(12) STANDARD PATENT
(19) AUSTRALIAN PATENT OFFICE

(11) Application No. AU 2004279474 B2

(54) Title
Casting steel strip

(51) International Patent Classification(s)
B22D 11/06 (2006.01)

(21) Application No: **2004279474** (22) Date of Filing: **2004.10.08**

(87) WIPO No: **WO05/035169**

(30) Priority Data

(31) Number	(32) Date	(33) Country
60/510,479	**2003.10.10**	**US**

(43) Publication Date: **2005.04.21**
(44) Accepted Journal Date: **2010.05.27**

(71) Applicant(s)
Bluescope Steel Limited;Ishikawajima-Harima Heavy Industries Company Limited

(72) Inventor(s)
Sosinsky, David J;Mahapatra, Rama Ballav;Pretorius, Eugene B

(74) Agent / Attorney
Griffith Hack, Level 3 509 St Kilda Road, Melbourne, VIC, 3004

(56) Related Art
jp04279246
wo98/57767
us4006044
jp01083339

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization
International Bureau

(43) International Publication Date
21 April 2005 (21.04.2005)

PCT

(10) International Publication Number
WO 2005/035169 A1

(51) International Patent Classification[7]: B22D 11/06, C22C 38/00

(21) International Application Number: PCT/AU2004/001375

(22) International Filing Date: 8 October 2004 (08.10.2004)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
60/510,479 10 October 2003 (10.10.2003) US

(71) Applicant (*for AE, AG, AL, AM, AT, AZ, BA, BB, BE, BG, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CY, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, FR, GB, GD, GE, GH, GM, GR, HR, HU, IE, IL, IN, IS, IT, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MC, MD, MG, MK, MN, MW, MX, MZ, NA, NI, NO, OM, PG, PL, PT, RO, RU, SC, SD, SE, SK, SL, SY, SZ, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, YU, ZA, ZM, ZW only*): **NUCOR CORPORATION** [US/US]; 2100 Rexford Road, Charlotte, North Carolina 28211 (US).

(71) Applicants (*for AU, ID, NZ, PH, SG, VN only*): **ISHIKAWAJIMA-HARIMA HEAVY INDUSTRIES COMPANY LIMITED** [JP/JP]; 2-1, Ohtemachi 2-Chome, Chiyoda-Ku, Tokyo 100-8182 (JP). **BLUESCOPE STEEL LIMITED** [AU/AU]; Level 11, 120 Collins Street, Melbourne, Victoria 3000 (AU).

(72) Inventors; and
(75) Inventors/Applicants (*for US only*): **MAHAPATRA, Rama, Ballav** [AU/AU]; 5 Grand Parade, Brighton-Le-Sands, New South Wales 2216 (AU). **PRETORIUS, Eugene, B** [US/US]; 1831 Cherokee Rose Cir, Mt Pleasant, SC 29466 (US). **SOSINSKY, David, J** [CA/US]; 4321 East 400 South, Whitestown, Indiana 46075 (US).

(74) Agent: **GRIFFITH HACK**; Level 3, 509 St Kilda Road, Melbourne, VIC 3004 (AU).

(81) Designated States (*unless otherwise indicated, for every kind of national protection available*): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NA, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

(84) Designated States (*unless otherwise indicated, for every kind of regional protection available*): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:
— *with international search report*

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: CASTING STEEL STRIP

(57) Abstract: A method of casting steel strip by introducing molten plain carbon steel on casting surfaces at least one casting roll with the molten steel having a free nitrogen content below 120 ppm and a free hydrogen content below about 6.5 ppm measured at atmospheric pressure. The free nitrogen content maybe below about 100 ppm or below about 85 ppm. The free hydrogen content maybe between 1.0 and 6.5 ppm at atmospheric pressure. Novel cast strip of plain carbon steel is produced having a strip thickness less than 5 mm or less than 2 mm by use of the method.

WO 2005/035169 A1

CASTING STEEL STRIP

Background and Summary of the Disclosure

This invention relates to the casting of steel strip. It has particular application for continuous casting of thin steel strip less than 5 mm in thickness in a roll caster.

In a roll caster, molten metal is cooled on casting surfaces of at least one casting roll and formed in to thin cast strip. In roll casting with a twin roll caster, molten metal is introduced between a pair of counter rotated casting rolls that are cooled. Steel shells solidify on the moving casting surfaces and are brought together at a nip between the casting rolls to produce a solidified sheet product delivered downwardly from the nip. The term "nip" is used herein to refer to the general region in which the casting rolls are closest together. In any case, the molten metal is usually poured from a ladle into a smaller vessel, from where it flow through a metal delivery system to distributive nozzles located generally above the casting surfaces of the casting rolls. In twin roll casting, the molten metal is delivered between the casting rolls to form a casting pool of molten metal supported on the casting surfaces of the rolls adjacent to the nip and extending along the length of the nip. Such casting pool is usually confined between side plates or dams held in sliding engagement adjacent to ends of the casting rolls, so as to dam the two ends of the casting pool.

When casting thin steel strip with a twin roll caster, the molten metal in the casting pool will generally be at a temperature of the order of 1500°C and above. It is therefore necessary to achieve very high cooling rates over the casting surfaces of the casting rolls. A high heat flux and extensive nucleation on initial solidification of the metal shells on the casting surfaces is needed to form the steel strip. US Patent No. 5,760,336 incorporated herein by reference describes how the heat flux on initial solidification can be increased by adjusting the steel melt chemistry such that a substantial portion of the metal oxides formed are liquid at the initial solidification temperature, and in turn, a substantially liquid layer formed at the interface between the molten metal and each casting surface. As disclosed in US Patent Nos. 5,934,359 and 6,059,014 and International Application AU 99/00641, the disclosures of which are incorporated herein by reference, nucleation of the steel on initial solidification can be influenced by the texture of the casting surface. In particular, International Application AU 99/00641 discloses that a random texture of peaks and troughs in the casting surfaces can enhance initial solidification by providing substantial nucleation sites distributed over the casting surfaces.

Attention has been given in the past to the steel chemistry of the melt, particularly in the ladle metallurgy furnace before thin strip casting. We have given attention in the past to the oxide inclusions and the oxygen levels in the steel metal and their impact on the quality of the steel strip produced. We have now found that the quality of the steel strip and the production of the thin steel strip are also enhanced by control of the hydrogen levels and nitrogen levels in the molten steel. Controlling hydrogen and nitrogen levels has in the past been the subject of investigation in slab casting, but to our knowledge has not been a focus of attention in thin strip casting. For example see *Control of Heat Removal in the Continuous Casting Mould*, by P.Zasowski and D. Solinsky, 1990 Steelmaking Conference Proceedings, 253-259; and *Determination and Prediction of Water Vapor Solubilities in CaO-MgO-SiO_2 Slags,* by D. Sosinsky, M. Maeda and A. Mclean, Metallurgical Transactions, vol. 16b, 61-66 (March 1985).

Specifically we have found that by controlling the hydrogen and nitrogen levels in the steel melt, with low levels of sulphur in the steel, plain carbon steel strip having unique composition and production qualities can be produced by roll casting.

According to the invention there is provided a method of casting steel strip comprising:

introducing molten pain carbon steel on casting surfaces of at least one casting roll with the molten steel having a free nitrogen content below about 120 ppm and a free hydrogen content below 6.5 ppm measured at atmospheric pressure; and solidifying the molten steel to form metal shells on the casting rolls having nitrogen and hydrogen levels reflected by the content thereof in the molten steel to form thin steel strip.

In a particular embodiment of the method said casting surfaces are provide by a pair of cooled casting rolls having a nip between them and confining end closures adjacent to ends of the casting rolls, said molten plain carbon steel is introduced between the pair of casting rolls to form a casting pool on casting surfaces of the casting rolls with the end closures confining the pool, the casting rolls are counter-rotated and the solidified thin steel strip is formed through the nip between the casting rolls to produce a solidified steel strip delivered downwardly from the nip.

The free nitrogen content may be below about 100 ppm or below about 85 ppm.

The free nitrogen content may be 60 ppm or less. The free hydrogen content may be 1.0 to 6.5 ppm at atmospheric pressure. The free hydrogen content may, for example, be between 2.0 and 6.5 ppm or between 3.0 and 6.5 ppm.

Plain carbon steel for purpose of the present invention is defined as less than 0.65% carbon, less than 2.5% silicon, less than 0.5% chromium, less thabn 2.0% manganese, less than 0.5% nickel, less than 0.25% molybdenum and less than 1.0% aluminium, together with of other elements such as sulfur, oxygen and phosphorus which normally occur in making carbon steel by electric arc furnace. Low carbon steel may be used in these method having a carbon content in the range 0.001% to 0.1% by weight, a manganese content in the range 0.01% to 2.0% by weight, and a silicon content in the range 0.01% to 2.5% by weight, and low carbon cast strip may be made by the method. The steel may have an aluminium content of the order of 0.01% or less by weight. The aluminium may, for example, be as little as 0.008% or less by weight. The molten steel may be a silicon/manganese killed steel.

In these method, the sulfur content of the steel may be 0.01% or less; and the sulfur content of the steel may be 0.007% by weight.

In these methods, the free nitrogen may be measured by optical emission spectrometry, calibrated against the thermal conductivity method as described below. The free hydrogen levels may be determined by a Hydrogen Direct Reading Immersed System ("Hydris") unit, made by Hereaus Electronite.

The maximum allowable free nitrogen and free hydrogen levels may be for total pressure not to exceed 1.0 atmospheres. Higher pressures may be utilised in certain conditions, and the levels of free nitrogen and free hydrogen can be corresponding higher. For example, as explained below, a ferrostatic head may be 1.15, causing the free nitrogen levels and free hydrogen levels to be higher as shown in Figure 3. But for purposes of the parameters of the above methods, the free nitrogen and free hydrogen levels are measured at 1.0 atmospheres even through the actual levels of free nitrogen and free hydrogen in the molten metal are higher when the methods are practiced with higher positive atmospheric pressure.

Having regard to the foregoing, the present invention also provides a method of casting steel strip comprising:

introducing molten plain carbon steel on casting surfaces of at least one casting roll with the molten steel having a free nitrogen content below about 120 ppm and a free hydrogen content below about 6.9 ppm and such that the sum of partial pressure of nitrogen and partial pressure of hydrogen is no more than 1.15 atmospheres;

forming a casting pool of molten metal on the casting surfaces of the casting rolls; and

solidifying the molten steel for form metal shells on the casting rolls having nitrogen and hydrogen levels reflected by the content thereof in the molten steel to form thin steel strip.

Brief Description of the Drawings

In order that the invention may be more fully explained, illustrative results of experimental work carried out to date will be described with reference to the accompanying drawings in which:

Figure 1 is a diagrammatic side elevation view of an illustrative strip caster;

Figure 2 is an enlarged sectional view of a portion of the caster of Figure 1;

Figure 3 is a graph showing allowable nitrogen levels and hydrogen levels in low carbon steel for a cast steel strip.

Detailed Description of the Drawings

Figures 1 and 2 illustrate a twin roll continuous strip caster which has been operated in accordance with the present invention. The following description of the described embodiments is in the context of continuous casting steel strip using a twin roll caster. The present invention is not limited, however, to the use of twin roll casters and extends to other types of continuous strip casters.

Figure 1 shows successive parts of an illustrative production line whereby steel strip can be produced in accordance with the present invention. Figures 1 and ______________________________

2 illustrate a twin roll caster denoted generally as 11 which produces a cast steel strip 12 that passes in a transit path 10 across a guide table 13 to a pinch roll stand 14 comprising pinch rolls 14A. Immediately after exiting the pinch roll stand 14, the strip may pass into a hot rolling mill 16 comprising a pair of reduction rolls 16A and backing rolls 16B by in which it is hot rolled to reduce its thickness. The rolled strip passes onto a run-out table 17 on which it may be cooled by convection by contact with water supplied via water jets 18 (or other suitable means) and by radiation. In any event, the rolled strip may then pass through a pinch roll stand 20 comprising a pair of pinch rolls 20A and thence to a coiler 19. Final cooling (if necessary) of the strip takes place on the coiler.

As shown in Figure 2, twin roll caster 11 comprises a main machine frame 21 which supports a pair of cooled casting rolls 22 having a casting surfaces 22A, assembled side-by-side with a nip between them. Molten metal of plain carbon steel may be supplied during a casting operation from a ladle (not shown) to a tundish 23, through a refractory shroud 24 to a distributor 25 and thence through a metal delivery nozzle 26 generally above the nip 27 between the casting rolls 22. The molten metal thus delivered to the nip 27 forms a pool 30 supported on the casting roll surfaces 22A above the nip and this pool is confined at the ends of the rolls by a pair of side closures, dams or plates 28, which may be positioned adjacent the ends of the rolls by a pair of thrusters (not shown) comprising hydraulic cylinder units (or other suitable means) connected to the side plate holders. The upper surface of pool 30 (generally referred to as the “meniscus” level) may rise above the lower end of the delivery nozzle so that the lower end of the delivery nozzle is immersed within this pool.

Casting rolls 22 are water cooled so that shells solidify on the moving casting surfaces of the rolls. the shells are then brought together at the nip 27 between the casting rolls sometimes with molten metal between the shells, to produce the solidified strip 12 which is delivered downwardly from the nip.

Frame 21 supports a casting roll carriage which is horizontally movable between an assembly station and a casting station.

Casting rolls 22 may be counter-rotated through drive shafts (not shown) driven by an electric, hydraulic or pneumatic motor and transmission. Rolls 22 have copper peripheral walls formed with a series of longitudinally extending and circumferentially spaced water cooling passages supplied with cooling water. The rolls may typically be about 500 mm in diameter and up to about 2000 mm long in order to produce strip product of about 2000 mm wide.

Tundish 25 is of conventional construction. It is formed as a wide dish made of a refractory material such as for example magnesium oxide (MgO). One side of the tundish receives molten metal from the ladle and is provided with an overflow spout 24 and an emergency plug 25.

Delivery nozzle 26 is formed as an elongate body made of a refractory material such as for example alumina graphite. Its lower part is tapered so as to converge inwardly and downwardly above the nip between casting rolls 22.

Nozzle 26 may have a series of horizontally spaced generally vertically extending flow passages to produce a suitably low velocity discharge of molten metal throughout the width of the rolls and to deliver the molten metal between the rolls onto the roll surfaces where initial solidification occurs. Alternatively, the nozzle may have a single continuous slot outlet to deliver a low velocity curtain of molten metal directly into the nip between the rolls and/or the nozzle may be immersed in the molten metal pool.

The pool is confined at the ends of the rolls by a pair of side closure plates 28 which are adjacent to and held against stepped ends of the rolls when the roll carriage is at the casting station. Side closure plates 28 are illustratively made of a strong refractory material, for example boron nitride, and have scalloped side edges to match the curvature of the stepped ends of the rolls. The side plates can be mounted in plate holders which are movable at the casting station by actuation of a pair of hydraulic cylinder units (or other suitable means) to bring the side plates into engagement with the stepped ends of the casting rolls to form end closures for the molten pool of metal formed on the casting rolls during a casting operation.

The twin roll caster may be of the kind illustrated and described in some detail in, for example, United States Patents 5,184,668; 5,277,243; 5,488,988; and/or 5,934,359; U.S. Pat. Application No. 10/436,336; and International Patent Application PCT/AU93/00593, the disclosures of which are incorporated herein by reference. Reference may be made to those patents for appropriate constructional details but forms no part of the present invention.

Results of the control of the free nitrogen and hydrogen levels in thin cast sheets of plain carbon steel are set out in Table 1 and in Figure 3. As Figure 3 shows, where the free nitrogen level was below about 85 ppm and the free hydrogen level was below about 6.5 ppm the thin cast strip produced was of premium "cold-rolled" steel quality. The heat(s) where the free nitrogen or free hydrogen level were above about 85 ppm or about 6.5 ppm, respectively, did not produce thin cast strip of premium cold-rolled steel quality. We have found, however, that hydrogen level is the significant parameter and the nitrogen level can be higher up to 100 ppm or 120 ppm.

The results shown in Figure 3 are for plain carbon thin rolled steel. Table 1 sets forth the analysis of each of the heats shown on Figure 3. As seen from Figure 3, the left-hand curve shown is based on calculated basis for total pressure of partial nitrogen and partial hydrogen equal to 1.0 atmosphere.

TABLE 1

Last LMF Chems								
Seq ID	LMF C	LMF Si	LMF Mn	LMF N	LMF S	LMF P	LMF Al	H, ppm
822*	0.0493	0.265	0.6266	0.0075	0.011	0.0112	0.0042	7.3
1019	0.049	0.282	0.6122	0.0055	0.012	0.0113	0.0009	7
1057*	0.0622	0.2818	0.4894	0.008	0.013	0.0102	0.0008	8.3
1060*	0.0541	0.2986	0.5642	0.0081	0.0084	0.0107	0.0012	7.3
1071*	0.0547	0.1939	0.5616	0.0056	0.0076	0.0088	0.0029	5.6
1074*	0.0504	0.2989	0.5531	0.0042	0.0087	0.0149	0.002	6.3
1078*	0.0598	0.3212	0.6165	0.0081	0.0092	0.0155	0.0018	6.5
1079	0.0572	0.3368	0.6122	0.0067	0.0095	0.0117	0.0014	8.9
1080*	0.0582	0.2508	0.5688	0.0087	0.0119	0.011	0.0017	7.3
1082*	0.0606	0.2777	0.5603	0.0084	0.0094	0.0131	0.0016	7.4
1087*	0.0568	0.2794	0.5981	0.0078	0.0067	0.0166	0.0019	8.4
1088*	0.0534	0.3077	0.6044	0.0081	0.0106	0.0155	0.0025	8.3
1091	0.0479	0.2262	0.5565	0.0084	0.0095	0.026	0.0024	9
1095	0.0448	0.2343	0.5963	0.007	0.0086	0.0072	0.0013	8.5
1098*	0.0567	0.3831	0.4559	0.008	0.0119	0.0111	0.0017	7
1099*	0.0532	0.2718	0.5324	0.0071	0.0109	0.0129	0.0015	6.8
1100*	0.0533	0.2685	0.5658	0.0074	0.0088	0.0108	0.0022	7.7
1103*	0.0548	0.2997	0.6137	0.0071	0.0115	0.012	0.0016	7.1
1104*	0.054	0.2799	0.6771	0.0067	0.008	0.0114	0.0024	7.4
1106*	0.047	0.3229	0.6281	0.0058	0.01	0.0104	0.0028	7.6
1110*	0.0434	0.3068	0.6848	0.0046	0.006	0.0111	0.0014	4.4
1111	0.0414	0.3002	0.5669	0.005	0.0089	0.0163	0.0019	5.6
1113*	0.0289	0.0798	0.4376	0.0044	0.0053	0.0101	0.0182	4.6
1113	0.0416	0.2212	0.5914	0.0053	0.0067	0.0119	0.0025	6.2
1114*	0.0489	0.3034	0.5943	0.0055	0.0058	0.008	0.0017	3.9
1115*	0.0594	0.3404	0.6565	0.0053	0.0064	0.0129	0.0021	4.7
1116	0.0507	0.3725	0.6806	0.0062	0.0095	0.0123	0.0051	5
1117	0.0437	0.2258	0.563	0.0067	0.008	0.0121	0.0012	5
1118*	0.0629	0.3149	0.633	0.0081	0.0086	0.0143	0.001	7.7
1120*	0.0486	0.2935	0.5384	0.0077	0.0063	0.0074	0.0048	7.7
1121*	0.0492	0.314	0.6371	0.0073	0.0093	0.0163	0.0012	7.9
1122*	0.0525	0.2639	0.5867	0.0085	0.011	0.0141	0.0009	7.5
1123	0.0578	0.3238	0.5966	0.0058	0.0082	0.0124	0.0023	5.2

Seq ID	LMF C	LMF Si	LMF Mn	LMF N	LMF S	LMF P	LMF Al	H, ppm
1125*	0.0682	0.3221	0.5786	0.0063	0.0055	0.0083	0.0005	4.7
1128*	0.0408	0.2456	0.5895	0.005	0.0083	0.0095	0.0016	5.1
1130	0.0378	0.3219	0.627	0.0073	0.0087	0.0172	0.0023	5.1
1133	0.0398	0.2899	0.574	0.0054	0.0084	0.0092	0.0033	5.2
1134	0.0558	0.2612	0.6039	0.0055	0.009	0.0148	0.0038	5.9
1135	0.0567	0.2085	0.6093	0.0052	0.0125	0.0151	0.0015	4.6
1144*	0.0554	0.3702	0.6315	0.0077	0.0098	0.0108	0.0027	6.7
1160*	0.0448	0.3338	0.5496	0.0054	0.0055	0.0078	0.004	4.4
1161	0.057	0.3182	0.6093	0.0054	0.0066	0.0092	0.0015	4.2
1163	0.0499	0.3198	0.6033	0.0053	0.0056	0.0078	0.0026	4.2
1164	0.0352	0.2783	0.59	0.0058	0.0058	0.0076	0.0025	3.6
1167	0.0451	0.3395	0.6026	0.0054	0.0073	0.0086	0.0024	3.5
1168	0.0515	0.2841	0.5897	0.0058	0.0043	0.0059	0.0018	3.9
1170	0.0366	0.2839	0.5958	0.0062	0.0054	0.0077	0.0018	4
1171	0.0454	0.304	0.586	0.007	0.0053	0.0073	0.0031	4.7
1172	0.0372	0.291	0.618	0.005	0.006	0.0087	0.0017	3.5
1173	0.0537	0.3049	0.6171	0.0051	0.0038	0.0086	0.0014	5.2
1180	0.054	0.2706	0.6285	0.0055	0.0069	0.006	0.001	4
1182	0.0543	0.3296	0.6386	0.0062	0.0082	0.0094	0.0013	4.5
1182	0.0511	0.3008	0.6025	0.0049	0.0057	0.0099	0.0015	4.2
1183	0.0549	0.2859	0.6147	0.0069	0.0082	0.0087	0.0003	3.7
1183	0.0492	0.2718	0.6245	0.0063	0.0054	0.0085	0.0007	3.8
1188	0.0511	0.3076	0.6298	0.0073	0.0042	0.0076	0.0048	4.4
1189	0.0562	0.3133	0.646	0.0063	0.0031	0.0083	0.0085	3.2
1189	0.0452	0.3536	0.6902	0.0049	0.0014	0.0079	0.0132	4.1
1193*	0.0556	0.2864	0.6116	0.0059	0.0063	0.0084	0.0017	3.7
1196	0.0103	0.2989	0.6053	0.0052	0.0018	0.0082	0.0171	4
1198	0.0531	0.2643	0.6123	0.007	0.0064	0.0079	0.003	5
1200*	0.0534	0.2627	0.6082	0.0078	0.0107	0.007	0.0018	6.7
1205*	0.0544	0.2696	0.6037	0.0078	0.0097	0.0063	0.0011	6.8
* indicates reduced Heat Flux Sequences								

The composition of all heats in Table 1 are in percent by weight, and are shown in Figure 3. The heats were measured for a heat flux index of ± 0.7 megawatt per square meter from the desired level, i.e., range about a standard heat flux for a given casting speed. Examples of standard heat flux for a given casting speed is 15 megawatts/ m^2 for a casting speed of 80 meters/ min and 13 megawatts/ m^2 for casting speed of 65 meters/ min. Astrerisk heats in Table 1 had the heat flux index within an acceptable range of ±0.7 megawatts pre square meter as shown in Figure 3. The curve in Figure 3 shows maximum allowable levels of free nitrogen and free hydrogen for the summed partial pressures of the free nitrogen and free hydrogen totaling 1.0 atmospheres to produce the acceptable heat flux indexof ±0.7 megawatts per square meter. As shown in Figure 3, all of the heats that had a free nitrogen level below about 85 ppm and a free hydrogen level below about 6.5 ppm had a heat flux within the desired range except heats 1110 and 1125. In heat 1110, the free oxygen levels were usually low, approximately 10 ppm, and in heat 1125, there were mechanical problems in the casting equipment.

More recently, additional heats have been made with low nitrogen and low hydrogen having compositions shown in Table 2. The nitrogen level range from 42 to 118 ppm and the hydrogen levels ranged from 3.0 to 6.9 ppm. However, the hydrogen level of 6.9 ppm is with a ferrostatic head of more than 1 atmosphere pressure, namely about 1.15 atmospheres, as shown by the right-hand curve in Figure 3.

TABLE 2

SEQ_ID	HEAT_ID	C	MN	N	S	SI	P	AL	H, ppm
1734	248991	0.0502	0.5653	0.0042	0.0079	0.2615	0.0124	0.0006	4.6
1705	248296	0.048	0.5767	0.0054	0.0087	0.3154	0.017	0.0019	4.6
1701	142523	0.0461	0.5798	0.0053	0.0051	0.2729	0.0112	0.0008	5.1
1696	248237	0.0513	0.5793	0.0055	0.0052	0.2902	0.0112	0.0014	5
1695	248227	0.0559	0.5701	0.0066	0.0039	0.2436	0.0115	0.0006	6
1694	248207	0.0487	0.5763	0.0059	0.0081	0.2643	0.0172	0.0007	4.3
1691	248031	0.0481	0.5851	0.0063	0.0063	0.2605	0.0119	0.0006	4.4
1690	142250	0.0507	0.5928	0.0058	0.007	0.2582	0.0138	0.0009	3.2
1690	142248	0.0554	0.5859	0.0079	0.0057	0.2583	0.017	0.001	4.3
1689	248008	0.0473	0.5747	0.0051	0.0049	0.2631	0.014	0.0011	2.9
1689	248007	0.0538	0.575	0.0056	0.0055	0.2611	0.0127	0.0007	3.6
1688	248005	0.0493	0.5802	0.0053	0.0038	0.2629	0.0127	0.0008	4.6
1687	247994	0.0467	0.5974	0.0055	0.0045	0.2653	0.0129	0.001	3.8
1687	247992	0.0497	0.5791	0.0049	0.0056	0.2541	0.0114	0.0009	3.7
1684	247975	0.0498	0.5839	0.0061	0.0064	0.248	0.012	0.0007	3.7
1684	247973	0.051	0.5716	0.0052	0.0031	0.2743	0.0122	0.0007	4.5
1683	247968	0.0488	0.5782	0.0062	0.0067	0.2774	0.0173	0.0008	3.9
1683	247965	0.0533	0.5753	0.0069	0.0081	0.2744	0.0183	0.0008	5
1681	247954	0.0532	0.5354	0.0058	0.0061	0.2432	0.0152	0.0017	4.1
1680	247934	0.0528	0.5861	0.0051	0.0049	0.2506	0.0106	0.0008	4.4
1679	247927	0.0524	0.5325	0.0063	0.0074	0.2521	0.0139	0.0007	4
1679	247925	0.0496	0.5266	0.0063	0.0065	0.2388	0.0121	0.0007	3.3
1679	247923	0.0549	0.5395	0.0063	0.0044	0.2354	0.0126	0.0007	4.5
1678	247917	0.0562	0.572	0.0052	0.0064	0.27	0.0156	0.0029	2.7
1678	247915	0.0499	0.6139	0.0052	0.0073	0.2789	0.0134	0.0009	3.3
1677	247910	0.0543	0.5721	0.0055	0.0088	0.2444	0.0163	0.0008	3.3
1677	247907	0.0491	0.5727	0.0076	0.008	0.2383	0.0214	0.0004	4.6
1676	142129	0.0505	0.5408	0.0061	0.0077	0.2374	0.0161	0.0005	3.9
1676	247898	0.0449	0.535	0.0052	0.0072	0.2589	0.0156	0.0008	3.9
1676	247896	0.0521	0.54	0.0071	0.0051	0.2273	0.0139	0.0005	5.1
1675	247894	0.0474	0.5398	0.006	0.0082	0.2442	0.0173	0.0005	3.3

SEQ_ID	HEAT_ID	C	MN	N	S	SI	P	AL	H, ppm
1675	247892	0.0476	0.5845	0.0062	0.0092	0.2641	0.0215	0.0007	4.1
1674	247886	0.0518	0.6002	0.0061	0.0087	0.2544	0.0178	0.0022	3.3
1674	247884	0.0538	0.5682	0.0062	0.0081	0.2553	0.0164	0.0015	4
1673	142103	0.0471	0.5582	0.007	0.0063	0.2293	0.0207	0.003	4.1
1673	247874	0.0516	0.5262	0.0062	0.0049	0.2469	0.0161	0.0007	5.4
1672	247871	0.0533	0.5458	0.007	0.0057	0.2457	0.0216	0.0009	4.4
1672	247869	0.0478	0.554	0.0063	0.0059	0.2095	0.0242	0.0012	5.2
1671	247859	0.049	0.5848	0.0059	0.0051	0.2666	0.0108	0.0005	5
1670	247848	0.0505	0.5728	0.0064	0.0062	0.2402	0.0207	0.0007	4.7
1667	247817	0.0468	0.5921	0.0052	0.0059	0.268	0.0141	0.0013	3.5
1662	247612	0.0495	0.5773	0.0072	0.0075	0.2548	0.018	0.001	5.6
1657	247525	0.048	0.57	0.0068	0.004	0.257	0.019	0	4.8
1657	247524	0.051	0.58	0.0077	0.004	0.246	0.016	0	5.8
1656	247515	0.0491	0.5768	0.0052	0.0076	0.2457	0.0115	0.0007	3.3
1656	247513	0.0496	0.5965	0.0053	0.0064	0.2916	0.0092	0.0008	4.2
1655	247507	0.0463	0.5777	0.0058	0.0093	0.2608	0.0117	0.0005	4.3
1655	247505	0.0503	0.5691	0.0053	0.0061	0.2403	0.0173	0.0008	6.9
1654	247490	0.0541	0.5753	0.0065	0.0064	0.2533	0.0094	0.001	4.2
1652	247484	0.0496	0.5877	0.0064	0.0064	0.251	0.0139	0.0009	5.3
1651	141683	0.0566	0.6004	0.0058	0.0061	0.2698	0.0094	0.0008	4.7
1650	247461	0.0467	0.5729	0.006	0.0038	0.2663	0.0095	0.001	4.2
1650	141675	0.0519	0.5787	0.006	0.0052	0.2629	0.0098	0.0013	5
1649	141666	0.0546	0.6045	0.0056	0.0065	0.2755	0.0108	0.0009	4.2
1648	247441	0.0502	0.5949	0.0057	0.0049	0.2708	0.0097	0.0008	3.4
1648	247439	0.0493	0.5818	0.0047	0.0079	0.2588	0.012	0.0008	4.2
1647	247430	0.0483	0.5972	0.006	0.0037	0.2643	0.0069	0.0012	4.2
1646	141641	0.0497	0.5954	0.0044	0.0054	0.3043	0.0062	0.0011	3.6
1645	247410	0.0482	0.5731	0.0051	0.008	0.2456	0.0083	0.0007	3.8
1644	247403	0.05	0.6043	0.0065	0.0053	0.2547	0.0073	0.0007	4.2
1643	247399	0.0536	0.5801	0.0061	0.0054	0.2433	0.0075	0.0012	4.9
1642	247392	0.0531	0.5978	0.005	0.0056	0.2651	0.009	0.001	3.5
1642	247390	0.0499	0.5788	0.005	0.0066	0.2669	0.0077	0.0008	3.1
1640	247377	0.0519	0.5601	0.0055	0.0085	0.2511	0.0099	0.0026	3.7
1639	247362	0.0507	0.5192	0.0069	0.0054	0.2132	0.0096	0.0005	3.7
1639	247360	0.0492	0.5146	0.006	0.0058	0.1896	0.0094	0.0004	4.5
1638	247352	0.0492	0.587	0.0065	0.0084	0.2734	0.009	0.0006	3.7
1638	141578	0.0517	0.5727	0.0067	0.0111	0.2632	0.0155	0.0006	4.5
1637	247337	0.0484	0.5415	0.0059	0.0069	0.2201	0.0115	0.0006	4.4
1637	247335	0.0531	0.5491	0.0068	0.0076	0.2374	0.0102	0.0009	4.5
1636	141557	0.0504	0.5592	0.0076	0.0087	0.2491	0.0114	0.0005	4.4
1634	247319	0.049	0.5424	0.0071	0.007	0.2094	0.0111	0.0003	4.6
1633	247310	0.0486	0.59	0.006	0.0089	0.2655	0.0098	0.0002	4.1
1632	247133	0.0519	0.5795	0.0067	0.005	0.2511	0.0093	0.0006	3.9
1632	247130	0.0461	0.5733	0.0058	0.0043	0.2421	0.0091	0.0004	4
1631	141348	0.0505	0.575	0.0057	0.0047	0.2434	0.0087	0.0007	3.5
1631	141347	0.0463	0.5886	0.0056	0.0065	0.2798	0.0098	0.0006	3.9
1630	341342	0.0521	0.5775	0.0075	0.0077	0.2387	0.0133	0.0005	4.6
1624	141300	0.0456	0.5921	0.005	0.0068	0.2586	0.0086	0.0006	4
1623	141288	0.051	0.5978	0.0055	0.0064	0.2766	0.0107	0.0012	3.5
1621	247048	0.047	0.5613	0.0043	0.0066	0.2423	0.0112	0.0005	3.5
1621	247046	0.0499	0.553	0.0048	0.0062	0.2546	0.0105	0.0006	3.9

SEQ_ID	HEAT_ID	C	MN	N	S	SI	P	AL	H, ppm
1620	247036	0.0531	0.5953	0.0053	0.0087	0.2463	0.0104	0.0008	3.5
1619	141253	0.0506	0.5932	0.005	0.007	0.2589	0.0152	0.0011	3.6
1619	141252	0.0485	0.5782	0.0064	0.0085	0.2363	0.0133	0.001	3.9
1618	247018	0.0532	0.589	0.0057	0.0077	0.2359	0.0104	0.0004	4.3
1617	247011	0.0457	0.5767	0.0051	0.0053	0.2647	0.0105	0.001	3.3
1616	246997	0.0521	0.6192	0.0118	0.0044	0.2344	0.0072	0.0007	3.3
1611	246957	0.0533	0.574	0.0076	0.0078	0.2251	0.0151	0.0004	4.2
1610	246942	0.0469	0.5853	0.0063	0.0085	0.2698	0.011	0.0007	3.3
1610	246940	0.0535	0.5926	0.0063	0.0081	0.2533	0.0093	0.0006	4
1609	141146	0.0529	0.5733	0.0054	0.0073	0.223	0.0101	0.0007	3.4
1609	141141	0.0547	0.5534	0.0069	0.009	0.2169	0.0093	0.0005	4
1608	246915	0.0489	0.5895	0.006	0.007	0.2751	0.0093	0.0008	3.4
1607	141117	0.0537	0.5756	0.007	0.0077	0.2419	0.0122	0.0007	3.4
1606	141097	0.0512	0.5936	0.0057	0.0065	0.2582	0.0115	0.0005	3.6
1605	246877	0.0527	0.6154	0.0078	0.0056	0.2507	0.0092	0.0009	3.5
1605	246879	0.0497	0.5939	0.0055	0.0072	0.2418	0.0124	0.0009	3.1
1604	246862	0.0483	0.6336	0.0053	0.006	0.2694	0.0088	0.001	4.6
1603	246854	0.0522	0.6157	0.0058	0.0069	0.2587	0.0103	0.0011	3.2
1603	246852	0.0536	0.5455	0.005	0.0057	0.2468	0.01	0.0011	3.8
1602	246836	0.0468	0.6049	0.0044	0.0062	0.2748	0.0109	0.001	4.6
1601	246824	0.052	0.5846	0.0044	0.0103	0.2392	0.0126	0.0004	4.8
1598	246806	0.0459	0.5803	0.0041	0.006	0.2684	0.0086	0.0006	4.4
1598	246804	0.0499	0.5795	0.0053	0.0077	0.2609	0.011	0.0005	5.2
1597	141011	0.044	0.5661	0.0061	0.0063	0.2635	0.0125	0.0006	5.3
1596	246777	0.0492	0.5378	0.0072	0.0052	0.2417	0.0115	0.0003	4.5
1595	140990	0.0428	0.5817	0.0053	0.0036	0.2529	0.0131	0.0009	4.3
1595	140988	0.0494	0.5583	0.0072	0.0071	0.2074	0.0107	0.0004	4.6
1594	246759	0.048	0.5355	0.0064	0.009	0.2218	0.0094	0.0005	5.1
1594	140978	0.0479	0.5645	0.0065	0.0068	0.228	0.0157	0.0005	5.6
1593	140976	0.0541	0.5799	0.0066	0.0074	0.2485	0.0143	0.001	4.5
1592	246741	0.047	0.5652	0.0053	0.0055	0.2348	0.0127	0.0009	4.9
1591	246739	0.0549	0.5755	0.0075	0.0041	0.2343	0.016	0.001	4.6
1590	246725	0.0404	0.575	0.0045	0.0079	0.2505	0.0109	0.0002	4
1589	140941	0.0524	0.5793	0.0053	0.0057	0.2414	0.0127	0.0011	4.9
1588	246565	0.0477	0.6328	0.0078	0.0065	0.2361	0.0166	0.0012	4
1587	246559	0.0457	0.5635	0.0055	0.0055	0.2446	0.0218	0.0002	3.8
1586	246546	0.0573	0.5793	0.0059	0.0094	0.2237	0.0134	0.0003	3.4
1585	246544	0.0601	0.5434	0.007	0.0067	0.2672	0.0198	0.001	3.5
1584	246536	0.0538	0.5664	0.0064	0.0061	0.2087	0.0161	0.0008	3.8
1584	246528	0.0488	0.559	0.0061	0.0051	0.2251	0.0166	0.0009	4.8
1583	246527	0.0519	0.5723	0.0067	0.0082	0.2173	0.0123	0.0007	4
1582	246520	0.0485	0.582	0.0058	0.0108	0.2435	0.0137	0.0008	3.6
1582	246518	0.052	0.5639	0.0068	0.0104	0.2441	0.0121	0.0005	3.8
1579	246481	0.0514	0.5968	0.0063	0.0058	0.2555	0.0135	0.0007	3.3
1577	246459	0.0496	0.5945	0.0055	0.0056	0.2538	0.017	0.0005	3.1
1577	246457	0.0488	0.5943	0.006	0.0044	0.249	0.0156	0.0007	3.4
1576	246445	0.0446	0.549	0.0054	0.0031	0.2429	0.0105	0.0003	3.1
1575	246439	0.0498	0.5975	0.0049	0.0054	0.2644	0.0142	0.0006	3.2
1573	246414	0.0514	0.606	0.0047	0.0081	0.2639	0.0108	0.0005	3.2
1573	246412	0.0475	0.5915	0.0043	0.006	0.2657	0.0144	0.0006	3.8
1572	246393	0.0475	0.5955	0.0061	0.0072	0.2398	0.0113	0.0005	4.3

SEQ_ID	HEAT_ID	C	MN	N	S	SI	P	AL	H, ppm
1570	246382	0.0501	0.5498	0.006	0.0071	0.2495	0.0122	0.0005	4.3
1569	246367	0.0563	0.5763	0.006	0.0064	0.2326	0.0108	0.0006	3.4
1569	246365	0.0501	0.5745	0.006	0.0063	0.229	0.0127	0.0003	3.6
1568	246356	0.0486	0.5478	0.0058	0.0082	0.2374	0.0129	0.0026	3
1568	246354	0.0499	0.5564	0.0062	0.0078	0.2437	0.013	0.0013	3.3
1567	246341	0.0489	0.5659	0.006	0.0083	0.2291	0.0153	0.0002	3.3
1567	140568	0.0469	0.539	0.0061	0.0069	0.2159	0.0137	0.0004	3.5
1566	246331	0.0452	0.5614	0.0051	0.0086	0.2491	0.0129	0	2.7
1566	246329	0.0433	0.5522	0.0054	0.0072	0.2514	0.0124	0.0006	3.4
1565	246318	0.0504	0.5674	0.0047	0.0068	0.241	0.0115	0	3.8
1564	246304	0.0483	0.5708	0.0038	0.0077	0.2519	0.0119	0	3.1
1564	246302	0.0502	0.5742	0.005	0.0073	0.2563	0.0121	0.0002	3.5
1563	140529	0.0537	0.582	0.0066	0.0061	0.2574	0.0131	0	3.6
1561	140516	0.0546	0.5888	0.0048	0.006	0.2504	0.014	0	3.7
1561	246272	0.0495	0.5774	0.0051	0.0051	0.2423	0.0142	0	3.9
1560	140502	0.0497	0.5865	0.005	0.0061	0.2626	0.0122	0.0004	3.2
1560	140500	0.0494	0.5902	0.0051	0.0037	0.2591	0.0154	0.0001	3.9
1558	246242	0.0479	0.6095	0.005	0.005	0.2586	0.0127	0.0006	3.9
1558	246240	0.0472	0.5867	0.0052	0.008	0.245	0.0107	0.0004	4.5
1556	246020	0.0522	0.607	0.0062	0.0077	0.2674	0.0085	0.0006	3.6
1555	140256	0.0554	0.5559	0.0061	0.0059	0.2504	0.0107	0.0003	4.3
1551	245974	0.0539	0.5876	0.0077	0.0064	0.2776	0.0128	0	4
1550	245965	0.0556	0.5781	0.0078	0.0054	0.2545	0.0127	0	3.9
1550	245963	0.0513	0.5759	0.0074	0.0057	0.2686	0.0131	0	4
1549	245948	0.0549	0.5936	0.0075	0.0069	0.2493	0.0118	0.0002	3.6
1548	245938	0.0528	0.6059	0.0064	0.0059	0.273	0.0142	0.0002	3.7
1548	245936	0.0525	0.602	0.0067	0.0051	0.2828	0.0145	0.0001	3.7
1547	245925	0.0516	0.585	0.0069	0.0061	0.2543	0.0163	0.0003	3.4
1547	445923	0.0593	0.5902	0.0087	0.0087	0.244	0.0195	0.0004	3.6
1545	245912	0.0509	0.567	0.0061	0.0076	0.2583	0.0171	0.0004	3.9
1544	245900	0.0535	0.5995	0.0055	0.0085	0.2546	0.0124	0.0007	3.4
1544	245898	0.0468	0.5968	0.0058	0.0086	0.2499	0.0143	0.001	3.4
1543	140119	0.0492	0.5673	0.0062	0.0081	0.2386	0.0093	0	4.9
1540	245864	0.0518	0.5756	0.0054	0.009	0.2595	0.0163	0.0004	3.6
1540	245863	0.0499	0.569	0.0055	0.0087	0.2646	0.015	0.0002	3.9
1539	245850	0.0544	0.5864	0.005	0.0082	0.2566	0.0125	0.0005	3.7
1538	245837	0.0542	0.5554	0.0057	0.007	0.2291	0.012	0.0002	4
1537	245825	0.0522	0.5892	0.0052	0.0051	0.2694	0.0098	0.0005	2.9
1537	245824	0.0505	0.5761	0.006	0.0065	0.2778	0.0134	0.0004	3.4
1536	140056	0.0512	0.5926	0.0065	0.0087	0.2416	0.0125	0.0002	3.5
1536	245814	0.0578	0.5835	0.0064	0.0098	0.2492	0.0121	0.0002	3.7
1535	140039	0.0492	0.5748	0.0072	0.0088	0.2393	0.012	0.0003	3.8
1535	245797	0.0507	0.5567	0.0075	0.0087	0.2404	0.0113	0.0003	4.1
1534	245789	0.0504	0.5519	0.0047	0.0068	0.2903	0.017	0.0007	2.9
1534	245788	0.0521	0.5839	0.0062	0.0048	0.2573	0.0152	0.0007	3.9
1533	245772	0.0539	0.5858	0.0067	0.0087	0.2602	0.014	0.0004	3.2
1533	245771	0.0557	0.5708	0.0069	0.0085	0.258	0.0143	0.0008	4.1
1532	245769	0.0483	0.5726	0.0055	0.0073	0.2318	0.0143	0.0001	3.6
1532	245767	0.0571	0.5644	0.0052	0.0059	0.2327	0.0137	0	3.8
1530	245559	0.0488	0.562	0.005	0.0043	0.2397	0.0191	0.0005	3.2
1529	245553	0.0541	0.6186	0.0072	0.009	0.2555	0.019	0.0004	3.7

SEQ_ID	HEAT_ID	C	MN	N	S	SI	P	AL	H, ppm
1528	245541	0.0507	0.5565	0.0066	0.0102	0.2477	0.0177	0.0003	3
1528	245539	0.048	0.5393	0.0068	0.0096	0.2412	0.0178	0.0003	4.2
1527	245525	0.0557	0.5628	0.0062	0.0058	0.2499	0.0141	0.0004	3.6
1527	149763	0.0526	0.5941	0.0081	0.0072	0.2513	0.0154	0.0005	4.4
1522	245462	0.0456	0.6022	0.005	0.0068	0.2665	0.0143	0.0006	2.9
1522	245461	0.0501	0.5844	0.0058	0.0077	0.2664	0.0153	0.0003	3.3
1521	149689	0.0478	0.6002	0.0054	0.0089	0.2797	0.0123	0.0005	3.6
1520	245443	0.0478	0.5367	0.0063	0.0064	0.2345	0.0173	0.0004	3.6
1517	245424	0.0541	0.5914	0.0071	0.0062	0.2368	0.0115	0.0003	3.7
1515	149635	0.051	0.6086	0.0064	0.0076	0.2751	0.0119	0.0004	3.5
1515	149634	0.0549	0.6079	0.0065	0.0033	0.2653	0.0116	0.0004	3.5
1514	245403	0.0491	0.5964	0.0071	0.0085	0.2261	0.0097	0.0001	3.5
1514	245400	0.051	0.5616	0.0064	0.0087	0.2517	0.0109	0.0001	3.9
1513	149612	0.0448	0.5826	0.0057	0.0068	0.2585	0.0147	0.0004	3.2
1513	149610	0.0537	0.5647	0.0066	0.0082	0.2466	0.0136	0	3.5
1512	245373	0.051	0.5857	0.0058	0.0086	0.2512	0.0117	0.0005	2.8
1512	245371	0.0507	0.5571	0.0071	0.0075	0.2447	0.0117	0	4
1511	245353	0.0498	0.5823	0.0065	0.0063	0.2387	0.0109	0.0001	3.5
1510	245352	0.0532	0.5931	0.0065	0.0063	0.2623	0.0112	0.0001	3.8
1509	245339	0.0504	0.564	0.0074	0.0089	0.2599	0.0137	0.0003	2.9
1508	245333	0.0561	0.591	0.0071	0.0073	0.2541	0.0119	0.0003	3.6
1507	245308	0.0514	0.5784	0.0053	0.0046	0.2385	0.0118	0.0001	3.6
1506	245295	0.0456	0.5876	0.0053	0.005	0.2488	0.0095	0.0004	3.6
1506	245294	0.0521	0.6418	0.006	0.0063	0.2718	0.0116	0.0005	2.9
1504	245287	0.0524	0.5863	0.0055	0.0042	0.2609	0.0127	0.0012	3.6
1503	245274	0.044	0.5684	0.0053	0.0068	0.2509	0.0096	0.0002	3.1
1503	149504	0.0485	0.5695	0.0057	0.0066	0.2449	0.0097	0.0002	3.5
1502	245262	0.0512	0.5974	0.004	0.0088	0.269	0.0091	0.0002	2.8
1502	245261	0.0475	0.579	0.0045	0.0068	0.256	0.0107	0.0008	4
1500	245082	0.052	0.5876	0.0062	0.0106	0.2418	0.0107	0.0003	2.7

From the heats reported in Table 2, it is seen that the levels of nitrogen can be up to 120 ppm, and the levels of hydrogen are between 1.0, 2.0 or 3.0 and 6.5 ppm at atmospheric pressure. Moreover, the hydrogen level of 6.9 ppm in heat 1655 is with a ferrostatic head of more than 1 atmosphere pressure, namely about 1.15 atmospheres, as shown in Figure 3

The free nitrogen was determined by analysis with optical emission spectrometry ("OES") calibrated against the thermal conductivity ("TC") method on a scheduled basis. Optical emission spectrometry (OES) using arc and spark excitation is the preferred method to determine the chemical composition of metallic samples. This process is widely used in the metal making industries, including primary producers, foundries, die casters and manufacturing. Due to its rapid analysis time and inherent accuracy, Arc/Spark OES systems are most effective in controlling the processing of alloys. These spectrometers may be used for many aspects of the production cycle including in-coming inspection of materials, metal processing, quality control of semi-finished and finished goods and many other applications where a chemical composition of the metallic material is required.

The Thermal Conductivity (TC) method, used to calibrate the OES, typically employs a microprocessor-based, software controlled instrument that can measure nitrogen, as well as oxygen, in a wide variety of metals, refractories and other inorganic materials. The TC method employs the inert gas fusion principle. A weighed sample, placed in a high purity graphite crucible, is fused under a flowing helium gas stream at temperatures sufficient to release oxygen, nitrogen and hydrogen. The oxygen in the sample, in all forms present, combines with the carbon from the crucible to form carbon monoxide. The nitrogen present in the sample releases as molecular nitrogen and any hydrogen is released as hydrogen gas.

In the TC method, oxygen is measured by infrared absorption (IR). Sample gases first enter the IR module and pass through CO and CO_2 detectors. Oxygen present as either CO or CO_2 is detected. Following this, sample gas is passed through heated rare-earth copper oxide to convert CO to CO_2 and any hydrogen to water. Gases then re-enter the IR module and pass through a separate CO_2 detector for total oxygen measurement. This configuration maximizes performance and accuracy for both low and high range.

In the TC method, nitrogen is measured by passing sample gases to be measured through heated rare-earth copper oxide which converts CO to CO_2 and hydrogen to water. CO_2 and water are then removed to prevent detection by the TC cell. Gas flow then passes through the TC cell for nitrogen detection.

As stated above, the free hydrogen is measured by a Hydrogen Direct Reading Immersed System ("Hydris") unit, made by Hereaus Electronite. This unit is believed to be described in the following referenced US patents: U.S. Patent Nos 4,998,432; 5,518,931 and 5,820,745.

While the invention has been illustrated and described in detail in the foregoing drawings and description, the same is to be considered as illustrative and not restrictive in character, it being understood that only illustrative embodiments thereof have been shown and described and that all changes and modifications that come within the spirit of the invention are desired to be protected. Additional features of the invention will become apparent to those skilled in the art upon consideration of the description. Modifications may be made without departing from the spirit and scope of the invention.

2004279474 04 May 2010

What is claimed is:

1. A method of casting steel strip comprising:

introducing molten plain carbon steel on casting surfaces of at least one casting roll with the molten steel having a free nitrogen content below about 120 ppm and a free hydrogen content below about 6.5 ppm measured at atmospheric pressure; and

solidifying the molten steel to form metal shells on the casting rolls having nitrogen and hydrogen levels reflected by the content thereof in the molten steel to form thin steel strip.

2. The method of claim 1 where the free hydrogen content is between 1.0 and 6.5 ppm at atmospheric pressure.

3. The method of claim 1 or claim 2, wherein:

said casting surfaces are provided by a pair of cooled casting rolls having a nip between them and confining end closures adjacent to ends of the casting rolls;

said molten plain carbon steel is introduced between the pair of casting rolls to form a casting pool on the casting rolls with the end closures confining the pool, the casting rolls are counter-rotated and the solidified thin steel strip is formed through the nip between the casting rolls to produce a solidified steel strip delivered downwardly from the nip.

4. The method of any one of claims 1 to 3, wherein the free nitrogen content is below about 100 ppm.

5. The method of any one of claims 1 to 3, wherein the free nitrogen content is below about 85 ppm.

2004279474 04 May 2010

6. The method of any preceding claim, wherein the strip thickness is less than 2 mm.

7. The method of any preceding claim where the free hydrogen content is between 3 and 6.5 ppm at atmospheric pressure.

8. A method of casting steel strip comprising:

introducing molten plain carbon steel on casting surfaces of at least one casting roll with the molten steel having a free nitrogen content below about 120 ppm and a free hydrogen content below about 6.9 ppm and such that the sum of partial pressure of nitrogen and partial pressure of hydrogen is no more than 1.15 atmospheres;

forming a casting pool of molten metal on the casting surfaces of the casting rolls; and

solidifying the molten steel to form metal shells on the casting rolls having nitrogen and hydrogen levels reflected by the content thereof in the molten steel to form thin steel strip.

9. Steel strip produced by the method according to any one of claims 1 to 8.

10. A method of casting steel strip, substantially as herein described with reference to the accompanying drawings.

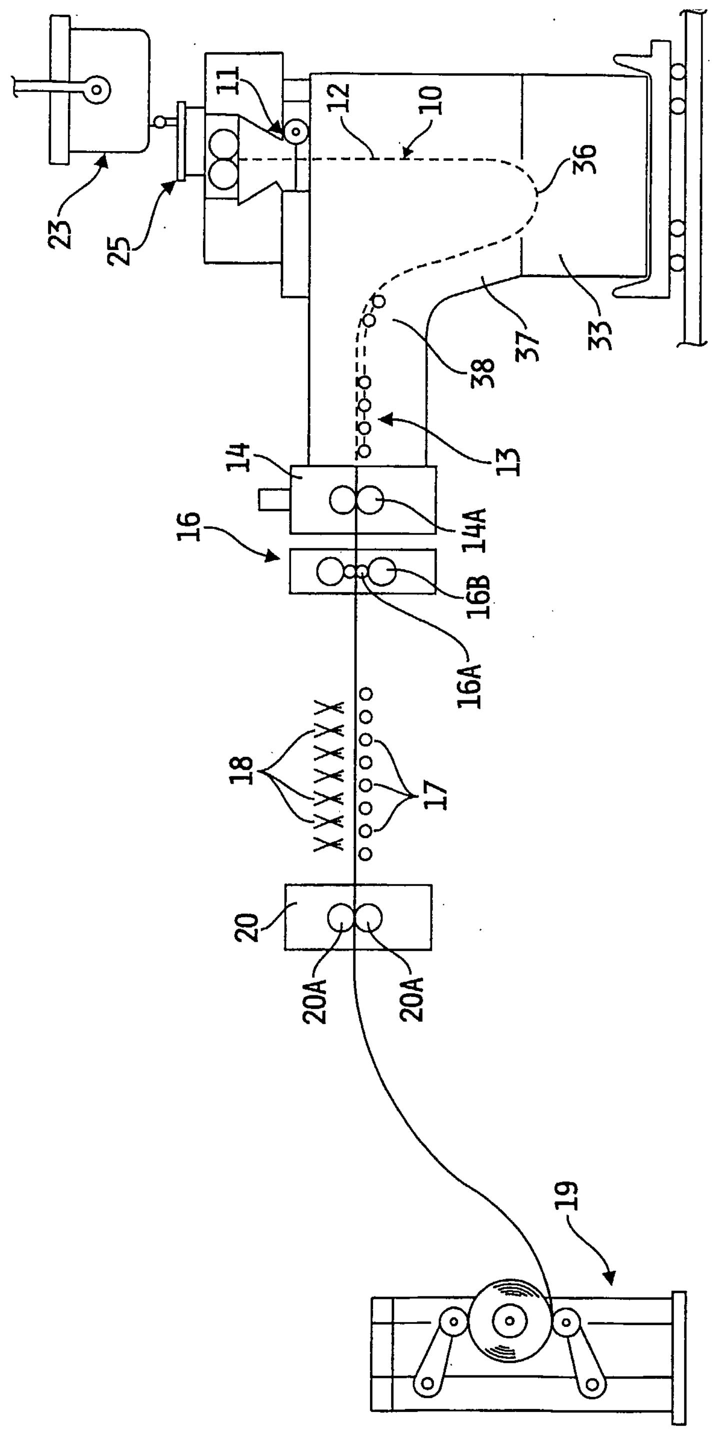

FIG. 1

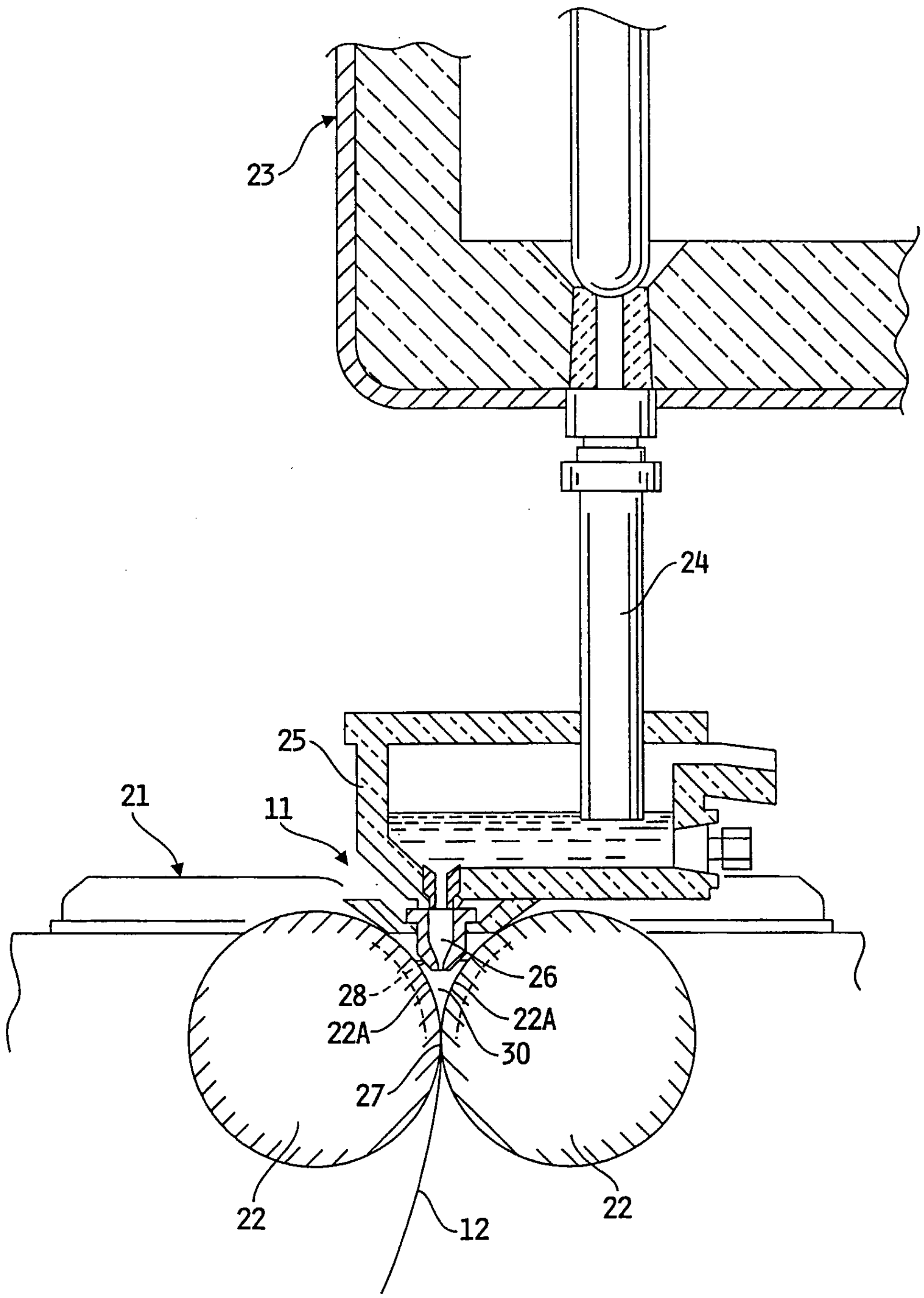

FIG. 2

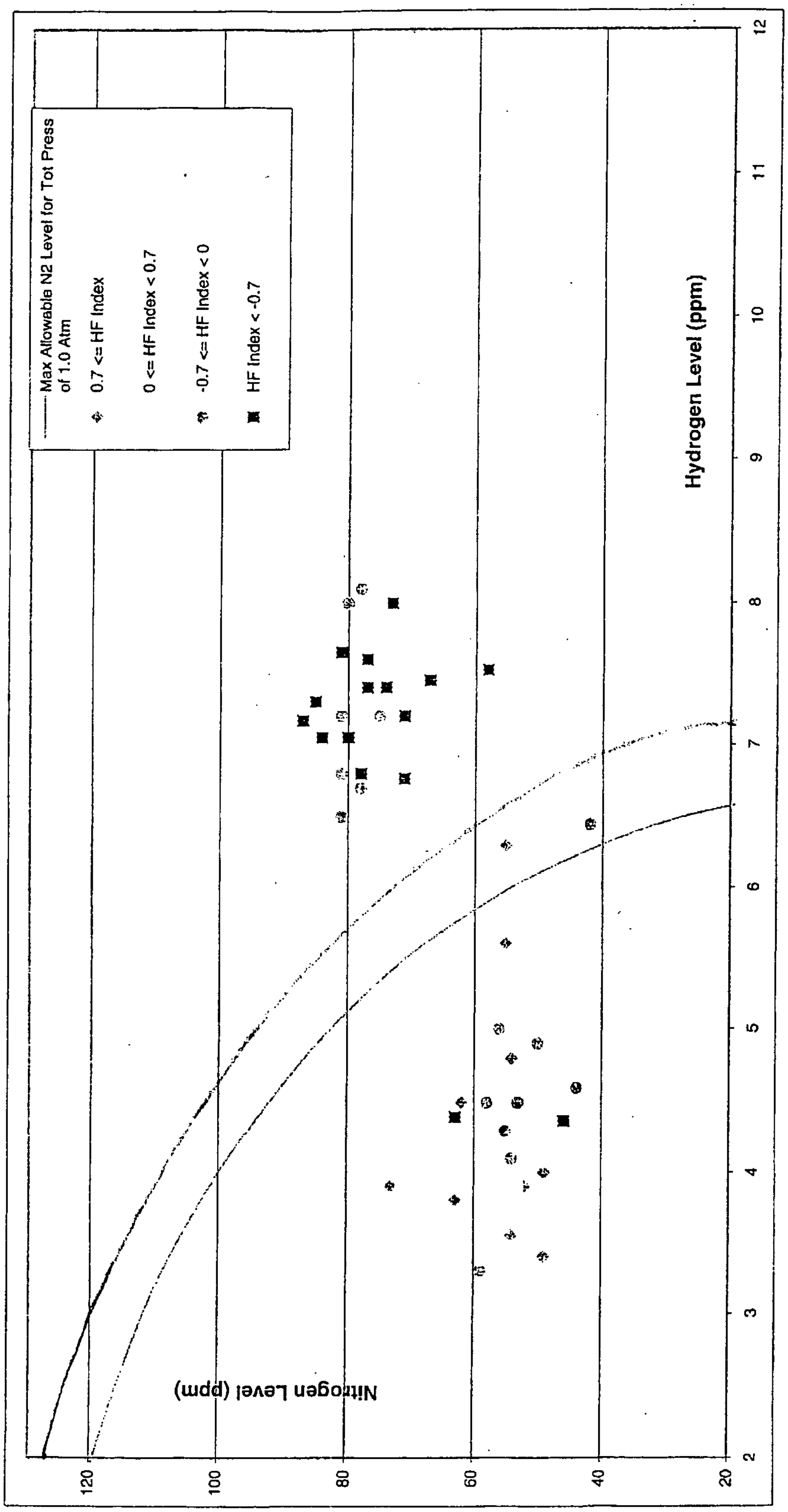
Max Allowable N2 Level for Tot Press of 1.0 Atm
0.7 <= HF Index
0 <= HF Index < 0.7
-0.7 <= HF Index < 0
HF Index < -0.7
Nitrogen Level (ppm)
Hydrogen Level (ppm)
120
100
80
60
40
20
2
3
4
5
6
7
8
9
10
11
12

FIG. 3