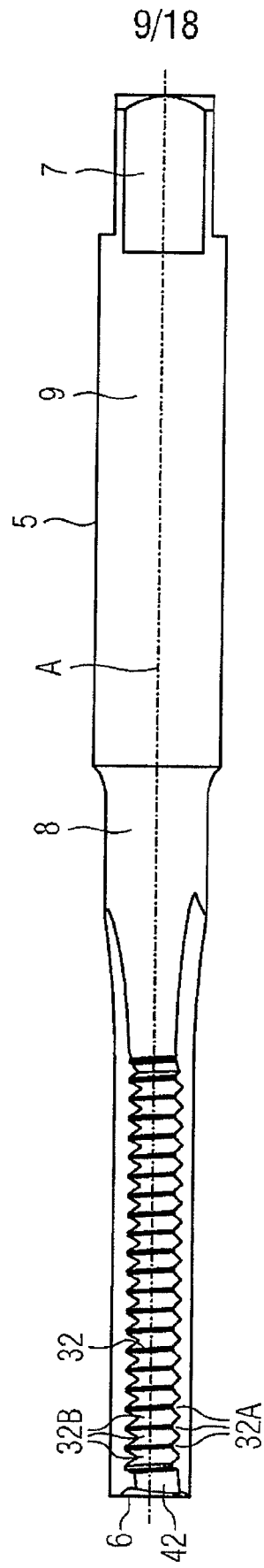
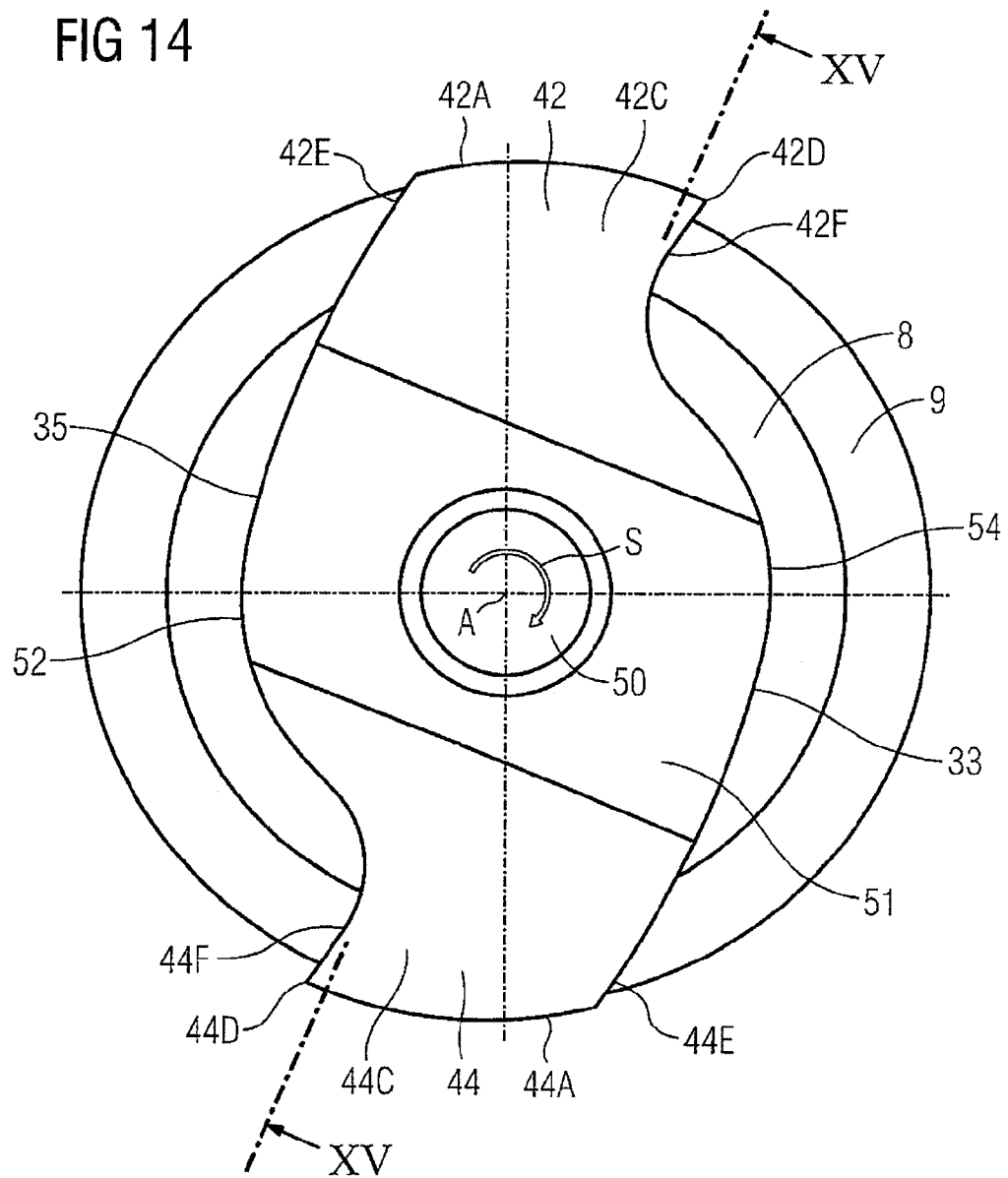


FIG 13



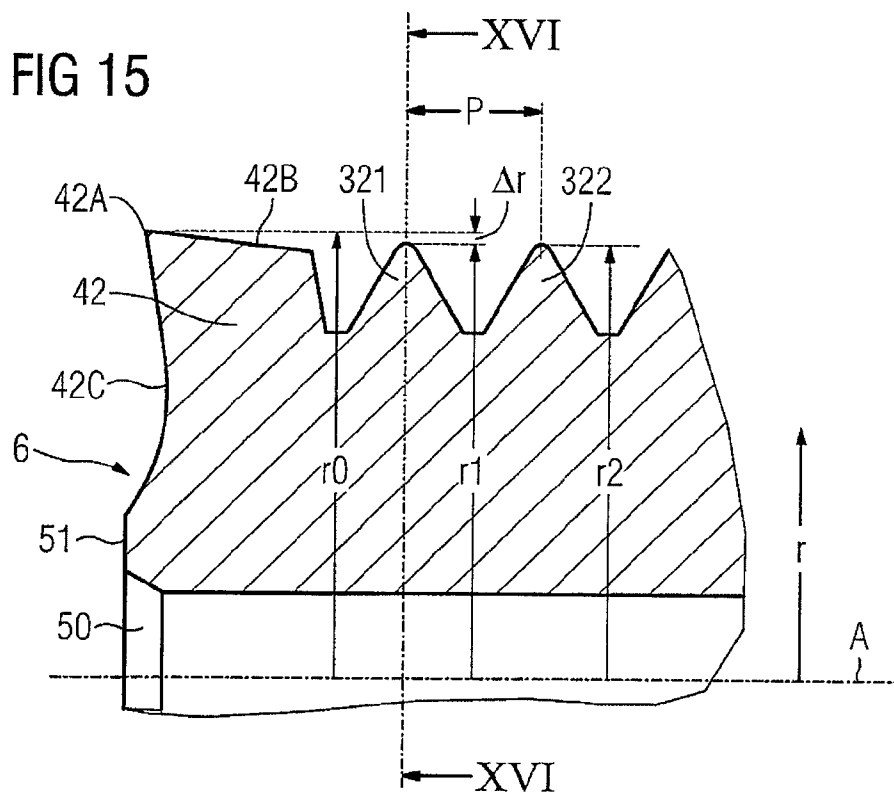
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FIG 14



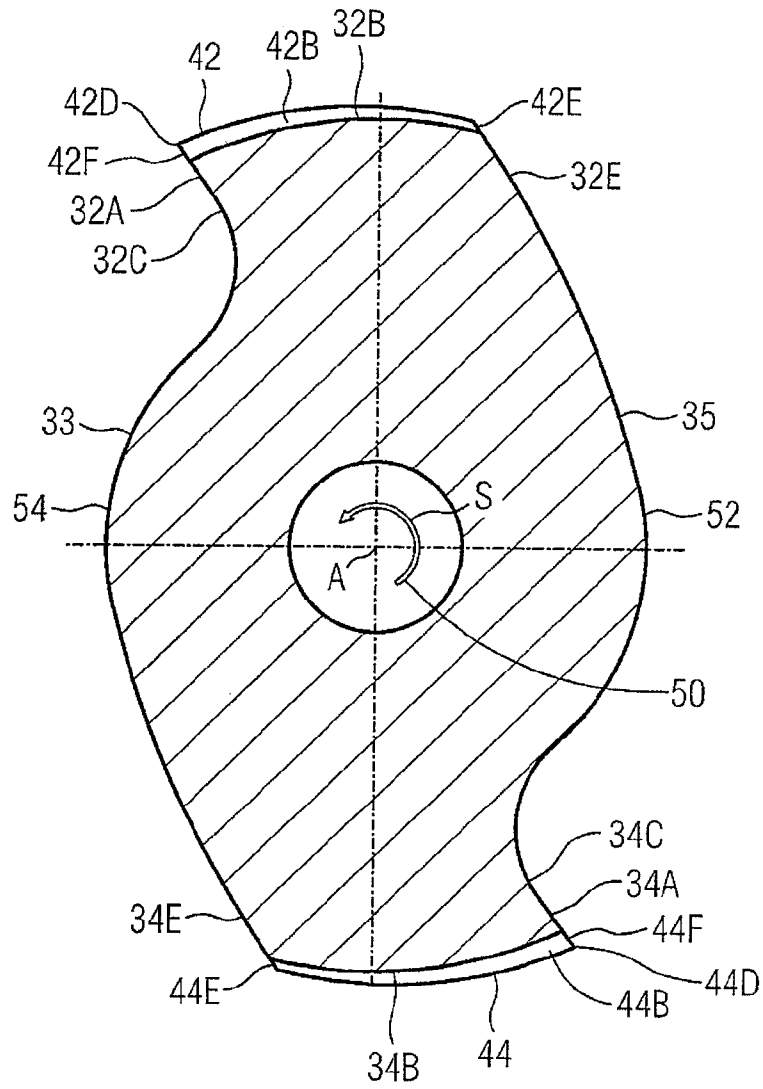
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FIG 15



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FIG 16



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FIG 17

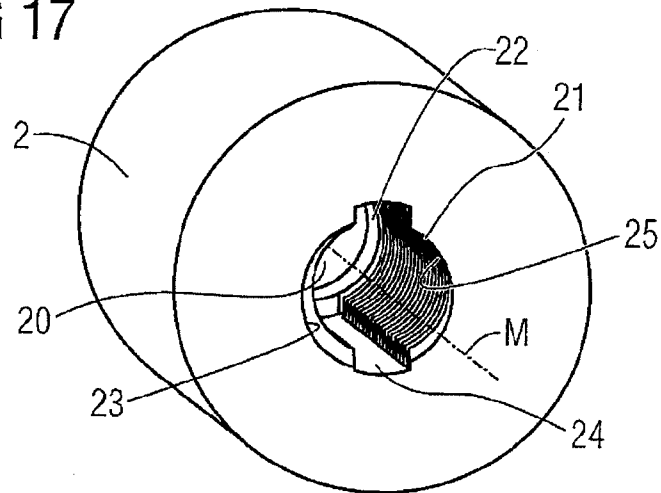


FIG 18

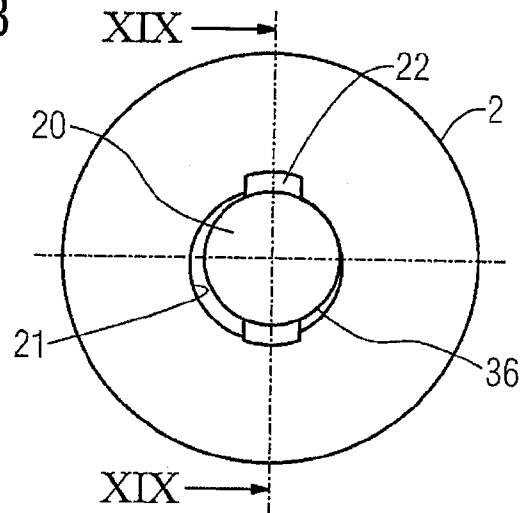
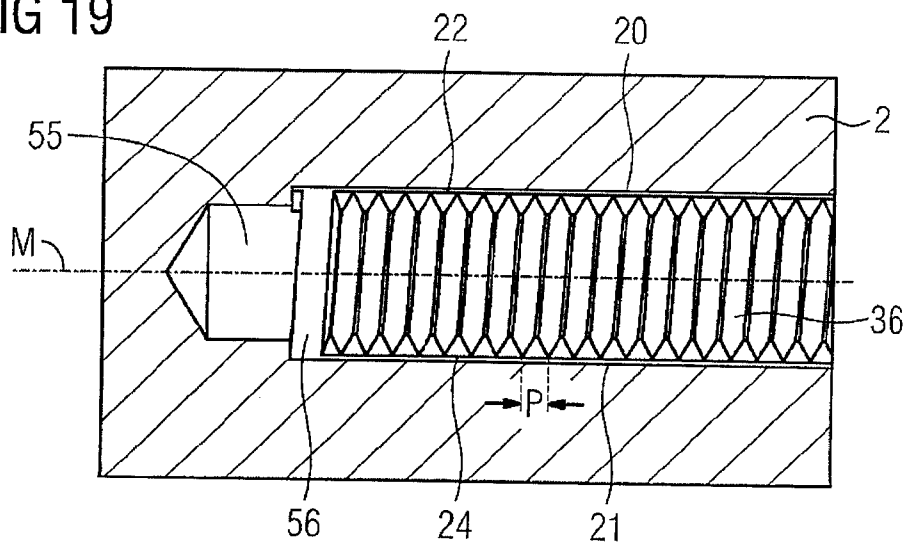


FIG 19



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FIG 20

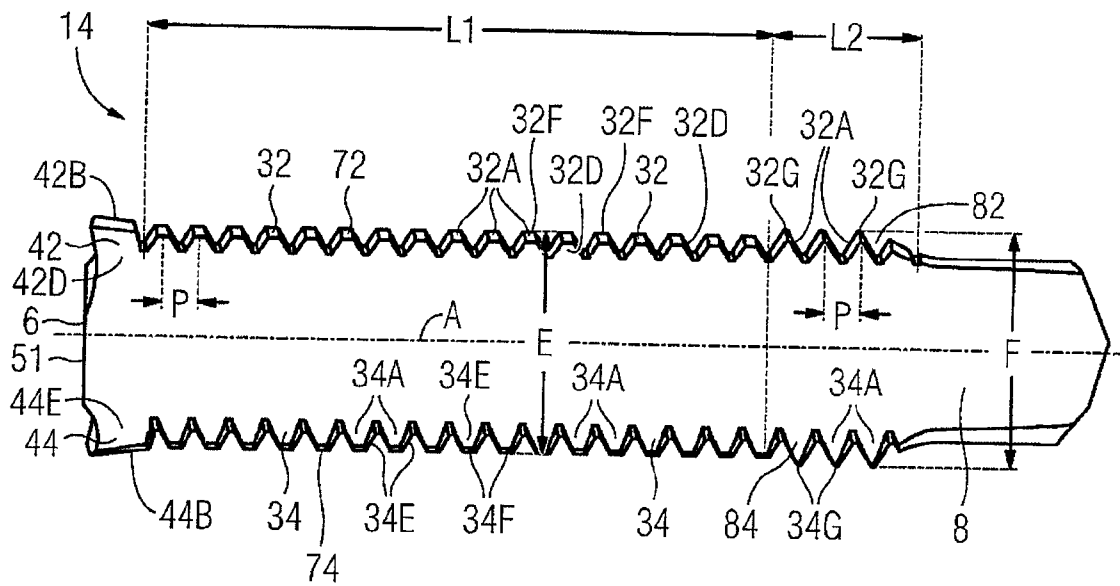
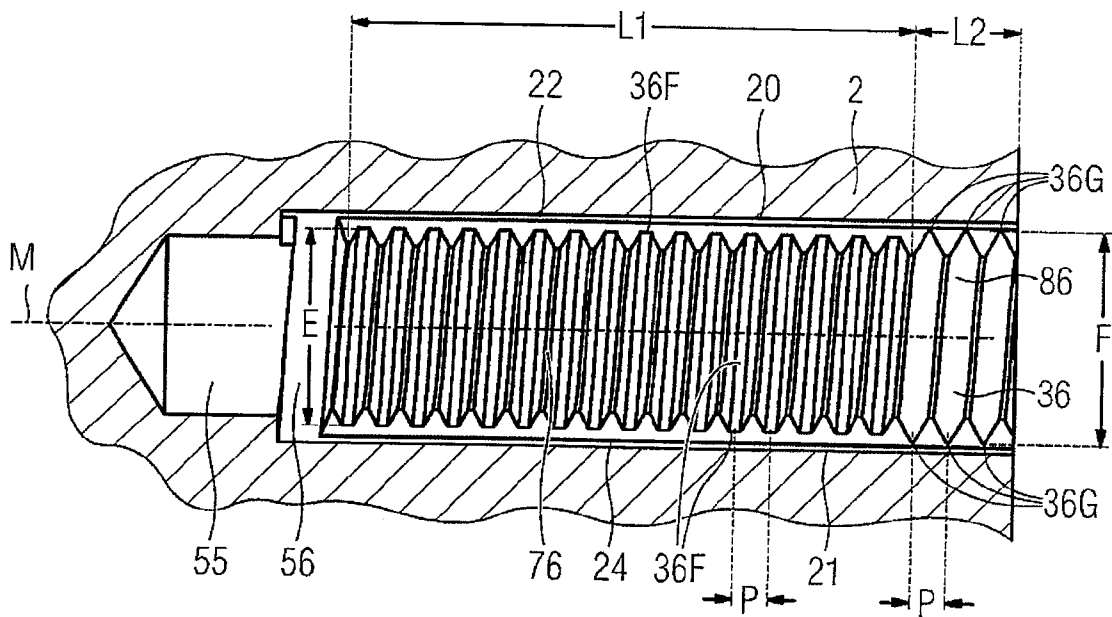


FIG 21



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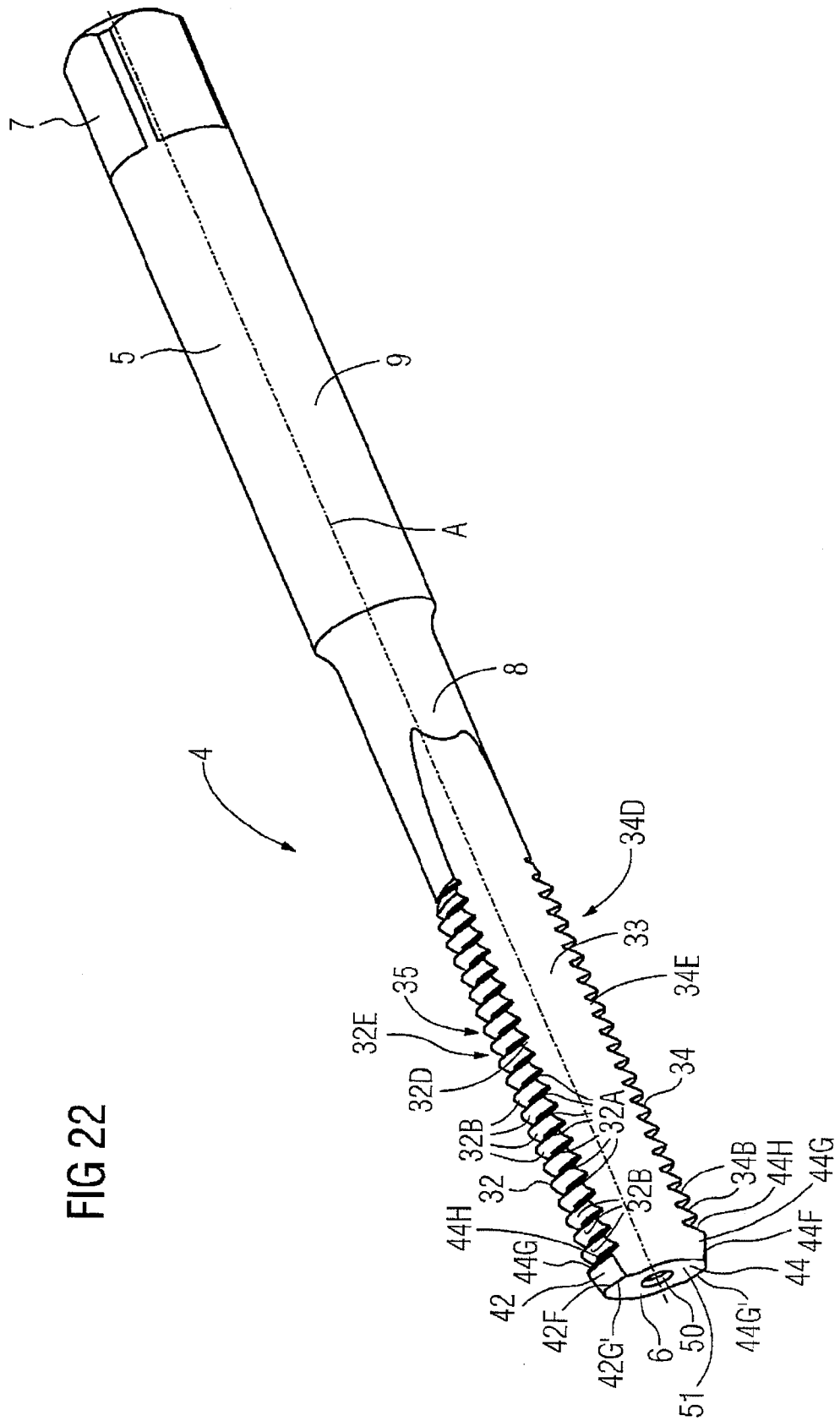
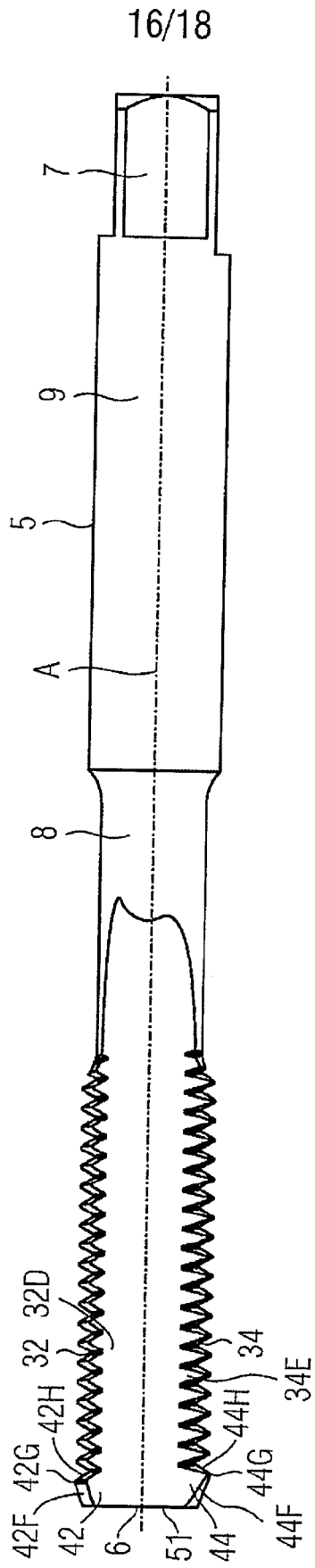


FIG 23



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FIG 24

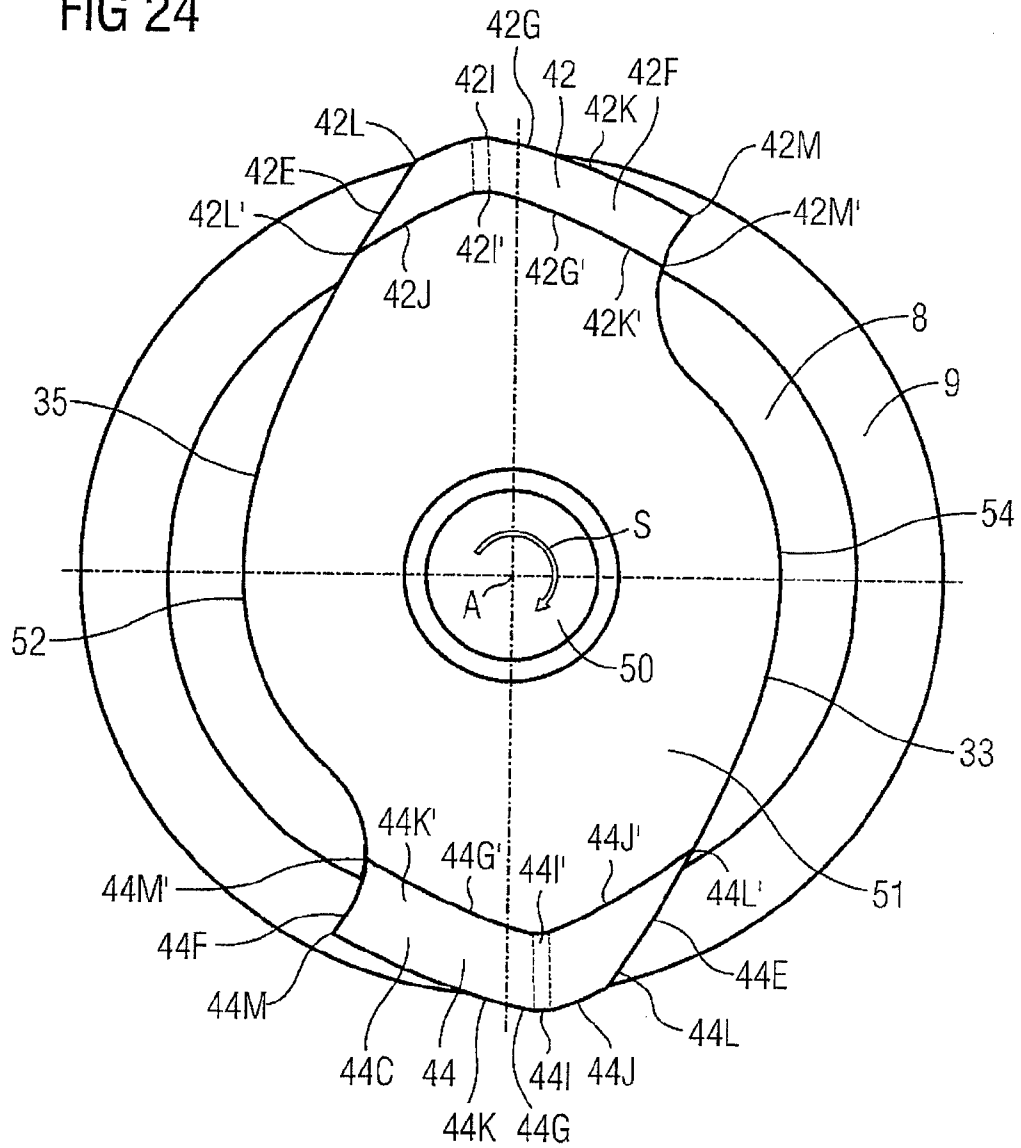


FIG 25

