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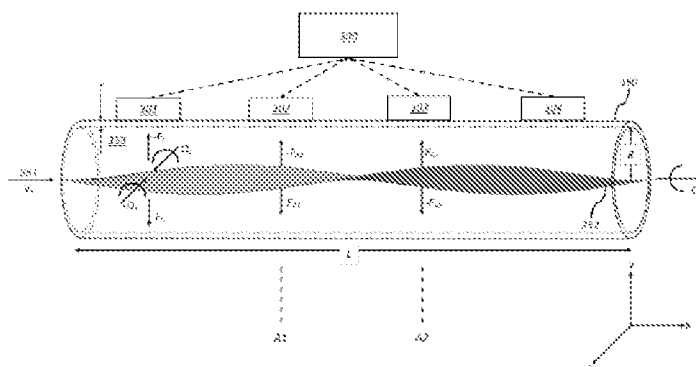
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(57)	Abstract	

A mass flow meter is disclosed. The mass flow meter has a tubular housing (250) extending along a longitudinal axis and configured to receive a flow of fluid (351) therethrough. A flexible plate (352) extends along at least a part of the tubular housing and is at least partially coupled to an interior wall of the tubular housing at opposed longitudinal ends of the flexible plate such that the flexible plate is able to vibrate in torsion. At least one electromagnetic actuator system (302, 303) is configured to apply at least two oscillating torques to the flexible plate sufficient to vibrate the flexible plate in torsion. At least two sensor systems (301, 304) are configured to measure oscillations of the flexible plate as a function of time at locations arising from the at least two applied oscillating torques. A method for measuring mass flow through the at least one tubular housing is also disclosed.



MASS FLOW METER

INTRODUCTION

The invention relates to a mass flow meter and a method for measuring a mass
5 flow of fluid through a tubular housing. In particular, the invention relates to a mass
flowmeter with a flexible plate. Uses of the mass flow meter and method are also
disclosed.

BACKGROUND

10 Fluids such as liquid CO₂ for carbon dioxide capture and storage (CCS), fluid
petroleum products, natural gas, hydrogen and water are often transported in
pipelines. Such fluids are often transported under high pressure. The pipelines
may be subsea on large depths, but also on land. Fluids may also be transported
through pipelines in land facilities such as oil refineries or other processing
15 facilities. The fluids are transported in pipelines with large dimensions and the
fluids typically may have low density. Liquid H₂ has e.g. low density while H₂ in gas
form has extremely low density. A high density fluid such as e.g. liquid CO₂, and
natural gas, are often transported/stored subsea at high depths and at a water
temperature of 4°C or in long pipelines with cooling arrangements. Liquid CO₂ may
20 not be transported at atmospheric pressure or at environmental temperatures
above 4°C as this would require a too high pressure to enable transport in a
pipeline for practical reasons (thickness of pipeline etc). At 4°C on the ocean floor
the pressure would be about 90 bar. Building a pipeline for transport of liquid CO₂
at the ocean floor would therefore be possible and practical. Liquid CO₂ has a
25 mass density of about 1,1 tons per cubic meter. Liquid H₂ has a mass density of
about 70kg per cubic meter. The fluid transport may be monitored in real-time by
measuring the amount of fluid moving through the pipeline. Mass flow
measurements may be preferred over volume flow, as mass do not vary with
changes in pressure or temperature. Mass flow measurements may thus be more
30 accurate. Mass flow meters based on ultrasound measurements may also not be
applicable for use with liquids such as e.g. liquid CO₂, as the ultrasound waves are
attenuated by the liquid.

Mass flow meters using traditional Coriolis technology can operate by vibrating a pipe carrying a flowing fluid between an inlet and an outlet. This vibration of the pipe provides an oscillation, a variation of a measure of the pipe (e.g. position) about a central value. The inertia of the flowing fluid resists the vibration motion and causes the pipe to twist. This twist results in a time lag (phase shift) of oscillations of the pipe between the inlet side and the outlet side and this phase shift is directly affected by the mass of the fluid passing through the pipe.

Traditional Coriolis flow meters divide the fluid flow in two pipes in order to provide net zero force from the drive.

Traditional Coriolis direct mass flow measurement may be unsuitable for measurements of mass flow for high pressure fluids, in particular for low density fluids. Indirect mass flow measurements of high pressure fluids may be performed by use of differential pressure and/or density of the fluid, but may be inaccurate.

E.g. hydrogen and CO₂ transport pipes have very large dimensions (diameter up to 24 or 30 inches) and the pressure is typically 100-200 bars. Presently existing Coriolis mass flow meters have a maximum diameter of 16 inches and may not be used for measuring mass flow of fluid in such large pipes. For transport of fluids at very high pressures e.g. 300 bars, the largest usable traditional Coriolis meter may be only 6-7 inches and with a large thickness to withstand the pressure. For measurement of fluids with low density a Coriolis flowmeter must have thin tubular walls to be able to detect the mass flow. Thin tubular walls cannot withstand high pressure. Existing Coriolis mass flow meters may therefore not be used in high pressure applications e.g. fluid at a pressure above 100 bars, if the line size are not very small. Existing Coriolis mass flow meters would have to be made with a large thickness to be able to withstand these high pressures that would result in a too stiff construction that are unable to vibrate for detection of mass flow. For high operation pressures and/or large diameter pipelines, the pressure carrying metal pipe for the Coriolis flow meter would be thick. Applying a force to the measuring pipe by use of electromagnetic actuators would then not be possible for such a thick pipeline. Traditional Coriolis flow meters may also not be able to measure the mass flow of low density fluids, as this would require a high speed of the fluid flow to provide a signal and such a high speed would not be possible. The design of

the traditional Coriolis flow meter with reduced diameter tubes as compared with the pipe for the fluid flow may also result in a pressure drop over the mass flow meter due to a venturi effect. For H₂ the pressure drop over the traditional Coriolis mass flow meter may e.g. be 50-100 bars. The pressure drop may result in boiling
5 of e.g. the fluid e.g. liquid CO₂, providing bubbles in the fluid flow resulting in a poor measurement by the mass flow meter.

US5,392,656 discloses a mass flowmeter with a nonvibrating conduit providing a flow passage divided into two parallel and equal subpassages by a planar member
10 with the leading and trailing edges secured to the wall of the flow passage. The planar member is torsionally vibrated about the central axis thereof substantially coinciding with the center line of the flow passage. Two actuators are arranged on the inside of the conduit facing each other. The actuators may extend into the wall of the conduit or through the wall to be close to the planar member. A pair of
15 vibration sensors detect the torsional vibration of the planar member respectively at two different cross sections of the flow passage. The mass flow rate of media moving through the flow passage is determined as a function of a phase angle difference between two alternating electrical signals respectively provided by the pair of vibration sensors. The arrangement of the actuators close to the planar
20 member provides a limited vibratory torque to the planar member.

US10393560B2, which is hereby incorporated by reference in its entirety, discloses a mass flow meter 200 with a tubular housing 202, a flexible plate 204, an actuator 210, and at least two sensors 214 (214a, 214b, 214c, 214d), 216
25 (216a, 216b, 216c, 216c, 216d) as illustrated in Fig.1. The tubular housing 202 may be in the form of a generally circular cylinder having av length L, a wall thickness T and an inner radius R defining av cavity 206. The tubular housing has an inlet 202i for a fluid flow 102, and an outlet 202o for the fluid flow 102. The flexible plate has a width W. The flexible plate 204 can be coupled to an interior
30 wall of the tubular housing such that the flexible plate can vibrate in torsion. The actuator 210 can be configured to apply an oscillating torque to the flexible plate sufficient to vibrate the flexible plate in torsion. The at least two sensors 214, 216 can each be configured to measure oscillations of the flexible plate as a function of time at different locations. The mass flow meter can also include a computing

device 212 in electrical communication with the at least two sensors and configured to determine a mass flow of fluid passing through the tubular housing from a phase shift between oscillations of the flexible plate measured by the at least two sensors.

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As high-pressure fluids are often transported in thick-walled pipes that can be difficult to vibrate with sufficient strength for mass flow meters, the mass flow meter disclosed in US10393560B2 is provided with a tubular housing containing a flexible plate that vibrates in a twisting manner (torsion). The vibration of the plate is altered by the fluid flow therethrough. By measuring oscillations of the flexible plate at different locations, a phase lag of the plate oscillations can be measured and related to mass flow of a fluid traveling through the tubular housing, regardless of its thickness.

10 For measurements of mass flow in low density fluids and/or high-pressure fluids there may be challenges with sensitivity for prior art solutions.

SUMMARY OF THE INVENTION

An improved mass flow meter is provided.

20 The invention provides a mass flow meter comprising a tubular housing extending along a longitudinal axis and configured to receive a flow of fluid therethrough and a flexible plate extending along at least a part of the tubular housing and at least partially coupled to an interior wall of the tubular housing at opposed longitudinal ends of the flexible plate such that the flexible plate is able to vibrate in torsion. At least one electromagnetic actuator system is configured to apply at least two oscillating torques to the flexible plate sufficient to vibrate the flexible plate in torsion. At least two sensor systems are configured to measure oscillations of the flexible plate as a function of time at locations arising from the at least two applied oscillating torques.

25 Further, a net sum of the at least two oscillating torques applied to the flexible plate may be zero or substantially zero. The at least two oscillating torques may have opposite directions. A sum of the at least two oscillating torques may be less than the largest of the at least two oscillating torques.

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It is further disclosed that the at least one electromagnetic actuator system may comprise an electromagnetic device arranged on the outside of the tubular housing and a magnetizable material arranged on the inside of the tubular housing. The electromagnetic device may comprise at least one coil arranged on
5 the outside of the tubular housing. The magnetizable material may be arranged on the flexible plate. The magnetizable material may comprise at least one permanent magnet. The magnetizable material may comprise at least one group of permanent magnets wherein the permanent magnets may be symmetrically arranged side by side forming a dipole. The magnetizable material may comprise
10 four groups of permanent magnets forming a quadrupole. The magnetizable material may alternatively comprise four groups of permanent magnets forming a dipole. Each of the two sensor systems of the mass flow meter may comprise a pick-up. In an embodiment the at least one electromagnetic actuator system may be adapted to also function as a sensor system.

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The at least one coil may also be arranged to provide an alternating electromagnetic field alternatingly magnetizing and demagnetizing the magnetizable material.

20 In an embodiment, the tubular housing of the mass flow meter may be a liner of a non-magnetizable material. A pressure housing may be arranged on the outside of the liner.

In a further aspect, the invention provides a method for measuring mass flow
25 through at least one tubular housing. The method comprising receiving a flow of fluid through the at least one tubular housing, wherein the tubular housing comprising a flexible plate extending along at least a part of the at least one tubular housing and is at least partially coupled to an interior wall of the at least one tubular housing at opposed longitudinal ends of the flexible plate such that the
30 flexible plate is able to vibrate in torsion. The method further comprising driving by at least one actuator system the flexible plate within the at least one tubular housing to vibrate in a torsional mode at a selected frequency by applying at least two oscillating torques to the flexible plate to vibrate the flexible plate in torsion; measuring a plurality of oscillations of the flexible plate by at least two sensor

systems configured to measure oscillations of the flexible plate as a function of time at at least two locations arising from the at least two applied oscillating torques; and determining a mass flow of the fluid flowing within the at least one tubular housing based on a phase shift between the oscillations measured at the
5 at least two locations.

A net sum of the at least two oscillating torques applied to the flexible plate may be zero or substantially zero. The at least two oscillating torques may have opposite directions. A sum of the at least two oscillating torques may be less than the
10 largest of the at least two oscillating torques. If e.g. applying three oscillating torques the sum of all the oscillating torques should be zero or substantially zero.

In a further aspect, the mass flow meter as disclosed above or the method as disclosed above may be used of for measuring mass flow of a fluid flow of CO₂,
15 NH₃, H₂ or natural gas.

The improved disclosed mass flow meter provides increased sensitivity in particular for fluids with lower density and lower viscosity such as gas, e.g. CO₂, NH₃, H₂ or natural gas. The mass flow meter also provides increased sensitivity for
20 liquid CO₂, liquid NH₃, liquid H₂ or liquid natural gas (LNG) that are often transported at high pressures. The mass flow meter is also able to measure mass flow of two-phase fluid flows or multiphase fluid flows.

Use of at least two actuating systems symmetrically arranged around the
25 longitudinal center of the flexible plate provides increased sensitivity. Two actuating systems may excite the flexible plate in 2nd harmonics oscillations or higher even order harmonics. This enables adaptation of the mass flow meter to the particular fluid flow that is to be measured. The use of two torques contribute to excite the desired modi. The torques are oppositely directed and the sum of the
30 torques may be around zero or substantially zero. The 2nd and the 4th harmonics oscillations may be the most practical choices for reasons described below, but also the 3rd harmonics may be performed by using unsymmetrical torques. Higher odd number harmonics may also be possible.

The use of two actuating systems provides an increased Q (quality) factor for the mass flow meter. A higher Q factor provides a sharper resonance peak for the flexible plate. A sharper resonance peak and hence a narrower frequency range results in a mass flow meter less prone to be affected by noise from the surroundings. A high Q factor also means that the ratio between the energy input from the actuators into the flexible plate and the resulting energy from the oscillations of the flexible plate is high. The energy required to drive the system would thus be reduced. An increased Q factor of the mass flow meter results in an increased signal, noise reduction and increased measuring sensitivity.

In some applications, it is not desirable nor possible to use a tubular housing that is electrically conductive. In some applications as for high operation pressures (e.g. typically above 200 bars) and/or large diameter pipes (e.g. typically above 24 inches), the pressure carrying metal tubular housing may also be too thick for electromagnetic actuation of the torsion of the flexible pipe. In these applications may then be desirable to arrange the actuator(s) and the sensor(s) on the inside of the tubular housing. The actuator and/or sensor coils should then be protected. The pressure from the flowing fluid inside the tubular housing should also be transferred to the outside pressure carrying housing. This may be done e.g. by use of a metal membrane filled with liquid (e.g. oil) or molded plastic which may transfer the process pressure to the pressure carrying metal tubular housing. The tubular housing may be a liner. A pressure housing may be arranged outside the liner. The electromagnetic actuators may be arranged on the inside of the pressure housing, but on the outside of the liner. The space between the pressure housing and the liner may be filled with a liquid or solid filler material to transfer the pressure from the fluid flow on the inside of the liner and out to the pressure housing. The filler material also serves to protect the electromagnetic actuator. As the tubular housing may be a liner it does not need to withstand the high pressure of the fluid flow- The flexible plate should also be soft enough to measure the mass flow of gas, as e.g. a fluid flow of CO₂, NH₃, H₂ or natural gas in liquid or gas form or multiphase flow and even at high pressures. The mass flow meter may be used in large diameter pipes, as the liner with flexible plate do not need to be able to withstand high pressures themselves and the design of the flexible plate would be flexible and soft enough even at large diameters.

The actuator systems and the sensor systems may be arranged in positions corresponding to the maximum amplitudes of a 4th harmonic torsional oscillation of the flexible plate; i.e. at 1/8, 3/8, 5/8, 7/8 of the length of the tubular housing.

These positions also leave enough room for both the actuator systems and the
5 sensor systems of the mass flow sensor.

BRIEF DESCRIPTION OF DRAWINGS

Example embodiments will be described with reference to the following drawings, where,

10 Figure 1A is a perspective view of one exemplary embodiment of a prior art mass flow meter including a tubular housing and flexible plate positioned within the tubular housing;

Fig.1B is the prior art solution from Fig.1A illustrated with forces for the torsion acting on the flexible plate, where the flexible plate is illustrated in a resulting
15 actuated state;

Figure 2A is a perspective view illustrating an exemplary embodiment of a mass flow meter including a tubular housing and a flexible plate positioned within the tubular housing and where the mass flow meter is provided with two actuating devices arranged about a longitudinal center of the flexible plate and two sensors
20 arranged about a longitudinal center of the flexible plate, and with the flexible plate illustrated in an actuated state;

Figure 2B is a perspective view illustrating an exemplary embodiment of a mass flow meter including a tubular housing and a flexible plate positioned within the tubular housing and where the mass flow meter is provided with two actuating
25 devices arranged about a longitudinal center of the flexible plate and two sensors arranged about a longitudinal center of the flexible plate, and with the flexible plate illustrated in an unactuated state and where the flexible plate is provided with groups of magnets or magnetizable material;

Figure 2C is a perspective view illustrating an exemplary embodiment of a mass
30 flow meter including a tubular housing and a flexible plate positioned within the tubular housing and provided with an actuating device arranged in an area about a longitudinal center of the flexible plate, and with the flexible plate illustrated in an unactuated state and with groups of magnets or magnetizable material arranged on the flexible plate;

Fig. 3A is a perspective view illustrating a flexible plate with four vanes that may be used in a mass flow meter, where the flexible plate is illustrated in an actuated, twisted 1st harmonic state;

Fig. 3B is a perspective view of the flexible plate from Fig. 3A where the flexible plate with four vanes that may be used in a mass flow meter, is illustrated in an actuated, twisted 2nd harmonic state;

Fig. 3C is a perspective view of the flexible plate from Fig. 3A where the flexible plate with four vanes that may be used in a mass flow meter, is illustrated in an actuated, twisted 3rd harmonic state;

Fig. 3D is a perspective view of the flexible plate from Fig. 3A where the flexible plate with four vanes that may be used in a mass flow meter, is illustrated in an actuated, twisted 4th harmonic state;

Fig.4A is a perspective view of a further exemplary illustration of a mass flow meter with two tubular housings arranged in parallel adjacent to each other and with a flexible plate positioned within each of the tubular housings. The two flexible plates include four vanes, and where the two flexible plates are illustrated in a 1st harmonic position of opposite phase.;

Fig. 4B shows the mass flow meter illustrated in Fig.4, illustrating the fluid flows V_{z1} and V_{z2} entering the respective tubular housings and where an actuator system actuates the two flexible plates with a force $-F_{x1}$ and F_{x2} respectively providing the 1st harmonic excitation of opposite phase respectively;

Fig.4C shows the cross-sections of each of the two tubular housings from Fig.4B illustrating the four vanes, actuator system and the forces $-F_{x1}$ and F_{x2} acting on the vanes;

Fig.5A illustrates in cross-section an embodiment of an electromagnetic actuator system for a mass flow meter, where groups of permanent magnets each forming a dipole are arranged in each of the four vanes of a flexible plate forming a quadrupole cross section, and with the coil systems of the electromagnetic actuator system arranged on the outside of the tubular housing;

Fig.5B illustrates in cross-section an embodiment of an electromagnetic actuator system for a mass flow meter, where groups of permanent magnets each group forming a dipole are arranged in each of the four vanes of a flexible plate forming a 4-group dipole cross section and with two coil systems surrounding the flexible plates on each side of the center of the flexible plate;

Fig.5C illustrates in cross-section an embodiment of an electromagnetic actuator system for a mass flow meter, where groups of permanent magnets each group forming a dipole are arranged in each of the four vanes of a flexible plate forming a 2-group dipole cross section and with two coil systems surrounding the flexible plates on each side of the center of the flexible plate;

Fig.6 illustrates in longitudinal cross-section of a tubular housing of a mass flow meter with an internal liner and outer tube working as pressure containing part;

Fig. 7 is a flow diagram illustrating an exemplary embodiment of a method for measuring mass flow.

The drawings are illustrations and are not necessarily to scale. The drawings are intended to illustrate example embodiments of the subject matter disclosed herein, and should therefore not be considered as limiting the scope of the disclosure.

DETAILED DESCRIPTION

Example embodiments are described with reference to the drawings. The drawings are illustrations for understanding of the principles of the disclosed mass flow meter concerning e.g. the construction, function, manufacture and use of the mass flow meter and its different parts. The drawings are not necessarily to scale.

Fig. 1 illustrates a prior art mass flowmeter 200 with a fluid channel 100 (e.g., a pipe or pipeline) containing a flowing fluid and a mass flow meter 200 at least partially coupled thereto at respective ends. The mass flow meter 200 has a tubular housing 202 and a flexible plate 204 configured to vibrate in torsion such that measurement of the movement of the flexible plate 204 can be related to mass flow of the flowing fluid. Mass flow can be measured directly by the mass flow meter 200 regardless of the geometry of the tubular housing 202. The prior art mass flowmeter is provided with one actuator 210 positioned on a surface of the tubular housing 204 in a longitudinal center of the tubular housing. The actuator is configured to apply an oscillating torque to the flexible plate sufficient to vibrate the flexible plate in torsion. The frequency of the actuator may be set to a resonance frequency of the flexible plate. Two sensors 214, 216 are arranged symmetrically about the longitudinal center of the tubular housing to measure a plurality of oscillations of the flexible plate as a function of time at these two locations arising from the applied oscillating torque.

Fig.1B illustrates the mass flow meter from Fig.1A where torsion is applied to the flexible plate. As shown, the longitudinal axis A of the flexible plate is parallel to the x-axis of the mass flow meter. Forces F_A , $-F_A$ applied by the actuator may have opposite directions parallel to the y-axis. The forces may act along the width, partly or whole width, of the flexible plate. The applied forces F_A , $-F_A$ is varied in magnitude and direction to provide an oscillating torque exciting the flexible plate to vibrate in a torsional mode. The resulting Coriolis forces $-F_C$, F_C acting on the flexible plate provides a torsional vibration with an angular velocity Ω_y and Ω_y .

When the flexible plate is excited and vibrates in a torsional mode and interacts with the fluid flow to be measured, a phase shift will occur between the oscillations in two different positions of the flexible plate. The mass of the flowing fluid effects the excitation of the flexible plate and causes a delay of the excitation or wave travelling along the flexible plate. This delay may be viewed as some sort of Doppler effect when travelling along the flexible plate in the longitudinal direction. The phase shift is approximately proportional to the mass flow of the fluid flow. The sensors may therefore be arranged a distance apart to provide a sufficiently long travel length for the fluid flow along the flexible plate before detection by the second sensor. A direct measurement of mass flow of the fluid may be achieved by determining the proportionality constant of the mass flow meter. Estimation of the mass flow of fluid may then be performed by a computing device receiving sensor signals from the sensor system.

Fig. 2A and 2B illustrate exemplary embodiments of a mass flow meter 310 with a tubular housing 350. The tubular housing may be in the form of a generally circular cylinder having a length L, a wall thickness T, and an inner radius R defining a cavity 353. The length L of the tubular housing 300 and the cavity 353 extend along a longitudinal axis A between a housing inlet and a housing outlet positioned at ends of the tubular housing 350. The tubular housing 300 may be substantially straight between the housing inlet and the housing outlet. The surfaces of the tubular housing in contact with the fluid flow may be rounded and smooth to avoid unnecessary friction disturbing the fluid flow.

The tubular housing 353 may take other geometric forms depending e.g. on the fluid channel (e.g. pipeline) and the fluid flow to be monitored, as well as other circumstances as e.g. temperature and/or pressure of the surroundings, temperature and/or pressure of the fluid flow, the material of the fluid channel , and
 5 the tubular housing. The geometry and/or materials of the tubular housing may be approximately the same as that of the fluid channel. The tubular housing may be formed from any suitable materials including, for example, polymers, ceramics, metals, and metal alloys (e.g., steels, copper and copper alloys, aluminum and aluminum alloys, etc.).

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The mass flow meter 310 may be integrally formed with the fluid channel. The entire fluid flow V_x 351 passes through the mass flow meter. An inlet and an outlet of the mass flow meter housing may form a fluid-tight coupling with the fluid channel or pipeline pumps, dispensers, etc. of the fluid flow system. Examples of
 15 fluid-tight couplings can include, but are not limited to, threaded engagements, clamps, welds, and the like.

The mass flow meter 310 may be arranged inside a pipeline. The tubular housing is then not exposed to pressure from the surroundings enabling use of the mass
 20 flow meter in high pressure environments. This enable the tubular housing to be made of a much thinner and lighter material than the pipeline. The tubular housing may be a liner. The liner may be made of non-magnetizable material. The liner may be made of an electrically conducting or electrically non-conducting material. A pressure housing 390 (Fig.6) may be arranged outside the liner 391. The
 25 pressure housing may be made of an electrically conducting material.

The electromagnetic actuator systems (302, 303) may include an electromagnetic device arranged on the outside of the tubular housing and a magnetizable material arranged on the inside of the tubular housing. The two forces from the actuator
 30 systems are indicated as F_{A1} , $-F_{A1}$ and F_{A2} , $-F_{A2}$ respectively. These force couples are the same as the torques. The resulting Coriolis forces $-F_C$, F_C acting on the flexible plate provides a torsional vibration with an angular velocity Ω_y and Ω_y . A net sum of the two oscillating torques applied to the flexible plate may be zero or substantially zero. The at least two oscillating torques may have opposite

directions as illustrated in Fig.2A. A sum of the at least two oscillating torques may be less than the largest of the at least two oscillating torques. If e.g. applying three oscillating torques the sum of all the oscillating torques should be zero or substantially zero. The mass flow meter is provided with two sensor systems (301, 304).

Fig.6 illustrates an embodiment a mass flow meter with an internal liner 391 and outer tube 390 working as pressure containing part. The electromagnetic actuators 302, 303 and the sensor systems 301, 304 may be arranged on the inside of the pressure housing, but on the outside of the liner. The space between the pressure housing and the liner may be filled with a liquid or solid filler material to transfer the pressure from the fluid flow 351 on the inside of the liner 391 and out to the pressure housing. The filler material may also serve to protect the electromagnetic actuators and sensor systems. As the tubular housing may be a liner it does not need to withstand the high pressure of the fluid flow. This solution may e.g. be used for measuring high pressure fluids where the outer pressure housing would be too thick and use of electromagnetic actuators would not be possible.

FIG. 2A illustrates the flexible plate 352 positioned within the tubular housing. The flexible plate is illustrated in a 2nd harmonic oscillation. The tubular housing forming a cavity 353. The flexible plate 352 can extend in the direction of the longitudinal axis A of the tubular housing 350. The flexible plate 352 may extend along at least a part of the tubular housing 350. The flexible plate can be at least partially coupled to an interior wall of the tubular housing 350 (e.g., a wall of the cavity 353) at one or more locations. The flexible plate may be partially coupled to an interior wall of the tubular housing at opposed longitudinal ends of the flexible plate. As an example, a first terminal end of the flexible plate can be at least partially coupled to the tubular housing at or near the housing inlet i and a second terminal end of the flexible plate can be at least partially coupled to the tubular housing at or near the housing outlet. The flexible plate may alternatively be mounted to the tubular housing 350 at one of the terminal ends of the flexible plate. In further embodiments, more than one flexible plate 352 can be positioned within the housing (not shown).

As illustrated in FIG. 2B, the flexible plate 352 can be in the form of a substantially planar plate. The flexible plate may have a width W approximately equal to an inner diameter ($2R$) of the tubular housing 350. As any gap between the wall of the cavity 353 and the flexible plate 352 is small this does not allow a significant amount of the fluid V_x to pass between opposite edges of the flexible plate 352 (e.g., vertically in FIG. 2B). As the gap is small, the flexible plate interacts with substantially the entire fluid flow passing through the tubular housing. In some embodiments, the flexible plate may have a curved shape in an equilibrium or unfixed state (not shown). The flexible plate may in some embodiments be extended/stretched and provided with a tension when attached inside the tubular housing, to change the resonance frequency of the flexible plate.

The mass flow meter can include an actuator system 302, 303. The actuator system may be configured to apply at least two oscillating torques to the flexible plate sufficient to vibrate the flexible plate in torsion. The actuator system may include two actuators 302, 303 as illustrated in Fig.2A and 2B. As shown in FIG. 2A and 2B, the two actuators are positioned outside the tubular housing 350. Positioning outside the tubular housing may e.g. involve on the surface of the tubular housing, or adjacent to the outer surface of the tubular housing. The actuator system 302, 303 may be arranged in different positions in the longitudinal direction of the tubular housing. The actuators may be positioned symmetrically about a longitudinal centre of the flexible plate 352.

The actuators 302, 303 can be configured to apply an oscillating torque to the flexible plate 352 to drive the flexible plate to vibrate in a torsional mode at a selected frequency. The torsional mode may be a resonance frequency of the flexible plate, including the fundamental frequency but also even and uneven harmonics. The torsional mode may be a 2nd harmonic oscillation, 3rd harmonic oscillation or 4th harmonic oscillation as illustrated in Figures 3A-3D respectively, but also higher harmonics may be applied. In Fig.2A-2B the actuators 302, 302 are positioned at $3/8$ and $5/8$ of the length of the flexible plate. Sensors or sensor system 301, 304 for detecting the result of the interaction between the fluid flow and the actuated flexible plate 352 are positioned in positions corresponding to $1/8$ and $7/8$ of the length of the flexible plate. These positions ($1/8$, $3/8$, $5/8$, $7/8$)

correspond to the positions of the amplitude maxima of a 4th harmonic oscillation of the flexible plate, which will be described later.

At least two actuators may be used. A net sum of the at least two oscillating
5 torques applied to the flexible plate by the at least two actuators may be zero or substantially zero. The at least two oscillating torques may have opposite directions. A sum of the at least two oscillating torques may be less than the largest of the at least two oscillating torques. If e.g. applying three oscillating torques the sum of all the oscillating torques should be zero or substantially zero.

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The actuators 302, 303 may be electromagnetic actuators. An electromagnetic actuator may be in the form of one or more electromagnetic coils. An electromagnetic coil is a coil that may have a magnetic core. The coils may be arranged around the tubular housing and the magnetic core provided by a
15 magnetic material 150, 151, 152, 153, 154, 155, 156, 157 arranged in or on the flexible plate. At least a portion of the flexible plate 352 can be formed from a magnetic material (e.g., metals, metal alloys, steels, polymers, etc.). The flexible plate 352 can include one or more embedded permanent magnets 150, 151, 152, 153, 154, 155, 156, 157. The magnetic material or permanent magnet(s) 150, 151,
20 152, 153, 154, 155, 156, 157 may also be arranged on the outer surface of the flexible plate 352. The magnetic material and permanent magnets 150, 151, 152, 153, 154, 155, 156, 157 may be arranged on the flexible plate in positions within the magnetic field from the coils. The permanent magnets or the magnetic material of the flexible plate may be arranged in corresponding positions as the coils as
25 illustrated in Fig.2B, to enable effective actuation of the flexible plate by the magnetic field from the coils. The coils may be connected to a controller 300 or e.g. computing device for controlling the current supplied to the coils generating the magnetic field to apply an oscillating torque to the flexible plate at a selected frequency. At least one of the magnitude, frequency and/or phase of the current
30 applied to the coils may be controlled to enable generating one or more magnetic field(s) to apply an oscillating torque to the flexible plate. The flexible plate may be driven at resonance frequency both at fundamental frequency, but also at even and uneven harmonics. The controller may e.g. be a computer or power supply.

The coils may be configured to receive feedback e.g. from a sensor system to drive the flexible plate at resonance.

As mentioned, the mass flow meter 310 can also include a sensor system 301, 304 to measure the interaction between the mass flow and the flexible plate vibrating in torsion. The sensor system 301, 304 may be configured to measure movement of the flexible plate 352 as a function of time. The sensor system 301, 304 may measure the movement of the flexible plate at positions upstream and downstream of the longitudinal centre C with respect to the flow of fluid V_x 351.

The movement of the flexible plate 352 can be characterized by any parameter of the flexible plate that oscillates as a function of time when the flexible plate vibrates in torsion. Example parameters can include, but are not limited to, linear and/or angular parameters such as position, speed, acceleration, and displacement. In certain embodiments, angle, angular speed, and angular acceleration can be measured. In other aspects, stress and/or strain can be measured. The sensor system 301, 304 may be in the form of pickup sensors arranged at positions along the tubular housing. The pickup sensors may measure rotational speed and direction of the flexible plate. The pick-up sensors may e.g. be based on the Hall effect or may be magnetic pick-up sensors. Magnetic pick-up sensors may have coils arranged on the outside of the tubular housing e.g. on, embedded in or partially embedded in or near the tubular housing. In other embodiments, the sensors may be in the form of electromagnetic sensors. The electromagnetic sensors may be electromagnetic coils with coils arranged around the tubular housing and with the magnetic core provided by magnetic material in or on the flexible plate as explained above for the actuating system. The electromagnetic sensors may also in some embodiments be the actuating system itself. The electromagnetic actuating system may then be controlled to switch between an actuating mode applying an oscillating torque to the flexible plate and a detecting mode detecting movements of the flexible plate. The mode switching may be performed continuously or intermittently during measurement by the mass sensor. In other embodiments the sensor system may be in the form of strain gauges arranged at the end of the flexible plate. In the end of the flexible plate, there is no speed or acceleration. The sensor system may be connected to a computing device or controller or other device receiving sensor signals from the

sensor system. The computer device, controller or other device may also control the sensor system.

The sensor system 301, 304 may include a number of sensors arranged in
5 different positions in the mass flow meter. The sensor system may be arranged in positions where the flexible plate exhibits the largest movement during excitation by the applied torque. In Fig. 2A, 2B the sensor system is as earlier described, provided with two sensors positioned where the 4th harmonic oscillation of the flexible plate has maximum amplitudes. These positions are at 1/8, 3/8, 5/8, 7/8 of
10 the length of the flexible plate. Measurement of the largest parameter values ensures a large signal output from the sensor system and thus an increased sensitivity. Actuating the flexible plate by the actuating system in positions of the largest amplitudes, results in a higher energy transfer to the flexible plate also contributing to an improved sensitivity for the mass flow sensor. Using two
15 sensors, a first sensor may be positioned at 1/8 and a second sensor at 7/8 of the length of the flexible plate as illustrated in Fig.2A. This leaves space for the positioning of the actuating systems at 3/8 and 5/8 of the length of the flexible plate as illustrated in Fig.2A and as explained above. Driving the flexible plate in 2nd, 3rd, 4th and higher harmonics may increase the Q-factor and the sensitivity of
20 the mass sensor. The Q-factor is in simplified terms in this context a relationship between the energy of the flexible plate in an oscillating behavior and the energy input into the flexible plate to provide the oscillating behavior. In general, the resulting torsion applied to the flexible plate should be in a position where an applied torque result in an oscillating behavior with large amplitudes of the flexible
25 plate. In these positions with the largest amplitudes, the flexible plate will also experience the largest changes in speed and acceleration when exposed to the fluid flow. These changes are measured by the sensor system of the mass flow meter. The positioning of sensors and actuating system in positions corresponding to the 4th harmonics of the flexible plate, may also be used for 2nd and 3rd
30 harmonics. The positioning of the sensors and actuating system would then also be close to the amplitude maxima for the oscillations of the flexible plate. The embodiment illustrated in Fig.2A, 2B enable the mass flow meter to be driven in both uneven and even harmonic states offering flexibility of the mass flow meter and the possibility of adaption of the mass flow meter to the actual flow situation

and the information desired from the mass flow meter. Even harmonic states provide an oscillation torque where a net sum of the oscillating torques applied to the flexible plate is zero or substantially zero. It may be possible to drive the mass flow meter in several modi simultaneously to enable detection of mass flow in a two-phase flow such as, e.g. a liquid flow with bubbles. This may be advantageous for measurement of mass flow for e.g. CO₂, NH₃, H₂ or LNG.

The flexible plate may be provided with a number of vanes . The number of vanes may be two, three, four or higher number of vanes as e.g. eight or more. The vanes may extend radially outward at about 90° with respect to one another. The angle between the vanes can be varied. The vanes can possess approximately equal width. The number of vanes and the angle between the vanes may vary depending on the characteristics of the fluid flow to be measured and other factors as the environment and surroundings of the fluid flow. The vanes increase the stiffness of the flexible plate and avoids bending of the flexible plate without increasing the torsional stiffness of the flexible plate. The mass sensor is based on applying oscillating torques to the flexible plate to vibrate the flexible plate in harmonic oscillations and a high sensitivity for torsion increases the flexible plate's sensitivity for viscosity of the fluid flow. E.g. for mass measurement of a low density fluid flow such as liquid gas e.g. H₂, or a high density liquid at high density such as e.g. CO₂, the torsional stiffness should be low to be able to measure the mass flow of H₂ and CO₂ with a sufficiently high sensitivity.

Fig.3A-D illustrate an embodiment of the flexible plate 352 with four vanes. The vanes are arranged in a cross-configuration with each vane arranged at an angle of 90 degrees with respect to each other. The figures illustrate the flexible plate in different torsional harmonic modes actuated by an actuating system. The illustrations show the maximum amplitude positions in the different harmonic modes. Fig. 3A illustrates the flexible plate in an actuated state in the 1st harmonic oscillation. In this 1st harmonic state, the maximum amplitude is at the longitudinal center of the flexible plate. Actuating systems arranged in the area around the longitudinal center would provide the largest Q-factor for the flexible plate. The positioning and arrangement of the sensors would depend on the type of sensor used. Fig. 3B illustrates the flexible plate in an actuated state in the 2nd harmonic

oscillation. The largest amplitudes are at positions $\frac{1}{4}$ and $\frac{3}{4}$ of the length of the flexible plate and these positions would provide the largest Q-factor for the system. Fig. 3C illustrates the flexible plate in an actuated state in the 3rd harmonic oscillation. The amplitude maxima are seen at positions $\frac{1}{6}$, $\frac{3}{6}$, $\frac{5}{6}$ of the length of the flexible plate. Fig. 3D illustrates the flexible plate in an actuated state in the 4th harmonic oscillation with maximum amplitudes at $\frac{1}{8}$, $\frac{3}{8}$, $\frac{5}{8}$ and $\frac{7}{8}$ of the length of the flexible plate.

Fig.2C illustrates an embodiment where an actuator system 305 is arranged in an area about a longitudinal center of the flexible plate extending over the assigned magnetic material or permanent magnet(s) 152, 153, 154, 155 in positions A_1 and A_2 . The magnetic material or permanent magnets are arranged anti-symmetrically with respect to their magnetic poles such that by driving the common coil system actuating forces F_{A1} , $-F_{A1}$ and F_{A2} , $-F_{A2}$ respectively are applied to the flexible plate in positions A_1 and A_2 with the directions illustrated by the arrows (Fig.2A). The sensor systems 301, 304 may be the same sensor systems as in Fig.2A and 2B. The actuator system covers an area of the flexible plate. The actuator system in Fig.2B may be provided by an electromagnetic actuating system with at least two coils arranged around the tubular housing and the magnets 152, 153, 154, 155 (e.g. permanent magnets or a magnetizable material) in, on or embedded in the flexible plate 352. Each coil may include a plurality of windings covering a first and a second area of the tubular housing. Each coil may be arranged side by side such that the first and second areas cover the entire area of the actuator system illustrated in Fig.2C. Each coil may also be arranged a distance from the center of the tubular housing in the area illustrated by the actuator system in Fig. 2C. Two groups of permanent magnets forming dipoles may be arranged on or in the flexible plate, or partly embedded or embedded in the flexible plate. The coils may be arranged at a distance sufficiently apart from each other to be able to apply at least two oscillating torques to the flexible plate to vibrate the flexible plate with the permanent magnets in torsion. The two groups of dipole permanent magnets may be anti-symmetrically arranged with respect to their magnetic poles. Each permanent magnet may be a bar magnet and a group may be formed by arranging each bar magnet side by side with the poles facing in the same direction to provide a more powerful magnet. A group may also include a plurality of layers of bar

magnets. Forming a group of permanent dipole magnets results in a forceful magnetic dipole increasing the magnetic field and thus the resulting torque applied to the flexible plate. By driving the two coils symmetrically; i.e. driving the two coils with a current having the same frequency and phase, the magnetic fields from the two coils will have the same direction at the same time. As the two groups of dipole magnets are arranged with opposed dipoles, the flexible plate will experience two oppositely directed oscillating torques applied to the flexible plate in the position A1, A2 of the group of magnets. The net sum of the oscillating torques applied to the flexible plate may be zero or substantially zero. By using two coils, the actuator system may be configured to apply at least two oscillating torques to the flexible plate sufficient to vibrate the flexible plate in torsion. The embodiment in Fig.2C may vibrate the flexible plate in a 1st harmonic oscillation.

Fig.4A, 4B illustrates a further embodiment of the mass flow meter 310, where two tubular housings 350 are arranged side by side. Each tubular housing is provided with a flexible plate 352. Each flexible plate extending along at least a part of the tubular housing and is at least partially coupled to an interior wall of the tubular housing at opposed longitudinal ends of the flexible plate such that the flexible plate is able to vibrate in torsion. The two flexible plates are illustrated in a 1st harmonic position of opposite phase. The fluid flow to be measured is made to flow through both the tubular housings. The flexible plate may be provided with a number of vanes. in Fig.4A, 4B each flexible plate is provided with four vanes arranged at an angle of 90 degrees with respect to each other. The actuator system 340 may be arranged in an area at the longitudinal center of the flexible plate. One actuator system may be provided covering both the tubular housings. This common actuator system may e.g. have a coil covering the two tubular housings. Permanent magnets or magnetizable material may be provided in each flexible plate. An actuator system may alternatively be provided for each of the tubular housings. The actuator system may actuate the two flexible plates with forces $-F_{x1}$ and F_{x2} respectively providing the 1st harmonic oscillation of opposite phase respectively as shown.

The two flexible plates are illustrated in a 1st harmonic torsional excitation, but where the torsional oscillation of the 1st harmonics have opposite phase. The fluid flow flows through both the tubular housings of the mass flow meter, and as the

fluid flow interacts with the oscillating flexible plates of opposite phase, the combined signals from the sensors of the mass flow meter may have increased sensitivity. The torsional stiffness of the flexible plate may have small variations along its length and using two similar flexible plates oscillating in different phase
 5 may even out these small variations in torsional stiffness.

Fig.4C shows the cross-sections of each of the two tubular housings from Fig.4B illustrating the four vanes, actuator system and the direction of the forces $-F_{x1}$ and F_{x2} acting on the vanes. The configuration of the flexible plate with four vanes as
 10 illustrated in Fig. 4A-4C may be used e.g. in the mass flow meter illustrated in Fig.2A-2C.

Possible configurations of the coils and the permanent magnets of an electromagnetic actuating system are illustrated in Fig.5A-5C for a flexible plate
 15 with four vanes. Fig. 5A-5C are shown in cross-section showing the configuration of the permanent magnets. Fig.5A illustrates a quadrupole cross section and with the coil systems 360, 361, 362, 363 of the electromagnetic actuator system arranged on the outside of the tubular housing. The magnets in the vanes are arranged with alternating magnetic poles facing outwards (north, south, north,
 20 south). Fig.5B illustrates a 4-group dipole cross section of permanent magnets and with two coil systems 370, 371 surrounding the flexible plates on each side of the center of the flexible plate. The magnets are arranged with pairs of magnetic poles facing outwards (north, north, south, south). Fig.5C illustrates a 2-group dipole cross section of permanent magnets and with two coil systems 380, 381
 25 surrounding the flexible plates on each side of the center of the flexible plate. The magnets in the vanes are arranged with different magnetic poles facing outwards (north, south,) forming a dipole.

In Fig.5A the electromagnetic actuator system has groups of permanent magnets
 30 arranged in each of the four vanes of the flexible plate. Each group of magnets may be formed by dipole bar magnets arranged side by side forming a dipole. The direction of the dipole is altered from one vane to the next vane as illustrated in Fig.5A. In a first vane the north pole N points outwards and in the second vane the north pole N points inwards, in the third vane the north pole N points outwards and

in the fourth vane the north pole N points inwards. The south poles S of the first vane and the third vane face each other, and the north poles for the second vane and the fourth vane face each other. In Fig.5A the groups of magnets facing each other also have dipoles facing each other. The groups of magnets may be
 5 arranged around the longitudinal center of the flexible plate. Two coils may form a common coil system surrounding the flexible plate in an area of the longitudinal axis of the flexible plate. By controlling the phase of the current applied to the coils, oscillating torques of opposite directions are applied to each of the vanes of the flexible plate due to alternation of the direction of the dipole between the
 10 vanes. The frequency of the current is also controlled to torsionally excite the flexible plate in a harmonic oscillation and the magnitude of the current controlled to provide a desired amplitude of the oscillations of the vanes.

In the embodiment of Fig.5B two electromagnetic actuator systems 370, 371,
 15 where each system is as illustrated in Fig. 5A, may be symmetrically arranged with respect to the longitudinal center of the flexible plate. The first actuator system may be arranged in position $3/8$ of the longitudinal length of the flexible plate, and the second actuator system may be arranged in position $5/8$ of the longitudinal length of the flexible plate. Each actuator system may include groups of
 20 permanent bar magnets arranged side by side with the same pole facing the same way (symmetrically arranged) forming a dipole in each vane in the same positions ($3/8$ and $5/8$) as the two coils surrounding the flexible plate. In this embodiment the two groups of magnetic dipoles of each vane have the same direction. The two electromagnetic actuator systems may be driven with current of opposite phase
 25 (anti-symmetrically) to apply a torsion to the flexible plate providing a 4th harmonic oscillation of the flexible plate. Increasing the number of windings increases the magnetic field from the coil.

In Fig.5B, if the two groups of permanent magnets in the actuator systems had
 30 been anti-symmetrically arranged with respect to each other; i.e. the magnetic poles of the two groups of permanent magnets had been facing in the opposite direction, the coils of each actuator system would be driven in symmetry, i.e. with the same frequency, phase and amplitude. In Fig.5A where the actuator system has two coils, these two coils are driven with current of opposite phase. The

groups of permanent magnets in Fig.5A may also be arranged with the dipoles of each group of magnets facing the same way. The applied current to the two coils illustrated in Fig.5A would then have opposite phase, but the same frequency and magnitude.

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The groups of magnets illustrated in Fig.5A form a quadrupole. Using eight vanes and one group of magnets in each vane, this form an octupole. Multipole arrangements of permanent magnets increase the torsion for the same applied current. In the illustrated embodiments in Fig. 5A and 5B, bar magnets are used, but also round magnets may be used. Also, several groups of magnets may be provided in each vane depending on the torsional force required.

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The configuration of the groups of magnets may vary. They may be symmetrically arranged as illustrated in Fig.5B. They may also be anti-symmetrically arranged (not shown) where the poles of a group of magnets have opposite direction in position 3/8 and 5/8 in the same vane. The current in the coils of the actuating system for anti-symmetrically arrange groups of magnets, are in phase (symmetrical) to apply a net sum of the at least two oscillating torques applied to the flexible plate being zero or substantially zero. The at least two oscillating torques have opposite directions. A sum of the at least two oscillating torques may be less than the largest of the at least two oscillating torques.

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The configuration of magnetizable material and the frequency, phase and magnitude of the current applied to the coils, may also be designed according to the principle of a reluctance motor to generate torque based on magnetic reluctance. The flexible plate with magnetizable material would correspond to the rotor of the reluctance motor. The coils arranged on the outside of the tubular housing would correspond to the stator poles. The current in the coil would be controlled such that the phase of the current changes as a function of time to provide the desired effect with respect to generating a torque corresponding to the movement between the stator and rotor of a reluctance motor. In this configuration corresponding to the reluctance motor principle, the actuator system may also be used as the sensor system may as explained earlier. The current phase and frequency applied to the coils would then also be driven intermittently in time to switch between a torque generation mode generation a torque in the flexible plate

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and a detection mode detecting the movement of the flexible plate as a result of the applied torque. The configuration based on the reluctance motor principle may be apply torques driving the flexible plate in the 1st harmonic state when two electromagnets are driven with opposite phase (anti-symmetric).

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The actuating system with electromagnetic actuators and permanent magnets (the embedded permanent magnets) may be arranged in various configurations to achieve torsional vibration of the flexible plate at resonance frequencies of the flexible plate. The material of the housing may not be made of magnetic material in an embodiment with electromagnetic actuators and embedded permanent magnets.

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Fig. 7 is a flow diagram illustrating an exemplary embodiment of a method for measuring mass flow. The mass flow meter is connected to the fluid flow to be measured. The fluid flow flows through the at least one tubular housing. The least one actuator system drive the flexible plate within the at least one tubular housing to vibrate in a torsional mode at a selected frequency by applying at least two oscillating torques to the flexible plate to vibrate the flexible plate in torsion. A plurality of oscillations of the flexible plate are measured by the at least two sensor systems configured to measure oscillations of the flexible plate as a function of time. The sensor systems measure the oscillations in at least two locations arising from the at least two applied oscillating torques. A mass flow of the fluid flowing within the at least one tubular housing is determined based on a phase shift between the oscillations measured at the at least two locations.

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A net sum of the at least two oscillating torques applied to the flexible plate may be zero or substantially zero. The at least two oscillating torques may have opposite directions. The two torques may then cancel each other and provide a significantly improved differential measurement. A sum of the at least two oscillating torques may be less than the largest of the at least two oscillating torques.

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The mass flow meter may be used for measuring mass flow of e.g. CO₂, NH₃, and H₂ or LNG or other gas flows at high pressures.

Having described example embodiments of the invention it will be apparent to those skilled in the art that other embodiments incorporating the concepts may be used. These and other examples illustrated above are intended by way of example only and the actual scope of the invention is to be determined from the following

5 claims.

CLAIMS

1. A mass flow meter (310), comprising:
 - a tubular housing (350) extending along a longitudinal axis and configured to receive a flow of fluid (351) therethrough;
 - a flexible plate (352) extending along at least a part of the tubular housing (350) and at least partially coupled to an interior wall of the tubular housing (350) at opposed longitudinal ends of the flexible plate (352) such that the flexible plate (352) is able to vibrate in torsion;
 - at least one electromagnetic actuator system (302, 303, 370, 371, 340) configured to apply at least two oscillating torques to the flexible plate (352) sufficient to vibrate the flexible plate in torsion; and
 - at least two sensor systems (301, 304) configured to measure oscillations of the flexible plate (352) as a function of time at locations arising from the at least two applied oscillating torques.
2. Mass flow meter according to claim 1, wherein a net sum of the at least two oscillating torques applied to the flexible plate (352) is zero or substantially zero.
3. Mass flow meter according to claim 1 or claim 2, wherein the at least two oscillating torques have opposite directions.
4. Mass flow meter according to claim 1, wherein a sum of the at least two oscillating torques are less than the largest of the at least two oscillating torques.
5. Mass flow meter according to claim 1, wherein the at least one electromagnetic actuator system (302, 303, 370, 371) comprising an electromagnetic device arranged on the outside of the tubular housing (350) and a magnetizable material arranged on the inside of the tubular housing (350).
6. Mass flow meter according to claim 1, wherein the electromagnetic device comprises at least one coil (360, 361, 362, 363, 370, 371, 380, 381) arranged on the outside of the tubular housing (350).

7. Mass flow meter according to claim 5, wherein the magnetizable material is arranged on the flexible plate (352).
8. Mass flow meter according to claim 5, wherein the magnetizable material comprises at least one permanent magnet.
9. Mass flow meter according to claim 5, wherein the magnetizable material comprises at least one group of permanent magnets wherein the permanent magnets are symmetrically arranged side by side forming a dipole.
10. Mass flow meter according to claim 5, wherein the magnetizable material comprises four groups of permanent magnets forming a quadrupole.
11. Mass flow meter according to claim 5, wherein the magnetizable material comprises four groups of permanent magnets forming a dipole.
12. Mass flow meter according to one of claims 1-11, wherein each of the two sensor systems comprising a pick-up.
13. Mass flow meter according to one of claims 1-12, wherein the at least one electromagnetic actuator system (302, 303, 370, 371, 340) is adapted to also function as a sensor system.
14. Mass flow meter according to claim 1-13, wherein the tubular housing (350) is a liner of a non-magnetizable material.
15. Mass flow meter according to claim 14, further comprising a pressure housing (390) arranged outside the liner.
16. Mass flow meter according to claim 6-15, wherein the at least one coil (360, 361, 362, 363, 370, 371, 380, 381) is arranged to provide an alternating electromagnetic field alternatingly magnetizing and demagnetizing the magnetizable material.

17. A method for measuring mass flow through at least one tubular housing (350), comprising:
- receiving a flow of fluid (351) through the at least one tubular housing (350), wherein the tubular housing (350) comprising a flexible plate (352) extending along at least a part of the at least one tubular housing and is at least partially coupled to an interior wall of the at least one tubular housing at opposed longitudinal ends of the flexible plate (352) such that the flexible plate (352) is able to vibrate in torsion;
 - driving by at least one actuator system the flexible plate (352) within the at least one tubular housing (350) to vibrate in a torsional mode at a selected frequency by applying at least two oscillating torques to the flexible plate (352) to vibrate the flexible plate in torsion;
 - measuring a plurality of oscillations of the flexible plate (352) by at least two sensor systems configured to measure oscillations of the flexible plate (352) as a function of time at at least two locations arising from the at least two applied oscillating torques; and
 - determining a mass flow of the fluid flowing within the at least one tubular housing (350) based on a phase shift between the oscillations measured at the at least two locations.
18. Method according to claim 17, wherein a net sum of the at least two oscillating torques applied to the flexible plate is zero or substantially zero.
19. Method according to claim 17 or claim 18, wherein the at least two oscillating torques have opposite directions.
20. Method according to one of claims 17-19, wherein a sum of the at least two oscillating torques are less than the largest of the at least two oscillating torques.
21. Use of the mass flow meter of one of claims 1-16 or the method according to one of claims 17-20 for measuring mass flow of a fluid flow of CO₂, NH₃, H₂ or natural gas.

PATENTKRAV

1. Massestrømsmåler (310), omfattende:

- et rørformet hus (350) som strekker seg langs en longitudinal akse og konfigurert til å motta en fluidstrøm (351) derigjennom;
- en fleksibel plate (352) som strekker seg langs minst en del av det rørformede huset (350) og minst delvis koblet til en indre vegg av det rørformede huset (350) ved motstående longitudinale ender av den fleksible platen (352) slik at den fleksible platen (352) er i stand til å vibrere i torsjon;
- minst ett elektromagnetisk aktuator-system (302, 303, 370, 371, 340) konfigurert til å påføre minst to oscillerende torsjonsmoment på den fleksible platen (352) tilstrekkelig til å vibrere den fleksible platen i torsjon; og
- minst to sensorsystemer (301, 304) konfigurert til å måle oscillasjoner av den fleksible platen (352) som en funksjon av tid i lokasjoner som oppstår fra de minst to påførte oscillerende torsjonsmoment.

2. Massestrømsmåler ifølge krav 1, hvor en netto sum av de minst to oscillerende torsjonsmoment påført på den fleksible platen (352) er null eller hovedsakelig null.

3. Massestrømsmåler ifølge krav 1 eller krav 2, hvor de minst to oscillerende torsjonsmoment har motsatte retninger.

4. Massestrømsmåler ifølge krav 1, hvor en sum av de minst to oscillerende torsjonsmoment er mindre enn den største av de minst to oscillerende torsjonsmomenter.

5. Massestrømsmåler ifølge krav 1, hvor det minst ene elektromagnetiske aktuator-systemet (302, 303, 370, 371) omfatter en elektromagnetisk anordning anordnet på utsiden av det rørformede huset (350) og et magnetiserbart materiale anordnet på innsiden av det rørformede huset (350).

6. Massestrømsmåler ifølge krav 1, hvor den elektromagnetiske anordning omfatter minst en spole (360, 361, 362, 363, 370, 371, 380, 381) anordnet på utsiden av det rørformede huset (350).
7. Massestrømsmåler ifølge krav 5, hvor det magnetiserbare materialet er anordnet på den fleksible platen (352).
8. Massestrømsmåler ifølge krav 5, hvor det magnetiserbare materialet omfatter minst en permanentmagnet.
9. Massestrømsmåler ifølge krav 5, hvor det magnetiserbare materialet omfatter minst en gruppe av permanentmagneter hvor permanentmagnetene er symmetrisk anordnet side ved side dannende en dipol.
10. Massestrømsmåler ifølge krav 5, hvor det magnetiserbare materialet omfatter fire grupper av permanentmagneter dannende en kvadrupol.
11. Massestrømsmåler ifølge krav 5, hvor det magnetiserbare materialet omfatter fire grupper av permanentmagneter dannende en dipol.
12. Massestrømsmåler ifølge ett av kravene 1-11, hvor hver av de to sensorsystemene omfatter en pickup.
13. Massestrømsmåler ifølge ett av kravene 1-12, hvor det minst ene elektromagnetiske aktuatorsystemet (302, 303, 370, 371, 340) er tilpasset til også å fungere som et sensor-system.
14. Massestrømsmåler ifølge krav 1-13, hvor det rørformede huset (350) er en liner av et ikke-magnetiserbart materiale.
15. Massestrømsmåler ifølge krav 14, videre omfattende et trykk-hus (390) anordnet på utsiden av lineren.

16. Massestrømsmåler ifølge krav 6-15, hvor den minst ene spolen (360, 361, 362, 363, 370, 371, 380, 381) er anordnet for å tilveiebringe et alternerende elektromagnetisk felt som alternerende magnetiserer og avmagnetiserer det magnetiserbare materialet.
17. Fremgangsmåte for å måle massestrøm gjennom minst ett rørformet hus (350), omfattende:
- å motta en fluidstrøm (351) gjennom det minst ene rørformede huset (350), hvor det rørformede huset (350) omfattende en fleksibel plate (352) som strekker seg langs minst en del av det rørformede huset og i det minste delvis er koplet til en indre vegg i det rørformede huset ved motstående longitudinale ender av den fleksible platen (352) slik at den fleksible platen (352) er i stand til å vibrere i torsjon;
 - å drive ved minst ett aktuatorsystem den fleksible platen (352) inne i det minst ene rørformede huset (350) til å vibrere i en torsjonsmodus ved en valgt frekvens ved å påføre minst to oscillerende torsjonsmoment på den fleksible platen (352) for å vibrere den fleksible platen i torsjon;
 - å måle et flertall av oscillasjoner av den fleksible platen (352) ved minst to sensor-systemer konfigurert til å måle oscillasjoner av den fleksible platen (352) som en funksjon av tid ved minst to lokasjoner som oppstår fra de minst to påførte oscillerende torsjonsmoment; og
 - å bestemme en massestrøm av fluidet som strømmer inne i det minst ene rørformede hus (350) basert på et faseskift mellom oscillasjonene målt ved de minst to lokasjoner.
18. Fremgangsmåte ifølge krav 17, hvor en netto sum av de minst to oscillerende torsjonsmoment påført på den fleksible platen er null eller hovedsakelig null.
19. Fremgangsmåte ifølge krav 17 eller krav 18, hvor de minst to oscillerende torsjonsmoment har motsatte retninger.
20. Fremgangsmåte ifølge ett av kravene 17-19, hvor en sum av de minst to oscillerende torsjonsmoment er mindre enn den største av de minst to oscillerende torsjonsmoment.

21. Anvendelse av massestrømsmåleren i ett av kravene 1-16 eller fremgangsmåten ifølge ett av kravene 17-20 for måling av massestrøm i en fluidstrømning av CO_2 , NH_3 , H_2 eller naturgass.

1/16

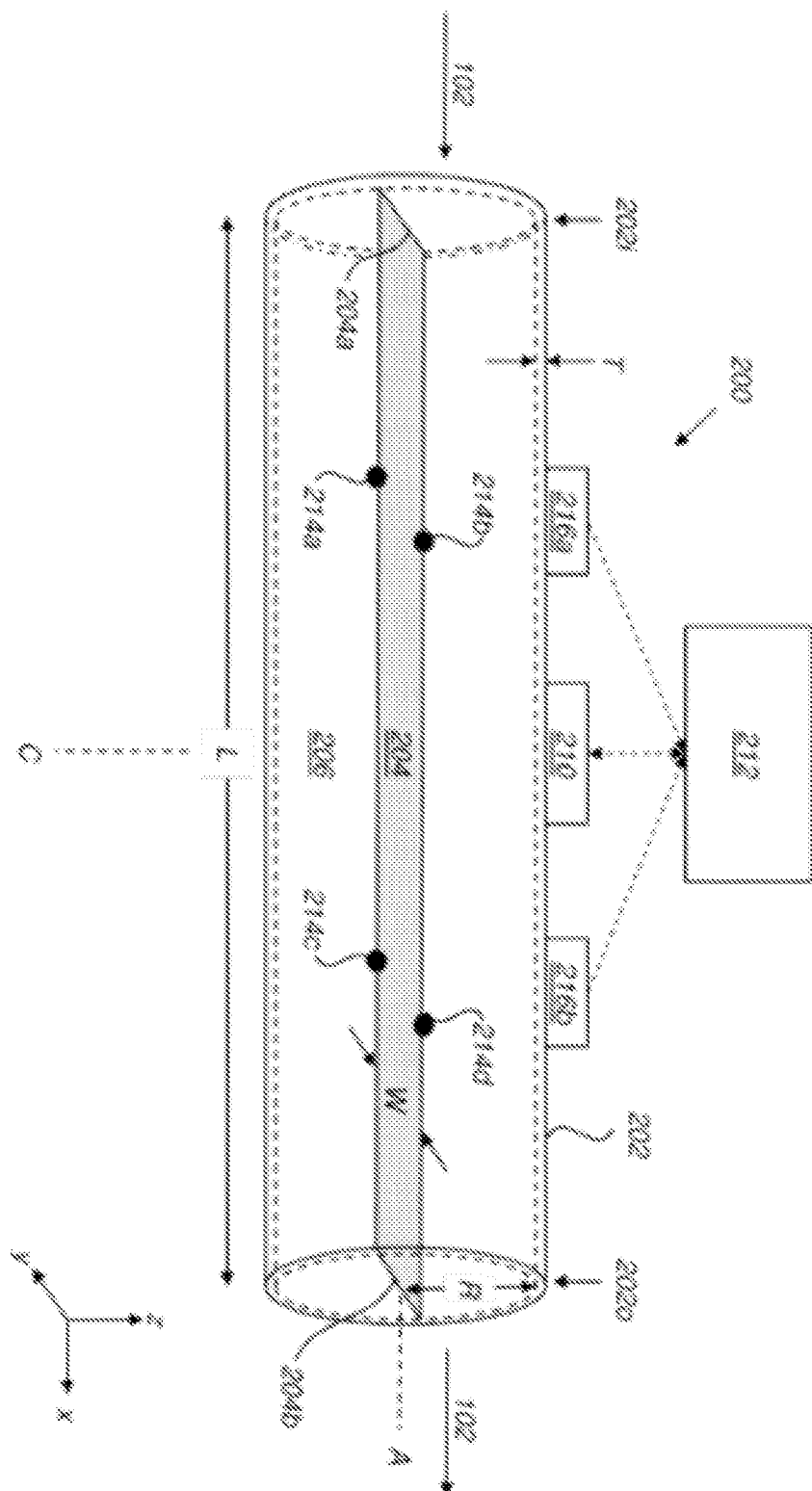


Fig. 1A

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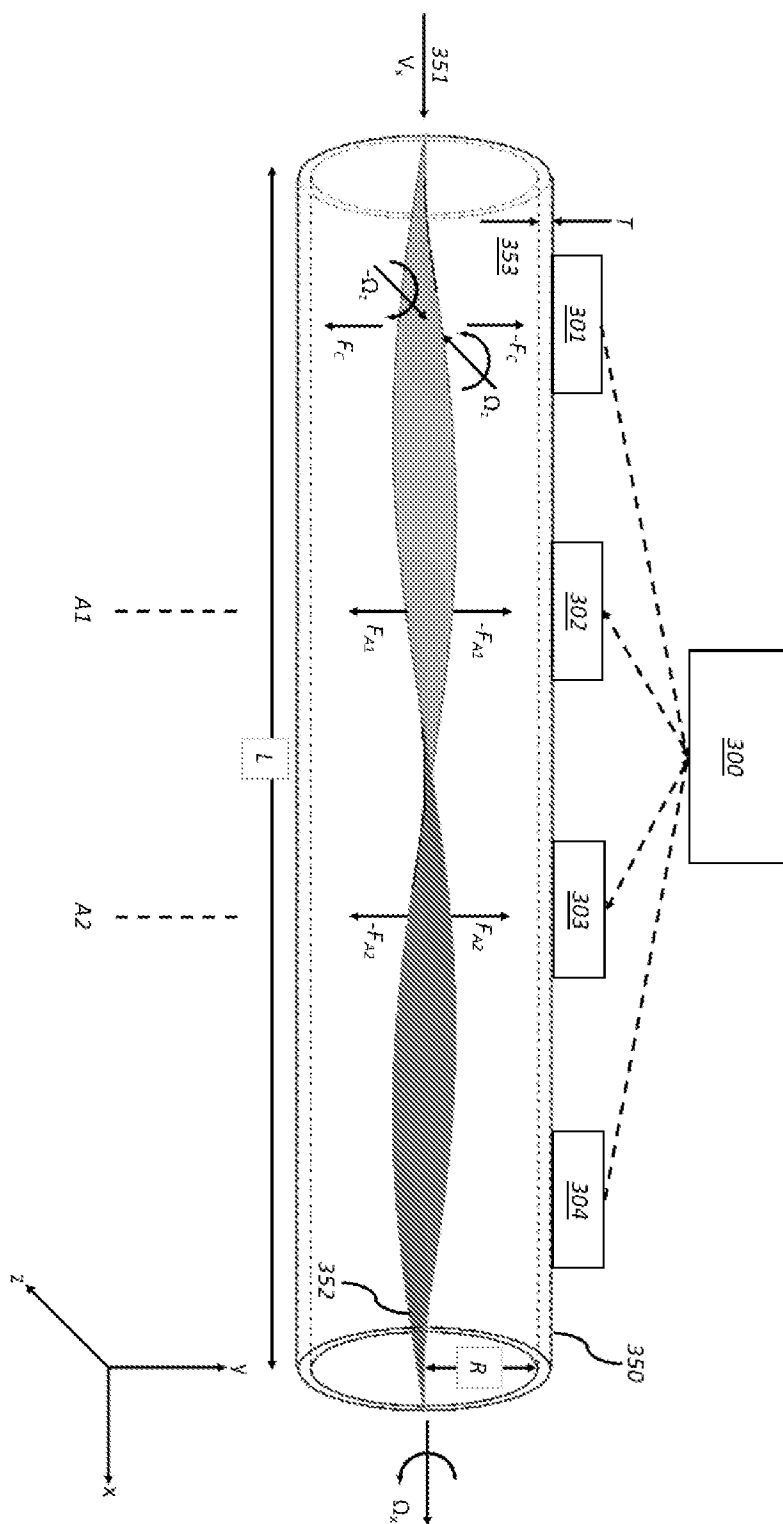


Figure 2A

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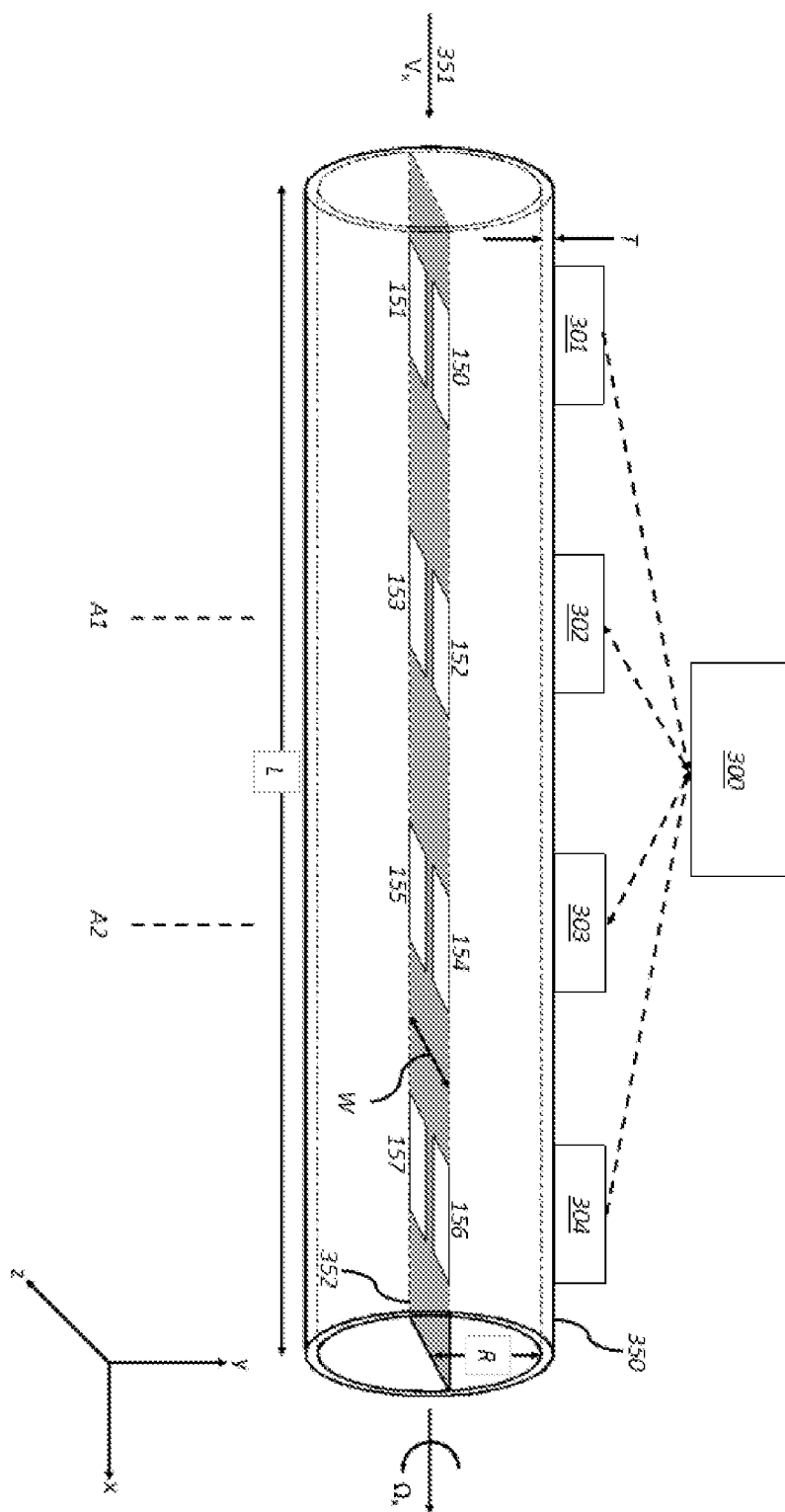


Fig. 2B

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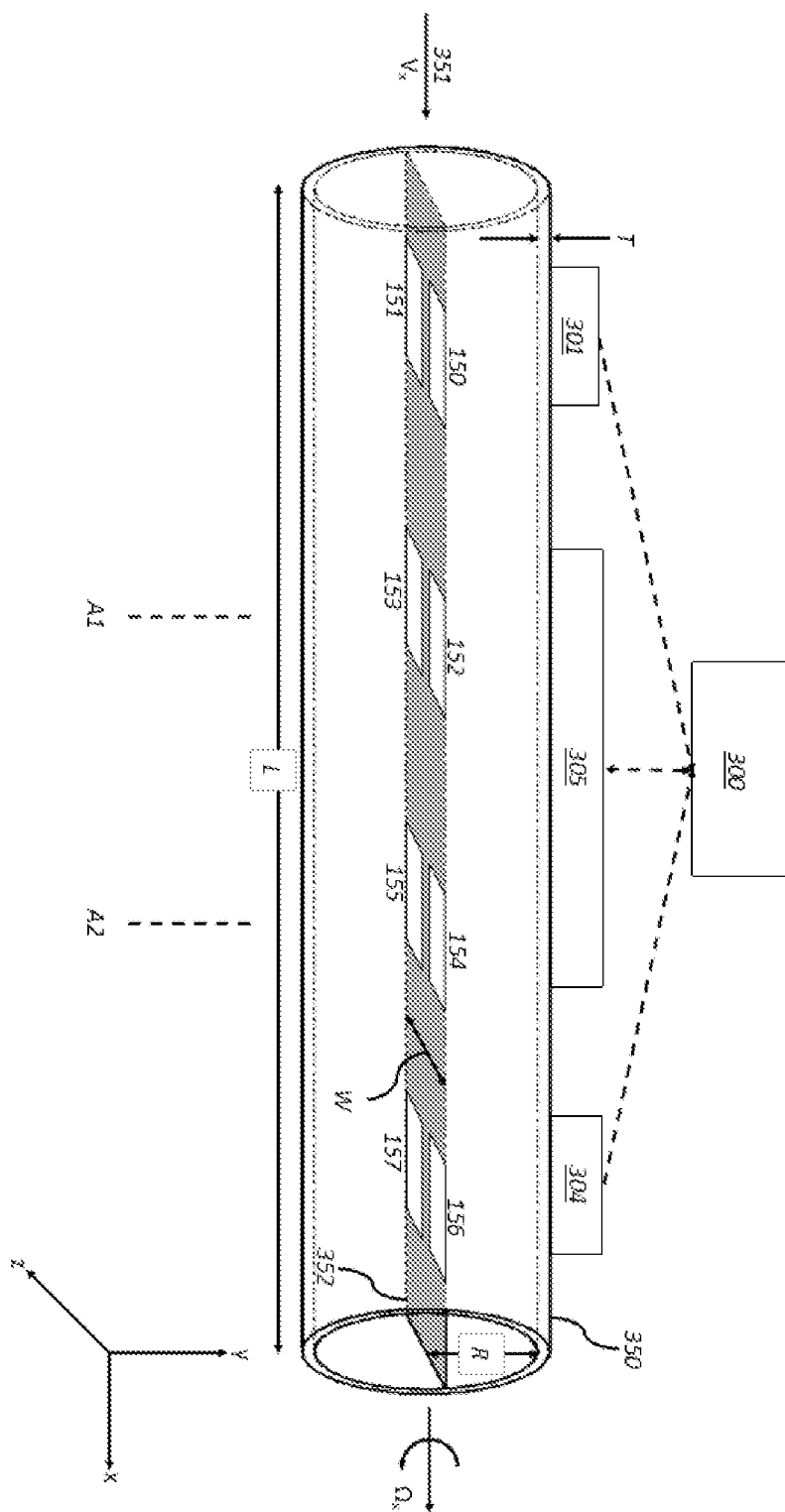


Figure 2C

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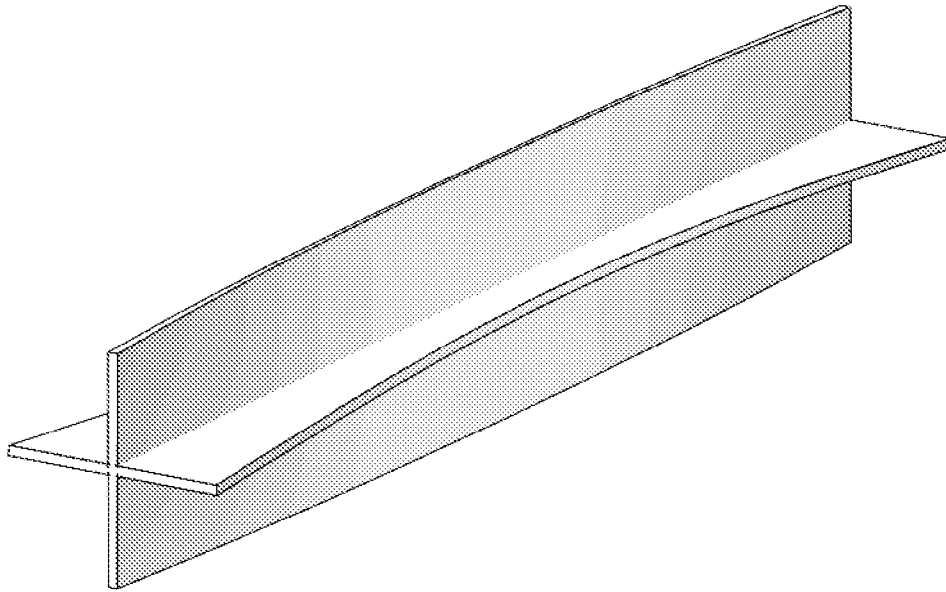


Fig. 3A

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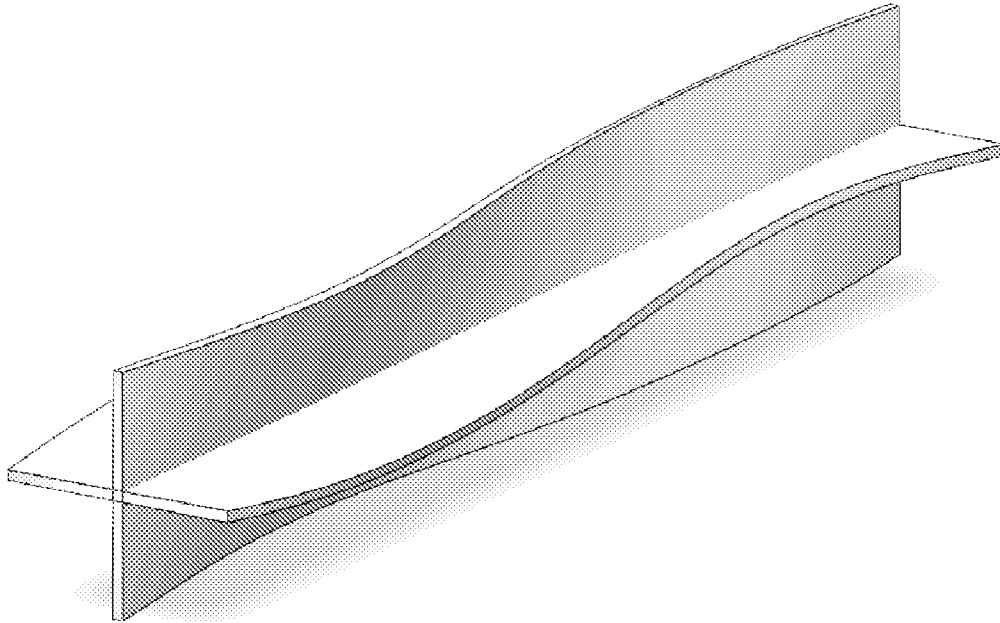


Fig. 3B

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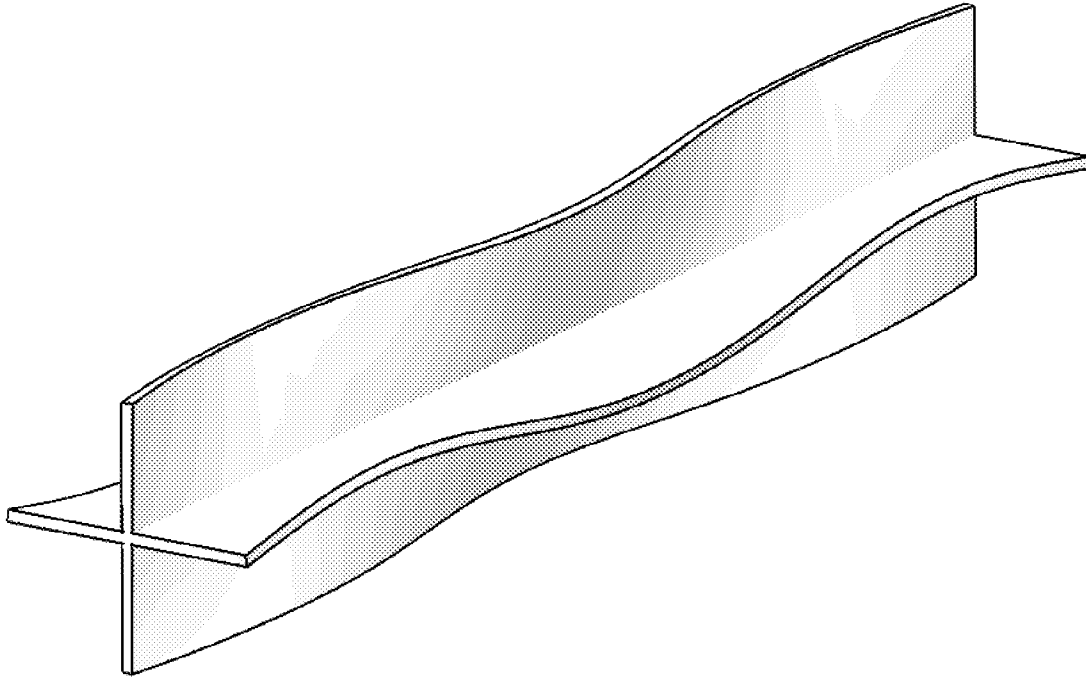


Fig. 3C

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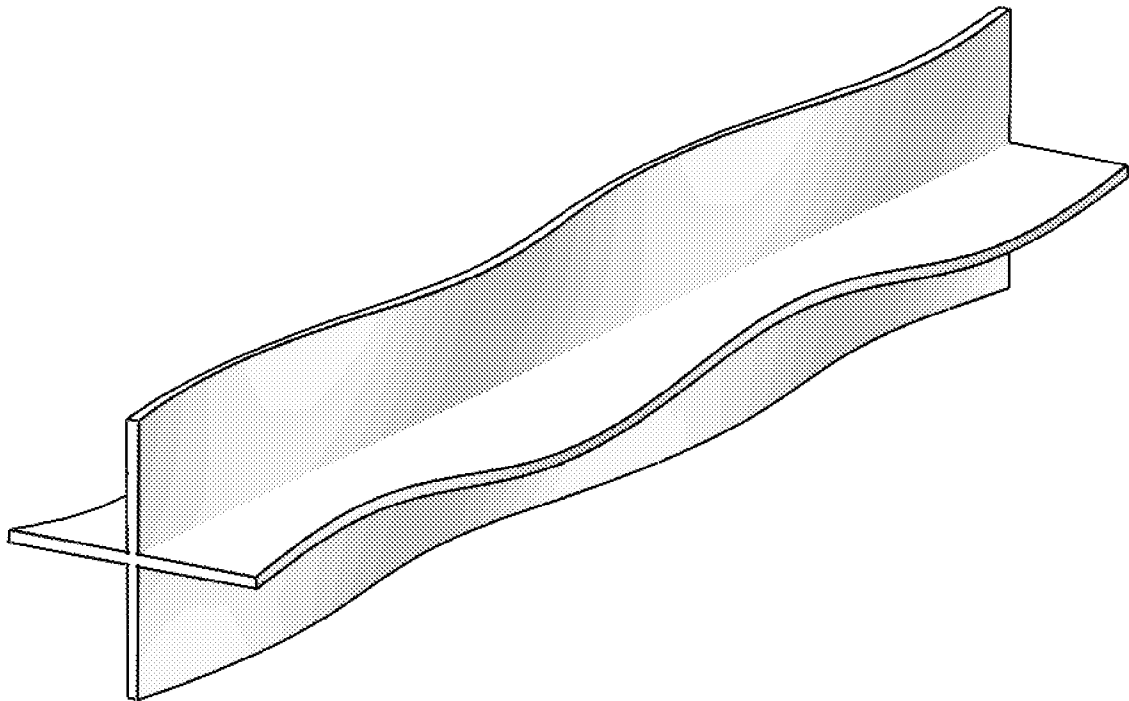


Fig. 3D

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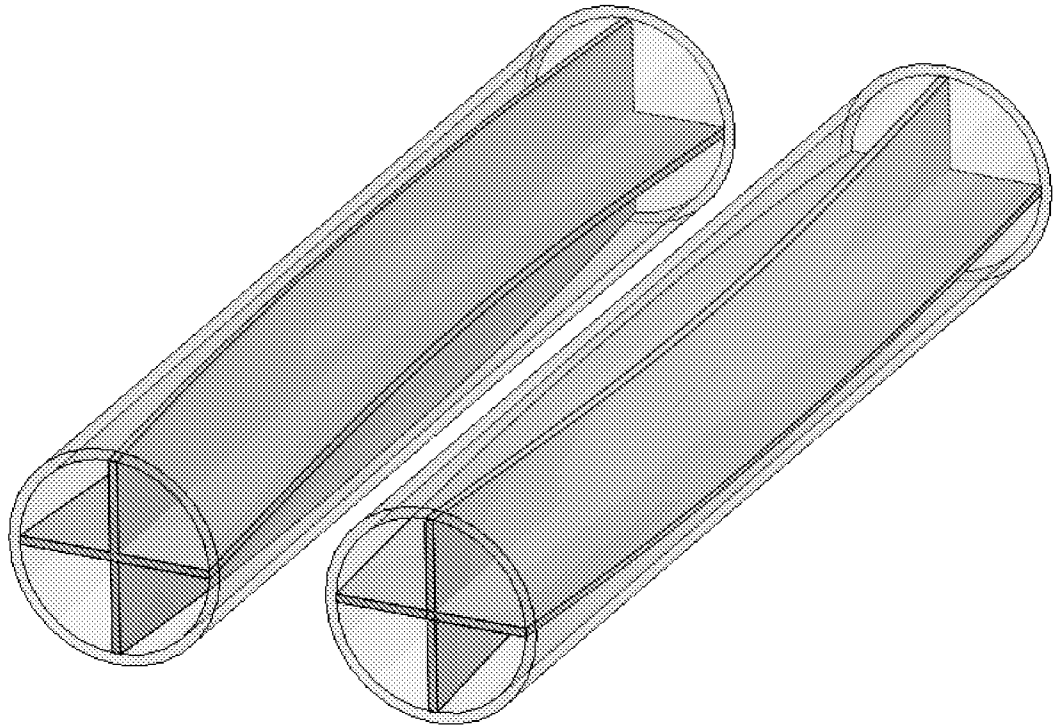


Fig.4A

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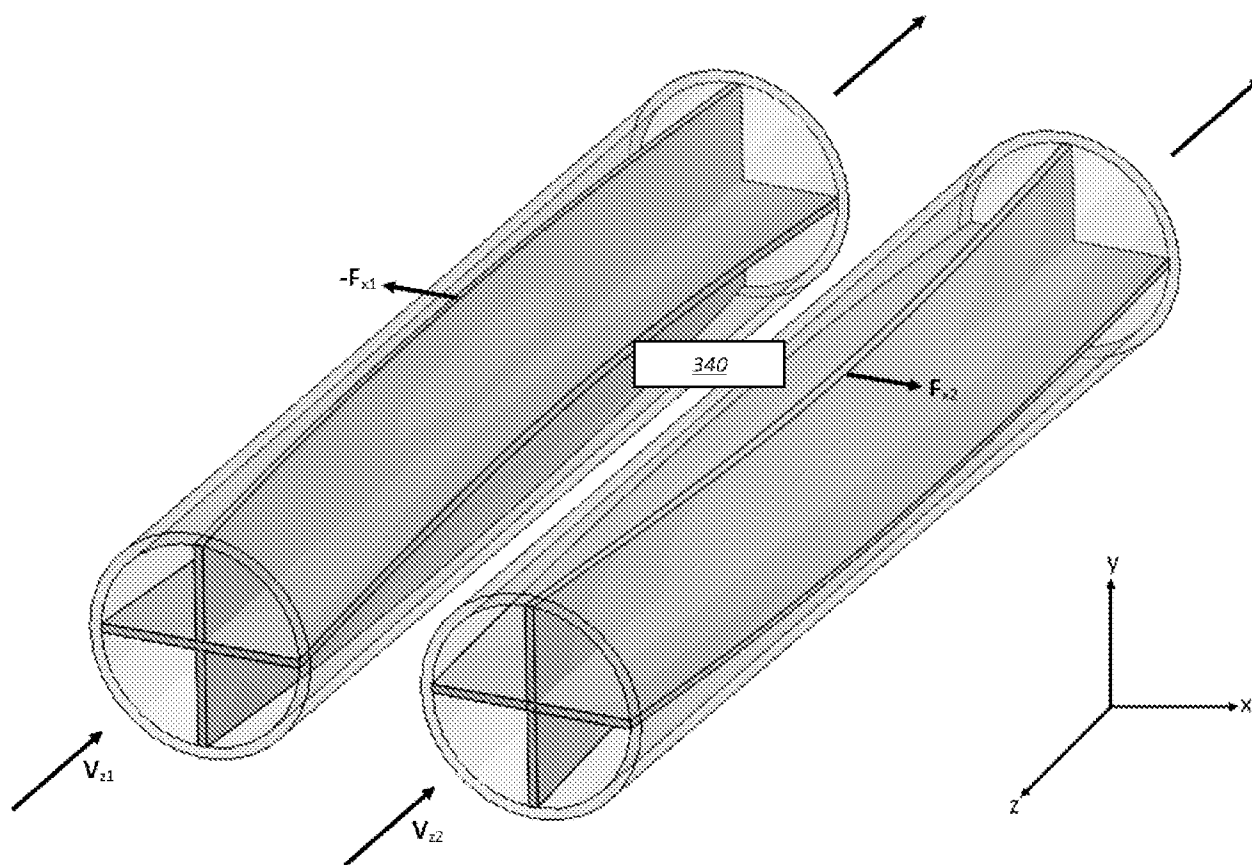


Fig.4B

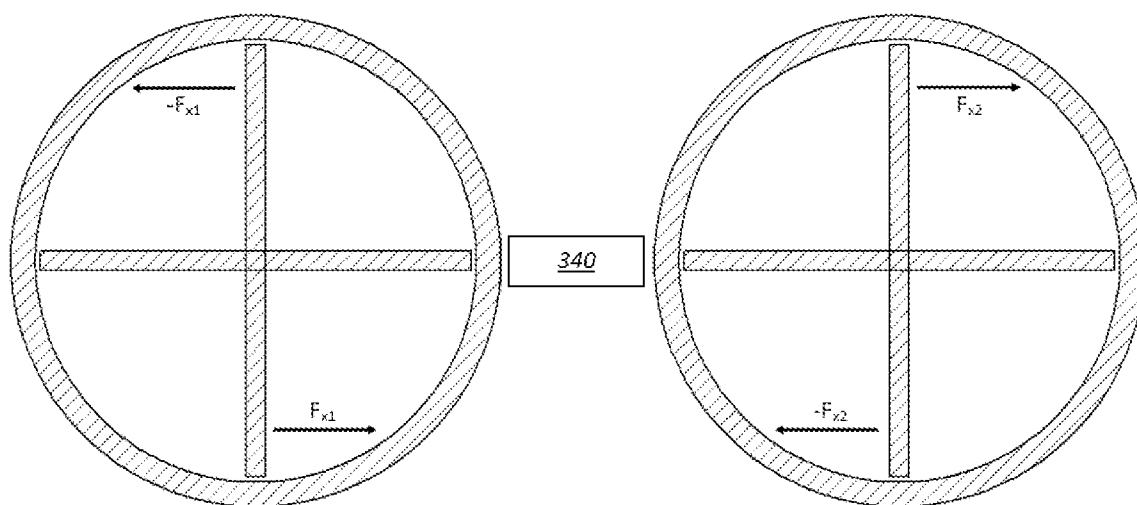


Fig.4C

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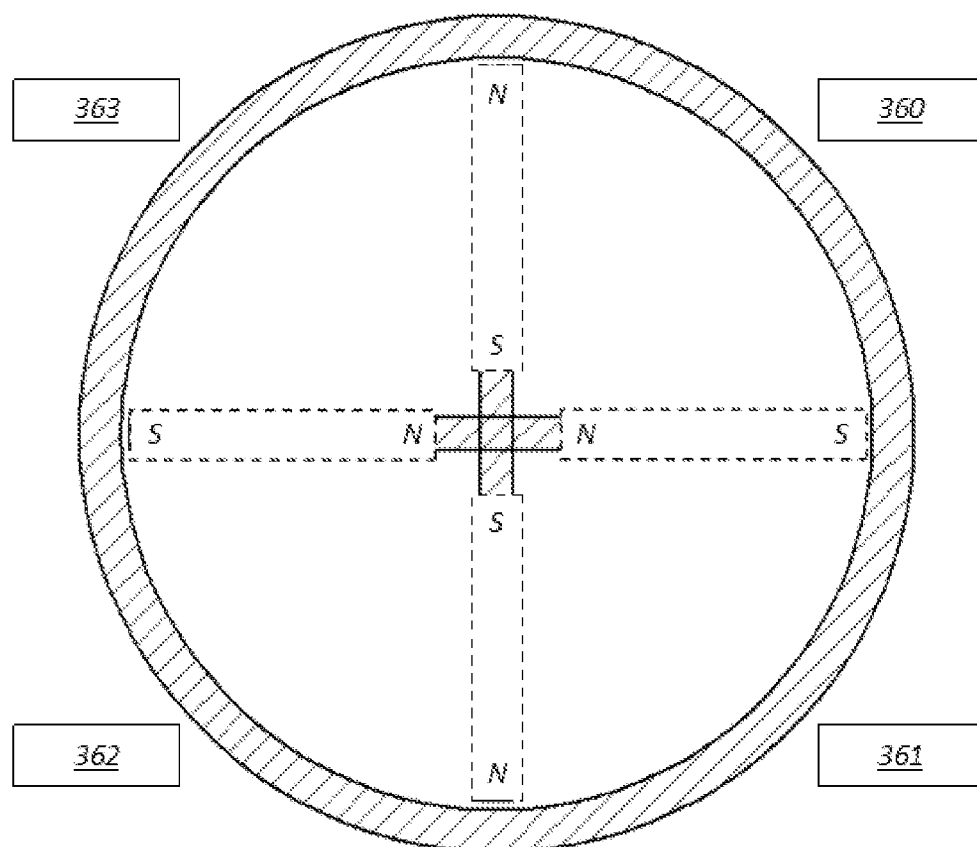


Fig.5A

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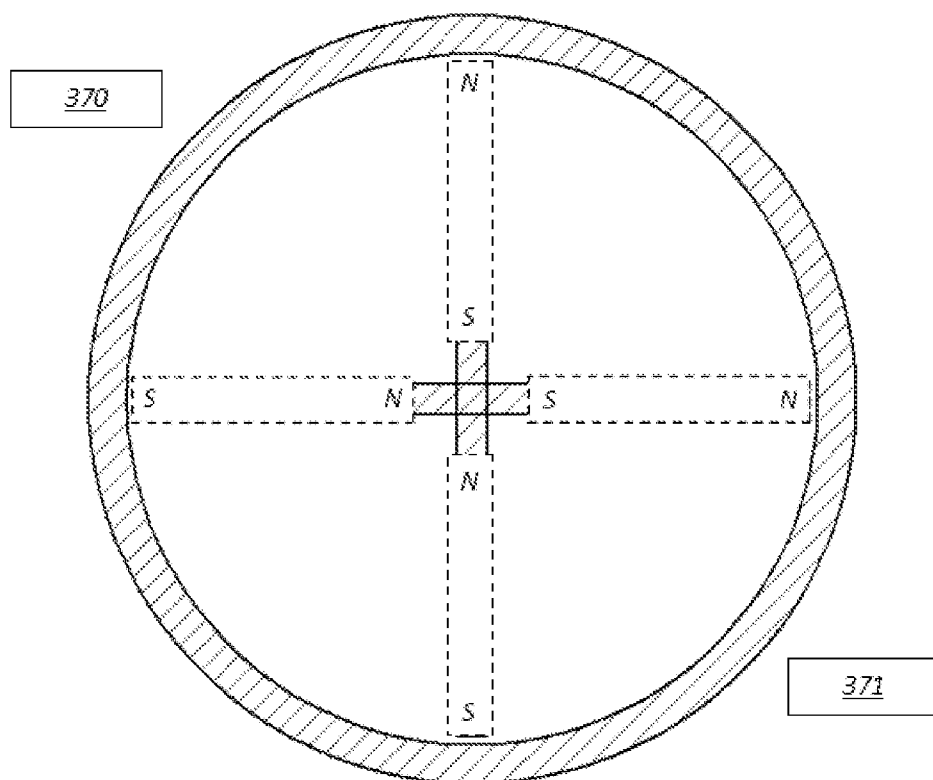


Fig.5B

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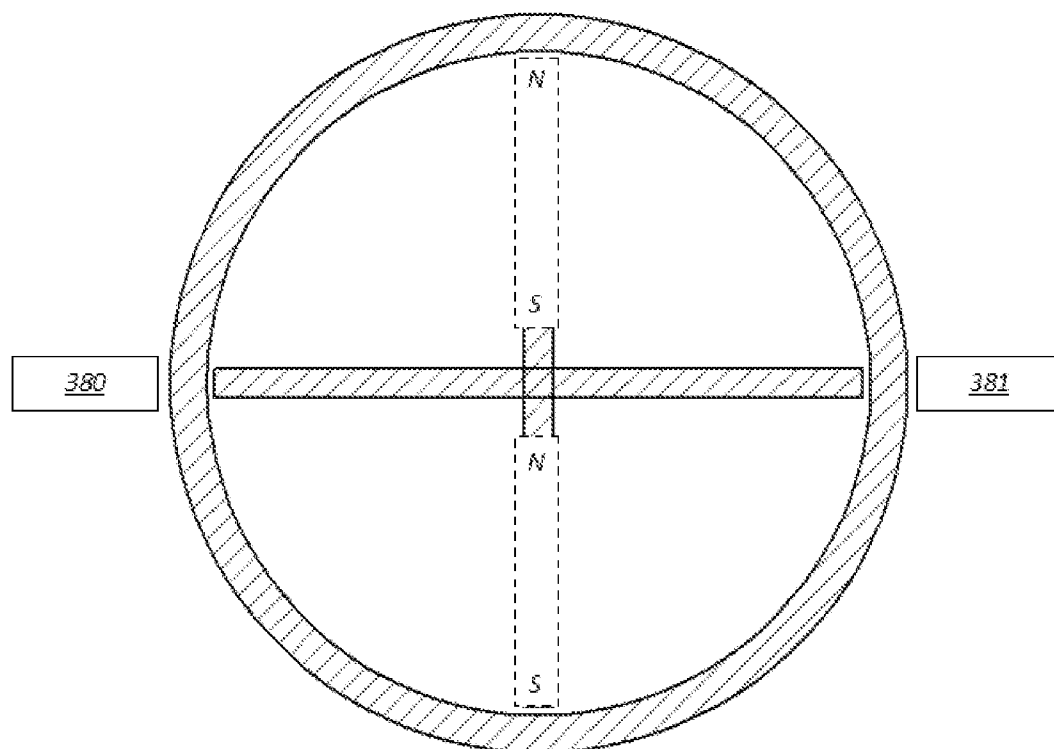


Fig.5C

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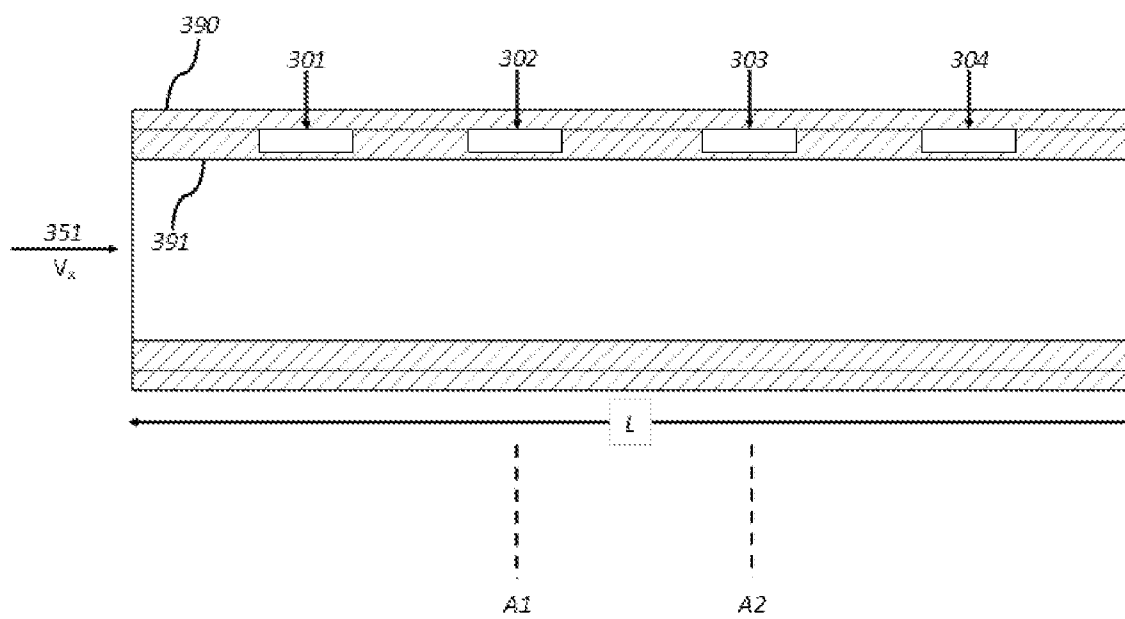


Fig.6

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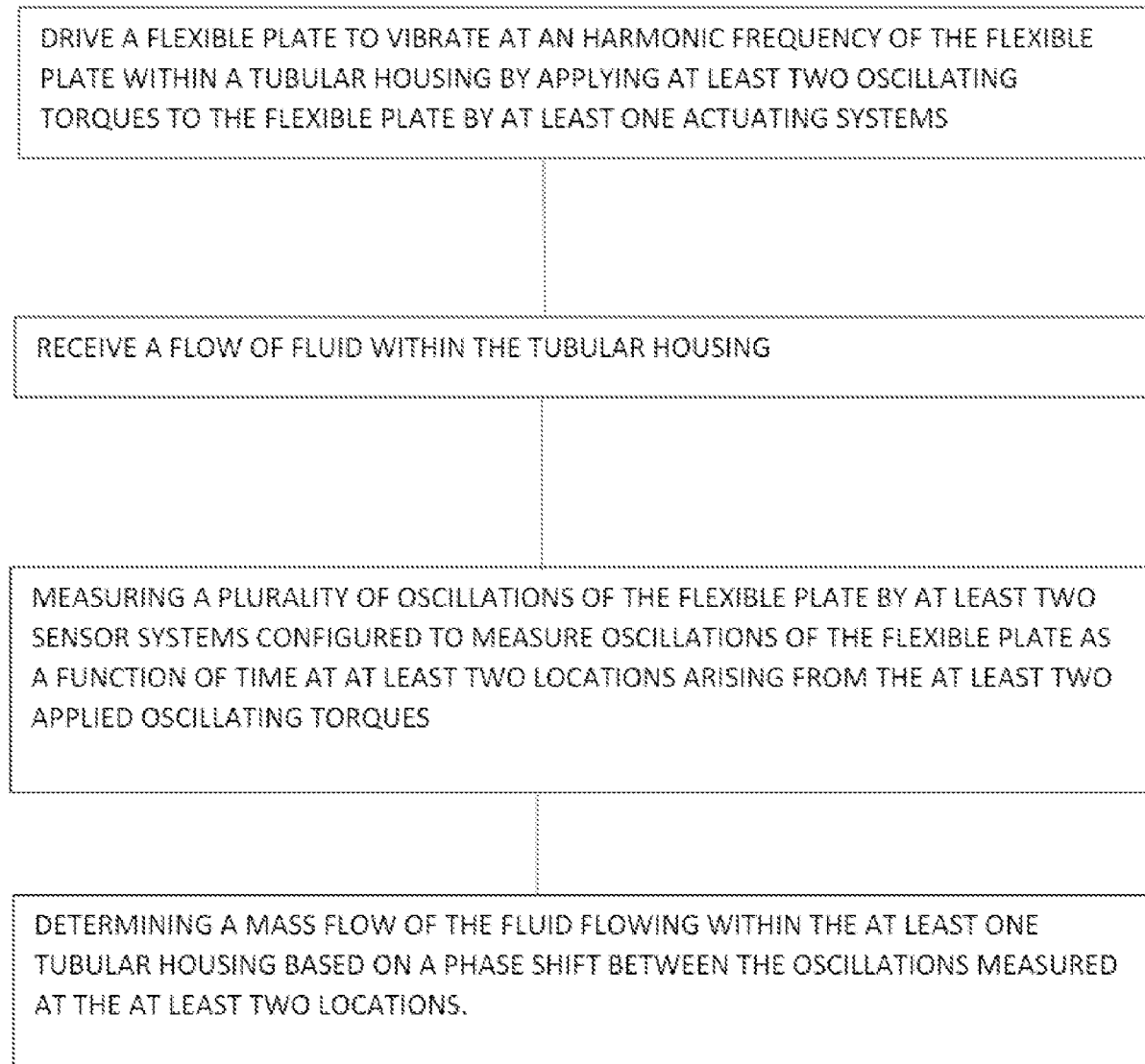


Fig.7