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CARL CRANZ GESELLSCHAFT e.V., Oberpfaffenhofen, DE, Lehrgang: "Sensoren in inertialen Mess- und Navigationssystemen", Braunschweig, DE, 17-21 October 1988; W.AUGH: "Faseroptische Rotationssensoren"

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Description**BACKGROUND OF THE INVENTION**

5 (Field of the Invention)

This invention relates to a phase modulated fiber-optic gyroscope according to the preamble of claim 1.

(Prior Art)

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The fiber-optic gyroscope is an apparatus for measuring the angular velocity of a moving object. Monochromatic light is launched at opposite ends of a coil of many turns of a single-mode optical fiber and is transmitted clockwise and counterclockwise simultaneously, with the light emerging from one end of the coil interfering with the light emerging from the other end. If the fiber-optic coil is rotating about its own axis, 15 a phase difference appears between the two light beams. Since this phase difference is proportional to the angular velocity of the rotation, one can determine the angular velocity of the rotation from the phase difference.

If the phase difference and angular velocity are written as $\Delta\theta$ and Ω , respectively, the following relationship holds:

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$$\Delta\theta = \frac{4\pi L a \Omega}{c \lambda} \quad (1)$$

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where L is the fiber length of the sensor coil, a is the coil diameter, c is the speed of the light in vacuum and λ is the wavelength of the light in vacuum. This effect is called the Sagnac effect and is well known.

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In practice, however, it is not easy to detect the phase difference $\Delta\theta$ because it contains non-rotational offsets inherent in the optical system. These offsets are subject to significant variations due to temperature changes. A further problem is that the output of a light-receiving device appears in the form of $(1 + \cos\Delta\theta)$ in a fiber-optic gyroscope of the most primitive design. This results in low sensitivity and failure to detect the direction of rotation if $\Delta\theta$ is small.

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To cope with these difficulties, three different types of fiber-optic gyroscopes have been proposed, which operate on the principles of frequency modulation, phase modulation and phase shift, respectively. The present invention relates to a fiber-optic gyroscope that operates on the principle of phase modulation.

The basic construction of a phase modulated fiber-optic gyroscope is described below with reference to Fig. 1. Phase modulation is produced from a piezoelectric device around which one end portion of the optical fiber cable in the sensor coil is wound. By picking up the first-order term of the modulated wave, the 40 phase difference can be determined in the form of $\sin\Delta\theta$.

Coherent light issuing from a light-emitting device 1 is split into two beams by a beam splitter 2. One of the two beams is converged by a coupling lens 4 and launched into end A of an optical fiber cable 5. This beam is transmitted through the sensor coil 6 counterclockwise. The other beam is converged by a coupling lens 3, launched into end B of the optical fiber 5 and transmitted through the sensor coil 6 45 clockwise.

The greater part of the optical fiber cable 5 forms the sensor coil 6 and only the part close to end B is wound around the piezoelectric device to form a phase modulation device 7.

An oscillator 10 produces an oscillating voltage that causes the piezoelectric device to expand or contract. The phase modulating part 8 of the optical fiber cable is wound onto the piezoelectric device, so it 50 will expand or contract together with the piezoelectric device to produce a light signal containing a modulated component.

The light beam transmitted clockwise through the phase modulating part 8 and the sensor coil 6 will emerge from end A, and the other beam transmitted counterclockwise through the sensor coil 6 and the phase modulating part 8 will emerge at end B. The emerging light beams are recombined by the beam 55 splitter 2 and launched as a single beam into a light-receiving device 9, which performs square-law detection on the light of interference.

Since the phase modulation device 7 is located asymmetrically with respect to the fiber-optic cable 5, the light being transmitted clockwise is phase-modulated at a slightly different time than the light being

transmitted counterclockwise. The time, τ , required for the light to pass through the sensor coil 6 is given by:

$$\tau = \frac{n L}{c} \quad (2)$$

where L is the fiber length of the sensor coil 6 and n is the refractive index of the fiber core. If the phase modulation device 7 is positioned close to end B, the light being transmitted clockwise will be first phase-modulated before it is launched into the sensor coil 6. On the other hand, the light being transmitted counterclockwise passes through the sensor coil 6 before it is launched into the phase modulation device 7.

Let us write Ω for the angular frequency of a modulating signal. Since the difference in time between the phase modulation caused by the device 7 and the launching of the light into the light-receiving device 9 is τ , the phase difference, ϕ , of the modulation signal contained in the light of interference is given by:

$$\phi = \Omega \tau \quad (3)$$

As described above, the Sagnac effect introduces a phase difference of $\Delta\theta$ between the light transmitted clockwise and the light transmitted counterclockwise, and the phase modulation applied on the two light beams creates an additional phase difference of ϕ in the phase-modulated portion.

If the amplitude due to the action of the phase modulation device 7 is written as b , the field strength E_R of the light transmitted clockwise is given by:

$$E_R = E_o \sin \left\{ \omega t + \frac{\Delta\theta}{2} + b \sin (\Omega t + \phi) \right\} \quad (4)$$

and the field strength E_L of the light transmitted counterclockwise is given by:

$$E_L = E_o \sin \left\{ \omega t - \frac{\Delta\theta}{2} + b \sin (\Omega t) \right\} \quad (5)$$

The two light beams having these field strengths are subjected to square-law detection in the light-receiving device 9. The output of the light-receiving device, $S(\Delta\theta, t)$, is given by:

$$S(\Delta\theta, t) = E_o^2 \cos \left\{ \Delta\theta + 2b \sin \frac{\phi}{2} \cos(\Omega t + \frac{\phi}{2}) \right\} + \text{D.C.} + \{\text{no less than } 2\omega\} \quad (6)$$

where D.C. denotes the dc component, and ω is the number of vibrations of light waves, with 2ω representing a component having twice the number of vibration ω . Such a fast signal cannot be detected by the light-receiving device 9 and hence is zero. The output signal from the light-receiving device 9 contains the phase-modulated component ϕ , so the phase difference $\Delta\theta$ can be determined in association with the amplitude of the modulation signal.

If the dc component is eliminated, $S(\Delta\theta, t)$ can be rewritten in the form of a sum as follows:

$$S(\Delta\theta, t) = E_o^2 [\cos \Delta\theta \cos \{2b \sin \frac{\phi}{2} \cos(\Omega t + \frac{\phi}{2})\} - \sin \Delta\theta \sin \{2b \sin \frac{\phi}{2} \cos(\Omega t + \frac{\phi}{2})\}] \quad (7)$$

This can be expanded in terms of Bessel functions. By the expansion of the generating function of Bessel functions, we obtain:

$$\exp \frac{x}{2} \left(t - \frac{1}{t} \right) = \sum_{n=-\infty}^{\infty} J_n(x) t^n \quad (8)$$

If $t = \exp i\theta$, we obtain:

$$\exp i \chi \sin \theta = \sum_{n=-\infty}^{\infty} J_n(X) e^{ni\theta} \quad (9)$$

By expanding the real and imaginary parts of equation (9), S_s which is the sine part of $S(\Delta\theta, t)$ and S_c which is its cosine part can be expanded into series. We define as follows;

$$S(\Delta\theta, t) = (S_c \cos \Delta\theta + S_s \sin \Delta\theta) E_o^2 \quad (10)$$

By performing conversion $\theta \rightarrow \theta + \pi/2$ and using the well known nature of Bessel functions, i.e.,

$$J_{-n}(X) = (-1)^n J_n(X) \quad (11)$$

(where n is a positive integer), together with the following substitution:

$$\xi = 2 b \sin \frac{\phi}{2} \quad (12)$$

We obtain:

$$S_c = J_0(\xi) + 2 \sum_{n=1}^{\infty} (-1)^n J_{2n}(\xi) \cos 2n\Omega t \quad (13)$$

$$S_s = 2 \sum_{n=0}^{\infty} (-1)^n J_{2n+1}(\xi) \cos(2n+1)\Omega t \quad (14)$$

By equations (13) and (14), the signal $S(\Delta\theta, t)$ can be rewritten as follows:

$$\begin{aligned} & + 2E_o^2 \sum_{n=1}^{\infty} (-1)^n J_{2n}(\xi) \cos 2n\Omega t \cdot \cos \Delta\theta \\ & + 2E_o^2 \sum_{n=0}^{\infty} (-1)^n J_{2n+1}(\xi) \cos(2n+1)\Omega t \sin \Delta\theta \end{aligned} \quad (15)$$

This is the expansion of the modulation frequency Ω by harmonic waves. A desired harmonic component can be obtained by passage through a filter. If the first-order term of the expansion is designated the fundamental component P and the second-order term designated as the second harmonic component Q , the following equations can be obtained:

$$P(t) = 2 E_o^2 J_1(\xi) \cos \Omega t \sin \Delta\theta \quad (16)$$

$$Q(t) = 2 E_o^2 J_2(\xi) \cos 2\Omega t \cos \Delta\theta \quad (17)$$

In most cases, the fundamental component P is detected to determine $\Delta\theta$. To attain a maximum sensitivity for P , $J_1(\xi)$ is maximized. To this end, the modulation index is set in such a way that $\xi = 1.8$. In this case, $J_0(\xi)$ is about 0.3.

The foregoing description concerns the basic construction of a phase modulated fiber-optic gyroscope operating.

When determining $\Delta\theta$ by detecting the fundamental component P , the modulation index ξ must be held constant. Otherwise, the value of $J_1(\xi)$ will fluctuate. A method heretofore proposed for maintaining a

constant value of modulation index consists of monitoring the second harmonic component Q to determine the value of $J_2(\xi)$. This method is described in Japanese Patent Application No. (JP-A-61-124817) 59-244641. Signal Ω and signal 2Ω which is an integral multiple of that signal are picked up from the drive circuit of a phase modulation device. The output of a light-receiving device is subjected to synchronous
 5 detection on the basis of these two signals. The detected output is passed through a low-pass filter to obtain a low-frequency component. The second harmonic component Q is:

$$Q = 2 E_o^2 J_2(\xi) \cos \Delta \theta \quad (18)$$

10 Since the modulation index ξ must be held constant, the phase modulation device is controlled in such a way that Q is constant. In other words, ξ is controlled to become 1.8. When ξ is 1.8, J_2 is about 0.3. If ξ becomes greater than 1.8, J_2 increases and vice versa. Hence, ξ can be adjusted to 1.8 by holding Q constant.

15 If the quantity of light from the light-emitting device is constant, $\Delta \theta$ can be immediately determined from $P(t)$ obtained by equation (16). In practice, however, the amplitude of the light, E_o , will fluctuate, so apparently different outputs will be produced for the same value of $\Delta \theta$ on account of fluctuations in the quantity of the light.

For the sake of simplicity, the foregoing discussion assumes that the two light beams, one transmitted clockwise and the other transmitted counterclockwise, have the same amplitude E_o . But this is not the case
 20 in practical situations. If it is necessary to distinguish the amplitudes of the two light beams, the amplitude of the light transmitted clockwise is written as E_1 and that of the light transmitted counterclockwise is written as E_2 . In other words, the square of E_o appearing in the previous discussion should be read $E_1 E_2$.

JP-A-60-135816 (the term "JP-A" as used herein means an "unexamined published Japanese patent application") proposes a control system that provides a constant dc component in output signal. But the
 25 problem associated with the quantity of reflected light is not discussed in this patent. By the term "reflected light" is meant those components of light which are reflected from the edge faces of lenses, fiber and other parts of the optical system. These components will not contribute to the measurement of angular velocity but simply become noise. In contrast, signal light passes through the sensor coil and contributes to the measurement of angular velocity.

30 The light-receiving device receives both signal light and reflected light. The reflected light does not pass through the sensor coil. The control system described in JP-A-60-135816 assumes either the absence of reflected light or the presence of reflected light that will vary in the same way as does the signal light. Only in that case is valid the statement that holding the dc component constant is equivalent to controlling the amplitude of the light to be constant. In practice, however, a quantity of reflected light that is by no
 35 means negligible is launched into the light-receiving device. Reflected light will not fluctuate in the same way as does the signal light, or one may say that it will hardly fluctuate. The phase modulation index will also sometimes fluctuate. Therefore, holding the dc component constant does not necessarily result in a constant amplitude of the signal light.

As already mentioned, the prior art fiber-optic gyroscope suffers the problem that substantial variations
 40 occur in the quantity of light that is issued from the light-emitting device to be launched into the optical fiber cable. In other words, substantial variations can occur in the amplitude E_o . Thus, apparently different outputs will be produced for the same angular velocity on account of these variations in the quantity of light.

JP-A-61-147106 proposes a control system that is capable of maintaining a constant level of the dc component in the signal. JP-A-60-135816 already cited above proposes that the effects of variations in the
 45 quantity of light be cancelled by dividing the phase-modulated frequency component of the signal by the dc component. A phase-modulated fiber-optic gyroscope that operates with the second harmonic component controlled to be constant has also been proposed (see the already cited Japanese Patent Application No. 59-244641). The second harmonic component contains $J_2(\xi)$ and holding it constant was considered to be equivalent to controlling the phase modulation index to become constant. However, holding the dc
 50 component constant is by no means equivalent to controlling the quantity of light to be constant. The dc component contains $\Delta \theta$ in the form of $\cos \Delta \theta$. The invention described in Japanese Patent Application No. 59-244641 adopts the approximation of $\Delta \theta \approx 0$ and controls the dc component to become constant on the assumption that it is proportional to the intensity of the light issuing from the light-emitting device. However, the phase difference $\Delta \theta$ sometimes has such a great magnitude that it cannot be neglected. If $\Delta \theta$ is
 55 substantial, the approximation of $\Delta \theta \approx 0$ will produce inaccuracy.

The approach of maintaining a constant value of the second harmonic component in order to hold the phase modulation index constant has the following problems.

As equation (17) shows, the second harmonic component Q has not only the $J_2(\xi)$ term but also the $\cos\Delta\theta$ term. The second harmonic component is held constant on the basis of the approximation that $\Delta\theta$ is nearly equal to zero. However, this approximation is by no means exact if $\Delta\theta$ is great. This will eventually result in failure to maintain a constant value of the phase modulation index.

Dividing the fundamental component by the dc component will cause the following additional problems. The dc component D of the light of interference which is the output of the light-receiving device can be written as:

$$D = \frac{1}{2} (E_1^2 + E_2^2) + E_1 E_2 J_0(\xi) \cos \Delta\theta + H \quad (19)$$

where H is the quantity of reflected light. If the modulated frequency component in equation (16) is eliminated and if E_0^2 is rewritten as $E_1 E_2$, the fundamental component P is given by:

$$P = 2 E_1 E_2 J_1(\xi) \sin \Delta\theta \quad (20)$$

In order to obtain correct results by dividing the fundamental component by the dc component, the following assumptions must be taken into account in addition to the problem of reflected light:

Assumption 1: There are no variations in the ratio of the quantity of the light transmitted clockwise to the quantity of the light transmitted counterclockwise;

Assumption 2: There are no variations in the phase modulation index.

If assumption 1 holds,

$$E_2 / E_1 = K \quad (21)$$

The dc component D can be rewritten as:

$$D = \frac{1}{2} (1 + K^2) E_1^2 + K E_1^2 J_0(\xi) \cos \Delta\theta \quad (22)$$

where the quantity of reflected light H is neglected. By dividing the fundamental component P by the dc component D, we obtain:

$$\frac{P}{D} = \frac{2 K J_1(\xi) \sin \Delta\theta}{\frac{1}{2} (1 + K^2) + K J_0(\xi) \cos \Delta\theta} \quad (23)$$

and the resulting output is independent of the quantity of the light emerging from the light-emitting device. Since K and $J_0(\xi)$ are known, $\Delta\theta$ can be determined. However, this relationship is established only when the above-mentioned assumptions hold and they are impractical.

Further, determination of $\Delta\theta$ from equation (23) involves quite complicated mathematical operations. This equation is by no means simple to deal with. One should also remember that the foregoing discussion disregards the quantity of the light inherent in the dc component.

A control system in which the constant DC component or the amplitude of the second harmonic of the output signal is additionally measured is also known from the following document: Carl Cranz Gesellschaft e.V., Oberpfaffenhofen, Lehrgang: "Sensoren in inertialen Mess-und Navigationssystemen", held in Braunschweig, DE, October 17-21, 1988; W. Auch: "Faseroptische Rotationssensoren", Teil 1.

The gyroscope according to the preamble of claim 1 is known from the EP-A-0 185 385. The phase modulation type fibre-optic gyroscope known from this reference has an improved output stability without a large increase in the number of basic components of the gyroscope system. The DC component of the output of a light detecting element which provides the two circulating beams is sensed and employed to control the output of the light emitting element so as to be constant.

It is the object of the present invention to provide a new phase modulation fibre-optic gyroscope which is improved over the prior art.

This object is solved by the features indicated in claim 1.

The fiber-optic gyroscope of the present invention may operate on the following principles:

(1) the gyroscope which is either at rest or rotating at an adequately small angular velocity is recognized by a signal coming either from the gyroscope itself or from another sensor;

(2) if the above condition or the amplitude of the second harmonic of the output signal is satisfied, the output of the light-emitting device is so controlled that the dc component of the output from the light-receiving device is held constant; and

(3) if the above condition or the amplitude of the second harmonic of the output signal is satisfied, the phase modulation index is so controlled that the second harmonic component of the output from the light-receiving device is held constant.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 shows the basic construction of a phase modulated prior art fiber-optic gyroscope;

Fig. 2 shows an example of the basic construction of the fiber-optic gyroscope of the present invention;

Fig. 3 shows diagrammatically another embodiment of the present invention;

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Fig. 2 shows an example of the basic construction of the phase modulated fiber-optic gyroscope of the present invention. A light-emitting device 101 is a light source of coherent light and may be composed of any apparatus such as a semiconductor laser, a super-luminescent diode or gas laser. A beam splitter 102 divides the coherent light from the light-emitting device 101 into two light beams. The term "beam splitter" is used herein to mean a light dividing device in its broad sense. The two split light beams are converged by lenses 103 and 104 and launched into an optical fiber cable 105 at opposite ends A and B. The optical fiber cable 105 is made of a single-mode optical fiber and includes a sensor coil 106 consisting of many turns of the optical fiber and a portion 108 wound around a phase modulation device 107. The sensor coil detects the angular velocity of rotation.

The phase modulation device 107 comprises a piezoelectric device, typically in cylindrical form, that is provided with electrodes on an outside and an inside surface and around which the optical fiber cable is wound. The phase modulation device 107 imparts periodic phase changes to the light being transmitted through the fiber-optic cable.

Between the electrodes are provided a modulation voltage of a frequency Ω from a phase modulation device excitation control unit 115. The amplitude of the applied voltage is proportional to the phase modulation index.

The light beam launched at end A is transmitted clockwise through the sensor coil 106, whereas the light beam launched at end B is transmitted counterclockwise. The two light beams emerging from the fiber-optic cable are re-combined by the beam splitter 102 and are launched as a single beam into a light-receiving device 109. The light-receiving device 109 detects the intensity of the light of interference and produces it as an output. The output from the light-receiving device contains the dc component D, the fundamental component P, the second harmonic component Q and harmonics of higher orders.

The dc component D is detected by a dc component detector 110. The detected signal is sent to a dc component control unit 112. The dc component is used to stabilize the output of the light-emitting device but it does not always control the latter. It is used to control the output of the light-emitting device only if a stop signal U is applied from another sensor or when the final output S of the gyroscope per se is zero.

The dc component control unit 112 supplies a light-emitting device control circuit 113 with a drive current W for the light-emitting device. The control unit 112 controls the dc component D of the output from the light-receiving device in such a way that said dc component is held constant when a stop signal U is supplied or when the final output S is zero. It should, however, be noted that the stop signal U need not refer to a "stop" in the strict sense of the term and a state close to "stop" may also be indicated. The same is true with the final output S and it need only be close to zero.

The dc component control unit 112 stores the dc component D when the gyroscope is either stopped or in a state close to stop; it then compares the stored dc component with a predetermined value D_0 and supplies a command to the light-emitting device output control circuit 113 so that the stored dc component will approach the predetermined value D_0 .

The fundamental component P of the output from the light-receiving device 109 is detected by the fundamental detector 117. A sync signal is supplied from the phase modulation device excitation control unit 115. The second harmonic component Q of the output from the light-receiving device 109 is detected by a second harmonic detector 111. The modulation signal from the control unit 115 is doubled in a multiplier 120 to produce a sync signal.

The modulation index of the control unit 115 is controlled in such a way as to provide a constant level of the second harmonic component. The modulation index is theoretically expressed by b but since it is proportional to ξ , ξ may also be designated as the modulation index. The second harmonic component is not always controlled to be constant. Only when a stop signal U is supplied from another sensor or if the final output S from the gyroscope is either equal or close to zero is the second harmonic component controlled to become equal to a predetermined value Q_0 .

Such an intermittent control is performed by a second harmonic control unit 114. The gyroscope which is at rest or in a state very close to it is identified by the supply of either a stop signal from another sensor or a substantially zero output S from the gyroscope. The value of the second harmonic component Q in that instance is adopted by the control unit 114 which compares it with Q_0 and supplies the modulation index ξ of the phase modulation device excitation control unit 115 in such a way that the difference between Q and Q_0 will be minimized.

The fundamental component P appears as the output of the fundamental detector 117, which serves as the final output S . This is equivalent to equation (16) except that the vibration term is eliminated:

$$S = P = 2 E_0^2 J_1(\xi) \sin \Delta\theta \quad (24)$$

By controlling the dc component to be constant, the intensity of the light E_0^2 can be held constant. By controlling the second harmonic component to be constant, the phase modulation index ξ can be held constant. Thus, the coefficients in equation (24) are held constant, and $\Delta\theta$ can be determined from the final output S in the form of $\sin\Delta\theta$.

In the foregoing discussion, the second harmonic component is detected and controlled to be constant in order to maintain a constant level of the phase modulation index. It should, however, be noted that in place of the second harmonic component, the third or fourth harmonic component may be controlled to be constant in order to maintain a constant level of the phase modulation index. This is possible since all the harmonics of interest contain the phase modulation index.

In the previous discussion of the operation of the fiber-optic gyroscope based on phase modulation, the amplitudes of the two light beams transmitted clockwise and counterclockwise were collectively written as E_0 without being distinguished from each other. In the discussion that follows, the amplitude of the light transmitted clockwise is written as E_1 and that of the light transmitted counterclockwise is written as E_2 . Thus, E_0^2 appearing in the previous discussion should in all instances be read $E_1 E_2$.

The dc component D of the output from the light-receiving device can be rewritten as:

$$\frac{1}{2} (E_1^2 + E_2^2) + E_1 E_2 J_0(\xi) \cos\Delta\theta \quad (25)$$

In the actual optical system, the amplitude of the light transmitted clockwise is substantially equal to that of the light transmitted counterclockwise as expressed below:

$$E_1 \approx E_2 \quad (26)$$

Thus, the following assumption will hold:

$$\frac{1}{2} (E_1^2 + E_2^2) \approx E_1 E_2 \quad (27)$$

The modulation index ξ may assume any value but here a special case is considered. In order to maximize the sensitivity for the fundamental component, the first-order Bessel function $J_1(\xi)$ need be maximized, with ξ selected at a value of approximately 1.8. In this case, the zero-order Bessel function $J_0(\xi)$ is approximately 0.3. The dc component D is therefore written as:

$$D = E_1 E_2 (1 + 0.3 \cos \Delta\theta) \quad (28)$$

When the fiber-optic gyroscope is either at rest or nearly at rest,

$$\Delta\theta \approx 0 \quad (29)$$

$$\cos \Delta\theta \approx 1 \quad (30)$$

Hence, when the gyroscope is either at rest or nearly at rest,

$$D = 1.3 E_1 E_2 \quad (31)$$

and by controlling D to become equal to the predetermined D_0 , the quantity of the light of interference, $E_1 E_2$, can be held constant. This is accomplished by the dc component detector 110, the dc component control unit 112, the light-emitting device output control circuit 113, and other associated components shown in Fig. 2.

We now describe the control of the second harmonic component Q, which is given by:

$$Q = -2E_1 E_2 J_2(\xi) \cos\Delta\theta \quad (32)$$

In equation (32), $E_1 E_2$ which is the quantity of light issuing from the light-emitting device is already constant. When the gyroscope is either at rest or in a state very close to it, $\cos\Delta\theta$ is unity. In this case,

$$Q = -2E_1 E_2 J_2(\xi) \quad (33)$$

The excitation voltage to be applied to the phase modulation device excitation control unit 15 is so controlled as to bring Q to a constant value. If the phase modulation index ξ can be controlled to be constant, the final output S or the fundamental component P is expressed as follows from equation (24):

$$S = P = 2 E_1 E_2 J_1(\xi) \sin \Delta\theta \quad (34)$$

The coefficients preceding $\sin\Delta\theta$ are invariable constants and the exact value of $\Delta\theta$ can be determined from the output S. This effect can never be attained simply by controlling the quantity of light or the modulation index alone.

Fig. 3 shows another embodiment of the present invention which employs the construction shown in Fig. 2. The components which are the same as those shown in Fig. 2 are identified by like numerals and will not be described in detail.

The dc component detector 110 is supplied with the output from the light-receiving device 109 and produces the dc component of said output as a voltage signal, which is converted to a digital signal in an A/D converter 122.

When the gyroscope receives a stop signal from another sensor or in response to a zero or nearly zero final output S from the gyroscope per se, the following operations are performed. A control signal for controlling the quantity of the light issuing from the light-emitting device in such a way that the dc component D becomes equal to the preset value D_0 is calculated and constructed. This control signal is converted to an analog signal in a D/A converter 121 and supplied to the light-emitting device output control circuit 113.

When the gyroscope is rotating at fast speed, the control signal constructed for the previous case where the gyroscope was at rest is retained and delivered as an output. Since it is handled as a digital signal by a digital processing unit 116, the control signal can be easily retained and continuously supplied as an output.

In response to this control signal, the light-emitting device output control circuit 113 controls the quantity of the light emerging from the light-emitting device.

An oscillator 118 generates a modulation signal having a frequency Ω . The output of the oscillator 118 is fed to a multiplier 119 where it is amplified by an appropriate factor. The amplified phase modulation signal is applied to the electrodes of the phase modulation device 107. Hence, ξ or the modulation amplitude b which is to be provided by the phase modulation device 107 can be freely adjusted by controlling the factor of amplification with the multiplier 119.

In response to the sync signal ($f = \Omega$) from the oscillator 118, the fundamental detector 117 elicits the fundamental component P from the output of the light-receiving device. The fundamental component P is fed to an A/D converter 124 and thence supplied into the digital processing unit 116.

Multiplier 120 multiplies the phase modulation signal from the oscillator 118 to form a sync signal having a frequency of 2Ω . In response to the sync signal ($f = 2\Omega$) from the multiplier 120, the second harmonic detector 111 detects the second harmonic component Q of the output from the light-receiving device. The detected signal is fed to an A/D converter 125 where it is converted to a digital signal which is thereafter supplied to the digital processing unit 116.

When the fiber-optic gyroscope is at rest or in a state very close to it, the digital processing unit 116 recognizes this situation either by its own final output S or in response to a stop signal U supplied from another sensor. In the latter case, a state signal from another sensor is supplied into the digital processing

unit 116 through a state signal detecting interface 126. The digital processing unit 116 then determines as to whether the applied state signal indicates that the gyroscope is at rest and if this is the case, a stop signal U is constructed. Alternatively, another sensor may itself produce a stop signal U when the gyroscope is at rest, which stop signal is then supplied into the digital processing unit 116. Of course, the gyroscope may itself produce a final output S which is nearly equal to zero.

When the fiber-optic gyroscope is at rest or in a state very close to it, the digital processing unit 116 performs the following two operations. First, it compares the dc component D with the preset reference D_0 and controls the output of the light-emitting device in such a way that the difference is minimized. The control signal is supplied into the light-emitting device output control unit 113 through the D/A converter 121. Second, the processing unit compares the second harmonic component Q with the preset reference Q_0 and controls the phase modulation index ξ in such a way that the difference is minimized. The control signal is supplied into the multiplier 119 through the D/A converter 123.

When the gyroscope is rotating at high speed, the values of the dc component and the second harmonic component for the previous case where the gyroscope was at rest are retained by the processing unit, which keeps supplying the respective values to the control unit 113 and the multiplier 119.

The angular velocity of the rotating gyroscope can be determined from the fundamental component P.

Claims

1. Phase modulated fibre-optic gyroscope for measuring the angular velocity of a moving object, comprising:

phase modulation means (107);

fibre-optic cable means (105) having two ends, said fibre-optic cable means comprising a sensor coil (106) and a portion (108) provided with said phase modulation means located asymmetrically with respect to said fibre-optic cable means;

light emitting device (101) for emitting coherent light;

beam splitter means (102) for splitting the coherent light from said light emitting device into two beams which are launched into the two ends of said fibre-optic cable means, and for re-combining the light beams transmitted through said fibre-optic cable means (105);

light receiving means (109) for receiving from the two ends of said fibre-optic cable means the light beams that have been transmitted through said fibre-optic cable means and that are recombined by said beam splitter means;

DC component detector means (110) that receives the output signal of said light receiving means for detecting the DC component of the output signal; and

synchronous detector means (111, 117) for receiving an output signal from said light receiving means for detecting a phase modulated frequency component of the output signal of said light receiving means;

characterised in that

said synchronous detector means comprise harmonic detector means (111) for detecting a harmonic component having a frequency which is an appropriate integral multiple of the angular phase modulation frequency, Ω , and

fundamental detector means (117) for detecting a fundamental component of the output signal, i.e. the first order term of the expansion of the modulation frequency Ω by harmonic waves, from said light receiving means; and in that the gyroscope further comprises means (112,113,114) for controlling both the output signal of said light emitting means and a phase modulation index, ξ , to bring the DC component and the harmonic component, in the case where the gyroscope is nearly at rest, close to respective predetermined values, the phase modulation index ξ being related to the amplitude, b, due to the action of the phase modulation means (107) and to the phase difference, ϕ , due to the difference in time, τ , of effecting said action on said two beams by the equations

$$\xi = 2b \sin \frac{\phi}{2} = 2b \sin \frac{\Omega \tau}{2} .$$

2. A phase modulated fibre-optic gyroscope as claimed in claim 1, further comprising means (112,113) for holding the DC component of the output signal from said light receiving means when the gyroscope is nearly at rest and for controlling the output signal of said light emitting means so that a level of the held DC component is held constant.

3. A phase modulated fibre-optic gyroscope as claimed in claim 1 or 2, further comprising means (114) for holding a second harmonic component Q of the output signal from said light receiving means when the gyroscope is nearly at rest, and for controlling the phase modulation index so that a level of the second harmonic component Q is held constant.

5

Patentansprüche

1. Phasenmoduliertes Faseroptikgyroskop zum Messen der Winkelgeschwindigkeit eines sich bewegendes Objektes, mit:

10 einer Phasenmodulationseinrichtung (107);

einer Faseroptikkabeleinrichtung (105) mit zwei Enden, wobei die Faseroptikkabeleinrichtung eine Sensorspule (106) und einen Abschnitt (108) umfaßt, welcher mit der Phasenmodulationseinrichtung versehen ist, die asymmetrisch in bezug auf die Faserkabeleinrichtung angeordnet ist;

einer Lichtemissionseinrichtung (101) zum Emittieren von kohärentem Licht;

15 einer Strahlteilereinrichtung (102) zum Aufspalten des kohärenten Lichts aus der Lichtemissionseinrichtung in zwei Strahlen, welche in die zwei Enden der Faseroptikkabeleinrichtung eingespeist werden, und zum Rekombinieren der durch die Faseroptikkabeleinrichtung (105) übertragenen Lichtstrahlen;

einer Lichtempfangseinrichtung (109) zum Empfangen der Lichtstrahlen von den zwei Enden der Faseroptikkabeleinrichtung, welche durch die Faseroptikkabeleinrichtung übertragen worden und welche durch die Strahlteilereinrichtung rekombiniert sind;

20 einer Gleichspannungskomponentendetektoreinrichtung (110), welche das Ausgangssignal der Lichtempfangseinrichtung zum Erfassen der Gleichspannungskomponente des Ausgangssignals empfängt, und

einer Synchrondetektoreinrichtung (111, 117) zum Empfangen eines Ausgangssignals aus der Lichtempfangseinrichtung zum Erfassen einer phasenmodulierten Frequenzkomponente des Ausgangssignals der Lichtempfangseinrichtung;

25

dadurch gekennzeichnet,

daß die Synchrondetektoreinrichtung eine harmonische Detektoreinrichtung (111) zum Erfassen einer harmonischen Komponente mit einer Frequenz, welche ein geeignetes ganzzahliges Vielfaches der Winkelphasenmodulationsfrequenz Ω ist, und eine Fundamentaldetektoreinrichtung (117) zum Erfassen einer Grundkomponente des Ausgangssignals, d.h. des Terms erster Ordnung der Entwicklung der Modulationsfrequenz Ω durch harmonische Wellen, aus der Lichtempfangseinrichtung umfaßt; und

30

daß das Gyroskop ferner eine Einrichtung (112, 113, 114) zum Steuern sowohl des Ausgangssignals der Lichtemissionseinrichtung als auch eines Phasenmodulationsindex ξ umfaßt, um die Gleichspannungskomponente und die harmonische Komponente, in dem Fall, in welchem das Gyroskop nahezu im Ruhezustand ist, nahe an jeweilige vorbestimmte Werte zu bringen, wobei der Phasenmodulationsindex ξ auf die Amplitude, b, infolge der Wirkung der Phasenmodulationseinrichtung (107), und auf die Phasendifferenz, ϕ , infolge der Zeitdifferenz, τ , der Realisierung dieser Wirkung auf die zwei Strahlen bezogen ist durch die Gleichung:

40

$$\xi = 2 b \sin \frac{\phi}{2} = 2 b \sin \frac{\Omega \tau}{2} .$$

2. Ein phasenmoduliertes Faseroptikgyroskop nach Anspruch 1, welches ferner eine Einrichtung (112, 113) zum Halten der Gleichspannungskomponente des Ausgangssignals aus der Lichtempfangseinrichtung, wenn das Gyroskop nahezu im Ruhezustand ist, und zum Steuern des Ausgangssignals der Lichtemissionseinrichtung, so daß ein Niveau der gehaltenen Gleichspannungskomponente konstant gehalten wird, umfaßt.

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3. Ein phasenmoduliertes Faseroptikgyroskop nach Anspruch 1 oder 2, welches ferner eine Einrichtung (114) zum Halten einer zweiten harmonischen Komponente Q des Ausgangssignals aus der Lichtempfangseinrichtung, wenn das Gyroskop nahezu im Ruhezustand ist, und zum Steuern des Phasenmodulationsindex, so daß ein Niveau der zweiten harmonischen Komponente Q konstant gehalten wird, umfaßt.

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Revendications

1. Gyroscopie à fibre optique modulé en phase pour mesurer la vitesse angulaire d'un objet mobile, comprenant :

5 un moyen de modulation de phase (107) ;
 un moyen de câble à fibre optique (105) comportant deux extrémités, ledit moyen de câble à fibre optique comprenant une bobine de capteur (106) et une partie (108) munie dudit moyen de modulation de phase positionné de façon asymétrique par rapport audit moyen de câble à fibre optique ;
 un dispositif émetteur de lumière (101) pour émettre une lumière cohérente ;
 10 un moyen de séparateur de faisceau (102) pour séparer la lumière cohérente provenant dudit dispositif émetteur de lumière selon deux faisceaux qui sont envoyés dans les deux extrémités dudit moyen de câble à fibre optique et pour recombiner les faisceaux lumineux transmis au travers dudit moyen de câble à fibre optique (105) ;
 un moyen de réception de lumière (109) pour recevoir depuis les deux extrémités dudit moyen de
 15 câble à fibre optique les faisceaux lumineux qui ont été transmis au travers dudit moyen de câble à fibre optique et qui sont recombinés par ledit moyen de séparateur de faisceau ;
 un moyen de détecteur de composante continue (110) qui reçoit le signal de sortie dudit moyen de réception de lumière pour détecter la composante continue du signal de sortie ; et
 un moyen de détecteur synchrone (111, 117) pour recevoir un signal de sortie provenant dudit
 20 moyen de réception de lumière pour détecter une composante de fréquence modulée en phase du signal de sortie dudit moyen de réception de lumière,
 caractérisé en ce que :
 ledit moyen de détecteur synchrone comprend un moyen de détecteur d'harmonique (111) pour
 25 détecter une composante d'harmonique présentant une fréquence qui est un multiple entier approprié de la fréquence de modulation de phase angulaire, soit Ω ; et
 un moyen de détecteur d'onde fondamentale (117) pour détecter une composante fondamentale du signal de sortie, c'est-à-dire le terme de premier ordre du développement de la fréquence de modulation Ω selon des ondes d'harmoniques, provenant dudit moyen de réception de lumière ; et en ce que
 30 le gyroscope comprend en outre un moyen (112, 113, 114) pour commander à la fois le signal de sortie dudit moyen émetteur de lumière et un indice de modulation de phase ξ pour amener la composante continue et la composante d'harmonique, dans le cas où le gyroscope est pratiquement au repos, proches de valeurs respectives prédéterminées, l'indice de modulation de phase ξ étant rapporté à l'amplitude b du fait de l'action du moyen de modulation de phase (107) et à la différence de phase
 35 ϕ du fait de la différence temporelle τ de réalisation de ladite action sur lesdits deux faisceaux par les équations :

$$\xi = 2b \sin \frac{\phi}{2} = 2b \sin \frac{\Omega \tau}{2} .$$

- 40 2. Gyroscopie à fibre optique modulé en phase selon la revendication 1, comprenant en outre un moyen (112, 113) pour bloquer la composante continue du signal de sortie provenant dudit moyen de réception de lumière lorsque le gyroscope est pratiquement au repos et pour commander le signal de sortie dudit moyen d'émetteur de lumière de telle sorte qu'un niveau de la composante continue
 45 bloquée soit maintenu constant.
3. Gyroscopie à fibre optique modulé en phase selon la revendication 1 ou 2, comprenant en outre un moyen (114) pour bloquer une composante d'harmonique d'ordre deux Q du signal de sortie provenant dudit moyen de réception de lumière lorsque le gyroscope est pratiquement au repos et pour
 50 commander l'indice de modulation de phase de telle sorte qu'un niveau de la composante d'harmonique d'ordre deux Q soit maintenu constant.

FIG. 1 PRIOR ART

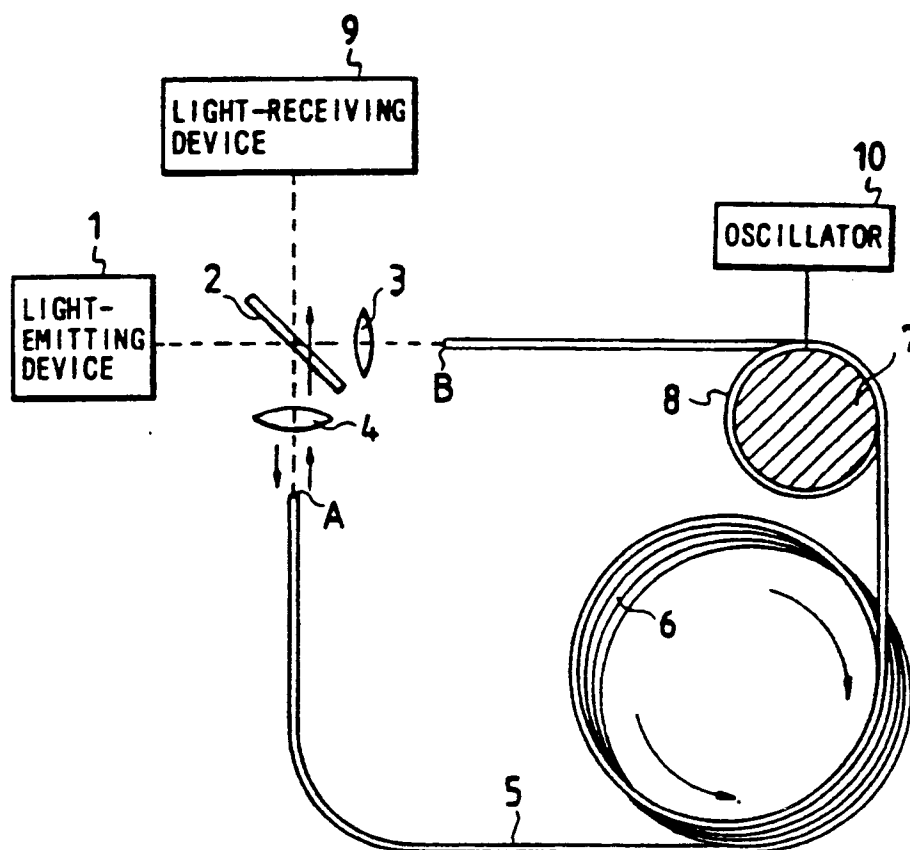


FIG. 2

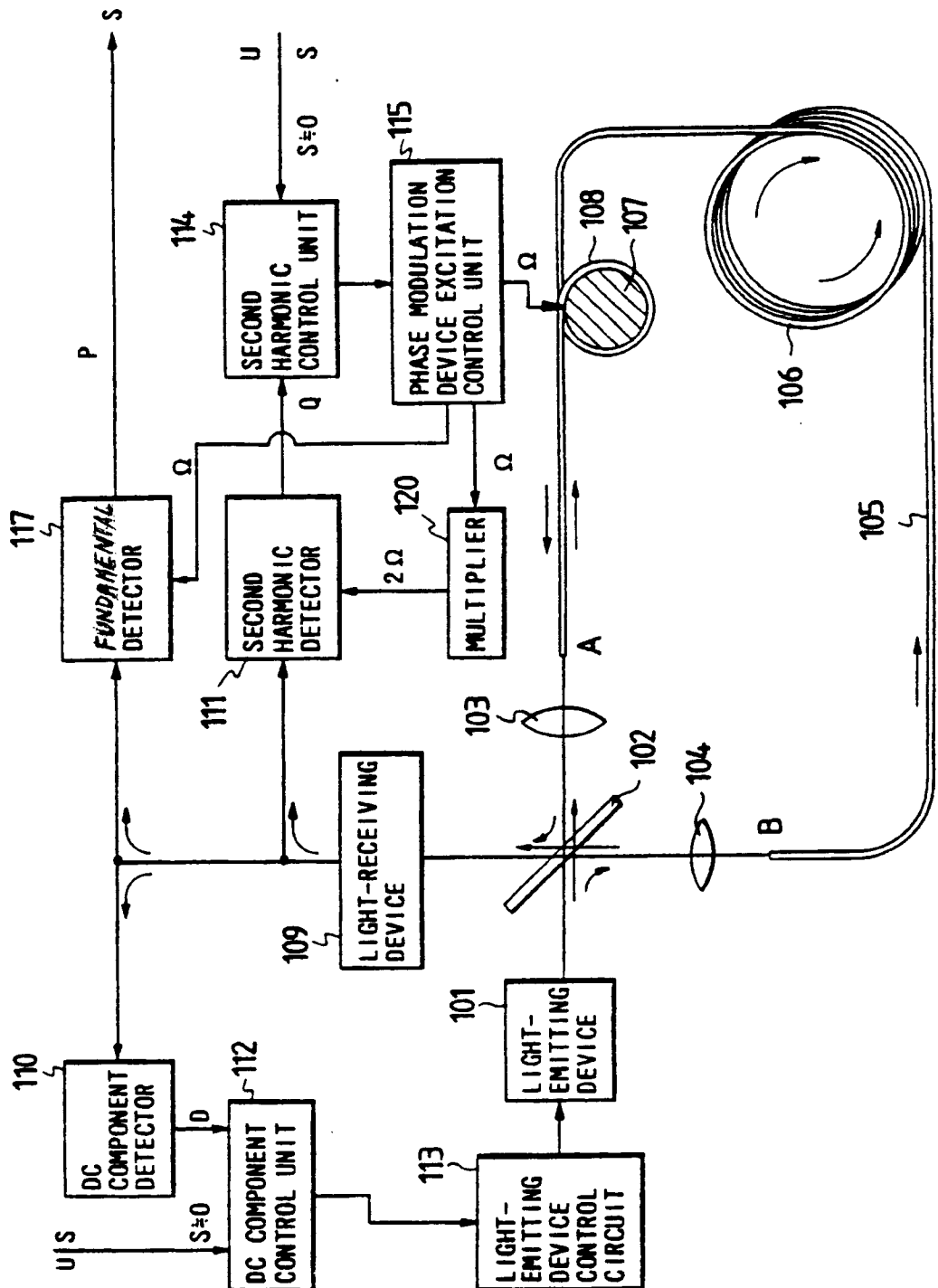


FIG. 3

