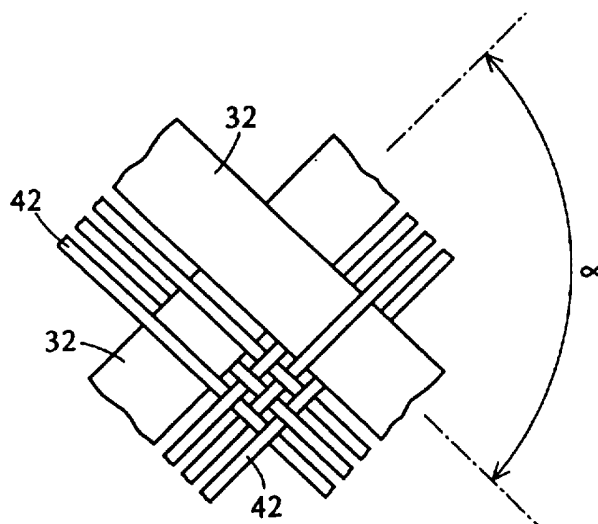


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<b>(21) International Application Number:</b> PCT/IB96/00792 <b>(22) International Filing Date:</b> 12 August 1996 (12.08.96)  <b>(30) Priority Data:</b> 60/005,209 11 October 1995 (11.10.95) US 08/640,062 30 April 1996 (30.04.96) US  <b>(71) Applicant:</b> SCHNEIDER (USA) INC. [US/US]; 5905 Nathan Lane, Plymouth, MN 55442 (US). <b>(72) Inventor:</b> THOMPSON, Paul, J.; 9125-40 1/2 Avenue North, New Hope, MN 55427 (US). <b>(74) Agents:</b> SPIEGEL, Allen, J. et al.; Pfizer Inc., Patent Dept., 235 East 42nd Street, New York, NY 10017 (US).		<b>(81) Designated States:</b> AU, CA, JP, MX, European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).  <b>Published</b> <i>With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>

**(54) Title:** BRAIDED COMPOSITE PROSTHESIS**(57) Abstract**

A prosthesis for transluminal implantation consists of a flexible tubular interbraided structure (18, 92, 100, 114) of metal or polymeric monofilaments (32, 94, 102, 112), and polymeric multifilament yarns (42, 108). The prosthesis can be elastically deformed to reduce its diameter through axial elongation. The monofilaments and multifilament yarns are arranged in axially spaced-apart helices, concentric on a common central axis of the prosthesis. The monofilaments are selectively shaped before their interbraiding with the multifilament yarns, either by an age-hardening or other heat-setting stage, or a cold-working stage that controllably plastically deforms the strands. The shaped structural strands cooperate to impart to the prosthesis its nominal shape and resilience. The textile strands cooperate to provide a sheeting (40, 96, 104) that occupies interstices between adjacent structural strands, to reduce permeability and thereby enhance the utility of the prosthesis as a vascular graft. An alternative embodiment prosthesis includes elastically and plastically deformable structural strands, selectively plastically deformed by cold-working then interbraided to form the prosthesis.

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## BRAIDED COMPOSITE PROSTHESIS

### BACKGROUND OF THE INVENTION

The present invention relates to body implantable devices, and more particularly to prostheses including  
5 stents and grafts intended for long term or permanent intraluminal fixation.

A variety of patient treatment and diagnostic procedures involve the use of devices inserted into the body of a patient and intraluminally implanted. Among  
10 these devices are prostheses as disclosed in U.S. Patent No. 4,655,771 (Wallsten). These devices are flexible, tubular, braided structures formed of helically wound thread elements. A delivery catheter includes gripping members for securing a prosthesis to the catheter. In  
15 deployment, the gripping members and catheter are removed, allowing the prosthesis to assume a substantially cylindrical shape as it radially expands and substantially conforms to a blood vessel wall or other tissue.

20 Metallic thread elements or strands are generally favored for applications requiring flexibility and effective resistance to radial compression after implantation. Metallic strands can be thermally formed by a moderately high temperature age-hardening process  
25 while wound about a mandrel in the desired helical configuration. The strands cooperate to provide the requisite strength, due to their high modulus of elasticity.

The flexibility of the strands also is important,  
30 as it permits a radial compression of the stent (by an axial elongation) that facilitates delivery of the stent through narrow blood vessels or other lumens toward the intended treatment site. Because the self-expanding device generally remains at least slightly radially  
35 compressed after fixation, its restoring force can provide acute fixation. The flexible stent can

accommodate a wider range of lumen diameters, reducing the need to precisely match the stent and lumen as to size. The favorable combination of strength and flexibility is due to the properties of the strands themselves, and the arrangement of strands, i.e. the axial spacing between adjacent helical strands, the braiding angles of the strands, etc. Accordingly, stents characteristically have an open mesh construction as shown in Figures 2a and 2b.

10 U.S. Patent No. 4,681,110 (Wiktor) discloses a flexible tubular liner, insertable into the aorta to treat an aneurisym. The liner is a tight weave of flexible plastic strands, designed to self-expand against the aneurisym to direct blood flow past the aneurisym.

15 In this context, a tight weave is intended to minimize leakage, so that the liner can effectively shunt blood through to eliminate the aneurysmal sack from the blood path.

Those of skill in the art have generally encountered difficulty in providing a device that simultaneously accommodates the competing needs of low permeability, and strength and flexibility for considerable radial compression and expansion.

One known approach to counter this problem is a combination stent/graft, in which a compliant but substantially fixed-radius and tightly-woven graft is sutured or otherwise coupled to a radially expandable stent. The stent upon release is intended to radially expand to the graft diameter. This, however, generally requires a careful matching of the graft diameter with the lumen diameter at the treatment site. Otherwise, either an oversized graft is compressed between the stent and body tissue with undesirable folds or gathering of the graft material, or an undersized graft prevents the stent from expanding sufficiently to anchor the device.

Several prosthesis constructions have been suggested, particularly involving three dimensional

braiding as disclosed in International Patent Publications No. WO91/10766. For example, see International Patent Publication No. WO92/16166, No. WO94/06372, and No. WO94/06373. These publications  
5 discuss composite grafts or other braided structures that combine different types of strands, e.g. multifilament yarns, monofilaments, fusible materials, and collagens. In all of these disclosures, the woven or braided structure is heat set after braiding to impart the  
10 desired nominal shape to the device. Accordingly, all strands and filaments must be compatible with the heat set conditions (primarily the high temperature), limiting the type of materials that can be interbraided into the device.

15 Therefore, it is an object of the present invention to provide a prosthesis including structural strands and other strands interbraided with the structural strands, in which the types of materials for such other strands are not limited by conditions necessary to thermally set  
20 or otherwise selectively shape the structural strands.

Another object is to provide a process for making a prosthesis, in which a certain portion of the strands ultimately incorporated into the prosthesis, e.g. structural strands, can be treated to assume  
25 predetermined nominal shapes without any undesirable impact on the other strands incorporated into the structure.

A further object is to provide, in a prosthesis manufacturing process involving the interbraiding of  
30 multiple strands, a means for selectively cold-working a portion of the strands to predetermine a nominal shape of the interbraided structure.

Yet another object is to provide an interbraided device incorporating the strength, resilience and range  
35 of diameters associated with stents, and the low permeability associated with grafts.

## SUMMARY OF THE INVENTION

To achieve these and other objects, there is provided a process for making a prosthesis, including the following steps:

- 5       a. providing a plurality of structural strands formed of structural material and having an original nominal shape, and providing a plurality of compliant textile strands;
- b. altering the structural strands to impart to  
10 each of the structural strands a selected nominal shape in lieu of the original nominal shape; and
- c. after altering, braiding the strands into an integrated structure of the structural strands and the textile strands.
- 15       Preferably the braiding forms a latticework of the structural strands. Then, the textile strands are formed as a textile sheeting that is supported by the latticework and occupies interstices between adjacent structural strands of the latticework.
- 20       A salient feature of the process is that the structural strands are selectively shaped, i.e. given their predetermined second nominal shapes, prior to the interbraiding step. Consequently, process conditions for selective shaping have virtually no impact on the textile  
25 strands. This is particularly beneficial when the structural strands are metallic, e.g. formed of Elgiloy or another cobalt-based alloy, certain stainless steels, or a recovery metal such as Nitinol nickel-titanium alloy. These metals provide the desired strength and  
30 resiliency, yet when thermally shaped require temperatures far above the melting points typical of the multifilament yarns suitable for the textile strands. In certain cases, significant damage can occur below (although near) the melting point. Certain polymers  
35 suitable for the structural strands likewise are advantageously shaped at temperatures unsuitably high for the textile strands. In either event, thermally setting

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or shaping the structural strands prior to interbraiding prevents this kind of damage to the textile strands.

In accordance with the present invention, structural strands may be selectively shaped by cold working as well. Certain resilient and ductile metals are particularly well suited to cold working. A primary advantage is the ability to incorporate the cold-working step and the braiding step into a continuous operation. In particular, each structural strand on its way to a braiding station can be wrapped about a shaping pulley under sufficient tension to achieve the needed plastic deformation. Continuous shaping and braiding can substantially reduce manufacturing cost.

The structural strands can be formed into a variety of shapes, most preferably helical. The helices can be wound in a single direction so that the interstices are helical. More frequently, the structural strands are wound as two sets of helices running in opposite directions, to form a latticework in which the interstices are rhombic. The oppositely directed helices can be interbraided, or can overlies one another, being interbraided only with the textile strands. The interbraided structure can incorporate further strands, for example of radiopaque material. The structure can incorporate one or more elastomeric strands running axially of the structure and fused to the structure along at least part of its axial length, thus to enhance radial self-expansion.

The process can be augmented with several steps that enhance the utility of the prosthesis, such as coating the structural strands, the textile strands, or both. A heat setting step may be performed after braiding, when the textile strands are formed of a yarn amenable to heat setting. An adhesive can be applied to the ends of the integrated structure after braiding, to reduce or prevent unraveling.

Another aspect of the present invention is a

prosthesis. The prosthesis includes an integrated structure including an interbraiding of a plurality of structural strands and a plurality of compliant textile strands. The structural strands are formed of a  
5 structural material having a tendency to assume a nominal shape when in a relaxed state. The structural strands further have respective selected nominal strand shapes imparted by at least one of: (i) a selective plastic deformation from an original nominal strand shape to the  
10 selected nominal strand shape; and (ii) a selective thermal setting including a heating of the structural strand to a temperature greater than a melting temperature of the textile strands while the structural strand is maintained in the selected nominal strand  
15 shape.

The structural strands have selected orientations within the integrated structure, to impart a predetermined nominal shape to the integrated structure. In a preferred prosthesis, the structural strands  
20 cooperate to form a latticework, and the textile strands cooperate to form a textile sheeting supported by the latticework and occupying interstices between adjacent structural strands of the latticework. Thus, the structural strength and resiliency of a self-expanding  
25 stent and the low permeability of a graft are combined in a single prosthesis.

The structural strands preferably are monofilaments of metal, e.g. a stainless steel, an alloy including cobalt or an alloy including titanium. Alternatively the  
30 monofilaments are polymeric, constructed of materials including PET, polypropylene, PEEK, HDPE, polysulfone, acetyl, PTFE, FEP, polycarbonate urethane, and polyurethane. In either event the preferred textile strands are multifilament polymeric yarns. Suitable  
35 materials for the multifilament yarns include PET, polypropylene, polyurethane, polycarbonate urethane, HDPE (high density polyethylene), polyethylene, silicone,



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PTFE, ePTFE and polyolefin.

Thus in accordance with the present invention, an interbraided structure incorporating structural and textile strands is manufactured according to a process that enables a controlled shaping of the structural strands without adversely affecting the textile strands. The result is an intraluminal device with the favorable qualities of an open weave stent and of a tightly woven graft. The structural strands are shaped either thermally or by plastic deformation, before they are brought together with the textile strands for interbraiding. The interbraiding step involves all strands simultaneously, interweaving a compliant textile sheeting among the structural strands as the structural strands are formed into a latticework that defines the shape of the prosthesis. As a result, the textile sheeting is supported by the latticework and tends to conform to the shape of the latticework. The textile sheeting exhibits low permeability and high compliance, occupying and more preferably filling the voids between adjacent structural strands to prevent leakage of blood or other fluids, yet readily conforming to the shapes of the voids, as these shapes change responsive to radial contractions and expansions of the structure.

#### IN THE DRAWINGS

For a further understanding of the above and other features and advantages, reference is made to the following detailed description and to the drawings, in which:

Figure 1 is a partial side sectional view of a prosthesis constructed in accordance with the present invention, contained within a deployment device;

Figures 2a and 2b illustrate an open weave stent consisting of resilient metal structural strands;

Figures 3 and 4 show the prosthesis of Figure 1 in a radially constrained state, and in a radially expanded state, respectively;

Figure 5 is an enlarged partial view of Figure 3, schematically illustrating an interbraiding of structural and textile strands of the prosthesis;

Figure 6 shows the prosthesis of Figure 1 deployed within a vessel and spanning an aneurysm;

Figures 7 and 8 schematically illustrate a process for manufacturing the prosthesis;

Figures 9 and 10 schematically illustrate an alternative process for manufacturing the prosthesis;

Figures 11a and 11b are photographs of a prosthesis constructed according to a first exemplary process according to the present invention;

Figure 12 is a photograph of a prosthesis constructed according to a second exemplary process;

Figure 13 is a photograph of a prosthesis constructed according to a third exemplary process;

Figure 14 is a photograph of a prosthesis constructed according to a fourth exemplary process;

Figure 15 is a diagrammatic view of an alternative embodiment prosthesis;

Figure 16 is an illustration of another alternative embodiment prosthesis;

Figure 17 illustrates a coated multifilament yarn of a further alternative embodiment prosthesis;

Figure 18 illustrates a coated structural strand of another alternative embodiment prosthesis; and

Figure 19 illustrates a further alternative embodiment coated prosthesis.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Turning now to the drawings, there is shown in Figure 1 a deployment device 16 for delivering a prosthesis 18 to an intended fixation location or treatment site within a body lumen, and then controllably releasing the prosthesis for radial self-expansion and fixation within the lumen.

The device includes an elongate and flexible outer catheter 20 constructed of a biocompatible polymer, e.g.

polyurethane. A central lumen 22 runs the length of catheter 20. A distal portion 24 of the outer catheter surrounds prosthesis 18. An inner catheter 26 is contained within lumen 22 and runs along substantially the entire length of outer catheter 20. At the distal end of inner catheter 26 is a tapered distal tip 28. Prosthesis 18 surrounds inner catheter 26, and thus is confined between the inner and outer catheters. A lumen 30 in the inner catheter can accommodate a flexible guidewire.

Prosthesis 18, shown completely rather than in section, is a tubular braided structure including helically wound monofilament structural strands 32 formed of a resilient material. In Figure 1, prosthesis 18 is elastically compressed into a reduced radius axially elongated delivery state. Outer catheter 20 confines the prosthesis, maintaining it in the delivery state against an elastic restoring force.

An annular detent 34, mounted to inner catheter 26, occupies a space between the inner and outer catheters to limit proximal travel of prosthesis 18 relative to the inner catheter. Thus, as outer catheter 20 is moved proximally relative to inner catheter 26, the detent prevents the prosthesis from moving with the outer catheter.

Catheters 20 and 26, while maintaining prosthesis 18 in the delivery configuration, are moved transluminally, e.g. through vasculature, to deliver the prosthesis to the intended treatment site. Once the prosthesis is positioned as intended, inner catheter 26 is held stationary, while outer catheter 20 is withdrawn proximally. Detent 34 prevents prosthesis 18 from moving proximally with the outer catheter, thus to maintain the prosthesis properly aligned as it progressively radially self-expands toward a relaxed state and into intimate contact with tissue at the treatment site. Because the prosthesis does not expand completely to the relaxed

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state, it exerts a residual force on the tissue that tends to maintain fixation of the prosthesis. At this point the prosthesis has a diameter much larger than the diameter of distal tip 28, so that the inner catheter and tip, along with the outer catheter, are easily proximally withdrawn.

Prosthesis 18 resembles a radially self-expanding stent, in that it is well suited for radially compressed delivery and self-expansion. Accordingly, familiarity with radially self-expanding stents is useful in considering prosthesis 18.

A radially self-expanding stent is pictured in Figures 2a and 2b. The stent consists of two oppositely directed and concentric sets of helically wound thread elements or wires. The wires can be formed of metal or a polymeric material and have good elastic recovery. Each wire is selectively shaped so that its nominal shape, i.e. its shape when in a relaxed state subject to no external stresses, is helical. The wires cooperate to give the stent its nominal tubular shape.

Adjacent helices in two opposite winding directions are spaced apart axially, resulting in rhombotic voids or interstices with dimensions substantially larger than the wire diameters. The open-mesh construction, in combination with the resiliency and strength of the selectively shaped wires, enables and facilitates (a) elastic compression of the stent to a much smaller radius suitable for intraluminal delivery; (b) virtually instantaneous radial expansion of the stent when released at a treatment site; and (c) a sufficient residual force to ensure acute fixation without hooks or barbs, although such fixation options may enhance fixation.

With reference to Figures 3 and 4 it can be appreciated that structural strands 32 form a latticework of prosthesis 18. Like the wires of the stent, strands 32 are arranged in two oppositely directed and concentric sets of helices, spaced apart axially from one another to

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define rhombotic interstices. Structural strands 32 further are similar to the wires in that they exhibit the requisite strength and elasticity, are biocompatible, resistant to fatigue and corrosion, and in vascular applications are hemocompatible as well. Materials meeting these needs include certain stainless "spring" steels, cobalt-based alloys, and alloys containing titanium. Several preferred cobalt-based alloys are sold under the brand names "Elgiloy", "Phynox" and "MP35N".

Particularly preferred CoCrMo alloys are described in U.S. Patent Application Serial No. 08/640,253 entitled "Cobalt-Chromium-Molybdenum Alloy Stent and Stent Graft" (J. Stinson), assigned to the assignee of this application and filed concurrently herewith. These alloys contain less than about 5 weight percent nickel, preferably less than about 2 weight percent nickel and more preferably no more than about 1 weight percent nickel. Chromium is preferably present in an amount between about 26.0 and 30.0 weight percent, and molybdenum preferably in an amount between about 5.0 and 7.0 weight percent. The alloys further can include nitrogen in an amount up to about 0.25 weight percent, and carbon in an amount up to about 0.35 weight percent. Other elements, preferably in amounts no greater than about 1.0 weight percent, include iron, silicon, manganese, copper, phosphorous, sulfur and tungsten. The balance of the alloy in each case can be cobalt, preferably in an amount of at least 60.0 weight percent. Specific examples are described in this application, which is incorporated by reference herein.

A preferred alloy of titanium is a recovery metal alloy of nickel and titanium, sold under the brand name "Nitinol". Other titanium alloys are disclosed in U.S. Patent Application Serial No. 08/598,751 entitled "Titanium Alloy Self-Expanding Stent", filed February 8, 1996 and assigned to the assignee of this application. Other suitable titanium alloys include titanium-

zirconium-niobium alloys and a titanium-aluminum-vanadium alloy known as Ti-6Al-4V.

Suitable polymeric monofilaments include PET, polypropylene, PEEK, HDPE, polysulfone, acetyl, PTFE, FEP, polycarbonate urethane and polyurethane. Suitable polyurethanes and polycarbonate urethanes include those sold under the following brand names: Chronoflex AR, Chronoflex Al, Corethane, and Biomer. These monofilaments preferably have diameters in the range of about 0.002-0.015 inches (0.051-0.38 mm).

As seen in Figure 4, structural strands 32 intersect each other to define a braid angle  $\alpha$ , which is bisected by a longitudinal axis 36 of the prosthesis. The braid angle, when prosthesis 18 is in the relaxed state, is in the range of about 60 to 150 degrees, and more preferably 80 to 140 degrees.

As seen in Figure 3, radial compression of the prosthesis substantially reduces the braid angle. The braid angle largely determines the relationship between radial compression and axial elongation of the prosthesis. More particularly, smaller braid angles yield less axial shortening for a given amount of radial expansion. On the other hand, for a given strand size and strength, a larger braid angle imparts greater resistance to radial compression and more positive acute fixation. Accordingly a smaller braid angle generally requires a structural strand that is resilient, but stronger, i.e. with a higher modulus of elasticity.

The interstices 38 between adjacent structural strands in prosthesis 18 are occupied by a textile sheeting or fabric 40. As seen in Figure 5, sheeting 40 is formed of multiple textile strands 42 interbraided with one another and further interbraided with structural strands 32. Strands 32 and 42 are illustrated in a one over one braiding pattern. However, it is to be appreciated that a variety of braiding patterns are known to those skilled in the art, and the pattern most

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suitable in a given instance depends on desired structural characteristics and materials involved. Textile strands 42 also are provided in sets of oppositely directed helices, and intersect one another at the same braid angle  $\alpha$  defined by the structural strands. Textile strands 42 preferably are multifilament yarns, although they can be monofilaments. In either event the textile strands are much finer than the structural strands, ranging from about 10 to 400 denier. Individual filaments of the multifilament yarns can range from about 0.25 to about 10 denier. The multifilament yarns generally have a high degree of compliance, which may or may not include elasticity. Suitable materials include PET, polypropylene, polyurethane, polycarbonate urethane, HDPE, polyethene, silicone, PTFE, ePTFE and polyolefin. One suitable high molecular weight polyethylene is sold under the brand name "Spectra".

Due to the fineness of textile strands 42 and a close or tight weave, textile sheeting 40 can be microporous, yet essentially impervious to body fluids. Also, the textile sheeting is highly compliant, conforming to changes in the shape of latticework 35 as prosthesis 18 either radially self-expands or is radially compressed. The shape of latticework 35 determines the shape of the prosthesis.

Thus, prosthesis 18 combines the favorable attributes of self-expanding stents and grafts. Latticework 35 provides radial compressibility, self-expansion over a wide range of radii and residual force for acute fixation, while textile sheeting 40 reduces permeability to the extent that the prosthesis is essentially impervious to blood and other body fluids. For these reasons, prosthesis 18 is particularly well suited to treating an aneurysm. Figure 6 illustrates fixation of prosthesis 18 within a blood vessel having a vessel wall 44. Along the vessel wall is in an aneurysm 46. Opposite end regions 48 and 50 of the prosthesis

have radially expanded into intimate contact with vessel wall 44 on opposite sides of the aneurysm. A medial region 52 of the prosthesis spans the aneurysm. End regions 48 and 50 effectively fix the prosthesis, due to the resilience and strength of the structural strand latticework. At the same time the prosthesis, because of textile sheeting 40, shunts blood past the aneurysm preventing any substantial leakage into the aneurysmal sack.

10 A particularly favorable structure for prosthesis 18 is an interbraiding of metallic structural strands with Dacron (polyester) multifilament yarns as the textile strands. The metal structural strands exhibit high strength in terms of elastic moduli. For example, 15 stainless steels can have elastic moduli of about  $28-30 \times 10^6$  psi. Titanium and alloys of titanium tend to have elastic moduli in the range of  $15.4-16.6 \times 10^6$  psi. In contrast polyethylene, for example, has an elastic modulus in the range of about  $0.02-0.055 \times 10^6$  psi, and 20 other polymeric materials have elastic moduli in this order of magnitude. Accordingly, for a given strand diameter, helical diameter and helical pitch, a latticework of metallic strands is considerably more resistant to radial compression, and provides a greater residual force for acute fixation. The Dacron polyester 25 multifilament yarn has a high elastic recovery and elongation (up to 36% for the polyester fiber) and a low elastic modulus, which ensure that textile sheeting 40 conforms to the latticework.

30 This favorable composite structure cannot be manufactured by forming a braided structure on a mandrel, then heating the mandrel to thermally set the strands in their helical shapes. Thermally setting metallic structural strands entails heating the strands to 35 temperatures up to about  $1000^\circ$  C. while the strands are maintained in the intended helical shape. Such temperatures are well above the melting points of



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polyesters and other materials most suitable for the multifilament yarn textile strands. Selectively shaping the structural strands is important in enhancing the predictability and control over prosthesis contractions and expansions, and also reduces any tendency of the prosthesis to unravel.

To attain favorable characteristics of stents and grafts, prosthesis 18 can be fabricated according to several steps as illustrated in Figures 7 and 8. Figure 7 shows two structural strands (metal monofilaments) 32a and 32b, one from each set of oppositely directed structural strands, wound about a mandrel 54 and supported by respective bobbins 56 and 58. While just strands 32a and 32b are illustrated as a matter of convenience, it is to be appreciated that all of the structural strands are wound about the mandrel and maintained together for shaping. Only structural strands are present, however, as shaping occurs before interbraiding with the textile strands.

Age-hardening is accomplished within a furnace 60 in a vacuum or a protective atmosphere. Temperatures are within the range of about 350-1000° C., with the specific temperature depending on the structural material. The filaments overlies one another to form multiple intersections, one of which is indicated at 62. Bobbins, including 56 and 58, are set to tension their respective strands during age-hardening. The appropriate duration for age-hardening varies with materials and dimensions, but can range from as brief as 30 seconds, to about 5 hours.

After age-hardening, the structural strands are allowed to cool, whereupon each structural strand retains the helical shape as its nominal shape. In the context of elastic materials, "nominal shape" refers to the shape in a relaxed state, i.e. when under no external stress. The age-hardened metallic monofilaments are highly resilient, i.e. deformable under external stress but

elastically returning to the nominal shape when free of the external stress. The strands when constructed of a recovery metal are plastically deformable when maintained below an activation temperature, which for Nitinol can be  
5 below body temperature (about 37° C.). When heated to the activation temperature or above, the structural strand returns to the selected nominal shape. In this context the "nominal shape" is the shape to which the strand returns when at or above the activation  
10 temperature.

When structural strands 32 are thermoplastic rather than metallic monofilaments, multiple strands are thermally set in similar fashion. More particularly, with the thermoplastic monofilaments wound in opposite  
15 sets about mandrel 54, the strands are heated to a heat-forming temperature in the range of about 100 to 400° C., more preferably 150 to 250° C., either within a furnace as previously described or by heating the mandrel. The strands are maintained at or above the heat-forming  
20 temperature for a duration generally shorter than that of thermally setting metal strands, i.e. from about 30 seconds to about 2 hours, or more preferably 5 to 15 minutes. Again, only the structural strands are shaped, and before they are interbraided with the textile  
25 strands. This sequence can be advantageous even when the structural strands and textile strands are formed of the same thermoplastic material, as it enables fabrication of a prosthesis in which only the structural strands are thermally set.

30 It is to be appreciated that the thermal setting process alters the structural strands, in the sense of changing their shapes from an original or first nominal shape to a second, selected nominal shape. Typically the original nominal shape is linear, with the selected  
35 nominal shape determined by the diameter of the mandrel and the pitch at which the structural strands are wound about the mandrel.

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Interbraiding of the structural and textile strands occurs after selective shaping. Figure 8 schematically illustrates a braiding apparatus 64 including an annular carrier assembly 66 including a circular array of  
5 bobbins, two of which are indicated at 68 and 70. The apparatus further includes a mandrel 72, centered within the annular assembly and movable longitudinally relative to the assembly as indicated by the arrow.

While those skilled in the art are acquainted with  
10 the use of braiding machinery, braiding apparatus 64 is used as follows:

First, carrier assembly 66 is loaded by winding different strands onto different bobbins. The type of strand wound on each bobbin depends on the desired  
15 braiding pattern and ratio of structural strands to textile strands. All strands are drawn from their respective bobbins to mandrel 72, and braiding proceeds by moving mandrel 72 longitudinally, while at the same time the bobbins are moved relative to one another as  
20 dictated by the desired pattern of braiding, e.g. a two-dimensional maypole braiding. The result is a simultaneous interbraiding of the structural and textile strands onto the mandrel, as indicated at 74. The mandrel determines the diameter of the braided structure.  
25 Mandrel longitudinal speed largely determines the braid angle. Prosthesis lengths are determined by the duration of braiding, or by cutting the braided structure to predetermined lengths upon its removal from the mandrel.

The braiding process includes controlling the  
30 structural strands as to orientation during braiding, to ensure that the individual helices cooperate to provide the desired nominal tubular configuration for the resulting latticework. Similar control of the textile strands is not necessary, due to their more compliant  
35 nature. Properly oriented structural strands diminish any unraveling tendency and result in more predictable contraction and expansion of the prosthesis. Further,

from Figure 5 it can be appreciated that the textile strands, in filling the interstices between structural strands, tend to maintain the structural strands in the desired configuration of intersecting helices.

5        Figure 9 schematically illustrates an alternative braiding apparatus 76 in which the structural strands are selectively shaped by cold-working. In particular, an annular carrier assembly 78 is mounted concentrically on a longitudinally movable mandrel 80. As before, the  
10       carrier assembly supports multiple bobbins in a circular array, with two of the bobbins being shown at 82 and 84. A structural strand 32 has been wound on the bobbin 82, while bobbin 84 carries a textile strand 42. The structural strand is not thermally shaped before  
15       braiding, and thus at first has a linear nominal shape.

      Structural strand 32 is plastically deformed by cold working as it travels from bobbin 82 to the mandrel. A small diameter shaping pulley 86 and a larger diameter idler pulley 88 are disposed along the path traversed by  
20       strand 32. Shaping pulley 86 exerts a bending stress on the moving structural strand trained about this pulley, particularly on radially outward portions of the strand. Although both pulleys are shown in side elevation, it is to be understood that shaping pulley 86 actually is  
25       orthogonal to idler pulley 88 to impart the selected nominal shape. Bobbin 82 is supported on a carrier that includes a clutch (not shown) adjustable to control the tension applied to the strand, thereby to adjust the amount of bending stress.

30       The tension is controlled so that the bending stress, at least along the radially outward portions of the strand along pulley 86, exceeds the yield stress of the material. The appropriate level of tension is within the range of about 200-1000 gms, depending on such  
35       factors as the material, the monofilament diameter, and the bending radius about pulley 86. The result is a cold-working plastic deformation, represented as a

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hatched segment 90 in Figure 10. It is to be appreciated that segment 90 is greatly exaggerated and intended for illustration only. The actual plastic flow is less pronounced and continuous, and changes the nominal shape of the structural strand from linear to helical. Further in this connection, it is noted that pulley 86 would impart a curved nominal shape to the structural strand in any event, and that the helical nominal shape with the desired pitch is obtained through proper orientation of the pulley with respect to the carrier assembly while the desired tension in the strand is maintained.

The CoCrMo alloys described in the aforementioned U.S. Patent Application Serial No. 08/640,253 entitled "Cobalt-Chromium-Molybdenum Alloy Stent and Stent Graft" are particularly well suited for this approach. Although shaping pulleys and tensioning clutches are required only in connection with the structural strands as shown, these components add complexity to the braiding apparatus. The advantage of this approach is that the selective shaping and braiding steps can occur closely in time and within a continuous process. In contrast, thermal shaping is followed by cooling the strands and winding the strands onto bobbins, and therefore involves processing in a batch mode.

Figures 11-14 are photographs of four different braiding structures, formed according to the following examples of the braiding process. In Examples 1-3, the metallic monofilaments are thermally shaped prior to braiding, although they can just as well be plastically formed to achieve the same result.

Example 1:

The bobbins of a braider carrier assembly are loaded with seventy-two textile filaments, each being a 100 denier polyester yarn composed of seventy filaments. At every third carrier around the braider, a structural strand is wound for co-braiding with the multifilament yarn, to provide twelve structural strands in each of two

opposite winding directions. Each structural strand is an Elgiloy wire having a diameter of 0.0043 inches (.11 mm). The strands are braided in a two over two braiding pattern onto an 8 mm diameter round mandrel, with the  
5 braider operated to determine a braid angle of 110°. The braid is formed to an adequate length, then removed from the mandrel.

The resulting interbraided structure, shown in Figures 11a and 11b, is a tubular composite of the  
10 polyester yarn and metal monofilaments. The wire latticework is formed as two sets of oppositely directed helices, with the wires in a two over two braided pattern.

Example 2:

15 Again, carrier bobbins are loaded with seventy-two polyester yarns of 100 denier and seventy filaments. A 0.0043 inch diameter Elgiloy wire, provided at every fourth carrier, is co-braided with the multifilament yarn to provide nine wires in each of two opposite winding  
20 directions. The strands are braided in a two over two braiding pattern on an 8 mm diameter round mandrel. The result, pictured in Figure 12, is a tubular interbraided structure of polyester yarn and metal monofilaments. The wire substructure consists of two concentric sets of  
25 oppositely directed helices, not interbraided but overlying one another.

Example 3:

The carrier bobbins are loaded with seventy-two 100 denier polyester yarns formed of seventy filaments. A  
30 0.0043 inch diameter Elgiloy wire is loaded at every other carrier around the braider in only one of two opposite winding directions, for a total of eighteen wires co-braided with the multifilament yarn. The strands are braided on an 8 mm diameter round mandrel in  
35 a two over two braiding pattern, with the braider set to form a braid angle of 110°. The result (Figure 13) is a hollow tubular interbraided structure of polyester yarn

and metal monofilaments. The wire substructure consists of a single layer of eighteen axially spaced helices in one winding direction.

Example 4:

5 Carrier bobbins are loaded with one hundred forty-four polyester yarns of 100 denier and seventy filaments. An Elgiloy wire of 0.0055 inches (0.13 mm) is loaded at every sixth carrier around the braider, to provide twelve  
10 wires in each of two opposite winding directions for co-braiding with the multifilament yarn. Prior to loading, the Elgiloy wire is plastically formed into the desired shape as described in connection with Figures 9 and 10. The strands are braided onto a 16 mm diameter round  
15 mandrel, with the braider set to provide a braid angle of 110°. The result, shown in Figure 14, is a tubular interbraided structure of polyester yarn and metal monofilaments, including a wire substructure consisting of twenty-four wires braided in a one over one braiding pattern.

20 Example 5:

The carrier bobbins are loaded with ninety-six polyester yarns of 100 denier and seventy filaments. A 0.0055 inch diameter Elgiloy wire is loaded at every third carrier around the braider, to provide sixteen  
25 wires in each of two opposite winding directions for co-braiding with the multifilament yarn. The strands are braided in a two over two braiding pattern on a 12 mm diameter round mandrel, with the braider set to provide a braid angle of 110°. The result is a tubular  
30 interbraided structure of the polyester yarn and metal monofilaments, including a wire substructure of thirty-two wires braided in a two over two pattern.

In all of these examples, the resulting prosthesis has water permeability comparable to that of a vascular  
35 graft, and can be constrained to a reduced diameter and allowed to expand like a radially self-expanding stent.

The prosthesis fabricating processes can be enhanced

to impart a variety of desired characteristics to the resulting prosthesis. For example, Figure 15 shows a prosthesis 92 formed of helical structural strands 94 interbraided with multifilament yarns forming a textile sheeting 96. A further strand 98 is interbraided with the textile strands. Strand 98 is formed of a radiopaque material, e.g. tantalum. Strand 98 improves the fluoroscopic imaging of prosthesis 92 at or near a treatment site, to facilitate recognition of proper placement or a need to move the prosthesis. Other approaches to enhancing radiopacity include use of composite structural strands (e.g. wires with radiopaque cores), plated monofilaments, radiopaque inks and marker bands.

Figure 16 illustrates a prosthesis 100 fabricated according to the following example:

Example 6:

A braiding device is provided with eighteen triaxial guide tubes arranged about the carrier assembly. The bobbins are loaded with seventy-two polyester yarns of 100 denier and seventy filaments. Every third carrier around the braider is loaded with a 0.0043 diameter Elgiloy wire, to provide twelve wires in each of two opposite winding directions for co-braiding with the multifilament yarns. Eighteen aliphatic polyurethane monofilaments of 0.004 inches (0.1 mm) in diameter are provided, one such monofilament fed into each of the triaxial guide tubes for incorporation into the braided structure as axial runners. The strands are braided about an 8 mm diameter round mandrel in a two over two braiding pattern, with the braiding device set to provide a braid angle of 110°. Following braiding, the prosthesis is removed and heated in an oven at 150° C. for approximately ten minutes to melt the polyurethane runners, thereby fusing them to the remaining structure.

The result is tubular interbraided prosthesis 100, incorporating metal monofilaments 102, a sheeting 104 of



the polyester yarns, and axial polyurethane runners 106. The wire substructure is braided in a two over two braiding pattern. The prosthesis has a water permeability comparable to that of a vascular graft, and  
5 can be constrained radially and allowed to self-expand like a self-expanding stent. Radial recovery is enhanced and the tendency to unravel or fray when cut is reduced, due to the axial runners.

Another approach to reduce unraveling of the  
10 prosthesis is to apply a silicone adhesive to the opposite ends, or to submerge the prosthesis ends into a solution of a polyurethane, a silicone, or a polycarbonate urethane and a solvent having a low percentage of solids. Residual polyurethane, silicone or  
15 polycarbonate urethane remains after drying and tends to prevent unraveling.

Figure 17 illustrates a multifilament yarn 108 with a coating 110 of TFE, or alternatively a copolymer of TFE and silicone. Coating 110 is applied by plasma  
20 polymerization prior to braiding. Coating 110 enhances surface properties of the yarn, for example by reducing friction. A prosthesis incorporating a sheeting composed of the coated yarns 108 can be deployed with less force. Also, inflammatory responses to the implanted stent may  
25 be reduced. An alternative approach, namely plasma polymerization of the stent after braiding, achieves substantially the same result.

According to another process enhancement, structural strands 112 in Figure 18, particularly metal  
30 monofilaments, are coated with PTFE, ePTFE, polypropylene, polyethylene, PET, or polyurethane. Coating may occur after selective shaping and before braiding, by over-extrusion, tape wrapping, serving or by an additional braiding step. This reduces exposure of  
35 the blood flow to metal.

The process also can be augmented with a surface coating step after braiding, to provide a prosthesis 114

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with a surface coating 116 as illustrated in Figure 19. A portion of the coating is removed to illustrate a covered portion of the prosthesis. At least one end of prosthesis 114 can be left uncovered as indicated at  
5 118, to enhance acute fixation at the exposed end. Alternatively, the prosthesis can be coated over its entire length. A surface coating of heparin or coumadin reduces thrombogenicity. A surface coating of steroids, e.g. dexamethasone, reduces the restenosis rate.  
10 Finally, coatings of albumin, collagen or gelatin can be incorporated to provide an acute reduction in permeability of the textile sheeting.

Further modifications to enhance utility for specific applications, include using a tapered mandrel for heat  
15 setting the structural strands, to form a tapered prosthesis. To reduce migration, prosthesis can be provided with flared ends, or may be braided with end portions that do not incorporate the multifilament yarns. Collagen, PGA and other biological or bioabsorbable  
20 materials can be substituted for portions of the monofilament or multifilament strands. Metallocene catalyzed polymers, e.g. polyolefins or polypropylene, and fluorination if desired, may also be incorporated.

Yet another modified approach utilizes three-  
25 dimensional braiding, as described in U.S. Application Serial No. 08/640,091 entitled "Three-Dimensional Braided Covered Stent" (P. Thompson), assigned to the assignee of this application and filed concurrently herewith.

Thus, in accordance with the present invention,  
30 a prosthesis incorporates structural strands interbraided with more tightly woven textile strands that reduce permeability. The structural strands are selectively shaped before their interbraiding with the textile strands, either by a thermal set or by selective plastic  
35 deformation, and in either event are shaped without adversely affecting the textile strands. Plastic deformation of structural strands by cold-working is

advantageous in permitting a continuous process of cold-working followed by interbraiding. The result is an interbraided prosthesis incorporating the strength, resilience and range of radii associated with self-expanding stents, and the impermeability associated with vascular grafts, in which a selective shaping of the structural strands does not limit the range of materials useable as additional strands in the interbraided structure to reduce permeability, alter porosity, reduce friction or enhance fluoroscopic imaging.

The scope of this disclosure is intended to comprehend the subject matter of the patent applications and publications identified herein. Accordingly, these applications and publications are incorporated by reference.

What is claimed is:

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## CLAIMS

1. A process for making a prosthesis, including:  
providing a plurality of structural strands  
(32,94,102,112) formed of structural material and having  
5 an original nominal shape, and providing a plurality of  
compliant textile strands (42,108);  
altering the structural strands to impart to  
each of the structural strands a selected nominal shape  
in lieu of the original nominal shape; and  
10 after said altering, braiding the strands into  
an integrated structure (18,92,100,114) of the structural  
strands and the textile strands.
2. The process of claim 1 wherein:  
said braiding includes forming a latticework  
15 (35) of the structural strands and forming a textile  
sheeting (40,96,104) of the textile strands supported by  
the latticework and occupying interstices between  
adjacent structural strands of the latticework.
3. The process of claim 2 further including:  
20 after said braiding, plastically deforming the  
latticework to reduce a diameter of the integrated  
structure while maintaining the structural strands below  
an activation temperature of the structural material,  
wherein said structural material is a recovery metal.
- 25 4. The process of claim 1 wherein:  
said structural material is thermally formable,  
and said altering includes winding the structural strands  
around a selectively sized and shaped mandrel (54), then  
heating the strands while so wound to a heat forming  
30 temperature sufficient to thermally impart the selected  
nominal shape.
5. The process of claim 4 wherein:  
said structural strands are heated by heating  
the mandrel, and the heat forming temperature exceeds a  
35 melting temperature of the textile strands.
6. The process of claim 4 wherein:  
the structural material is a metal, and said

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heating includes maintaining the structural strands at a temperature in the range of 350° C. to 1000° C., followed by allowing the structural strands to cool before said braiding.

5           7. The process of claim 4 wherein:

          said structural material is a thermoplastic, and said heating of the structural strands includes maintaining them at least at the heat forming temperature for at least 30 seconds, to impart to each of the  
10 structural strands its selected nominal shape.

          8. The process of claim 7 wherein:

          said heating includes maintaining the structural strands at least at the heat forming temperature for 5-15 minutes, and the heat forming  
15 temperature is in the range of 100-400° C.

          9. The process of claim 8 wherein:

          said heat forming temperature is in the range of 150-250° C.

          10. The process of claim 1 wherein:

20           said braiding includes selectively orienting the structural strands, to impart a predetermined configuration to the integrated structure based on the selected nominal shapes of the structural strands.

          11. The process of claim 1 wherein:

25           the structural material is a metal, and said altering includes selectively plastically deforming the structural strands.

          12. The process of claim 11 wherein:

          said plastic deformation includes bending each  
30 of the strands about a form having a selected radius while maintaining the strands at a selected tension.

          13. The process of claim 12 wherein:

          each of said forms is a rotatable pulley (86), and each of the structural strands is maintained at said  
35 tension and wrapped about its associated pulley.

          14. The process of claim 1 wherein:

          the structural material is a metal, and said

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altering includes selectively applying a force to each of the structural strands, said force exceeding a yield stress of the structural material.

15. The process of claim 1 further including:

5           after said altering and before said braiding, winding each of the structural filaments onto a bobbin (68,82), wherein said braiding includes supplying the strands from their respective bobbins to a braiding station.

10          16. The process of claim 1 wherein:

          said altering includes forming each of the structural strands into a helix.

17. The process of claim 16 wherein:

15           said braiding includes providing the structural strands as first and second sets of helices running in opposite directions, thereby braiding the structural strands into a latticework in which the interstices are rhombic.

18. The process of claim 17 wherein:

20           said braiding includes interbraiding the first and second sets of oppositely directed helices.

19. The process of claim 17 wherein:

25           said braiding includes winding the first and second sets of oppositely directed helices with one of the sets overlying the other set.

20. The process of claim 17 wherein:

30           said oppositely directed helices are braided at a predetermined braid angle, and the braiding further includes braiding the textile strands in two oppositely directed textile strand sets and substantially at said braid angle.

21. The process of claim 16 wherein:

          said braiding includes winding the helices in a single direction, whereby the interstices are helical.

35          22. The process of claim 1 wherein:

          said braiding includes interbraiding at least one strand (98) comprising a radiopaque material.

23. The process of claim 1 wherein:

said composite integrated structure is tubular,  
and said braiding further includes incorporating at least  
one elastic strand (106) running axially of the  
5 integrated structure, and fusing the elastic strand to  
the integrated structure.

24. The process of claim 1 further including:

forming a coating over the strands by plasma  
polymerization.

10 25. The process of claim 1 further including:

after said altering and prior to said braiding,  
coating the structural strands.

26. The process of claim 2 further including:

after said braiding, selectively heating the  
15 composite structure to heat set the textile sheeting,  
wherein said textile strands are composed of a  
multifilament yarn amenable to heat shrinking.

27. The process of claim 1 further including:

after braiding, applying an adhesive at least  
20 to the ends of the composite structure to reduce  
unraveling.

28. The process of claim 1 wherein:

said braiding the strands consists essentially  
of interbraiding the structural strands and the textile  
25 strands into a single layer, and the integrated structure  
is formed of said single layer.

29. A prosthesis, including:

an integrated structure (18,92,100,114)  
including an interbraiding of a plurality of structural  
30 strands (32,94,102,112) and a plurality of compliant  
textile strands (42,108);

wherein said structural strands are formed of a  
structural material having a tendency to assume a nominal  
shape when in a relaxed state, and have respective  
35 selected nominal strand shapes imparted by at least one  
of: (i) a selective plastic deformation from an original  
nominal strand shape to the selected nominal strand

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shape; and (ii) a selective thermal setting including a heating of the structural strand to a temperature greater than a melting temperature of the textile strands while the structural strand is maintained in the selected  
5 nominal strand shape.

30. The prosthesis of claim 29 wherein:  
the structural strands have selected  
orientations within the integrated structure to impart a  
predetermined nominal configuration to the integrated  
10 structure; and

the structural strands cooperate to form a  
lattice work (35), and the textile strands cooperate to  
form a textile sheeting (40,96,104) supported by the  
lattice work and occupying interstices between adjacent  
15 structural strands of the lattice work.

31. The prosthesis of claim 29 wherein:

said structural strands are monofilaments.

32. The prosthesis of claim 31 wherein:

said monofilaments are metal, and formed of at  
20 least one of the following materials: stainless steel, an  
alloy including cobalt, and an alloy including titanium.

33. The prosthesis of claim 31 wherein:

said monofilaments are polymeric, and  
constructed of at least one of the following materials:  
25 PET, polypropylene, PEEK, HDPE, polysulfone, acetyl,  
PTFE, FEP, polycarbonate urethane, and polyurethane.

34. The prosthesis of claim 31 wherein:

said monofilaments have diameters in the range  
of about 0.002-0.015 inches.

30 35. The prosthesis of claim 29 wherein:

said textile strands are polymeric.

36. The prosthesis of claim 35 wherein:

said textile strands are multifilament yarns in  
the range of about 10-400 denier.

35 37. The prosthesis of claim 36 wherein:

said multifilament yarns are composed of  
filaments in the range of about 0.25-10 denier.



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38. The prosthesis of claim 36 wherein:

said multifilament yarn is formed of at least one of the following: PET, polypropylene, polyurethane, polycarbonate urethane, HDPE, polyethylene, silicone,  
5 PTFE, ePTFE, and polyolefin.

39. The prosthesis of claim 29 wherein:

said predetermined nominal shapes of the structural strands are helical.

40. The prosthesis of claim 39 wherein:

10 said structural strands cooperate to form a latticework (35) including first and second sets of helices running in respective first and second opposite directions, whereby the interstices of the latticework are rhombic.

15 41. The prosthesis of claim 40 wherein:

the first and second sets of helices are interbraided.

42. The prosthesis of claim 40 wherein:

20 the first set of helices overlies the second set of helices.

43. The prosthesis of claim 40 wherein:

the first and second sets of helices define a braid angle in the range of about 60-150 degrees.

44. The prosthesis of claim 40 further including:

25 at least one elastomeric strand (106) running axially of the integrated structure and fused to the integrated structure along at least part of its axial length.

45. The prosthesis of claim 29 wherein:

30 at least one of said strands incorporates a radiopaque material.

46. The prosthesis of claim 29 further including:

a coating applied to the structural strands.

47. The prosthesis of claim 29 further including:

35 a coating applied to the textile strands.

48. The prosthesis of claim 29 further including:

an adhesive applied to the integrated structure

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at least at opposite ends thereof.

49. The prosthesis of claim 29 wherein:  
said integrated structure is tubular.

50. The prosthesis of claim 29 wherein:  
5 said integrated structure consists essentially  
of a single layer of the interbraided structural strands  
and textile strands.

51. A medical device, including:  
an elongate and flexible catheter (26);  
10 a braided prostheses (18) mounted to the  
catheter at a distal end thereof in surrounding relation  
thereto, said prosthesis including an interbraiding of a  
plurality of structural strands (32) and a plurality of  
compliant textile strands (42);  
15 wherein said structural strands are formed of a  
structural material tending to assume a nominal shape  
when in a relaxed state, and have respective selected  
nominal shapes imparted by at least one of: (i) a  
selective plastic deformation from an original nominal  
20 shape to the selected nominal shape; and (ii) a selective  
thermal setting including a heating of each structural  
strand to a temperature greater than a melting  
temperature of the textile strands while the structural  
strand is maintained in its selected nominal shape.

25 52. The device of claim 51 further including:  
a means (20) for releasably maintaining the  
prosthesis at said distal end of the catheter in a  
resiliently radially compressed state, and operable to  
release the prosthesis for a radial self-expansion at an  
30 intraluminal treatment site; and

wherein the structural strands have selected  
orientations within the prosthesis to impart a  
predetermined shape to the prosthesis.

53. A process for making a prosthesis, including:  
35 providing a plurality of strands  
(32,94,102,112) for interbraiding at a braiding station,  
said strands including elastically and plastically

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deformable structural strands formed of metal and having an original nominal shape;

controllably plastically deforming the structural strands to impart to each structural strand a  
5 selected nominal shape; and

after plastically deforming the structural strands, braiding the strands into an integrated structure, and selectively orienting the structural strands while braiding to impart a predetermined  
10 configuration to the integrated structure.

54. The process of claim 53 further including:

before said braiding, moving said strands in concert toward a braiding station, wherein said plastic deformation of the structural strands is performed when  
15 the structural strands are being so moved.

55. The process of claim 54 wherein:

said plastic deformation includes wrapping each of the structural strands about a rotatable pulley (86) and maintaining the strand wrapped about its associated  
20 pulley and at a selected tension while so moving the strand.

56. The process of claim 53 wherein:

said strands further include a plurality of compliant textile strands (42,108), and said braiding  
25 strands includes braiding the textile strands into a textile sheeting (40,96,104) supported by the structural strands and occupying interstices between adjacent structural strands.

57. A medical prosthesis, including:

30 a prosthesis structure (18,92,100,114) including an interbraiding of a plurality of strands, said strands including elastically and plastically deformable structural strands (32,94,102,112) formed of metal and having respective selected nominal strand  
35 shapes imparted by a controlled plastic deformation from an original nominal shape to the selected nominal shape.

58. The prosthesis of claim 57 wherein:

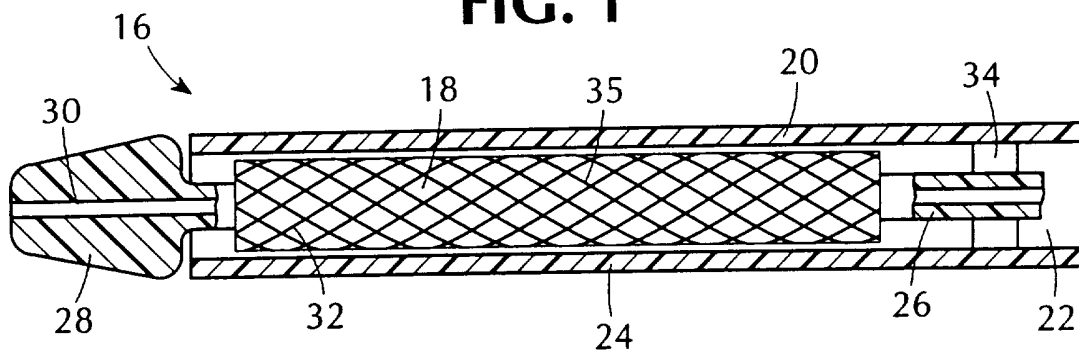
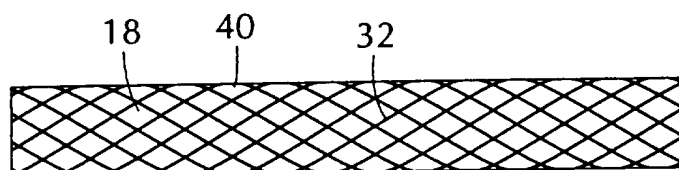
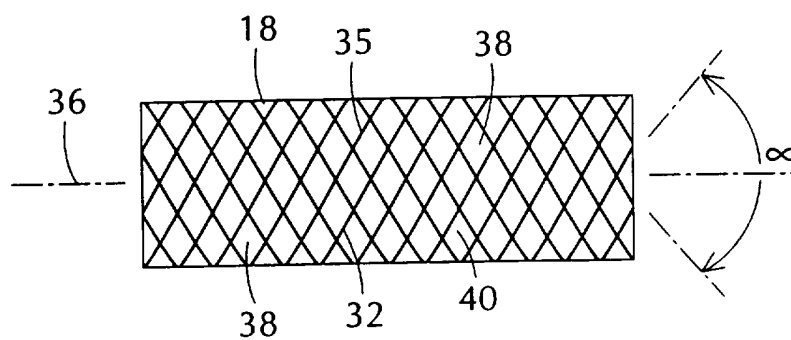
-34-

the structural strands further have selected orientations within the prosthesis structure to impart a predetermined configuration to the prosthesis structure; and

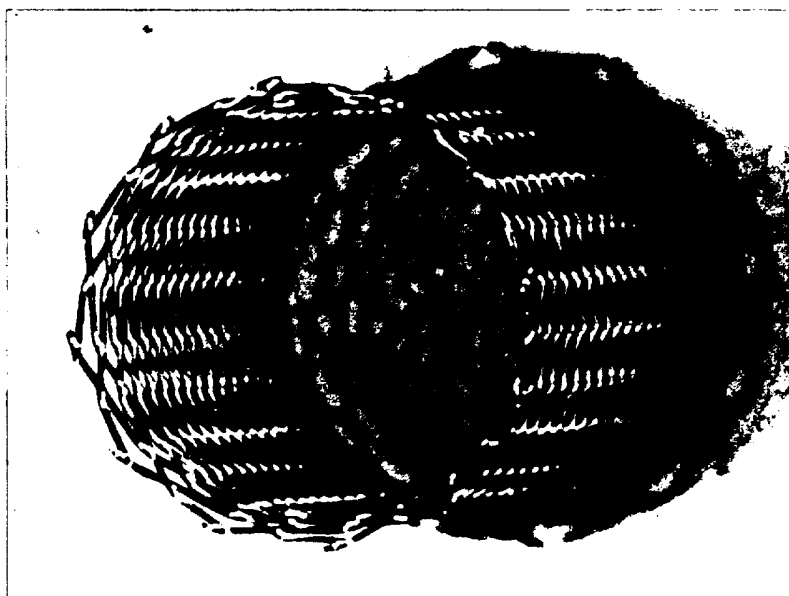
5           the plurality of strands further includes a plurality of compliant textile strands (42,108) interbraided with the structural strands, supported by the structural strands and occupying interstices between adjacent structural strands.

10           59. The prosthesis of claim 58 wherein:

          said structural strands are monofilaments, and said textile strands are multifilament yarns.

**FIG. 1****FIG. 3****FIG. 4**

**FIG. 2a**



**FIG. 2b**

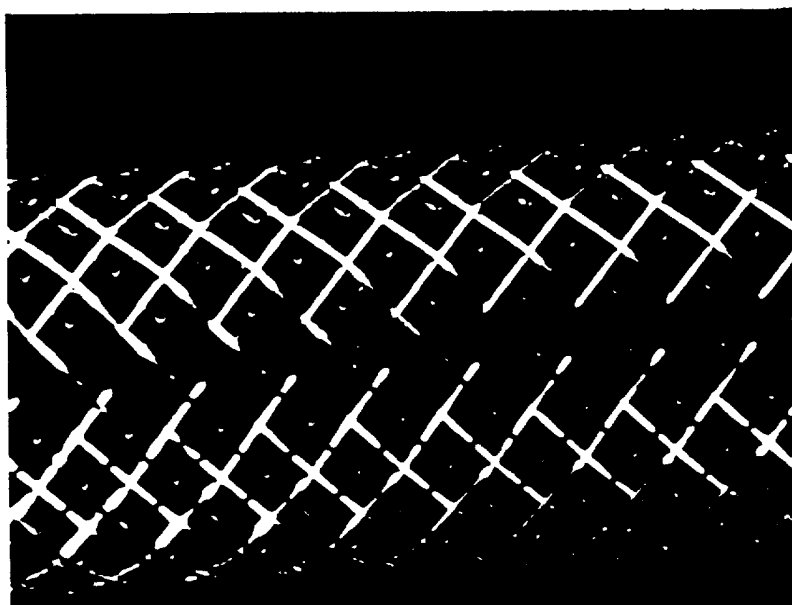


FIG. 5

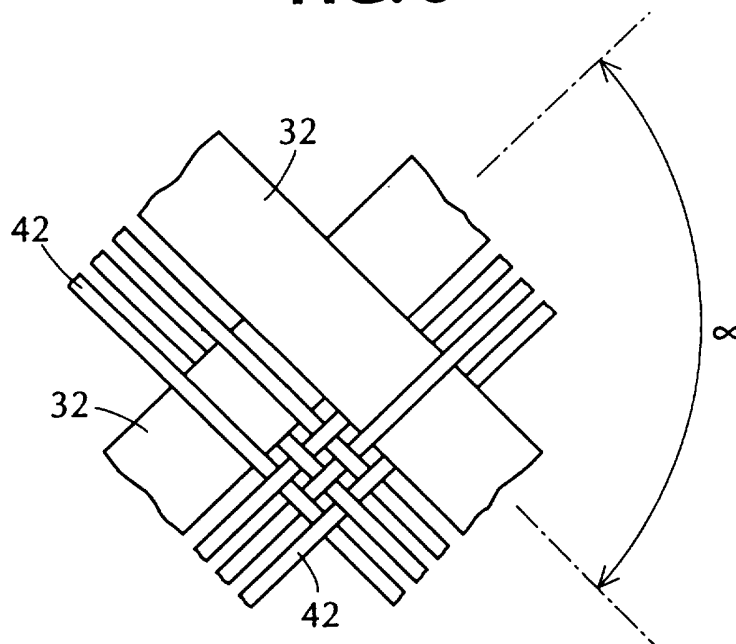
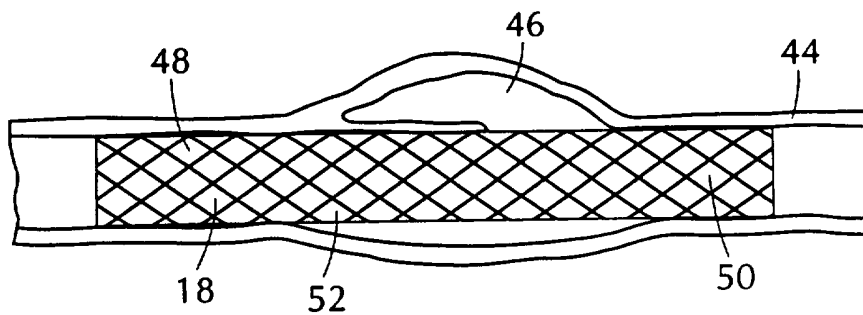
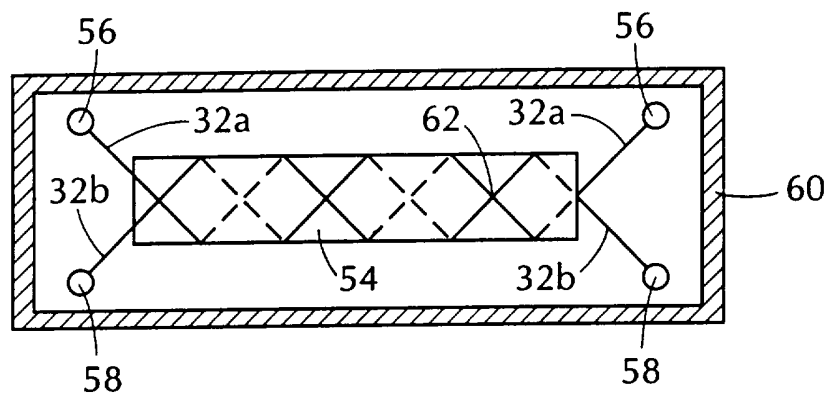
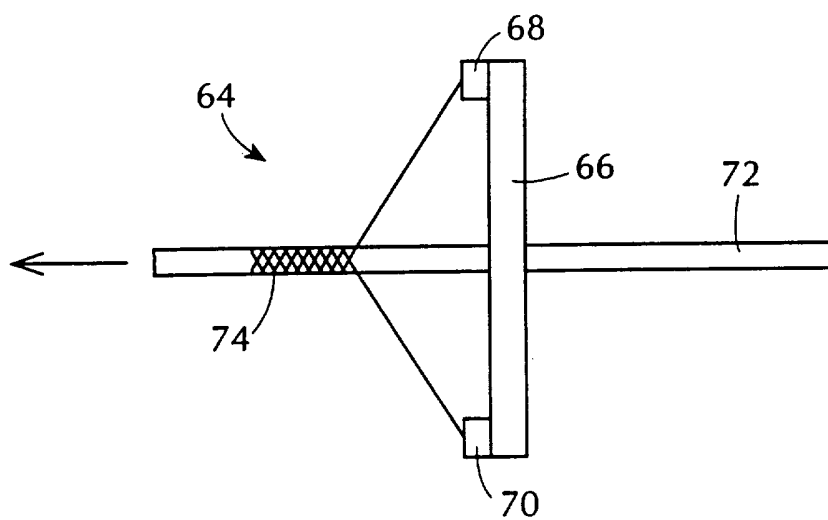


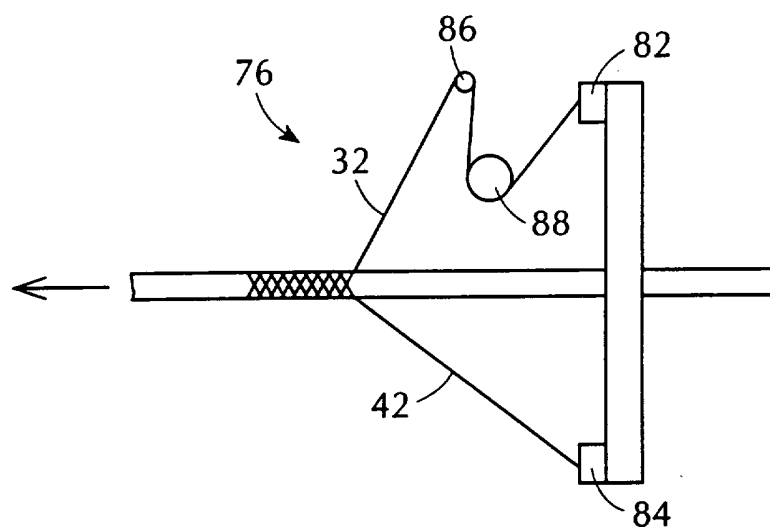
FIG. 6



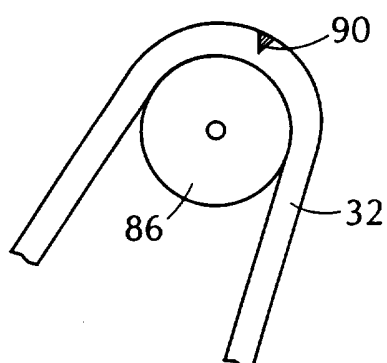
**FIG. 7****FIG. 8**



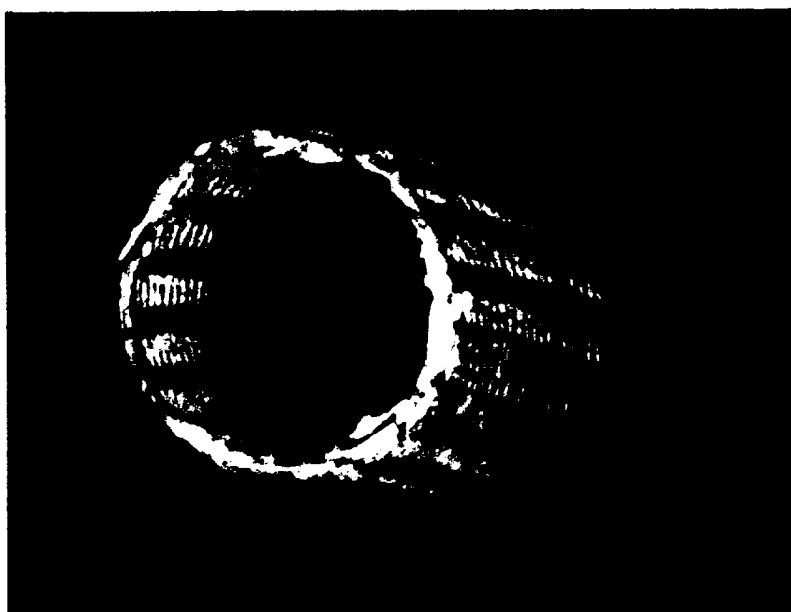
**FIG. 9**



**FIG. 10**



**FIG. 11a**



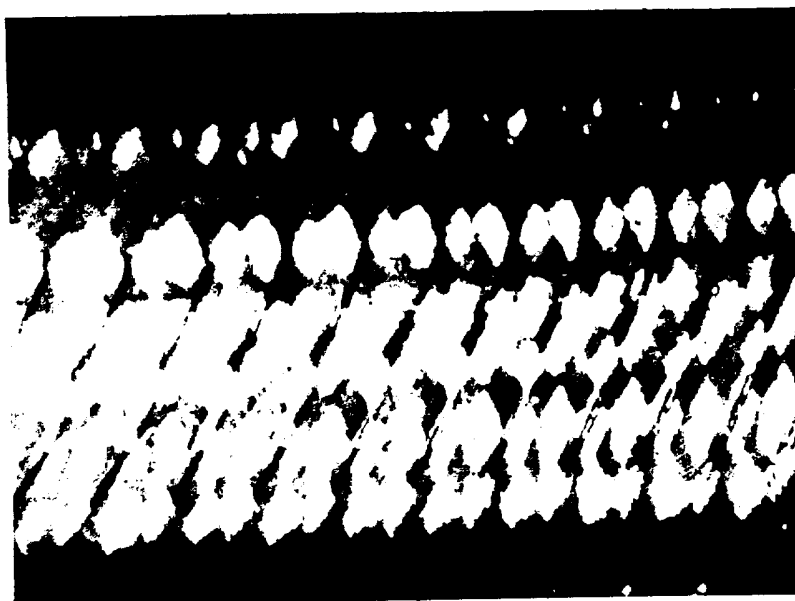
**FIG. 11b**



**FIG. 12**



**FIG. 13**

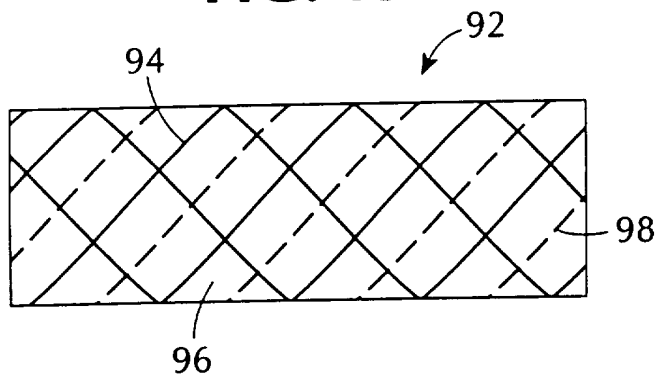


**FIG. 14**

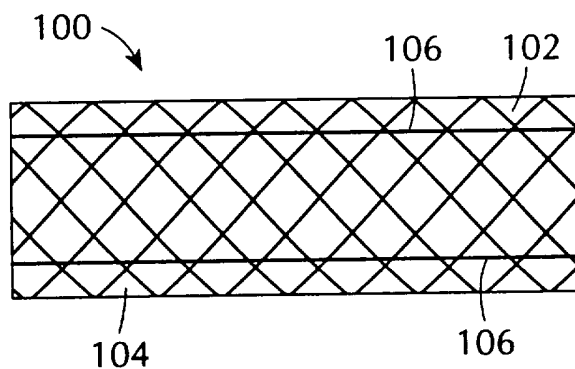


9/9

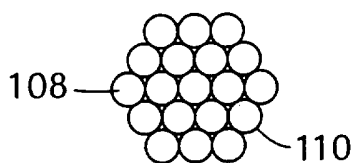
**FIG. 15**



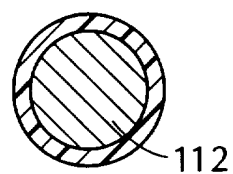
**FIG. 16**



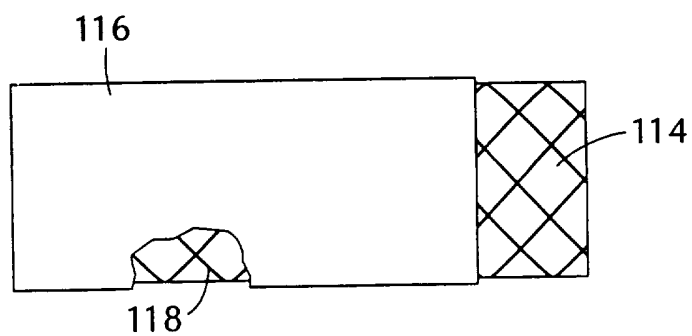
**FIG. 17**



**FIG. 18**



**FIG. 19**



# INTERNATIONAL SEARCH REPORT

Intern: al Application No  
PCT/IB 96/00792

A. CLASSIFICATION OF SUBJECT MATTER  
IPC 6 A61F2/06 D04C1/04

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
IPC 6 A61F D04C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

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☒ Further documents are listed in the continuation of box C.

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Date of the actual completion of the international search

12 February 1997

Date of mailing of the international search report

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# INTERNATIONAL SEARCH REPORT

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