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I –Technical field of the invention

The invention relates to a method and a reactor for the treatment by
5 flocculation of a raw fluid to be treated, which can be used in particular in the field of
treatment of industrial process water, drinking water and municipal or industrial waste
water.

II-Prior art

Various fluid treatments, in particular in the field of water treatment,
10 involve mixing a raw fluid to be treated with a secondary fluid or flow in order to make
the secondary flow react with components of the main fluid; in practice the secondary
fluid contains a flocculating agent and most often a granular material on which flocs
resulting from the action of the flocculating agent on the impurities of the raw fluid to
be treated are formed; in practice this process is known as ballasted floc physical-
15 chemical treatment; the fluids are usually mixed and reacted in full-mixing open
reactors equipped with axial-flow vertical-shaft agitators.

In principle a physical-chemical reaction treatment involves dispersing the
secondary fluid or fluids in the raw fluid to be treated and intensive mixing followed by
a reaction time (as short as possible) with stirring at a low intensity (compared to the
20 intensive mixing step), these steps usually leading to the use of a plurality of vats or
reactors in series.

The possible existence of a bypass (short circuit) between the vat inlet and
outlet and the fact that in practice use of the volume of the vats is incomplete, as is
easily demonstrated by mathematical modeling linked to physical models, usually
25 lead to increasing the size of the reactors and/or to the use of additional agitation
power. This induces an increase in the investment and operating costs, however.

Furthermore, it is standard practice to have the inlet and the outlet of a given vat at the greatest possible distance from each other, for example by using a low-level inlet at one end of the vat and a high-level outlet at the other end, although this proves to be a problem if it is necessary to connect a plurality of vats in series.

5 What is more, to prevent rotation of the liquid mass, usually called a vortex, which has been recognized as compromising mixing performance, it has already been proposed to place vertical baffles against the lateral walls (see book "Mixing in the chemical industry", Sterbacek and Tausk, Pergamon Press, 1965, pp 278-301). According to that document, adding vertical baffles increases turbulence
10 (and therefore improves mixing) provided that the width of the chicanes is from 0.056 to 0.12 times the diameter of the agitator and it is preferable for the baffles to be in the flow rather than against the walls. In fact the above document also mentions, for historical reasons, a cruciform baffle formed of two vertical walls mounted on the bottom of the vat, near the agitator, but indicates that the process is then difficult to
15 control and the circulating liquid rapidly becomes contaminated with solid particles. It also indicates that these walls induce an increase in power consumption.

 In the case of deep vats, it is known in the art to dispose a plurality of mobiles in the volume of the vat, along the agitation shafts, to increase the fraction of the volume in which turbulence is induced; it has nevertheless been realized that
20 such stacked mobiles can be dispensed with by disposing a concentric tube (flow-guide) around the mobile, which is mounted at the tube outlet (see the 1965 book cited above). A flow-guide of this kind acts like an aspiration tube which contributes to increasing the fraction of the volume that is stirred and has the advantage of allowing internal recirculation. However, this aspiration effect is often associated with
25 a vortex type rotation movement.

 In the field of water treatment, in particular with regard to the flocculation step, it has already been proposed, for example in the document FR-2 553 082, to produce a reaction chamber with a central area provided with an upward axial flow propeller and a peripheral area around the central area. The water to be treated,
30 where appropriate with the necessary reagents added to it, which has been mixed

with sludge obtained previously during the treatment, is introduced at the base of the central area, and an additive such as a polymer is introduced into this area. This produces internal recirculation, the peripheral area constituting a slow flocculation area. The central area is delimited by a vertical tube disposed in a parallelepiped-shaped enclosure, and so the central area may be described as a double area. The mixture then enters an intermediate enclosure before passing into a separation area. Note that architecture of this kind involves a large number of areas.

There is also known, from the document WO-98/14258, an installation in which a central internal recirculation enclosure includes a central tube containing one or more upward axial flow propellers, a granular material inlet and a flocculating agent inlet. The raw fluid to be treated is introduced at the base of the tube, overflows into the annular area of the central area and then, depending on the size of the flocs, rises either inside the tube, to be recirculated, or in the peripheral clarification area. The propeller produces just sufficient turbulence to maintain the solids in suspension without shearing them, which can lead to slow mixing and therefore degrade performance.

Reference FR – 2 380 056 deals with decantation techniques and in particular with a mechanical decanter intended to continuously separate solids contained in a solution, in particular by mixing with flocculation agents. The mechanical decanter is intended to treating mineral sludge, industrial waste and wastewater. The mechanical decanter comprises a vat intended to contain a quiet mass of water; a tubular column mounted vertically in the vat; a device which, mounted at the upper end of the column, discharges a flow of the primary solution; compartments which, superposed in the column, are intended to successively collect the solution which is mixed with flocculation agents; members which, mounted in each of the compartments, are intended to mix the liquid contained therein; nozzles which, mounted in each of the compartments, are intended to disperse in the solution contained therein a chemical reagent so as to further flocculate solids which are in suspension: a conduit which, communicating with the lowest compartment, on one hand and with the vat, on the other hand, is intended to drive out the solution treated by the flocculation agents into the layer of thick sludge which is at the bottom of the

vat; a mechanism which, mounted in the vat and comprising raking arms, brings the solid content of said layer towards a conduit which evacuates same from below; and an overflow which, mounted on the vat, evacuates the supernatant clarified liquid which extends from above.

5 **III – Technical problems and solutions according to the invention**

The invention aims to provide an enhanced combination of compactness, efficacy and moderate cost, whether from the plant or operation point of view.

10 Accordingly, the invention aims to provide a flocculation reactor which, thanks to one or more agitators and the delimitation of areas with different levels of agitation, improves the kinetics of the reaction between a raw fluid to be treated and a flocculating agent (and where applicable a granular material forming a flocculation ballast), increases the usable fraction of the volume of the reactor and reduces the risk of bypassing the process (i.e. the risk of no circulation occurring in the areas with different levels of agitation), with a moderate level of the power devoted to the
15 agitation levels.

The invention further aims to provide a method of treating a raw fluid to be treated by flocculation and separation, the method combining, within the overall dimensions of a single vat, two areas with different levels of agitation, maximizing the turbulence for a given energy level and for a given contact time.

20 A subsidiary aim of the invention is to facilitate the series connection of a plurality of reactors of the same or different types and of the same or different sizes, either at the time of manufacture or subsequently.

To this end, the invention firstly proposes a method of treating a raw fluid to be treated by flocculation and separation charged with impurities in suspension,
25 colloidal impurities or dissolved impurities, wherein:

- the raw fluid to be treated is circulated with a flocculating reagent in a flocculation vat to obtain a flocculated mixture in which the impurities form flocs, and

- this flocculated mixture is circulated in a separation area in which the flocculated mixture is separated into clarified effluent and sludge containing the flocs,

5 characterized in that:

- a completely immersed flow-guide tube delimits a central area in the flocculation vat in which agitation brings about turbulent axial flow of the mixture of the raw fluid to be treated and the flocculating agent in an axial direction of the flow-guide tube,

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- that flow is divided angularly by means of a static system opposing rotation of the flow disposed at the flow-guide tube outlet,

- this mixture is allowed to circulate in an opposite direction in a peripheral area around the central area in order to reach the inlet of the central area, and,

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- a fraction of the mixture is passed to the separation area.

It may be noted that the invention therefore teaches the use of a static device opposing rotation of the fluid at the outlet from the flow-guide tube to combine delimitation of a central area with a high level of agitation from a peripheral area with a lower level of agitation with an angular distribution of the outflow from the central area, so that turbulence is maximized and dead areas escaping the circulation induced in the volume of the central and peripheral areas are minimized. As stated above, using a static system to prevent the rotation of a flow had been abandoned as being difficult to control and had been proposed only in combination with an agitator; the person skilled in the art would therefore have had no reason to think that a static system of this kind could contribute to solving the stated technical problem. Also, there has been nothing, even drawing inspiration from prior art solutions using a flow-guide in a flocculation area, to suggest that it might be beneficial to use a static system of this kind in combination with a flow-guide.

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According to preferred features of the invention which may, where appropriate, be combined:

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- the flow in the central area is maintained at a flowrate from 1 to 20 times the inlet flowrate of the raw fluid to be treated, which corresponds to sufficient recirculation to reduce the risk of bypassing the system and to induce sufficient turbulence to ensure good mixing without necessitating excessive consumption of energy,

- the peripheral area is at least divided into an upstream peripheral area communicating with the inlet into the flocculation vat for raw fluid to be treated and a downstream peripheral area communicating with the flocculated mixture outlet, so as to cause the raw fluid to be treated that enters the flocculation vat to enter the central area at least once before passing to the separation area; this of course contributes to avoiding bypassing the system without significant consumption of energy and without involving a large number of recirculation cycles,

- the turbulent axial flow of the mixture is vertical; this corresponds to a proven conventional configuration,

- the vertical turbulent axial flow is brought about by agitation at mid-height in the central area, which contributes to obtaining good aspiration movement at the inlet of the central area and good discharge at its outlet, therefore with an angular distribution at that outlet, without requiring more than one agitator,

- the turbulent axial flow of the mixture is downward and the mixture is divided angularly over at least substantially two thirds of the height between the level of the outlet from the central area and the level of the bottom of the flocculation vat; it is worth mentioning that this is the opposite of the direction used at present when there is internal recirculation in a flocculation area; however, recent modeling studies have shown that, in contrast to what the person skilled in the art might think, it is entirely realistic to use a downward movement in combination with a static angular distribution system without this inducing unwanted contamination of the latter system by flocs being formed or growing; indeed, selecting a downward direction avoids causing wavelets on the surface as a consequence of the turbulence induced and uses the vat bottom to bring about a rapid change in the direction of flow of the mixture between the central area and the peripheral area.

In the case of downward movement, it is preferable if:

- the mixture is divided angularly over substantially all of the height between the level of the central area and the level of the bottom of the flocculation

vat, which guarantees an angular distribution of the whole flow leaving the flow-guide tube,

- the flow-guide tube delimiting the central area is disposed so that its bottom end forming its outlet faces the bottom of the flocculation vat at a distance from 1/3 to 2/3 the average width of the tube therefrom, which contributes to reversing the direction of flow with no great risk of unwanted slowing of the flow,

- the flow-guide tube delimiting the central area is disposed so that its top end forming its inlet faces the surface of the contents of the flocculation vat at a distance from 1/3 to 2/3 of the average width of the tube therefrom, which contributes to ensuring efficient feeding of the flow-guide tube without inducing unwanted surface movements,

- the peripheral area is divided over an upper portion of its height into at least an upstream peripheral area communicating with the inlet into the flocculation vat for the raw fluid to be treated and a downstream peripheral area communicating with the flocculated mixture outlet, so as to cause the raw fluid to be treated entering the flocculation vat to enter the central area at least once before passing to the separation area, which is a particularly simple way to obtain the advantages cited above in respect of the general use of this kind of division,

- said division is effected over substantially the upper half of that height, which represents a height sufficient to minimize the risk of circumventing the central area.

According to other preferred features of the method of the invention:

- the raw fluid to be treated enters and the flocculated mixture leaves substantially at the level of the inlet area of the flow-guide tube, which contributes to allowing the series connection of installations for implementing the method and participates in efficient guidance of the fluid to be treated towards the central area and of the mixture that has circulated in the peripheral area,

- the flocculating agent is a natural, mineral or synthetic polymer,
- the flocculating reagent with which the raw fluid to be treated is mixed in the flocculation vat is introduced into the fluid to be treated upstream of said vat,

- alternatively, the flocculating reagent with which the raw fluid to be treated is mixed is introduced into the flocculation vat, for example between the inlet of the flocculation vat and the inlet of the flow-guide tube; however, it is

recommended that the flocculating reagent is introduced into the central area, preferably at the boundary of the central area, which ensures very fast mixing with the fluid to be treated; this effect is reinforced if at least a fraction of the flocculating reagent is injected annularly at the periphery of the inlet of the central area and

5 coaxially with the flow-guide tube,

- further, a powder material is mixed with the raw fluid to be treated in the flocculation vat, and is preferably a ballast consisting of an insoluble granular material heavier than the raw fluid to be treated, to serve as ballast for the flocs being formed or growing; the ballast advantageously consists of fine sand with a particle

10 size range from 20 to 300 microns, the cost price of which is particularly reasonable,

- the sludge is treated at the outlet from the separation area, where ballast is recovered and recycled to the flocculation vat, which avoids losing the powder in the sludge that is discarded on reaching the separation area outlet, as well as reducing the volume of these discarded products,

- the raw fluid to be treated is mixed with coagulating agent before it is introduced into the flocculation vat which contributes all the more to the efficacy of final separation if the raw fluid to be treated is water to be treated; in this case, the water to be treated is preferably mixed with a coagulating agent including a mineral salt such as an iron or aluminum salt before it is introduced into the flocculation vat,

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- separation is effected by sedimentation or flotation, advantageously with the assistance of separation aid members such as inclined or vertical tubes or plates; the flocculated mixture is advantageously introduced tangentially into the separation area so as to combine a vortex effect with the sedimentation effect, which improves separation for a given treatment time or accelerates the treatment, for a

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25 given level of separation.

Another aspect of the invention proposes, for implementing a preferred embodiment of the method, a reactor for treating a raw fluid to be treated by flocculation charged with impurities in suspension, colloidal impurities or dissolved

30 impurities, including a vat having at least a fluid inlet, and at least a fluid outlet, and at least a flocculation area in a bath in which the fluid to be treated is mixed with a flocculating agent so as to form flocs, said reactor including:

- a flow-guide tube open at both ends and disposed vertically so that it is completely immersed in the bath in the vat but remains at a distance from the bottom

of the vat, delimiting a central area from a peripheral area, the central and peripheral areas communicating with each other at both ends of the tube and the peripheral area communicating with the fluid inlet and outlet,

- a vertical-axis agitator disposed in the tube so as to generate therein

5 vertical turbulent axial movement,

- a cruciform baffle formed of a plurality of vertical walls extending horizontally from a common edge substantially aligned with the axis of the agitator, on the downstream side thereof, so as to divide angularly the flow towards the peripheral area leaving the tube.

10 A reactor of the above kind has the advantages described hereinabove in the case of using the method with a vertically downward turbulent movement.

According to preferred features of the invention, in some instances analogous to those mentioned hereinabove with regard to the method of the
15 invention:

- the flow-guide tube has a constant section, which contributes to ensuring a fast flow of the mixture,

- the flow-guide tube has a cylindrical shape (in the narrow sense of the term, namely that its section is a circle), which represents a particularly simple
20 structure; alternatively, the section is a regular polygon, etc.,

- the agitator is disposed substantially at mid-height in the tube,

- the flow-guide tube has a diameter from 102% to 120% of the diameter of the agitator, which ensures good stirring throughout the section of the flow-guide tube,

25 • the hydraulic diameter of the central area is from 40% to 60% of the average width of the flocculation area formed by the central area and the peripheral area,

- the agitator is disposed and driven so as to generate a downward vertical movement in the tube, the cruciform baffle being disposed between the
30 bottom of the flow-guide and the bottom of the vat,

- the tube has a bottom end facing the bottom of the vat at a distance from 1/3 to 2/3 of its diameter therefrom,

- the tube has a top end facing the surface of the bath contained in the vat at a distance from $1/3$ to $2/3$ of its diameter therefrom,

- the distance between the bottom end of the tube and the bottom of the vat and the distance between the top end of the tube and the level of the bath are at least approximately 50% of the diameter of the tube,

- the cruciform baffle has a height substantially equal to at least $2/3$ of the distance between the bottom end of the tube and the bottom of the vat,

- the cruciform baffle has a height substantially equal to the distance between the bottom end of the tube and the bottom of the vat,

- the vertical walls of the cruciform baffle extend over a horizontal distance substantially from $3/4$ to $5/4$ of the radius of the tube, which ensures that all or virtually all of the flocculated mixture is distributed angularly; the vertical walls of the cruciform baffle preferably extend over a horizontal distance substantially equal to the radius of the flow-guide tube,

- the cruciform baffle comprises four walls offset at 90° around the axis of the flow-guide tube, which represents a particularly simple structure (two plates crossing at a right angle),

- two of the walls are disposed transversely to the direction in which the raw fluid to be treated enters the flocculation vat, which contributes to good division of the flow,

- vertical walls divide the peripheral area between said inlet and outlet areas over at least a portion of the total height between the bottom of the vat and the surface of the bath, which helps to guarantee that the raw fluid to be treated passes through the flow-guide tube at least once,

- these vertical walls extend over a vertical distance from 40% to 60% of the total height, which is a good compromise relative to the height, to ensure good efficiency without using up too much baffle area,

- the reactor includes two or more vertical baffles extending substantially over the upper half of the vat, between the flow-guide tube, the fluid inlet and the fluid outlet, respectively, so as to cause the fluid to be treated to enter the central area between the fluid inlet and the fluid outlet at least once; in fact, these walls are most effective in the upper portion, at the level of the flow-guide tube inlet,

- the vertical walls extend over a height between the main fluid inlet level and the level of the agitator,

- the vertical walls extend from the periphery of the peripheral area to the tube, which ensures good partitioning of the peripheral area,

5 • the inlet and outlet areas are near the level of the surface and each is provided with a transverse plate facing the inlet and the outlet, respectively, to form a siphon, which helps to ensure regular arrival of fluid to be treated and to prevent unwanted movement on the bath surface,

10 • it further comprises a flocculating reagent injection tube connected to a supply of flocculating reagent,

- the flocculating reagent injection tube is situated between the inlet for raw fluid to be treated and the inlet of the flow-guide tube; the reactor preferably includes an annular flocculating reagent injection tube coaxial with the inlet of the flow-guide tube,

15 • it further comprises a powder injection tube connected to a supply of powder,

- the supply of powder is a supply of fine sand,

20 • the vat includes a single flocculation area including a tube, although the invention also covers situations in which the same vat comprises a plurality of juxtaposed flocculation areas.

The invention also provides a fluid treatment installation including a reactor of the type cited above and a separation area connected to the outlet from the vat of that reactor.

Preferably:

25 • the reactor comprises a powder injection tube connected to a powder supply and the separation area includes an outlet connected to a powder recovery system and adapted to collect sludge containing flocs and connected to a powder recovery system, said powder supply being connected to said recovery system,

30 • the separation area is a sedimentation unit disposed on the downstream side of the vat,

- the separation area is a sedimentation unit around the vat.

Accordingly, in a particularly beneficial combination of features of the invention, the flow-guide tube is disposed above a cruciform baffle, the two devices advantageously having at least approximately the same diameter. The recommended pumping direction is downwards, to allow the introduction of one or more secondary
5 flows or fluids at the surface, thereby ensuring continuous control of the injection thereof. The steep velocity gradients that the cruciform baffle produces in the lower portion of the vat (in producing turbulent kinetic energy) have the advantage of preventing the formation of deposition areas, whereas the person skilled in the art has ruled out horizontal bottom walls of this kind in order to prevent deposition areas.

10 The combined effect of the above systems is to convert a major portion of the radial component of the screw propeller of the agitator into an axial component, thereby significantly increasing the pumping throughput for the same absorbed power.

It is worth making the following remarks in relation to preferred
15 embodiments of the invention:

- The presence of two perfectly delimited areas having radically different mixing intensities allows that functions usually necessitating two vats with different mixing intensities can be accomplished in the same vat.

- The use of a single vat having two areas with different mixing intensities
20 allows providing both functions with a single agitator instead of two.

- For exactly the same usable volume, as a result of the reduction in dead areas resulting from improved control of mixing intensity and homogeneity, the total volume of a single vat may be significantly less than that of two joined vats.

- For the same treatment efficiency, the same consumption of reagent
25 and the same pumping throughput, the energy consumption may be reduced through the conversion of a major portion of the radial flow into axial flow.

- In deep vats that normally use a plurality of stacked mobiles, by eliminating the consumption specific to the additional mobiles and improving efficiency by using the new design, the presence of the flow-guide with its associated

cruciform baffle helps achieving the same hydraulic effect with a single mobile and using less electrical power.

- The vertical baffles may simply be two in number, filling completely the space between the flow-guide and the vat and disposed only in the upper half of the liquid depth; in this case, they are wider and shorter than indicated in the literature. In the horizontal plane they are parallel to the inlet walls and therefore parallel to the outlet walls.

- The cruciform baffles preferably have a diameter equal to that of the flow-guide and a height contained between the flow-guide and the bottom of the vat.

- An optimum performance may be achieved with the present reactor, by virtue of the advantageous combination of flow-guides, surface baffles, cruciform baffles, feed and outlet areas and agitator positioning and secondary fluid injection mode.

IV-Description of the invention

Objects, features and advantages of the invention emerge from the following description, which is given by way of illustrative and non-limiting example and with reference to the appended drawings, in which:

- FIG. 1 is a diagrammatic perspective view of a preferred embodiment of a reactor of the invention,

- FIG. 2 is a diagrammatic plan view of the reactor,

- FIG. 3 is a diagram of a water treatment installation using the reactor shown in FIGS.1 and 2,

- FIG. 4 is a diagrammatic plan view of a reactor that is a variant of the reactor shown in FIGS. 1 and 2,

- FIG. 5 is a diagrammatic plan view of a reactor that is also a variant of the reactor shown in FIGS. 1 and 2,

- FIG. 6 is a diagram of one variant of the installation shown in FIG. 3, and

- FIG. 7 is a diagram of another variant of the installation shown in FIG. 3.

Reactor Shape

The reactor **10** shown in FIGS. 1 and 2 is of rectangular shape in order to facilitate connecting a plurality of reactors of the same type in series. In a variant that is not shown, the reactor may be square, which may be beneficial given the symmetry of the central area (see above).

It should be noted that most features described hereinafter are equally applicable to circular reactors (see FIG. 5), which are also within the scope of the invention, the results obtained being practically identical.

Generally speaking, the reactor 10 comprises in the preferred embodiment here considered:

- A fluid inlet area 1 receiving a raw fluid to be treated, often constituting turbulent flow, and into which a first reagent, such as a coagulating reagent of any appropriate type known in the art, may already have been injected,

- A central area 2, inside a tube 2A serving as a flow-guide, with high dissipated energy, generated by an agitator 8, and in which the raw fluid to be treated is dispersed and mixed completely with at least one flocculating reagent; in line with this tube is a cruciform baffle 5,

- A low-energy peripheral area 3 (outside the flow-guide), in which the required flocculation is completed,

- A fluid outlet area 4 that advantageously dissipates the stirring energy and evenly divides the mixed flocculated fluid, which here exits across the full width of the vat, in order to encourage solid-liquid separation in a downstream separator reactor, if any,

- a set of vertical baffles 6A and 6B forming deflectors to minimize bypassing between the inlet and the outlet and making mixing more efficient.

To facilitate the (initial or later) chaining of a plurality of treatment steps based on the same principle, the inlet and the outlet of each reactor are disposed at substantially the same level, preferably in the upper portion, substantially at the level of the tube inlet, here at the surface; this also minimizes dynamic bypassing and enables any floating material to be evacuated in the downstream direction, for

example by raising the level of the bath above spillways in the fluid outlet or by modifying the position of the spillways.

Inlet area 1

5 The raw fluid to be treated, also known as effluent, is introduced into each reactor at the surface (as shown in FIG. 1) and across its entire width (via a spillway 1A, immersed or not in practice formed by the lower edge of a slot defining the inlet in the wall of the reactor), or in an underflow arrangement (this variant is not shown), or at a single point (at or under the surface).

10 Generally speaking, introduction at a single point may be selected in the case of a single reactor or of the first reactor of a series, communication between two successive reactors preferably being achieved by means of a spillway.

 The inlet or admission area can be delimited from the remainder of the reactor by a siphon-shaped baffle 1B (or a jet breaker plate, achieving a siphon
15 effect). This siphon-shaped baffle allows dissipating upstream turbulent kinetic energy, essentially in the case of introduction at a single point, and changes the flow direction (to vertical instead of horizontal).

 A first reagent, such as a coagulant (for example a mineral salt such as an iron or aluminum salt) may be introduced into this highly turbulent area in order to
20 facilitate its dispersion. The manner of introducing this reagent (or any other reagent) depends on how the raw fluid to be treated is introduced: single-point or multipoint injection over the whole of the width of the admission area.

Central area 2

25 This is the area of maximum turbulence inside the flowguide in which the various components are intimately mixed.

 Using a flow-guide allows using a single agitator 8 on each shaft, regardless of the depth of the liquid.

 The tube has an axis z-z of symmetry and preferably has a constant and
30 advantageously cylindrical section, which here is a circular section (i.e. it is cylindrical in the common sense of the term), but may have other shapes, for example a polygonal shape.

 This tube, which is completely immersed in the bath, is preferably vertical (the axis z-z is therefore vertical), although inclined (or even horizontal) directions are

possible if the general configuration of the reactor as a whole, including its inlet/outlet, makes this desirable.

As shown in FIG. 4, a plurality of agitators equipped with flow-guides may be installed in the same vat, as a function of requirements and if the longitudinal and transverse dimensions of the vat allow it. The number of agitators to be disposed in each direction (longitudinal and transverse) depends on the ratio between the diameter of the mobiles of the agitators and the corresponding sides, the maximum diameter itself being a function of the depth of the liquid.

It is particularly advantageous if the agitator is controlled so as to cause a vertical downward flow.

The flowrate pumped by all of the agitators, which advantageously represents from 1 to 20 times the through-flowrate (that between the inlet and the outlet), is aspirated at the top of the tube 2A (or tubular sheath) and discharged towards the bottom of the reactor, and thus in a downward flow. This allows that the reagent or reagents are injected at the surface, at a single point or through a perforated annular tube, shown diagrammatically at **14**, coaxial with the tube 2A and disposed at the inlet thereof at its upper end. Here a flocculating reagent is injected through this perforated tube, but it may instead be injected at the inlet, between the inlet and the central area, or even at the inlet of the tube.

The agitator 8 is advantageously disposed at the mid-height of the tube, which preferably has a diameter from 102% to 120% of that of the agitator.

The diameter is advantageously at most equal to 60% and at least equal to 40% of the largest horizontal dimension of the peripheral area, and is preferably of the order of 50% thereof. The hydraulic diameter of the central area is from 40% to 60% of the average side dimension of the vat.

Its lower end advantageously faces the bottom at a distance from 1/3 to 2/3 of the diameter of the tube, and the same applies to the distance between the surface and the level of the upper end of the tube. These distances are advantageously of the order of 50% of the diameter of the tube.

The cruciform baffle 5 disposed under the flow-guide is formed of a plurality of vertical walls 5A extending from a common edge 7 that is substantially aligned with the axis Z-Z of the agitator. This is a static system to oppose continued rotation of the flow leaving the flow-guide tube; it allows channelling the flow, dividing it angularly into a plurality of equal parts, and preventing the formation of a circular

current at the bottom of the apparatus. Eliminating the radial effect that is the cause of this rotation of the flow has the parallel effect of increasing the axial effect and thus of increasing the pumped flowrate without increasing power consumption. This also prevents particles accumulating in the comers formed by the cruciform baffle.

5 The cruciform baffle advantageously has a diameter from 75% to 125% of the diameter of the tube. Its walls extend over a significant fraction (at least 2/3) of the height between the bottom of the vat and the outlet of the tube, preferably over substantially the whole of that distance.

10 Here the cruciform baffle is formed of four walls joining at a right angle (thus at 90%), two of which are preferably disposed transversely to the direction of flow between the inlet and the outlet of the vat. In a variant that is not shown the cruciform baffle may include a different number of walls, only three walls or five walls or even more.

15 Peripheral Area 3

 Situating outside the flow-guide tube, this area is characterized by the upward movement of the pumped liquid (which has been well mixed but is still only in the process of flocculation), low speed and turbulence and good homogeneity, which allows that the required process may be completed within a time period that has
20 been minimized.

 The disposition of the baffles 6A and 6B at the surface, transversely to the through-flow, eliminates the rotational movement formed at the surface and preferentially directs the whole of the incoming flow of fluid towards the flow-guide tube, guaranteeing that the raw fluid to be treated passes through the flow-guide tube
25 at least once in order to be mixed with the recirculated flow and the injected reagents.

 The vertical baffles extend over only a portion of the height of the central area, and therefore of the height of the bath, preferably over 40% to 60% of the height thereof and advantageously over the upper half of the bath (especially when
30 the inlet and the outlet are in the upper portion, as in the situation shown here). They advantageously extend between the surface and the level at which the agitator is disposed inside the tube.

In a variant that is not shown there may be a greater number of these baffles, for example three (or even four (or even more)) baffles disposed between the inlet and the outlet and angularly distributed in a regular or irregular manner.

5 **Outlet Area 4**

This area is opposite the inlet area and preferably at the same height and advantageously includes a siphon-shaped baffle 4B and an immersed spillway 4A generally covering the whole of the width of the reactor.

10 Disposed at an optimum distance and at an appropriate immersion depth, these devices allow minimizing bypassing and dissipation of turbulence that compromises treatment carried out downstream of the reactor (for example if a phase separation is wished).

15 Appropriate partitioning of the space between the siphon shaped baffle and the downstream wall (not shown) ensures a flowrate that is evenly distributed over the whole length of the spillway.

Specific configurations

The reactor shown in FIGS. 1 and 2 is advantageously followed by a separation area. Various configurations may be used.

20 FIG. 3 is a diagram representing the reactor 10 followed by a separation area 100 of this kind.

It must be clearly understood that it is possible to connect in series a plurality of reactors like that of FIGS. 1 and 2, depending on the specific requirements.

25 In FIG. 3, entry is from the left, downstream of a coagulating reagent injection line 11, if any, into a shaded area diagrammatically representing the portion of the peripheral area in which upward flow is confined angularly by the baffles 6A and 6B and in which mixing with the incoming raw fluid to be treated occurs. The diagram shows in the clear central area, at 14 the injection of flocculating reagent
30 (from a flocculating reagent source 14A) and at 15 the optional injection of powder from a source 15A of granular material. After flocculation, fluid leaves the right-hand portion of the peripheral area (shaded) and enters the separation area. In this separation area, the flocculated fluid is separated into clarified effluent and sludge containing the flocs formed in the reactor 10.

The raw fluid to be treated is preferably water, which is in principle pre-coagulated by injecting a coagulating reagent such as an iron or aluminum salt via the line 11 or into an upstream vat. Feeding is obtained by overflow or underflow.

It is advantageous to inject powder to encourage the formation of flocs from impurities in suspension, colloidal impurities or dissolved impurities in the raw fluid to be treated. This material is preferably ballast consisting of a granular material that is insoluble (or only very slightly soluble) in water and heavier than the raw fluid to be treated. This material is preferably sand, advantageously with a particle size range from 20 to 300 microns.

FIG. 4 represents another reactor 10' including in a same vat, not one, but three fluxguide tubes combined with a static system such as the cruciform baffle shown FIGS. 1 and 2. The expression "flocculation area" refers to the area formed conjointly by each central area defined by a tube and the peripheral area around it, so that it may be said that the FIG. 4 reactor includes a plurality of flocculation areas disposed in parallel between an inlet (at the top in the drawing) and an outlet (at the bottom in the same drawing).

FIG. 5 shows another reactor 10" that is similar to that shown in FIGS. 1 and 2 except that the wall of the vat is cylindrical and the flocculated fluid leaves the vat by overflowing along a large fraction of its periphery. Here there are four lateral deflector baffles 6"A to 6"D delimiting four quarters of the upper portion of the peripheral area, one of which (that at the top in the drawing) is reserved for the entry of raw fluid to be treated and the other three provide an outlet for the flocculated fluid.

Generally speaking, the flocs formed by the intensive mixing grow in the less agitated peripheral area, with partial recycling in the flow-guide before being finally transferred to the sedimentation area.

In the FIG. 6 embodiment, the sedimentation area is a separation vat 100' that is independent of the flocculation reactor 10; further, this vat includes sedimentation assisting members 110 that here consist of inclined plates (in a different embodiment these members are omitted); finally, the sludge separated from the clarified effluent, which in practice leaves the separation vat by underflow, is here pumped by a pump 112 connected by a line to a unit 113 capable of recovering a significant portion of the granular material contained in the sludge, in practice a hydrocyclone or any other suitable system capable of this separation, in which case the unit 113 is part of the powder source (the material injected into the flocculation

reactor consists partly of this recovered material used and partly of new material, of course).

The powder forming a ballast is a completely inert material (for example sand, garnet, etc.) or an active material (for example activated carbon powder or resin), which explains why it is sometimes listed in the water treatment "reagents", even if it is sand. As indicated above, it may be injected either at the inlet with the pre-coagulated fluid or in the area upstream of the agitation mobile, preferably at the top of a flow-guide coaxial with that mobile. Injecting ballast allows carrying out with a single vat with two effective areas, for example, the ballasted flocculation treatment disclosed in French patents FR 2627704 and FR 2719234, which correspond to a process sometimes known as the "Actiflo" process, with or without sedimentation assistance plates, thereby reducing the overall implementation cost and minimizing agitation energy requirements. According to tests carried out by the Applicant, and going against the received wisdom of the person skilled in the art, the cruciform baffle of the present invention, by improving agitation efficiency, helps minimizing the deposition of ballast sand on the bottom of the agitation vat.

FIG. 7 represents another installation for treating raw fluid, typically water. This installation differs from that shown in FIG. 6 essentially in that here the separation area is a vat 100" around the flocculation vat 10, rather than downstream of the vat; the configuration of the reactor 10 is the same as in FIG. 6 and, as in FIG. 6, the powder injected includes material recovered in the sludge pumped from the bottom of the vat 100". In this embodiment there are no sedimentation assistance members, for example sedimentation assistance plates, but the latter could exist.

In a variant that is not shown, the separation area uses a flotation principle, whereby the solids float on the surface of the clarified effluent, rather than sedimentation, whereby the clarified effluent is lighter than the sludge; separation assistance members may also be used here.

Tangential entry of the flocculated fluid into the separation area may also be advantageous, so as to benefit from a vortex effect in addition to the sedimentation effect.

Model-Based Comparative Study of the New Configuration and the Standard Configuration

The advantages of the invention have been assessed by a study of the velocity fields, turbulent gradient and treatment time distribution using the fluid mechanics simulation program Fluent (v.5, Fluent Inc).

Two configurations were studied, based on the same operating conditions, which differed as indicated hereinafter:

1-Highlighting the Advantages of a Surface Inlet-Outlet, a Shorter Rotation Shaft and a Cruciform Baffle

Table 1 shows the advantages obtained on changing from a standard configuration A, with an underflow and/or overflow effluent inlet and outlet, to a configuration B conforming to certain aspects of the invention, namely: inlet and outlet at the same height, inclusion of a jet breaker plate and a siphon- shaped baffle, shorter rotation shaft and cruciform baffle placed at the bottom of the vat; it may be seen that the maximum and average values of the velocity fields and the turbulent gradient are higher and more homogeneous with the new configuration B.

Benefits of the new configuration:

- increased mixing efficiency for the same energy consumption;
- maximum use of the vat volume;
- reduced bypass;
- facilitated series connection;
- elimination of rotation shaft vibration problems as a result of reducing its length;
- reduced treatment time;
- elimination of the risk of a preferred path in the vat by creating a kinetic energy dissipation outlet area.

2-Highlighting the Advantages of Coupling the Cruciform Baffle, Flow-Guide and Chicanes

Table 2 shows the advantages obtained, for continuous operation, on changing from a standard configuration C with a single agitator to a configuration D with a vat equipped with a mobile, a cruciform baffle, a flow-guide resting on the cruciform baffle and two chicanes supporting the flow-guide.

Analyzing the velocity fields and the turbulent gradient using the Fluent fluid mechanics simulation software shows that, for the same operating conditions:

- The maximum and average values of the velocity fields and the turbulent gradient are higher and more homogeneous with the new configuration D.

- Two clearly separate areas are created: a highly agitated area with very high values of the velocity and velocity gradient inside the flow-guide and at the cruciform baffles and a less agitated area outside the flow-guide.

Benefits of the new configuration:

- improved mixing efficiency for the same energy consumption;
- creation of two mixing areas differing in terms of mixing level; this would enable fast and efficient mixing of a reagent and the fluid in the strongly agitated area and a circulation time in the less agitated area that is the optimum for the reagent to act.

- creation of a highly agitated area at the level of the cruciform baffles; this will allow returning to suspension solid particles that have settled out, or increasing the interface area in the case of a gas-liquid flow;

3-Highlighting the Advantage of Adding the Reagent by Toroidal Injection

Around the Flow-Guide (FIG. 3, Reference 14)

Graphical simulation of the distribution of a reagent shows that dispersion is improved and faster with annular injection than with single-point injection.

Parameters	Ratio A to B	Benefit for B
Treatment time/average treatment time	0.9	+9%
Mixing time/average treatment time	0.79	+20%
Mixing proportion after 1 minute	0.62	+40%
Average velocity (m/s)	0.42	+60%
Average turbulent gradient (s^{-1})	0.21	+80%

TABLE 1

Parameters	Ratio C to D	Benefit for D
Treatment time/average treatment time	0.956	+4%
Mixing time/average treatment time	0.861	+14%
Mixing proportion after 15 minutes	1	0%
Average velocity (m/s)	0.17	+83%
Average turbulent gradient (s^{-1})	0.044	+96%

TABLE 2

Patentkrav

1. Fremgangsmåde til flokkuleringsbehandling og separation af en råfluid, der skal behandles og er fyldt med kolloidale eller opløste urenheder i suspension, hvor:

- den råfluid, som skal behandles, cirkuleres med et reaktivt flokkuleringsmiddel i en flokkuleringsbeholder for at opnå en flokkuleringsblanding, hvor urenhederne danner flokke,

- denne flokkuleringsblanding cirkuleres i en separationszone, hvor denne flokkuleringsblanding adskilles i et klart spildevand og slam, som indeholder disse flokke,

kendetegnet ved, at

* i flokkuleringsbeholderen, ved hjælp af et fuldstændig nedsænket strømledningsrør, afgrænses en midtzone, hvor der ved omrøring (8) frembringes en aksial, turbulent strømning af blandingen af den fluid, der skal behandles, og af flokkuleringsmidlet i en aksial retning af dette strømledningsrør,

* denne strøm fordeles (5) vinkelmæssigt ved hjælp af en statisk indretning, som modstiller rotationen af denne strøm og er anbragt ved udgangen af dette strømledningsrør,

* denne blanding cirkuleres i en perifer zone (3), som omgiver midtsonen, i modsat retning, frem til indgangen af midtsonen, og

* en del af denne blanding føres til separationszonen.

2. Fremgangsmåde ifølge krav 1, **kendetegnet ved, at** strømmen fastholdes i en midtzone ved en gennemstrømning, der ligger mellem 1 og 20 gange indgangsgennemstrømningen af den fluid, som skal behandles.

3. Fremgangsmåde ifølge krav 1 eller krav 2, **kendetegnet ved, at** den perifer zone inddeles i mindst én perifer opstrømszone, som kommunikerer med indgangen af den råfluid, der skal behandles, i flokkuleringsbeholderen, og en perifer nedstrømszone, som kommunikerer med udgangen af flokkuleringsblanding, således at den råfluid, der skal behandles og kommer ind i flokkuleringsbeholderen, tvinges til at strømme mindst én gang i midtsonen, inden den strømmer til separationszonen.

4. Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 3, **kendetegnet ved, at** den aksiale, turbulente strøm af blandingen frembringes i en vertikal retning.
- 5 5. Fremgangsmåde ifølge krav 4, **kendetegnet ved, at** den aksiale, turbulente og vertikale strøm frembringes ved omrøring (8) i halv højde af midtzonen.
- 10 6. Fremgangsmåde ifølge krav 5, **kendetegnet ved, at** den aksiale, turbulente strøm af blandingen frembringes i nedadgående retning, og blandingen fordeles i det væsentlige vinkelmæssigt på mindst to tredjedele af højden mellem udgangsplanet af midtzonen og bundplanet af flokkuleringsbeholderen.
- 15 7. Fremgangsmåde ifølge krav 6, **kendetegnet ved, at** blandingen fordeles vinkelmæssigt i det væsentlige i hele højden mellem planet af midtzonen og bundplanet af flokkuleringsbeholderen.
- 20 8. Fremgangsmåde ifølge krav 6 eller krav 7, **kendetegnet ved, at** strømledningsrøret, som afgrænser midtzonen, anbringes på en sådan måde, at dens nederste ende, som danner udgangen, befinder sig over for bunden af flokkuleringsbeholderen i en afstand, som ligger mellem $1/3$ og $2/3$ af dette rørs gennemsnitsbredde.
- 25 9. Fremgangsmåde ifølge krav 8, **kendetegnet ved, at** strømledningsrøret, som afgrænser midtzonen, anbringes på en sådan måde, at dens øverste ende, som danner indgangen, befinder sig over for planet af den frie overflade af indholdet af flokkuleringsbeholderen i en afstand, som ligger mellem $1/3$ og $2/3$ af dette rørs gennemsnitsbredde.
- 30 10. Fremgangsmåde ifølge et hvilket som helst af kravene 6 til 9, **kendetegnet ved, at** denne perifere zone på en øvre del af sin højde inddeles i mindst én perifer opstrømszone, der kommunikerer med indgangen af den råfluid, som skal behandles i flokkuleringsbeholderen, og en perifer nedstrømszone, der kommunikerer med udgangen af flokkuleringsblandingen, således at den
- 35 råfluid, der skal behandles og kommer ind i flokkuleringsbeholderen, tvinges til at strømme mindst én gang i midtzonen, inden den strømmer til separati-

onszonen.

11. Fremgangsmåde ifølge krav 10, **kendetegnet ved, at** denne deling udføres i det væsentlige på den øvre halvdel af denne højde.

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12. Fremgangsmåde ifølge et hvilket som helst af kravene 4 til 11, **kendetegnet ved, at** den råfluid, som skal behandles, indføres, og flokkuleringsblandingen udføres i det væsentlige på planet af strømledningsrørets indgangszone.

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13. Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 12, **kendetegnet ved, at** flokkuleringsmidlet er en naturlig, mineralsk eller syntetisk polymer.

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14. Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 13, **kendetegnet ved, at** det reaktive flokkuleringsmiddel, hvormed den råfluid, der skal behandles, blandes i flokkuleringsbeholderen, indføres i den fluid, der skal behandles, opstrøms for denne beholder.

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15. Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 13, **kendetegnet ved, at** det reaktive flokkuleringsmiddel, hvormed den råfluid, der skal behandles, blandes, indføres i flokkuleringsbeholderen.

16. Fremgangsmåde ifølge krav 15, **kendetegnet ved, at** det reaktive flokkuleringsmiddel indføres mellem indgangen af flokkuleringsbeholderen og indgangen af strømledningsrøret.

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17. Fremgangsmåde ifølge krav 15, **kendetegnet ved, at** det reaktive flokkuleringsmiddel indføres i midtzonen.

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18. Fremgangsmåde ifølge krav 15, **kendetegnet ved, at** det reaktive flokkuleringsmiddel indføres ved grænsen af midtzonen.

19. Fremgangsmåde ifølge krav 18, **kendetegnet ved, at** mindst en del af det reaktive flokkuleringsmiddel indsprøjtes ringformet ved omkredsen af

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indgangen af midtzonen, koaksialt til strømledningsrøret.

- 5 **20.** Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 19, **kendetegnet ved, at** der i den råfluid, der skal behandles i flokkuleringsbeholderen, yderligere blandes et pulverformet materiale.
- 10 **21.** Fremgangsmåde ifølge krav 20, **kendetegnet ved, at** det pulverformede materiale er en ballast, som består af et uopløseligt kornet materiale, der er tungere end den råfluid, som skal behandles.
- 15 **22.** Fremgangsmåde ifølge krav 21, **kendetegnet ved, at** ballasten består af fint sand med en kornstørrelse, som ligger mellem 20 og 300 mikron.
- 20 **23.** Fremgangsmåde ifølge krav 21 eller krav 22, **kendetegnet ved, at** den opnåede slam behandles ved udgangen af separationszonen, og man genvinder ballasten, som genanvendes i flokkulationsbeholderen.
- 25 **24.** Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 23, **kendetegnet ved, at** den råfluid, som skal behandles, inden sin indføring i flokkulationsbeholderen, er blandet med et koaguleringsmiddel.
- 30 **25.** Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 24, **kendetegnet ved, at** hovedfluiden er vand, som skal behandles.
- 35 **26.** Fremgangsmåde ifølge krav 25, **kendetegnet ved, at** det vand, som skal behandles, inden sin indføring i flokkulationsbeholderen, blandes med et koaguleringsmiddel, som indeholder et mineralsk salt, så som et jern- eller aluminiumssalt.
- 30 **27.** Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 26, **kendetegnet ved, at** separationen udføres med bundfældning.
- 35 **28.** Fremgangsmåde ifølge et hvilket som helst af kravene 1 til 26, **kendetegnet ved, at** separationen udføres med flotation.

29. Fremgangsmåde ifølge krav 27 eller krav 28, **kendetegnet ved, at** separationen udføres ved hjælp af separationshjælpemidler, så som plader, lameller eller krumme eller vertikale rør.

5 **30.** Fremgangsmåde ifølge et hvilket som helst af kravene 27 til 29, **kendetegnet ved, at** flokkuleringsblandingen indføres tangentielt i separationszonen for at tilføje en hvirvelstrømsvirkning, som tilføjes bundfældningsvirkningen.

10 **31.** Reaktor til flokkuleringsbehandling af en råfluid, der skal behandles og er fyldt med kolloidale eller opløste urenheder i suspension, omfattende en beholder (10,10', 10"), der er forsynet med mindst én fluidindgang og mindst én fluidudgang og minst én flokkulationszone i et bad, hvor den fluid, der skal behandles, blandes med et flokkuleringsmiddel, omfattende:

15 - et strømledningsrør (2A), der er åben ved begge sine ender og anbragt vertikalt for at være fuldstændig nedsænket i badet i beholderen og samtidig forblive i en afstand til bunden af denne beholder, afgrænser en midtzone (2) over for en perifer zone (3), hvor midtzone og den perifere zone kommunikerer indbyrdes ved de to ender af røret, hvor den perifere zone kommunikerer med fluidindgangen og -udgangen,

20 - en omrører (8) med vertikal aksel, som er anbragt på en sådan måde i røret, at den genererer en aksial, turbulent bevægelse i en vertikal retning,

25 - en tværstiver (5), der er dannet af flere vertikale vægge, der strækker sig horisontalt fra en fælles kant (7), der i det væsentlige er anbragt i forlængelse af omrørerens akse, nedstrøms derfor, for at fordele den strøm, der kommer ud af røret, vinkelret mod den perifere zone.

30 **32.** Reaktor ifølge krav 31, **kendetegnet ved, at** strømledningsrøret har et konstant tværsnit.

33 **33.** Reaktor ifølge krav 32, **kendetegnet ved, at** strømledningsrøret har en cylindrisk form.

35 **34.** Reaktor ifølge et hvilket som helst af kravene 31 til 33, **kendetegnet ved, at** omrøreren er anbragt i det væsentlige halvt oppe i røret.

35. Reaktor ifølge et hvilket som helst af kravene 31 til 34, **kendetegnet ved, at** strømledningsrøret har en diameter, som ligger mellem 102% og 120% af omrørerens diameter.
- 5 36. Reaktor ifølge et hvilket som helst af kravene 31 til 35, **kendetegnet ved, at** den hydrauliske diameter af midtzonen ligger mellem 40% og 60% af gennemsnitsbredden af flokkuleringszonen, der dannes af midtzonen og den perifere zone.
- 10 37. Reaktor ifølge et hvilket som helst af kravene 31 til 36, **kendetegnet ved, at** omrøreren er anbragt og styres bevægeligt, således at den genererer en vertikal bevægelse, der går ned i røret, hvor tværstiveren er anbragt mellem det nederste af strømledningsrøret og beholderens bund.
- 15 38. Reaktor ifølge krav 37, **kendetegnet ved, at** røret har en nedre ende, som befinder sig over for beholderens bund i en afstand, som ligger mellem $1/3$ og $2/3$ af diameteren.
- 20 39. Reaktor ifølge krav 38, **kendetegnet ved, at** røret har en øvre ende, der befinder sig over for planet af overfladen i det bad, som indeholdes i beholderen, med en afstand, som ligger mellem $1/3$ og $2/3$ af diameteren.
- 25 40. Reaktor ifølge et hvilket som helst af kravene 37 til 39, **kendetegnet ved, at** afstanden mellem den nedre ende af røret og beholderens bund, og afstanden mellem den øvre ende af røret og planet af badet svarer mindst ca. til 50% af rørets diameter.
- 30 41. Reaktor ifølge et hvilket som helst af kravene 37 til 40, **kendetegnet ved, at** tværstiveren har en højde, der i det væsentlige er lig med $2/3$ af afstanden mellem den nedre ende af røret og beholderens bund.
- 35 42. Reaktor ifølge krav 41, **kendetegnet ved, at** tværstiveren har en højde, der i det væsentlige er lig med afstanden mellem den nedre ende af røret og beholderens bund.

43. Reaktor ifølge et hvilket som helst af kravene 37 til 42, **kendetegnet ved, at** de vertikale vægge af tværstiveren strækker sig horisontalt over en afstand, der i det væsentlige ligger mellem $\frac{3}{4}$ og $\frac{5}{4}$ af rørets radius.
- 5 44. Reaktor ifølge krav 43, **kendetegnet ved, at** de vertikale vægge af tværstiveren strækker sig horisontalt over en afstand, der i det væsentlige er lig med radius af strømledningsrøret.
- 10 45. Reaktor ifølge et hvilket som helst af kravene 37 til 44, **kendetegnet ved, at** tværstiveren omfatter fire vægge, der er forskudt med 90° omkring akse af strømledningsrøret.
- 15 46. Reaktor ifølge krav 45, **kendetegnet ved, at** to af væggene er anbragt på tværs af den retning, langs hvilken den råfluid, som skal behandles, kommer ind i flokkulationsbeholderen.
- 20 47. Reaktor ifølge et hvilket som helst af kravene 37 til 46, **kendetegnet ved, at** vertikale vægge opdeler den perifere zone, mellem indgangs- og udgangszoner, over mindst en del af den samlede højde, som adskiller beholderens bund og badets overflade.
- 25 48. Reaktor ifølge krav 47, **kendetegnet ved, at** disse vertikale vægge strækker sig over en vertikal afstand, som svarer til 40% og 60% af denne samlede højde.
- 30 49. Reaktor ifølge krav 47 eller krav 48, **kendetegnet ved, at** reaktoren omfatter mindst to skillevægge, som strækker sig i det væsentlige over beholderens øvre halvdel, mellem strømledningsrøret og henholdsvis fluidindgangen og fluidudgangen for at tvinge den fluid, der skal behandles, til at strømme mindst én gang ind i midtzonen mellem fluidindgangen og fluidudgangen.
- 35 50. Reaktor ifølge et hvilket som helst af kravene 47 til 49, **kendetegnet ved, at** disse vertikale vægge strækker sig over højden, som ligger mellem planet af hovedfluidindgangen og planet af omrøreren.

51. Reaktor ifølge et hvilket som helst af kravene 47 til 50, **kendetegnet ved, at** de vertikale vægge strækker sig fra omkredsen af den perifere zone frem til røret.
- 5 52. Reaktor ifølge et hvilket som helst af kravene 37 til 51, **kendetegnet ved, at** indgangs- og udgangszonerne er anbragt i nærheden af planet af overfladen og er hver især forsynet med en plade, som er anbragt tværgående over for henholdsvis indgangen og udgangen for at danne en sifon.
- 10 53. Reaktor ifølge et hvilket som helst af kravene 31 til 52, **kendetegnet ved, at** den yderligere omfatter en studs til indsprøjtning af reaktivt flokkuleringsmiddel, som er forbundet med en kilde af reaktivt flokkuleringsmiddel.
- 15 54. Reaktor ifølge krav 53, **kendetegnet ved, at** denne studs til indsprøjtning af reaktivt flokkuleringsmiddel befinder sig mellem indgangen af råfluid, som skal behandles, og indgangen af strømledningsrøret.
- 20 55. Reaktor ifølge krav 53, **kendetegnet ved, at** den omfatter en rørformet studs til indsprøjtning af reaktivt flokkuleringsmiddel, som er anbragt koaksialt med indgangen af strømledningsrøret.
- 25 56. Reaktor ifølge et hvilket som helst af kravene 31 til 55, **kendetegnet ved, at** den yderligere omfatter en studs til indsprøjtning af pulverformet materiale, som er forbundet med en kilde af pulverformet materiale.
- 30 57. Reaktor ifølge krav 56, **kendetegnet ved, at** denne kilde af pulverformet materiale er en kilde af fint sand.
- 35 58. Reaktor ifølge et hvilket som helst af kravene 31 til 57, **kendetegnet ved, at** beholderen omfatter en enkelt flokkulationszone, som omfatter et strømledningsrør.
59. Anlæg til behandling af fluid, omfattende en reaktor ifølge et hvilket som helst af kravene 31 til 57 og en separationszone, der er forbundet af udgangen af beholderen af reaktoren.

5 **60.** Anlæg ifølge krav 59, **kendetegnet ved, at** reaktoren omfatter en studs til indsprøjtning af pulverformet materiale, som er forbundet med en kilde af pulverformet materiale, og separationszonen omfatter en udgang, der er indrettet til at optage slam med flokke, og forbundet med en indretning til genvinding af pulverformet materiale, hvor kilden af pulverformet materiale er forbundet med denne genvindingsindretning.

10 **61.** Anlæg ifølge krav 59 eller krav 60, **kendetegnet ved, at** separationszonen er en bundfældningsindretning, som er anbragt nedstrøms for beholderen.

62. Anlæg ifølge et hvilket som helst af kravene 59 til 61, **kendetegnet ved, at** separationszonen er en bundfældningsindretning, som er anbragt omkring beholderen.



