



- (51) International Patent Classification:
F16D 27/09 (2006.01)
- (21) International Application Number:
PCT/US2016/014243
- (22) International Filing Date:
21 January 2016 (21.01.2016)
- (25) Filing Language: English
- (26) Publication Language: English
- (30) Priority Data:
14/675,853 1 April 2015 (01.04.2015) US
- (71) Applicant: MEANS INDUSTRIES, INC. [US/US]; 3715 E. Washington Road, Saginaw, Michigan 48601-2893 (US).
- (72) Inventors: KIMES, John W.; 34633 Ash Street, Wayne, Michigan 48184 (US). HENDRICK, Terry O.; 6414 Garfield Ave., Cass City, Michigan 48726 (US).

(74) Agents: SYROWIK, David R. et al.; Brooks Kushman, 1000 Town Center, Twenty-Second Floor, Southfield, Michigan 48075 (US).

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, JP, KE, KG, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK,

[Continued on next page]

(54) Title: ELECTRONIC VEHICULAR TRANSMISSION, CONTROLLABLE COUPLING ASSEMBLY AND COUPLING MEMBER FOR USE IN THE ASSEMBLY

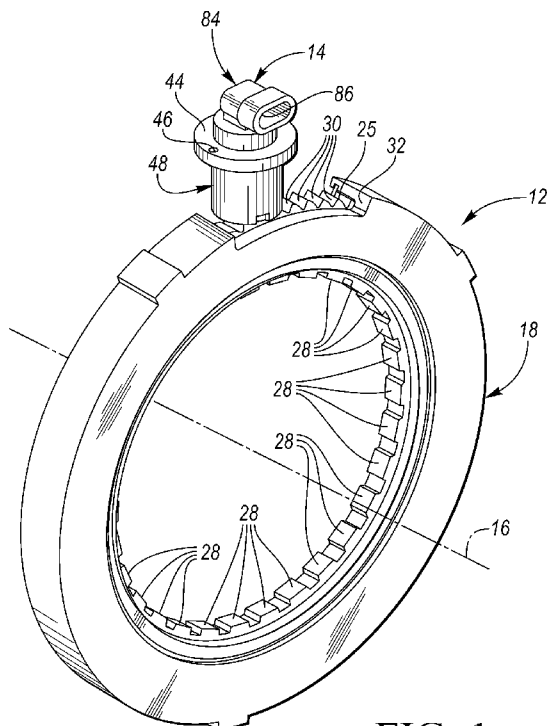


FIG. 1

(57) Abstract: An electronic vehicular transmission, a controllable coupling assembly and a coupling member for use in the assembly are provided. The member is configured for rotation about a rotational axis and includes a first coupling face oriented to face axially along the axis and has a set of pockets angularly-spaced about the axis. Each of the pockets receives a first locking element and defines a first load-bearing surface adapted for abutting engagement with a load-bearing surface of its respective first locking element. A second coupling face is oriented to face radially with respect to the axis and has a set of locking formations. Each of the set of locking formations defines a second load-bearing surface adapted for abutting engagement with a load-bearing surface of a second locking element.

WO 2016/160101 A1

SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG). — *as to the applicant's entitlement to claim the priority of the earlier application (Rule 4.17(iii))*

Declarations under Rule 4.17:

— *as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii))*

Published:

— *with international search report (Art. 21(3))*

ELECTRONIC VEHICULAR TRANSMISSION, CONTROLLABLE COUPLING ASSEMBLY
AND COUPLING MEMBER FOR USE IN THE ASSEMBLY

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application is a continuation of U.S. application Serial No. 14/675,853 filed April 1, 2015; this application is also continuation-in-part of U.S. application Serial No. 14/288,819 filed May 28, 2014, now pending, which claims benefit of U.S. provisional application Serial No. 61/941,741 filed February 19, 2014 and claims benefit of U.S. provisional application Serial No. 61/870,434 filed August 27, 2013; this application is also a continuation-in-part of U.S. application Serial No. 13/992,785 filed June 10, 2013 which is a 371 of PCT/US2011/036634 filed May 16, 2011, which claims benefit of U.S. provisional application Serial No. 61/421,856 filed December 10, 2010. This application is also a continuation-in-part of U.S. application Serial No. 14/300,275 filed June 10, 2014 which claims benefit of U.S. provisional application Serial No. 61/870,434 filed August 27, 2013.

TECHNICAL FIELD

[0002] This invention generally relates to electronic vehicular transmissions, controllable coupling assemblies and coupling members for use in such assemblies.

Overview

[0003] Coupling assemblies such as clutches are used in a wide variety of applications to selectively couple power from a first rotatable driving member, such as a driving disk or plate, to a second, independently rotatable driven member, such as a driven disk or plate. In one known variety of clutches, commonly referred to as “one-way” or “overrunning” clutches, the clutch engages to mechanically couple the driving member to the driven member only when the driving member rotates in a first direction relative to the driven member. Further, the clutch otherwise permits the driving member to freely rotate in the second direction relative to the driven member. Such “freewheeling” of the driving member in the second direction relative to the driven member is also known as the “overrunning” condition.

[0004] One type of one-way clutch includes coaxial driving and driven plates having generally planar clutch faces in closely spaced, juxtaposed relationship. A plurality of recesses or pockets is formed in the face of the driving plate at angularly spaced locations about the axis, and a strut or pawl is disposed in each of the pockets. Multiple recesses or notches are formed in the face of the driven plate and are engageable with one or more of the struts when the driving plate is rotating in a first direction. When the driving plate rotates in a second direction opposite the first direction, the struts disengage the notches, thereby allowing freewheeling motion of the driving plate with respect to the driven plate.

[0005] When the driving plate reverses direction from the second direction to the first direction, the driving plate typically rotates relative to the driven plate until the clutch engages. As the amount of relative rotation increases, the potential for an engagement noise also increases.

[0006] Controllable or selectable one-way clutches (i.e., OWCs) are a departure from traditional one-way clutch designs. Selectable OWCs add a second set of locking members in combination with a slide plate. The additional set of locking members plus the slide plate adds multiple functions to the OWC. Depending on the needs of the design, controllable OWCs are capable of producing a mechanical connection between rotating or stationary shafts in one or both directions. Also, depending on the design, OWCs are capable of overrunning in one or both directions. A controllable OWC contains an externally controlled selection or control mechanism. Movement of this selection mechanism can be between two or more positions which correspond to different operating modes.

[0007] U.S. Patent No. 5,927,455 discloses a bi-directional overrunning pawl-type clutch, U.S. Patent No. 6,244,965 discloses a planar overrunning coupling, and U.S. Patent No. 6,290,044 discloses a selectable one-way clutch assembly for use in an automatic transmission. U.S. Patent Nos. 7,258,214 and 7,344,010 disclose overrunning coupling assemblies, and U.S. Patent No. 7,484,605 discloses an overrunning radial coupling assembly or clutch.

[0008] A properly designed controllable OWC can have near-zero parasitic losses in the “off” state. It can also be activated by electro-mechanics and does not have either the complexity or parasitic losses of a hydraulic pump and valves.

[0009] In a powershift transmission, tip-in clunk is one of most difficult challenges due to absence of a torque converter. When the driver tips-in, i.e., depresses the accelerator pedal following a coast condition, gear shift harshness and noise, called clunk, are heard and felt in the passenger compartment due to the mechanical linkage, without a fluid coupling, between the engine and powershift transmission input. Tip-in clunk is especially acute in a parking-lot maneuver, in which a vehicle coasting at low speed is then accelerated in order to maneuver into a parking space.

[0010] In order to achieve good shift quality and to eliminate tip-in clunk, a powershift transmission should employ a control strategy that is different from that of a conventional automatic transmission. The control system should address the unique operating characteristics of a powershift transmission and include remedial steps to avoid the objectionable harshness yet not interfere with driver expectations and performance requirements of the powershift transmission. There is a need to eliminate shift harshness and noise associated with tip-in clunk in a powershift transmission.

[0011] For purposes of this disclosure, the term “coupling” should be interpreted to include clutches or brakes wherein one of the plates is drivably connected to a torque delivery element of a transmission and the other plate is drivably connected to another torque delivery element or is anchored and held stationary with respect to a transmission housing. The terms “coupling”, “clutch” and “brake” may be used interchangeably.

[0012] A pocket plate may be provided with angularly disposed recesses or pockets about the axis of the one-way clutch. The pockets are formed in the planar surface of the pocket plate. Each pocket receives a torque transmitting strut, one end of which engages an anchor point in a pocket of the pocket plate. An opposite edge of the strut, which may hereafter be referred to as an active edge, is movable from a position within the pocket to a position in which the active edge extends outwardly from the planar surface of the pocket plate. The struts may be biased away from the pocket plate by individual springs.

[0013] A notch plate may be formed with a plurality of recesses or notches located approximately on the radius of the pockets of the pocket plate. The notches are formed in the planar surface of the notch plate.

[0014] Another example of an overrunning planar clutch is disclosed in U.S. Pat. No. 5,597,057.

[0015] Some U.S. patents related to the present invention include: U.S. Patent Nos. 4,056,747; 5,052,534; 5,070,978; 5,449,057; 5,486,758; 5,678,668; 5,806,643; 5,871,071; 5,918,715; 5,964,331; 5,979,627; 6,065,576; 6,116,394; 6,125,980; 6,129,190; 6,186,299; 6,193,038; 6,386,349; 6,481,551; 6,505,721; 6,571,926; 6,814,201; 7,153,228; 7,275,628; 8,051,959; 8,196,724; and 8,286,772.

[0016] Yet still other related U.S. patents include: U.S. Pat. Nos. 4,200,002; 5,954,174; and 7,025,188.

[0017] U.S. Pat. No. 6,854,577 discloses a sound-dampened, one-way clutch including a plastic/steel pair of struts to dampen engagement clunk. The plastic strut is slightly longer than the steel strut. This pattern can be doubled to dual engaging. This approach has had some success. However, the dampening function stopped when the plastic parts became exposed to hot oil over a period of time.

[0018] Metal injection molding (MIM) is a metalworking process where finely-powdered metal is mixed with a measured amount of binder material to comprise a `feedstock` capable of being handled by plastic processing equipment through a process known as injection mold forming. The molding process allows complex parts to be shaped in a single operation and in high volume. End products are commonly component items used in various industries and applications. The nature of MIM feedstock flow is defined by a science called rheology. Current equipment capability requires processing to stay limited to products that can be molded using typical volumes of 100 grams or less per "shot" into the mold. Rheology does allow this "shot" to be distributed into multiple cavities, thus becoming cost-effective for small, intricate, high-volume products which would otherwise be quite expensive to produce by alternate or classic methods. The variety of metals capable of implementation within MIM feedstock are referred to as powder metallurgy, and these contain the same alloying constituents found in industry standards for common and exotic metal applications. Subsequent conditioning operations are performed on the molded shape, where the binder material is removed and the metal particles are coalesced into the desired state for the metal alloy.

[0019] Other U.S. patent documents related to at least one aspect of the present invention includes U.S. Patent Nos. 8,813,929; 8,491,440; 8,491,439; 8,286,772; 8,272,488; 8,187,141; 8,079,453; 8,007,396; 7,942,781; 7,690,492; 7,661,518; 7,455,157; 7,455,156; 7,451,862; 7,448,481; 7,383,930; 7,223,198; 7,100,756; and 6,290,044; and U.S. published application Nos. 2015/0000442; 2014/0305761; 2013/0277164; 2013/0062151; 2012/0152683; 2012/0149518; 2012/0152687; 2012/0145505; 2011/0233026; 2010/0105515; 2010/0230226; 2009/0233755; 2009/0062058; 2009/0211863; 2008/0110715; 2008/0188338; 2008/0185253; 2006/0124425; 2006/0249345; 2006/0185957; 2006/0021838, 2004/0216975; and 2005/0279602.

[0020] Some other U.S. patent documents related to at least one aspect of the present invention includes U.S. Patent Nos. 8,720,659; 8,418,825; 5,996,758; 4,050,560; 8,061,496; 8,196,724; and U.S. published application Nos. 2014/0190785; 2014/0102844; 2014/0284167; 2012/0021862; 2012/0228076; 2004/0159517; and 2010/0127693.

[0021] As used herein, the term “sensor” is used to describe a circuit or assembly that includes a sensing element and other components. In particular, as used herein, the term “magnetic field sensor” is used to describe a circuit or assembly that includes a magnetic field sensing element and electronics coupled to the magnetic field sensing element.

[0022] As used herein, the term “magnetic field sensing element” is used to describe a variety of electronic elements that can sense a magnetic field. The magnetic field sensing elements can be, but are not limited to, Hall effect elements, magnetoresistance elements, or magnetotransistors. As is known, there are different types of Hall effect elements, for example, a planar Hall element, a vertical Hall element, and a circular vertical Hall (CVH) element. As is also known, there are different types of magnetoresistance elements, for example, a giant magnetoresistance (GMC) element, an anisotropic magnetoresistance element (AMR), a tunneling magnetoresistance (TMR) element, an Indium antimonide (InSb) sensor, and a magnetic tunnel junction (MTJ).

[0023] As is known, some of the above-described magnetic field sensing elements tend to have an axis of maximum sensitivity parallel to a substrate that supports the magnetic field sensing element, and others of the above-described magnetic field sensing elements tend to have an axis of maximum sensitivity perpendicular to a substrate that supports the magnetic field sensing element.

In particular, planar Hall elements tend to have axes of sensitivity perpendicular to a substrate, while magnetoresistance elements and vertical Hall elements (including circular vertical Hall (CVH) sensing element) tend to have axes of sensitivity parallel to a substrate.

[0024] Magnetic field sensors are used in a variety of applications, including, but not limited to, an angle sensor that senses an angle of a direction of a magnetic field, a current sensor that senses a magnetic field generated by a current carried by a current-carrying conductor, a magnetic switch that senses the proximity of a ferromagnetic object, a rotation detector that senses passing ferromagnetic articles, for example, magnetic domains of a ring magnet, and a magnetic field sensor that senses a magnetic field density of a magnetic field.

SUMMARY OF EXAMPLE EMBODIMENTS OF THE INVENTION

[0025] An object of at least one embodiment of the present invention is to provide a low cost electronic vehicular transmission, a controllable coupling assembly and a coupling member for use in the assembly.

[0026] In carrying out the above object and other objects of at least one embodiment of the present invention, a coupling member for use in a controllable coupling assembly is provided. The member is configured for rotation about a rotational axis. The member includes a first coupling face oriented to face axially along the axis and has a set of pockets angularly-spaced about the axis. Each of the pockets receives a first locking element and defines a first load-bearing surface adapted for abutting engagement with a load-bearing surface of its respective first locking element. The member further includes a second coupling face oriented to face radially with respect to the axis and has a set of locking formations. Each of the set of locking formations defines a second load-bearing surface adapted for abutting engagement with a load-bearing surface of a second locking element.

[0027] The member may be a plate wherein the set of pockets are forward pockets and the set of locking formations are spaced-apart reverse cams.

[0028] The reverse cams may be greater in number than the forward pockets.

[0029] The spaced-apart reverse cams may be spaced-apart locking teeth.

[0030] The plate may have a width wherein each reverse cam extends the entire width of the plate.

[0031] The member may be a splined ring having an outer circumferential surface formed with the set of locking formations.

[0032] The set of pockets may be forward pockets for receiving forward locking elements and the set of locking formations may be reverse locking formations.

[0033] Further in carrying out the above object and other objects of at least one embodiment of the present invention, a controllable coupling assembly having multiple operating modes is provided. The assembly includes first and second coupling members supported for rotation relative to one another about a common rotational axis. The first coupling member includes a first coupling face oriented to face axially along the axis and has a set of pockets angularly-spaced about the axis. Each of the pockets receives a first locking element and defines a first load-bearing surface adapted for abutting engagement with a load-bearing surface of its respective first locking element. The first coupling member also includes a second coupling face oriented to face radially with respect to the axis and has a set of locking formations. Each of the set of locking formations defines a second load-bearing surface adapted for abutting engagement with a load-bearing surface of a second locking element.

[0034] The first coupling member may be a plate wherein the set of pockets are forward pockets and the set of locking formations are spaced-apart reverse cams.

[0035] The reverse cams may be greater in number than the forward pockets.

[0036] The spaced-apart reverse cams may be spaced-apart locking teeth.

[0037] The plate may have a width wherein each reverse cam extends the entire width of the plate.

[0038] The first coupling member may be a splined ring having an outer circumferential surface formed with the set of locking formations.

[0039] The set of pockets may be forward pockets for receiving forward locking elements and the set of locking formations may be reverse locking formations.

[0040] Still further in carrying out the above object and other objects of the present invention, an electronic vehicular transmission is provided. The transmission includes a transmission case and a coupling member supported for rotation about a rotational axis. The member has a first coupling face with a set of locking formations. Each of the locking formations defines a load-bearing first surface. The transmission also includes an electromechanical component attached to the transmission case and which includes a housing part having a closed axial end including an end wall having a second coupling face in close-spaced opposition to the first coupling face and having a single pocket defining a load-bearing second surface in communication with an inner face of the end wall. The component also includes an electromagnetic source including at least one excitation coil at least partially surrounded by the housing part and an element received within the pocket in an uncoupling position and movable outwardly from the pocket to a coupling position to couple the coupling member to the case. The coupling position is characterized by abutting engagement of the element with a respective surface of one of the locking formations and the end wall. The component further includes a reciprocating armature arranged concentrically relative to the at least one excitation coil and being axially movable when the at least one excitation coil is supplied with current. The armature is connected to the element to move the element between the coupling and uncoupling positions.

[0041] The element may include at least one projecting leg portion. Each leg portion may have an aperture. The component may further include a pivot pin received within each aperture to allow rotational movement of the element in response to reciprocating movement of the armature.

[0042] The transmission may further include a plunger connected to the armature to move therewith. A leading end of the plunger may be connected to the element via the pivot pin.

[0043] The plunger may be spring-loaded.

[0044] The housing part may have at least one attachment flange to attach the component to the transmission case.

[0045] While exemplary embodiments are described above, it is not intended that these embodiments describe all possible forms of the invention. Rather, the words used in the specification are words of description rather than limitation, and it is understood that various changes may be made without departing from the spirit and scope of the invention. Additionally, the features of various implementing embodiments may be combined to form further embodiments of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

[0046] FIGURE 1 is a schematic, perspective view of a controllable coupling assembly and an electromechanical component constructed in accordance with at least one embodiment of the present invention;

[0047] FIGURE 2 is an exploded, perspective view of the assembly and component of Figure 1;

[0048] FIGURE 3 is a view of the assembly and component similar to the view of Figure 2 but from a different angle;

[0049] FIGURE 4 is an enlarged side view, partially broken away, of the assembly and component of Figure 1 together with a second electromechanical component in phantom with locking elements of the components partially extended towards locking formations of a coupling member of the assembly;

[0050] FIGURE 5 is a partial block diagram and side view, opposite the side view of Figure 4, but with one of the components in cross section and inserted in a case (also in cross section) of an electronic vehicle transmission constructed in accordance with at least one embodiment of the present invention;

[0051] FIGURE 6 is a perspective, schematic bottom view of the electromechanical component of the prior Figures; and

[0052] FIGURE 7 is an exploded, perspective view of the electromechanical component.

DETAILED DESCRIPTION

[0053] As required, detailed embodiments of the present invention are disclosed herein; however, it is to be understood that the disclosed embodiments are merely exemplary of the invention that may be embodied in various and alternative forms. The figures are not necessarily to scale; some features may be exaggerated or minimized to show details of particular components. Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting, but merely as a representative basis for teaching one skilled in the art to variously employ the present invention.

[0054] Referring now to the drawing figures, there is illustrated one embodiment of an electronic vehicular transmission, generally indicated at 10 in Figure 5. The transmission 10 includes a transmission case 40 having a bore 41 which extends completely through the case 40. As is well known in the art, the transmission case 40 has associated therewith an environment which is hostile to electrical components during use of the transmission 10 primarily because of: (1) hot oil contained therein, (2) contaminants in the oil which cause shorting of any electrical circuits therein and (3) vibration.

[0055] The transmission 10 also includes an electromechanical component, generally indicated at 14, which is capable of operating in the hostile environment of the case 40. The component 14 may be referred to herein below as an SSI (i.e. selectable solenoid insert). The component 14 is inserted through the bore 41 and held therein by threaded fasteners (not shown) which extend through holes 46 formed through an annular flange 44 of a housing, generally indicated at 48, of the component 14. The fasteners extend into threshold holes 42 formed in the case 40 about the bore 41 to secure the component 14 to the case 40.

[0056] Referring now to Figures 1-3, the transmission 10 also includes a controllable coupling assembly, generally included at 12, which, in turn, includes first and second coupling members, 18 and 22, respectively, mounted for rotation relative to one another about a rotational axis 16. The first coupling member 18 has a first coupling face 19 oriented to face axially in a first direction with respect to the axis 16 and the second coupling member 22 has a second coupling face 23 oriented to face axially in a second direction opposite the first direction with respect to the axis 16. The second coupling member 22 also has a third coupling face 25 oriented to face radially with

respect to the axis 16 and having a set of locking formations or teeth 30 formed therein. The teeth 30 are preferably ferromagnetic or magnetic teeth 30.

[0057] The coupling assembly 12 also includes a set of forward locking elements or struts 20 which are received within angularly spaced pockets 26 formed in the face 23 of the coupling member 22. The coupling member 22 has a set of splines 28 formed on its inner diameter for drivingly engaging a drive or driven member (not shown) for rotation about the axis 16.

[0058] The assembly 12 also includes a locking ring or plate, generally indicated at 24, for insertion into an annular groove 36 of an axially extending wall 37 of the coupling member 18 to hold the coupling members 18 and 22 together. The locking plate 24 has a circumferential cutout 34 which coincides or is aligned with a circumferential cutout 32 provided in the wall 37 of the member 18 when the plate 24 is inserted into the groove 36. This feature allows a locking element or strut 52 of the component 14 to engage the teeth 30 of the member 22 as shown in Figures 4 and 5.

[0059] The housing part or housing 48 has an outer coupling face 49 (Figure 5) in close-spaced opposition to the coupling face 25 of the member 22 when the members 18 and 22 are joined and assembled together by the locking ring 24 and after insertion of the component 14 into the bore 41 of the case 40.

[0060] The outer coupling face 49 of the housing part 48 has a single, T-shaped recess or pocket 51. The recess 51 defines a load-bearing first surface shoulder 53. The coupling face 25 of the member 22 has a plurality of reverse notches or teeth 30. Each tooth of the teeth 30 defines a load-bearing second surface or shoulder 31.

[0061] The locking strut or element 52 is capable of extending between the coupling faces 25 and 49 of the member 22 and the part 48, respectively, between coupling and uncoupling positions when the assembly 12 and case 40 are assembled together as is shown in Figures 4 and 5.

[0062] The element 52 may comprise a ferromagnetic locking element or strut movable between first and second positions. The first position (i.e. coupling position) is characterized by abutting engagement of the locking element 52 with the load-bearing surface or shoulder 31 of one of the teeth 30 and the shoulder 53 of the pocket 51 formed in an end wall of the housing part 48. The second position (i.e. non-coupling position) is characterized by non-abutting engagement of the

locking element 52 with a load-bearing shoulder 31 of at least one of the teeth 30 and the end wall of the housing part 48.

[0063] The electromechanical component or apparatus (i.e. SSI) 14 includes the housing part 48 which has a closed axial end including the end wall. The end wall has the outer coupling face 49 with the single pocket 51 which defines the load-bearing shoulder 53 which is in communication with an inner face of the end wall. The housing part 48 may be a metal (such as aluminum) injection molded (MIM) part.

[0064] The apparatus 14 also includes an electromagnetic source, including at least one excitation coil 62 which is at least partially surrounded by a skirt of the housing part 48.

[0065] Electrical insulated wiring 64 supplies electrical power to the coil 62 from a power source located outside the hot oil environment. The wiring 64 extends from the coil 62, through a hole 65 (Figure 5) formed through an end seal 82, through a cavity 86 formed through an overmold 84 and to a solenoid controller.

[0066] The strut 52 is retained within the pocket 51 by a clevis-shaped retainer 50. The strut 52 is movable outwardly from the pocket 51 to its extended, coupling position characterized by abutting engagement of the strut 52 with a load-bearing surface or shoulder 31 of one of the teeth 30.

[0067] The apparatus 14 also includes a reciprocating plunger, generally indicated at 70, arranged concentrically relative to the at least one excitation coil 62 and is axially movable when the at least one excitation coil 62 is supplied with current via the wires 64. The coil 62 is wound or located about an actuator core or armature 76 and is potted between plates 60 and 78. The armature 76 is also axially movable upon coil excitation. The plate 60 abuts against the inner face of the housing end wall. The plunger 70 extends through a hole 61 (Figure 7) formed through the plate 60 and is connected at its leading end 72 to the element 52 to move the element 52 between its coupling and uncoupling positions. The plunger 70 also extends through an aperture 75 formed through the armature 76. The opposite end of the plunger 70 has a locking nut or cap 80 positioned thereon which limits movement of the plunger 70 in the aperture 75 towards the teeth 30 by abutting against the lower surface of an annular spacer 68 which abuts against the lower surface of the armature 76.

[0068] The element 52 is pivotally connected to the apertured leading end 72 of the plunger 70 wherein the plunger 70 pivotally moves the element 52 within the pocket 51 in response to reciprocating movement of the plunger 70 which, in turn, moves axially in response to reciprocating movement of the armature 76.

[0069] The apparatus 14 also preferably includes a return spring 66, which extends between the plate 60 and a shoulder in the outer surface of the actuator core or armature 76, to return the plunger 70 and the armature 76 to their home position when the coil 62 is de-energized, thereby returning the element 52 to its uncoupling position. The apparatus 14 also includes a spring 74 which urges the plunger 70 to move the element 52 towards its coupling position. In other words, the biasing member or spring 66, urges the plunger 70 via the armature 76 to a return position which corresponds to its uncoupling position of the element 52 while the biasing member or spring 66 urges the plunger 70 and its connected element 52 to its coupled position.

[0070] The housing part 48 and/or the plate 78 may have holes (not shown) to allow oil to circulate within the housing part 48. Preferably, the at least one coil 62, the housing part 48, the armature 76 and the plunger 70 comprise a low profile solenoid. The locking element 52 may be a metal (such as aluminum) injection molded (i.e. MIM) strut.

[0071] The element 52 includes at least one and, preferably, two projecting leg portions 55 which provide an attachment location for the leading end 72 of the plunger 70. Each leg portion 55 has an aperture 57. The apparatus 14 further comprises a pivot pin 54 received within each aperture 57 and the aperture leading end 72 to allow rotational movement of the element 52 in response to reciprocating movement of the plunger 70 wherein the leading end 72 of the plunger 70 is connected to the element 52 via the pivot pin 54.

[0072] Preferably, each aperture 55 is an oblong aperture which receives the pivot pin 54 to allow both rotation and translational movement of the element 52 in response to reciprocating movement of the plunger 70. Each locking strut 52 may comprise any suitable rigid material such as ferrous metal, (i.e. steel).

[0073] The component 14 also includes a magnetic field speed sensor or device 56 which may comprise a differential Hall-effect device which senses speed of the teeth 30 as they rotate past

the sensor 56. The teeth 30 may carry or support a rare-earth, automotive grade, magnet or pellet (not shown) which may be embedded in a hole formed in the outer surface of the teeth. In that case, the teeth 30 may be non-ferrous teeth such as aluminum teeth. Alternatively, and preferably, the teeth 30 are ferromagnetic teeth.

[0074] The device 56 is typically back-biased, has two wires 58 (Figure 7) and provides a current output based on speed of rotation of the teeth 30 past the sensor 56. The device 56 accurately detects the speed with a single output (i.e., current output). The device 56 is preferably mounted adjacent to the pocket 51 and the wires 58 extend through the aperture 61 formed in the plate 60. The wires 58 and the wires 64 of the coil 62 are coupled to the solenoid controller which, in turn, is coupled to a main controller to supply drive signals to the coil 62 in response to control signals from the main controller. The device 56 may be held in place by fasteners or by an adhesive so that a side surface of the device 56 is in close proximity to a side surface of the strut 52 in the uncoupling position of the strut 52.

[0075] The sensor 56 is typically back-biased when the teeth 30 are ferromagnetic and typically includes a Hall sensor or sensing element mounted on a circuit board on which other electronics or components are mounted, as is well-known in the art. The sensor 56 is preferably back-biased in that it includes a rare-earth magnet which creates a magnetic flux or field which varies as the teeth 30 move past the sensor 56. The sensor 56 may comprise a back-biased, differential Hall Effect device.

[0076] In other words, the device 56 is preferably a back-biased device wherein the device 56 includes a rare earth pellet or magnet whose magnetic field varies as the teeth 30 move therepast. The variable magnetic field is sensed by the magnetic sensing element of the device 56.

[0077] The output signal from the device 56 is a feedback signal which is received by the solenoid controller. By providing feedback, the resulting closed-loop control system provides for true speed operation.

[0078] As described above, the number of forward struts (i.e. 14) is greater than the number of reverse struts (i.e. one or two). Also, the number of reverse notches is greater than the number of forward notches. In this situation, there is a possibility of a coupling assembly such as the coupling

assembly 12 to enter a “lock-lock” condition wherein the transitional backlash (i.e., distance the clutch can move between forward and reverse directions) is extremely low. This results in the locking elements not being allowed to drop out of their coupling positions upon command.

[0079] As described and claimed in U.S. patent application Serial No. 14/675,850 filed on the same day as this application and having the same assignee, in order to avoid the above-described problem, the number of reverse struts and notches and the number of forward struts and notches are chosen so that the forward backlash is a non-zero integer multiple (i.e. “N”) of the reverse backlash and the forward pockets are uniformly angularly spaced about the axis 16. The following is a table of 36 entries wherein only entries 11, 14 and 15 do not satisfy the above criteria.

Entry	N	Reverse Notches	Reverse Struts	Reverse Backlash	Forward Notches	Forward Strut Sets	Forward Backlash	Transitional Backlash
1	2	79	1	4.556962	79	2	2.278481	1.139241
2	2	77	1	4.675325	77	2	2.337662	1.168831
3	3	80	1	4.5	80	3	1.5	0.75
4	3	79	1	4.556962	79	3	1.518987	0.759494
5	3	77	1	4.675325	77	3	1.558442	0.779221
6	3	76	1	4.736842	76	3	1.578947	0.789474
7	3	74	1	4.864865	74	3	1.621622	0.810811
8	3	73	1	4.931507	73	3	1.643836	0.821918
9	3	71	1	5.070423	71	3	1.690141	0.84507
10	3	70	1	5.142857	70	3	1.714286	0.857143
11	3	62	1	5.806452	62	3	1.935484	0.967742
12	3	61	1	5.901639	61	3	1.967213	0.983607

13	3	59	1	6.101695	59	3	2.033898	1.016949
14	3	58	1	6.206897	58	3	2.068966	1.034483
15	3	56	1	6.428571	56	3	2.142857	1.071429
16	3	55	1	6.545455	55	3	2.181818	1.090909
17	3	53	1	6.792453	53	3	2.264151	1.132075
18	3	52	1	6.923077	52	3	2.307692	1.153846
19	1	79	2	2.278481	79	2	2.278481	1.139241
20	1	77	2	2.337662	77	2	2.337662	1.168831
21	1	79	3	1.518987	79	3	1.518987	0.759494
22	1	80	3	1.5	80	3	1.5	0.75
23	1	79	3	1.518987	79	3	1.518987	0.759494
24	1	77	3	1.558442	77	3	1.558442	0.779221
25	1	76	3	1.578947	76	3	1.578947	0.789474
26	1	74	3	1.621622	74	3	1.621622	0.810811
27	1	73	3	1.643836	73	3	1.643836	0.821918
28	1	71	3	1.690141	71	3	1.690141	0.84507
29	1	70	3	1.714286	70	3	1.714286	0.857143
30	1	61	3	1.967213	61	3	1.967213	0.983607
31	1	59	3	2.033898	59	3	2.033898	1.016949

32	1	58	3	2.068966	58	3	2.068966	1.034483
33	1	56	3	2.142857	56	3	2.142857	1.071429
34	1	55	3	2.181818	55	3	2.181818	1.090909
35	1	53	3	2.264151	53	3	2.264151	1.132075
36	1	52	3	2.307692	52	3	2.307692	1.153846

[0080] General Advantages

[0081] Wiring is outside the transmission.

[0082] Eliminates the difficulty in routing lead wires from the clutch around rotating parts to the bulk head inside the box.

[0083] Does not impact the number of wires passing through the bulk head connector.

[0084] Coils are potted, leads are over molded, connector is external, completely segregated from the hot oil environment which prevents:

[0085] Long term embrittlement of connector and wire insulation from hot oil exposure;

[0086] Eliminates the possibility of contamination in oil shorting the circuit to power; and

[0087] Vibration failures are greatly reduced (potted and over molded).

[0088] High Power Density – every surface of the inner and outer race is used. The radial surfaces are for reverse and the planar surfaces are for 1st gear. They are independent and do not compete for the same real estate in the races. The concentric design competes for radial cross section and co-planar designs add a PM race. The largest possible strut/cam geometry can be used in a smaller package. This increases the power density of the clutch.

[0089] Using the SSI 14 as a common electro-mechanical component.

- [0090] Tend to make it a high volume commodity thus reducing cost.
- [0091] Streamlines design, validation, and manufacturing – one and done approach.
- [0092] Better resource allocation. Engineering can focus on clutch design without the burden of designing a new electro-mechanical solution for each unique application.
- [0093] Eliminate the slide plate and failure modes associated with the slide plate.
- [0094] Traditional MD approach – no concentric, co-planar design. Tried and true approach.
- [0095] Cost competitive – highest power density, 2 races, and an across the board approach for controls using the SSIs 14.
- [0096] Reduction of partial engagements.
- [0097] The SSI 14 strut 52 turns on faster than a hydraulic design using a slide plate.
- [0098] The SSI 14 can be turned on closer to the sync point when doing a rolling forward reverse shift because it takes only 20 ms or less to fire on. No hydraulic delay or temperature effects.
- [0099] Soft turn off capable reduces impact loads when turning off
- [0100] No special driver is required. The SSI 14 can fire initially and can be PWMed down to hold on. The higher pulse is to overcome a return spring designed for a 20g impact.
- [0101] NVH Advantages – Maximizing cams is great approach to reducing backlash. Many more cams can be formed into the race in the radial direction as opposed to the planar direction. Using the SSI 14 in the radial direction takes advantage of this feature.
- [0102] Usually there is one outer race where the forward and reverse flanks of a spline are the path to ground. This design splits the paths. There is no backlash in the reverse direction as the path passes through a press fit SSI 14 into the case 40. The SSI 14 only reacts reverse torque. The outer race for the passive clutch conversely only sees forward reaction torque. The result is a system where the clutch does not travel through an external lash. The drive side spline stays on the drive

side and the reverse drive path is in a press fit SSI 14. This reduces tick/clunk in the splines. A rubber washer/spring clip can be added to the coast side of the spline to keep the spline engaged with the case at all times. It never experiences reverse torque.

[0103] Advantages over Hydraulic

[0104] Temperature insensitive.

[0105] Faster reaction time with small tolerance (20ms or less).

[0106] Much less energy to operate over life of application.

[0107] Easier to route wires outside of box compared to packaging worm trails.

[0108] Easy for diagnostic – software maintenance loop with a trickle voltage can measure resistance for temperature, continuity, or a short instantly setting a code.

[0109] Contamination insensitive

[0110] Advantages of two springs

[0111] If the armature 76 was directly connected to the strut 52 with a single return spring, a constant high current would have to be applied to ensure the device turns ON. The lowest stroking force occurs initially at the highest gap when the armature 76 is in the OFF position. If the armature 76 was directly attached to the strut 52 and the strut 52 was in between notches or teeth 30, a high current would have to be held to ensure the device would always stroke to ON eventually. The cam plate 22 would have to rotate so the strut 52 could drop in. So a consistently high current would have to be maintained as long as the solenoid 14 was ON. This is a problem. The solenoid 14 could overheat using this approach. The solution is to use two springs 66 and 76, an actuator core or armature 76, and a second internal piston called the plunger 70 that attaches to the strut 52 via a clevis connection. In this arrangement, the armature 76 always strokes ON and travels the full 3 mm closing the gap independent of the position of the strut 52 relative to the cams or teeth 30. The forces keeping the armature 76 in the ON position increase by a magnitude when the gap is closed. The armature 76 pushes the second spring 74 that pushes the plunger 70 attached to the strut 52.

[0112] Once the armature 76 strokes the 3 mm, the current can be dropped to a holding current that is a fraction of the initial pulse current. The strut 52 is loaded by the second spring 74 in the apply direction. If the strut 52 is in between cams or teeth 30, there is a second spring force pushing the strut 52 into the ON position as soon as the cam plate 22 rotates. The armature 70 is now independent of strut position and can be PWMed.

[0113] If one used a single spring in a tooth butt condition, the armature 76 would only stroke 1.3 mm and stop with a force of about 2 lbs. In a two-spring system the armature 76 always strokes the full 3 mm in 20ms allowing the current to drop to a holding current. The second spring 74 applies the force to exit tooth butt.

[0114] Advantages of Speed Sensor with the Component (i.e. SSI)

[0115] The prior art has a speed sensor that passes through the outside of the outer race of the clutch to sense the speed of the inner race. It was presumed that it is for the non-sync reverse shift when rolling in the forward direction.

[0116] At least one embodiment of the present invention provides the structure for a speed sensor chip set. It is possible to pot in a speed sensor chip set right into the SSI 14. This has the advantage of flexing the structure of the SSI 14 to not only lock the inner race to ground in reverse, but also to sense the inner race speed all in the same part. This would eliminate the stand alone speed sensor, case machining and clutch machining to accommodate the stand alone speed sensor. This is a significant cost save.

[0117] As required, detailed embodiments of the present invention are disclosed herein; however, it is to be understood that the disclosed embodiments are merely exemplary of the invention that may be embodied in various and alternative forms. The figures are not necessarily to scale; some features may be exaggerated or minimized to show details of particular components. Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting, but merely as a representative basis for teaching one skilled in the art to variously employ the present invention.

WHAT IS CLAIMED IS:

1. A coupling member for use in a controllable coupling assembly, the member being configured for rotation about a rotational axis, the member comprising:

a first coupling face oriented to face axially along the axis and having a set of pockets angularly-spaced about the axis, each of the pockets receiving a first locking element and defining a first load-bearing surface adapted for abutting engagement with a load-bearing surface of its respective first locking element; and

a second coupling face oriented to face radially with respect to the axis and having a set of locking formations, each of the set of locking formations defining a second load-bearing surface adapted for abutting engagement with a load-bearing surface of a second locking element.

2. The coupling member as claimed in claim 1, wherein the member is a plate and wherein the set of pockets are forward pockets and the set of locking formations are spaced-apart reverse cams.

3. The coupling member as claimed in claim 2, wherein the reverse cams are greater in number than the forward pockets.

4. The coupling member as claimed in claim 2, wherein the spaced-apart reverse cams are spaced-apart locking teeth.

5. The coupling member as claimed in claim 2, wherein the plate has a width and wherein each reverse cam extends the entire width of the plate.

6. The coupling member as claimed in claim 1, wherein the member is a splined ring having an outer circumferential surface formed with the set of locking formations.

7. The coupling member as claimed in claim 1, wherein the set of pockets are forward pockets for receiving forward locking elements and the set of locking formations are reverse locking formations.

8. A controllable coupling assembly having multiple operating modes, the assembly comprising:

first and second coupling members supported for rotation relative to one another about a common rotational axis, the first coupling member including:

a first coupling face oriented to face axially along the axis and having a set of pockets angularly-spaced about the axis, each of the pockets receiving a first locking element and defining a first load-bearing surface adapted for abutting engagement with a load-bearing surface of its respective first locking element; and

a second coupling face oriented to face radially with respect to the axis and having a set of locking formations, each of the set of locking formations defining a second load-bearing surface adapted for abutting engagement with a load-bearing surface of a second locking element.

9. The assembly as claimed in claim 8, wherein the first coupling member is a plate and wherein the set of pockets are forward pockets and the set of locking formations are spaced-apart reverse cams.

10. The assembly as claimed in claim 9, wherein the reverse cams are greater in number than the forward pockets.

11. The assembly as claimed in claim 9, wherein the spaced-apart reverse cams are spaced-apart locking teeth.

12. The assembly as claimed in claim 9, wherein the plate has a width and wherein each reverse cam extends the entire width of the plate.

13. The assembly as claimed in claim 8, wherein the first coupling member is a splined ring having an outer circumferential surface formed with the set of locking formations.

14. The assembly as claimed in claim 8, wherein the set of pockets are forward pockets for receiving forward locking elements and the set of locking formations are reverse locking formations.

15. An electronic vehicular transmission comprising:

a transmission case;

a coupling member supported for rotation about a rotational axis, the member having a first coupling face with a set of locking formations, each of the locking formations defining a load-bearing first surface; and

an electromechanical component attached to the transmission case and including:

a housing part having a closed axial end including an end wall having a second coupling face in close-spaced opposition to the first coupling face and having a single pocket defining a load-bearing second surface in communication with an inner face of the end wall;

an electromagnetic source including at least one excitation coil at least partially surrounded by the housing part;

an element received within the pocket in an uncoupling position and movable outwardly from the pocket to a coupling position to couple the coupling member to the case, the coupling position being characterized by abutting engagement of the element with a respective surface of one of the locking formations and the end wall; and

a reciprocating armature arranged concentrically relative to the at least one excitation coil and being axially movable when the at least one excitation coil is supplied with current, the armature being connected to the element to move the element between the coupling and uncoupling positions.

16. The transmission as claimed in claim 15, wherein the element includes at least one projecting leg portion, wherein each leg portion has an aperture and wherein the component

further includes a pivot pin received within each aperture to allow rotational movement of the element in response to reciprocating movement of the armature.

17. The transmission as claimed in claim 16, further comprising a plunger connected to the armature to move therewith wherein a leading end of the plunger is connected to the element via the pivot pin.

18. The transmission as claimed in claim 15, wherein the plunger is spring-loaded.

19. The transmission as claimed in claim 15, wherein the housing part has at least one attachment flange to attach the component to the transmission case.

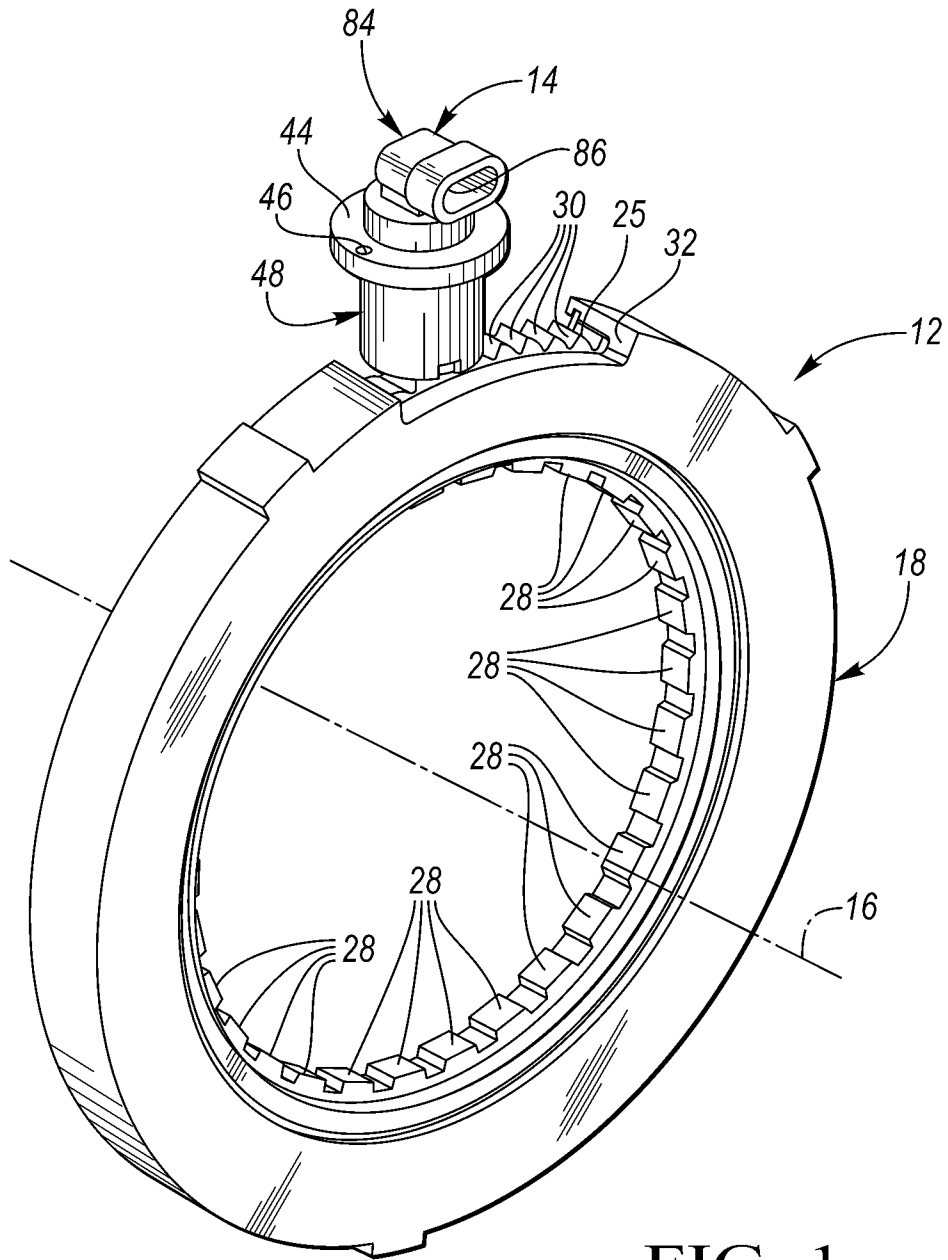


FIG. 1

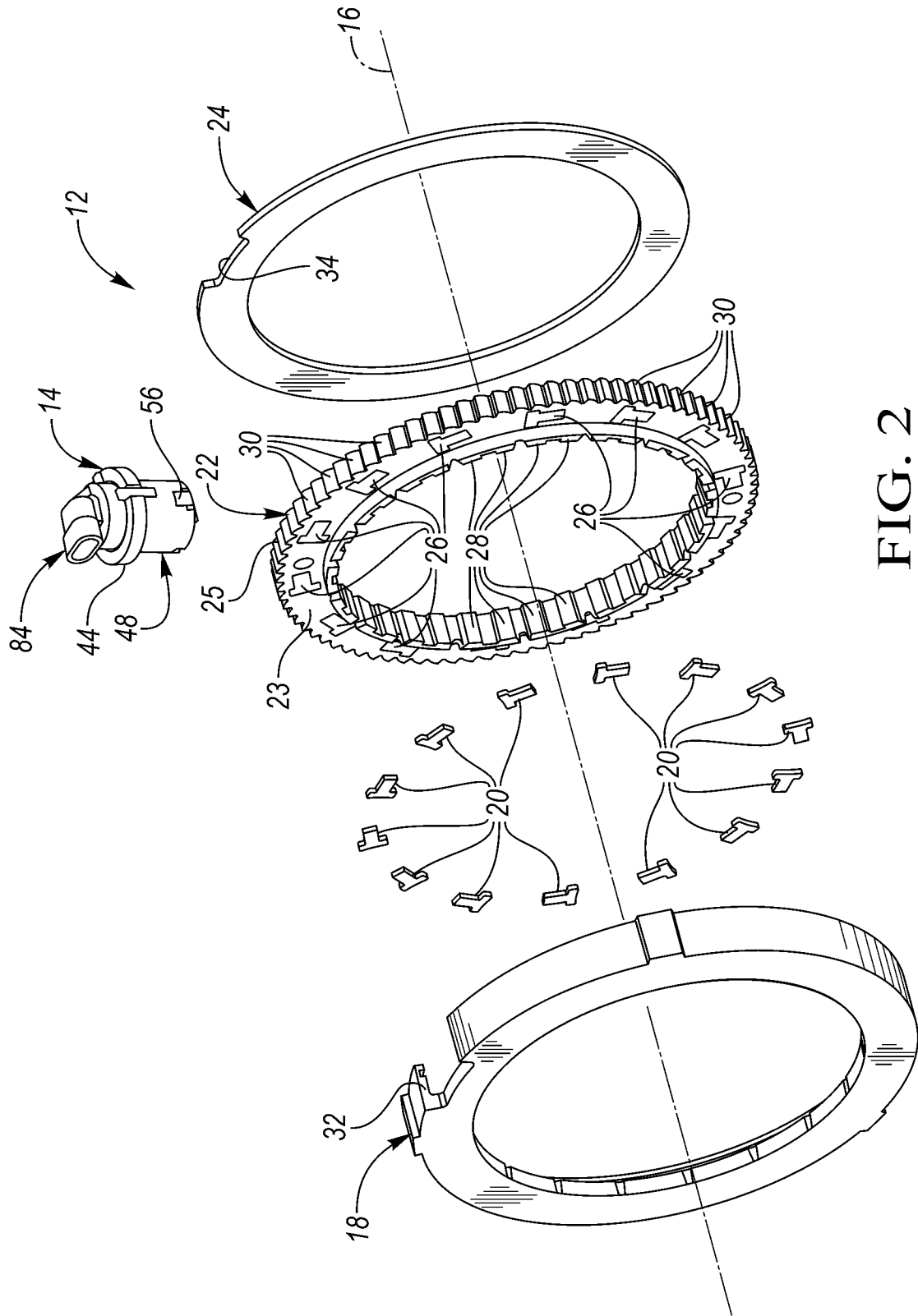


FIG. 2

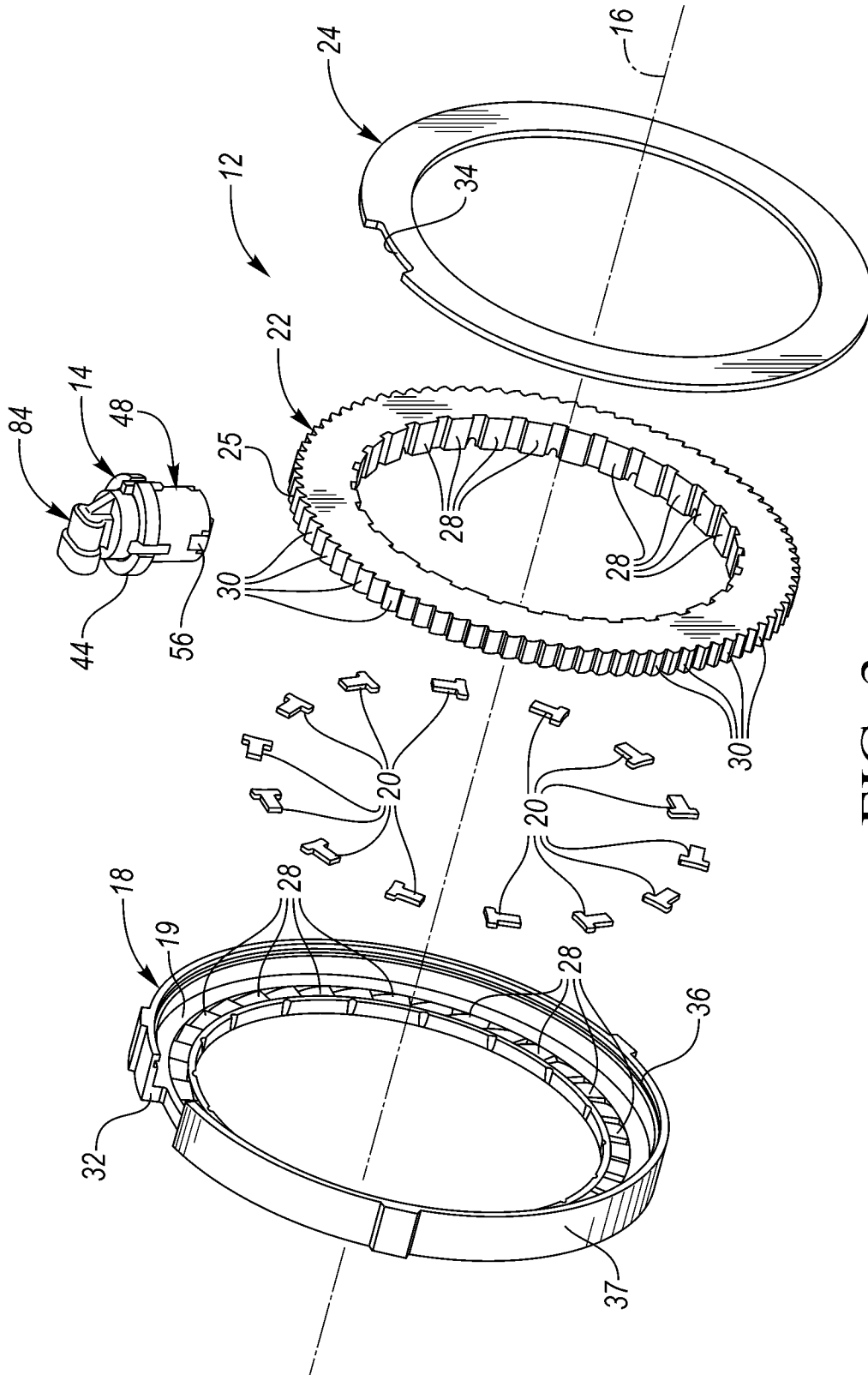


FIG. 3

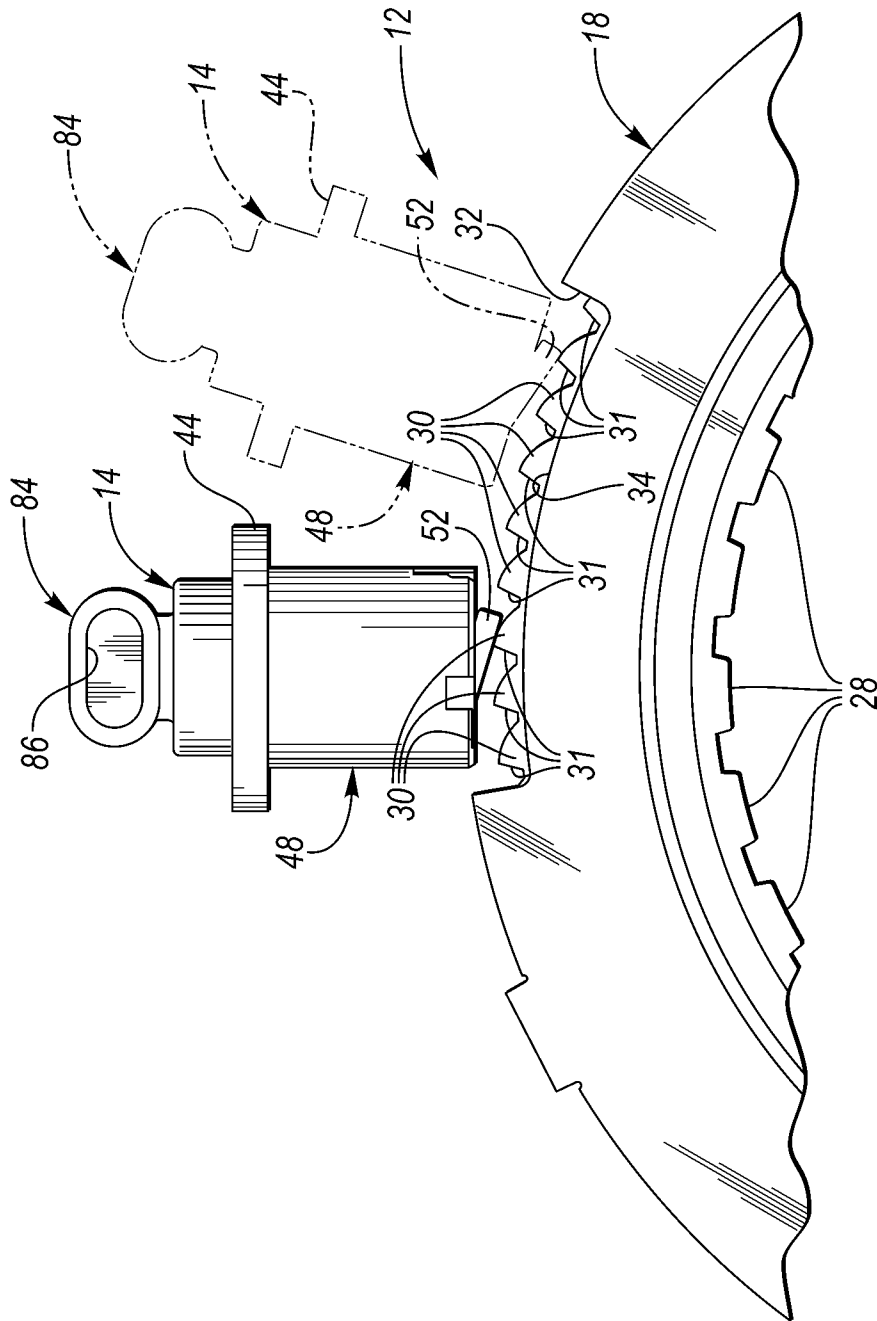


FIG. 4

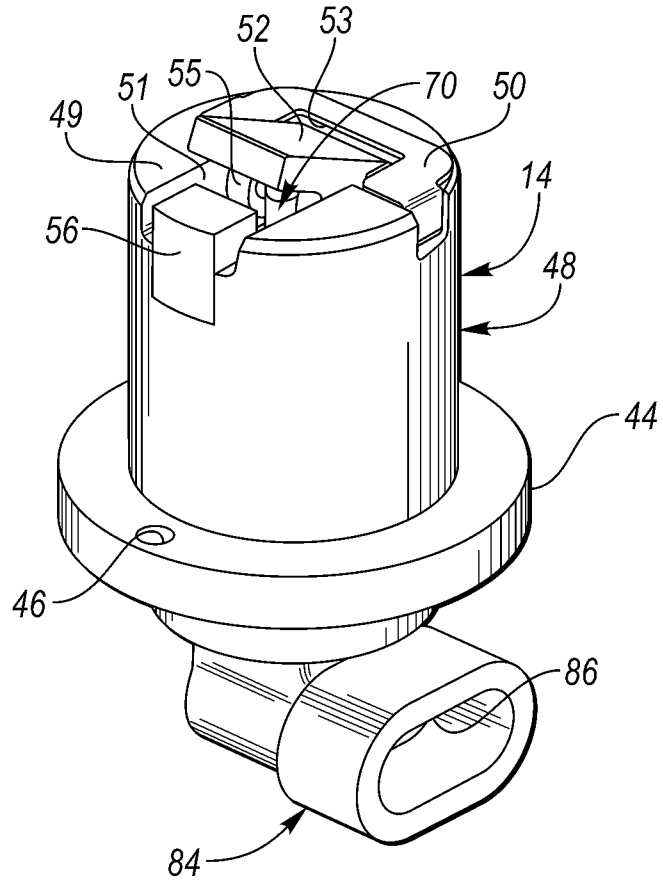
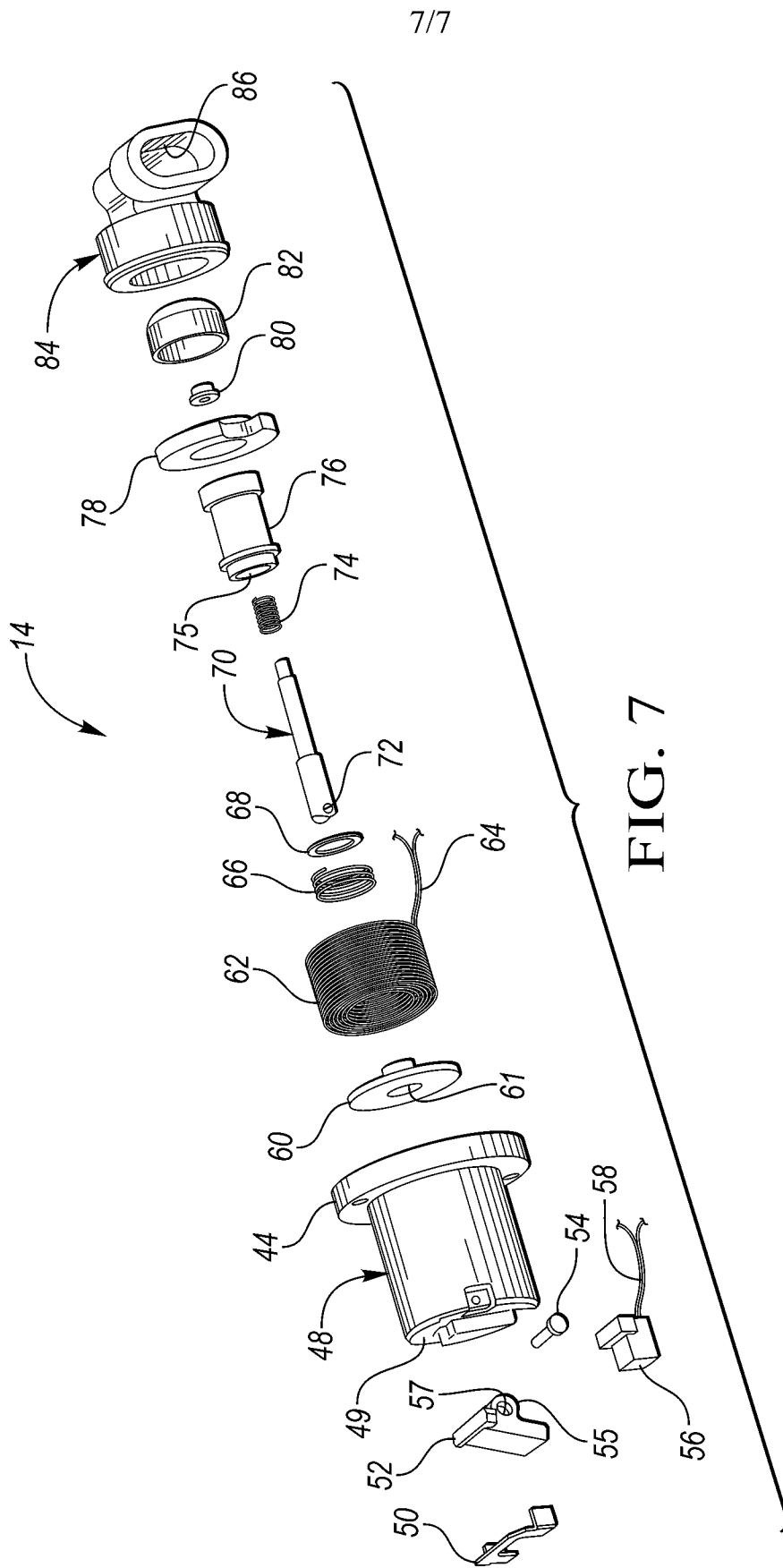


FIG. 6



INTERNATIONAL SEARCH REPORT

International application No.

PCT/US2016/014243

<p>A. CLASSIFICATION OF SUBJECT MATTER IPC(8) - F16D 27/09 (2016.01) CPC - F16D 27/09 (2016.02) According to International Patent Classification (IPC) or to both national classification and IPC</p>																				
<p>B. FIELDS SEARCHED</p> <p>Minimum documentation searched (classification system followed by classification symbols) IPC(8) - F16D 11/00, 11/02, 27/00, 27/02, 27/09, 27/10, 27/102, 27/118, 27/14, 41/16 (2016.01) CPC - F16D 11/00, 11/02, 27/00, 27/02, 27/09, 27/10, 27/102, 27/118, 27/14, 41/16 (2016.02)</p> <p>Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched USPC - 192/18B, 35, 41R, 43.1, 43.2, 46, 48.1, 51, 69, 69.7, 82, 84.1, 84.92, 218, 222 (keyword delimited)</p> <p>Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) Orbit, Google Patents, Google, YouTube Search terms used: teeth, sensor, sense, electro, magnet, magnetic, solenoid, peripheral, radial, face</p>																				
<p>C. DOCUMENTS CONSIDERED TO BE RELEVANT</p> <table border="1"> <thead> <tr> <th>Category*</th> <th>Citation of document, with indication, where appropriate, of the relevant passages</th> <th>Relevant to claim No.</th> </tr> </thead> <tbody> <tr> <td>A</td> <td>US 2012/0231913 A1 (SAMIE et al) 13 September 2012 (13.09.2012) entire document</td> <td>1-19</td> </tr> <tr> <td>A</td> <td>WO 2015/030899 A1 (MEANS INDUSTRIES, INC.) 05 March 2015 (05.03.2015) entire document</td> <td>1-19</td> </tr> <tr> <td>A</td> <td>US 8,051,959 B2 (EISENGRUBER) 08 November 2011 (08.11.2011) entire document</td> <td>1-19</td> </tr> <tr> <td>A</td> <td>US 7,344,010 B2 (FETTING, JR. et al) 18 March 2008 (18.03.2008) entire document</td> <td>1-19</td> </tr> <tr> <td>A</td> <td>US 2013/0319812 A1 (WYS et al.) 05 December 2013 (05.12.2013) entire document</td> <td>1-19</td> </tr> </tbody> </table>			Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.	A	US 2012/0231913 A1 (SAMIE et al) 13 September 2012 (13.09.2012) entire document	1-19	A	WO 2015/030899 A1 (MEANS INDUSTRIES, INC.) 05 March 2015 (05.03.2015) entire document	1-19	A	US 8,051,959 B2 (EISENGRUBER) 08 November 2011 (08.11.2011) entire document	1-19	A	US 7,344,010 B2 (FETTING, JR. et al) 18 March 2008 (18.03.2008) entire document	1-19	A	US 2013/0319812 A1 (WYS et al.) 05 December 2013 (05.12.2013) entire document	1-19
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.																		
A	US 2012/0231913 A1 (SAMIE et al) 13 September 2012 (13.09.2012) entire document	1-19																		
A	WO 2015/030899 A1 (MEANS INDUSTRIES, INC.) 05 March 2015 (05.03.2015) entire document	1-19																		
A	US 8,051,959 B2 (EISENGRUBER) 08 November 2011 (08.11.2011) entire document	1-19																		
A	US 7,344,010 B2 (FETTING, JR. et al) 18 March 2008 (18.03.2008) entire document	1-19																		
A	US 2013/0319812 A1 (WYS et al.) 05 December 2013 (05.12.2013) entire document	1-19																		
<p><input type="checkbox"/> Further documents are listed in the continuation of Box C. <input type="checkbox"/> See patent family annex.</p>																				
<p>* Special categories of cited documents:</p> <table border="0"> <tr> <td style="vertical-align: top;"> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier application or patent but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </td> <td style="vertical-align: top;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&" document member of the same patent family</p> </td> </tr> </table>			<p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier application or patent but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p>	<p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&" document member of the same patent family</p>																
<p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier application or patent but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p>	<p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&" document member of the same patent family</p>																			
<p>Date of the actual completion of the international search</p> <p>09 March 2016</p>		<p>Date of mailing of the international search report</p> <p>24 MAR 2016</p>																		
<p>Name and mailing address of the ISA/ Mail Stop PCT, Attn: ISA/US, Commissioner for Patents P.O. Box 1450, Alexandria, VA 22313-1450 Facsimile No. 571-273-8300</p>		<p>Authorized officer</p> <p>Blaine R. Copenheaver</p> <p>PCT Helpdesk: 571-272-4300 PCT OSP: 571-272-7774</p>																		