

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
18 June 2009 (18.06.2009)

PCT

(10) International Publication Number
WO 2009/076061 A2

(51) International Patent Classification:
C04B 14/06 (2006.01)

(21) International Application Number:
PCT/US2008/084591

(22) International Filing Date:
25 November 2008 (25.11.2008)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
11/953,081 10 December 2007 (10.12.2007) US

(71) Applicant and

(72) Inventor: **DE ARELLANO, Eduardo, Ramirez**
[US/US]; P.O. Box 6451, Mayaguez, PR 00681 (US).

(74) Agent: **RIOS, Roberto, J.**; Hoglund & Pamias, 256,
Eleanor Roosevelt, San Juan, PR 00918 (US).

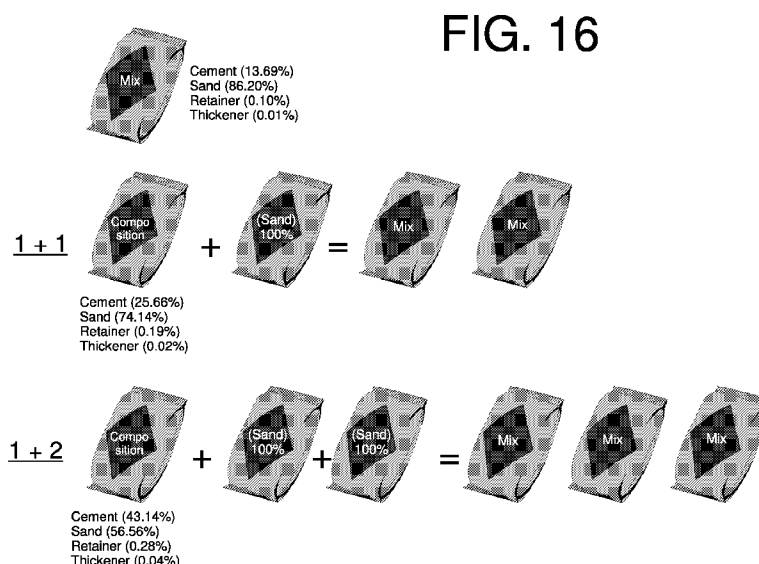
(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MT, NL, NO, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:

— without international search report and to be republished upon receipt of that report

(54) Title: CONCRETE-BASED MATERIAL AND METHOD OF APPLYING THE SAME



(57) Abstract: A composition is applied by spraying or projecting the resulting composition on the surface of a structure by projection. The composition is prepared by selectively mixing sand and cement with at least one additive, wherein the sand comprises a specific grain diameter distribution. The composition is prepared so that when mixed with water pumping of said mixture is facilitated while at the same time application by spraying or projecting the resulting composition on the surface of a structure by projection is allowed. The composition optimizes the traditional method of application by allowing the integration of new steps: pumping, expulsion and adhesion.

PRIORITY

This application is a continuation-in-part of application Ser. No. 10/807,895, filed Mar. 24, 2004 now U.S. Pat. No. 7,185,472, which is a continuation-in-part of application Ser. No. 09/730,526, filed Dec. 5, 2000 now U.S. Pat. No. 6,746,717.

FIELD OF THE INVENTION

The invention relates to an improved composition of a concrete-based material used to cover the interior or exterior of a building or other structure and methods of applying the composition. More specifically, the improved composition optimizes surface properties of a one-coat mortar and improves labor efficiency in the application process.

BACKGROUND OF THE INVENTION

Concrete-based materials are used in a variety of applications. For example, concrete-based materials are often used to cover walls or other structures. U.S. Pat. No. 6,046,269, issued Apr. 4, 2000, by Nass et al., teaches a concrete-based compound that is used to create a Fresco-like finish on a wall or other structure. The drying time of certain mixtures taught by this patent can be reduced by the use of propylene glycol and methyl carbitol. In effect, these compounds act as accelerants that speed the drying process.

Other accelerates for concrete-based materials are commercially available. For example, BETTOR MBT, S.A., manufactures and sells an accelerant, which is commercially available as BETTACEL. BETTOR MBT may be contacted through their Internet web site, which is hosted at: www.bettor-mbt.es, or at either of the following physical addresses: Headquarters, BETTOR MBT, S.A., Joiers, s/n,

08184 Palau de Plegamans, (Barcelona), Spain; Telephone: 93 862 00 23; Facsimile: 93 862 00 19; or Production, BETTOR MBT, S.A., Duero, 23, Poligono Ind. Mejorada, 28840 Mejorada del Campo, (Madrid), Spain; Telephone: 91 668 21 56; Facsimile: 91 668 17 75.

The accelerant, BETTACEL, is an aqueous solution made with inorganic salts and halogens. Its main function is to accelerate drying time and hardening of mortar, increasing the mortar resistance in the process. The accelerant may be used even at low temperatures. This accelerant comes in a liquid state, and should be mixed first with part of the water to be used with the mortar, and then added to the mortar as the rest of the water is added. It comes in containers weighing 30 kg or 250 kg. The characteristics of this accelerant are as follows:

Color:	Cloudy, non-color
pH:	9 ± 1
Density:	$1.3 \pm 0.02 \text{ g/cm}^3$
Chloride ions amount	$25.5 \pm 1.5\%$

The recommended dosage is 2 to 5% of the weight of the mortar being used. This percentage varies according to the desired effect (how fast you want the mortar to dry), the temperature and the type of cement with which the accelerant will be applied.

Again, concrete-based materials are widely used on buildings or other structures to provide an even exterior surface. The concrete-based materials are spread over a rough concrete surface. Such rough concrete surfaces include bricks, blocks or stones that are held together by cement or concrete.

Concrete-based materials for providing an even exterior surface are widely known, and commonly used in the construction arts. For example, U.S. Pat. No. 4,222,785, issued Sep. 16, 1980, by Henderson,

teaches a concrete-based material suitable for application to the exterior of a building. This particular mixture provides certain insulating characteristics.

U.S. Pat. No. 4,229,225, issued Oct. 21, 1980, by Kraszewski et al., teaches another concrete-based material suitable for application to the exterior of a building. This particular mixture includes:

20-60% cement;

30-70% inorganic or organic filler;

2-10% zirconium, hafnium, vanadium or cesium silicate fibers;

0.2-1% plasticizers for cement;

1-3% adhesive; and

0.1-0.5% water-repellent.

This above mixture provides certain water-repellent characteristics discussed therein.

U.S. Pat. No. 4,946,505, issued Aug. 7, 1990, by Jungk, teaches yet another concrete-based material.

More specifically, it teaches certain methods of dyeing concrete-based materials. The dyed materials may be applied to the exterior of a building or other structure. Each of the above-identified patents are expressly incorporated herein by reference.

Similar one-coat concrete-based materials are also widely available in commercial markets. For example, Lafarge Texsa Morteros and Sermarksa sell many generic one-coat grey or white concrete-based products. Lafarge Texsa Morteros can be contacted at the following physical address: Lafarge Texsa Morteros, Pol. Can Peligri, C/Ferro, 7-08755, Catellbisbal(Barcelona), Spain; Tel. 936351290. Sermarksa can be contacted at the following physical address: Sermarksa, Carr. 152 Km9, 08110

Monocada, Rey Sak, Barcelona, Spain; Tel. 935726500.

PROPAMSA, S.A., is another company that manufactures and sells a number of concrete-based (or mortar-based) products that may be used to create an even interior or exterior surface on a building or other structure. These include PROPAM REVOC and REVAT RASPADO. PROPAMSA may be contacted at the following physical address: PROPAMSA, S.A., Ctra. N-340 Km 1242.3, Pol. Ind. Les Fallulles, San Vincent Del Horts, 08620 Barcelona, Spain. The application and characteristics of these products are discussed below.

The PROPAM REVOC and REVAT RASPADO products can be used by following a simple three-step process. First, the products are mixed with water to the desired consistency. Second, the products are applied to a rough concrete surface using a smooth trowel 100 (shown in FIG. 1). Third, when the product becomes semi-dry, the exterior skin is removed using a rough trowel 200 (shown in FIG. 2). This creates an even exterior finish that is both attractive and resistant to weather. FIG. 3 shows the application of these concrete-based materials 310 to a block wall 320.

PROPAM REVOC is a mortar based on cement, additives and aggregates that give it the property of high impermeability. It must be applied to a base that is resistant, completely hardened and extremely clean (free of dust, paint, oil, etc.). Also, if the base is exposed to sun or is made of a highly absorbent material, then the surface must first be dampened before applying PROPAM REVOC.

PROPAM REVOC is sold in 25 kg bags that are mixed manually or mechanically with 17% water (about 4.5 L). Once it is mixed it must be applied within 25 minutes or it will begin to harden. This mixture comes in gray and white and will cover approximately 2 kg/m^2 per cm of thickness. This,

however, depends upon both the flatness and the roughness of the surface. For example, rough brick surfaces will require more, relatively smooth and even concrete walls will require less.

The characteristics of this particular product are as follows:

Apparent density of the powder:	1.6 g/cm ³
Mixing water:	17%
Apparent density of the paste:	2.0 g/cm ³
Mixtures lifetime:	90 minutes
Density of hardened product:	1.7 g/cm ³
Flexotraction strength:	20 kg/cm ²
Compressive resistance:	60 kg/cm ²
Coefficient of capillarity:	0.6 g/dm ² min ^{1/2}
Modulus of elasticity:	85.000 kg/cm ²

REVAT RASPADO is a one-coat mortar also based on cement, additives and aggregates that give protection as well as a decorative finish to a building. This product is impermeable to rain water and permeable to water vapor to prevent condensation.

REVAT RASPADO is prepared by mixing the 30 kg bag with 20% water (6 L) until a smooth paste is formed. Once the mixture is made, it must stand for 5 minutes so the mixture will settle. Then the mixture is spread with a trowel. If it is applied to a highly absorbent surface, a first coat should be applied as a primer. The additives include dyes, and the product is available in a variety of colors. It will cover approximately 20 kg/m² per cm of thickness. The type of finish and lack of flatness of the surface will alter the coverage of this mortar. The characteristics of this particular product are as follows:

Product in powder form:

Apparent density:	1.4 g/cm ³
Loss in 450 ^C fire:	1%
Loss in 900 ^C fire:	35%
Particles greater than 1.2 mm	4.0% (by weight)
Particles greater than 0.18 mm	55.0% (by weight)

Product in paste form:

Mixing water:	20%
Apparent density:	1.8 g/cm ³
<u>Hardened product:</u>	
Product density:	1.6 g/cm ³
Flexural strength:	35 kg/cm ²
Compressive resistance:	80 kg/cm ²
Tensile strength:	8.3 kg/cm ²
Elasticity modulus:	90,000 kg/cm ²
Shrinkage:	1.0 mm/m
Coefficient of capillarity:	1 g/dm ² min ^{1/2}
Permeability to vapor:	0.5 g/m ² h mmHg

The traditional method for applying plaster is a cumbersome manual system, in which a worker mixes the mortar, the sand (which is usually located near the working area) and cement either manually with the help of a shovel or mechanically with the aid of a mixing apparatus. Once the final mixture is prepared and deposited in a container, it is then relocated to the area where it must be applied. If the area to be applied is not located at ground level a crane is generally used to transport the mixture. There are other instances where the area to be applied is remotely located from the preparation area. In such cases, it is well known to transport the mixture manually or by means of a mechanical vehicle/crane.

Once the mixture is finally transported to the application area, a trained worker selectively applies the mixture to a desired surface in a well known manner. This application step is repeated as many times as necessary until the surface is completely filled and a desired surface level is achieved. Finally, a desired surface finish such as but not limited to: stucco, stamped, or smooth is created. However, this entire process takes a considerable amount of time that could affect the properties of the mixture. Thus, a

more efficient method and system to transport said mixture to a remote location without negatively affecting the properties of the mixture is needed.

Under typical application conditions (approximately 80 degrees Fahrenheit and high humidity), the expected dry time of PROPAM REVOC or REVAT RASPADO can exceed 4 hours (as long as 6 hours has been observed). As will be appreciated from the foregoing, the application of these products is labor intensive. First, the application requires a significant expenditure of labor hours even for a relatively small area. Then, after the product has set, another significant expenditure of labor hours is required to remove the exterior skin with the rough trowel. Some methods of reducing the required labor hours have been developed. For example, the mortar can be sprayed upon the surface of a building rather than applied manually. This somewhat reduces labor hours, but still requires a significant effort to smooth and remove the exterior skin. The labor-intensive nature of these products is not unique. Other concrete-based materials used to treat the interior and exterior of a building also require a significant expenditure of labor hours.

In addition to labor hours, another important feature of a one-coat mortar is its finish. When the product is finished it must present a smooth attractive surface. Preferably, the surface is flat and even, however, a perfectly flat and even surface lacks a certain desirable aesthetic. Indeed, the cold, hard look of a concrete surface has limited the acceptance of one-coat mortar finishes. Developing a more attractive aesthetic remains an important object of one-coat mortar finishes.

SUMMARY OF THE INVENTION

According to one aspect of the invention, an even interior or exterior surface is formed on a building. The method is especially suited for reducing the labor requirements of applying a concrete-based

material to the building. An exterior portion of the mortar surface is removed by scraping a rough trowel against the mortar surface.

According to further aspects of the invention, the concrete-based mortar has at least fifty-percent of particles greater than 0.18 millimeters in diameter (by weight) and at least two-percent of particles greater than 1.2 millimeters in diameter (by weight).

According to a further aspect of the invention, the concrete-based mortar includes particles, such as sand, having a diameter of greater than 0.18 millimeters as at least half (by weight) of the composition of the concrete-based mortar. At least a percent of those particles (by weight) have a diameter greater than 1.2 millimeters.

According to another aspect of the invention, a concrete-based mortar, including sand, is mixed with water to form a resulting composition that hardens. The sand includes grains approximately 1 millimeter in diameter and grains less than 0.5 millimeters in diameter. The resulting composition is applied to an exterior of a building. The resulting composition hardens on the building for a time sufficient to prevent reformation of the composition. The resulting composition is scraped to remove an exterior portion of the resulting composition. The surface of the composition defines a plane after the step of scraping. At least a portion of the grains approximately 1 millimeter in diameter lie along the plane and are removed by the step of scraping so that the surface includes a plurality of divots where the grains approximately 1 millimeter in diameter have been removed.

According to another aspect of the invention, the resulting composition is applied by spreading the resulting composition on the exterior of the building with a trowel.

According to another aspect of the invention, the resulting composition is applied by spraying or projecting the resulting composition on the surface of a structure by projection. In order to achieve this, the composition according to another aspect of the invention is formed by selectively mixing aggregates and cement with at least one additive. In another aspect of the invention, a desired composition is achieved by selectively combining cement, sand and additive, wherein the sand comprises a specific grain diameter distribution.

According to a further aspect of the invention, the composition is prepared so that when mixed with water pumping of said mixture is facilitated while at the same time application by spraying or projecting the resulting composition on the surface of a structure by projection is allowed.

According to another aspect of the invention, the composition optimizes the traditional method of application by allowing the integration of new steps: pumping, expulsion and adhesion.

DESCRIPTION OF THE DRAWINGS

FIG. 1 is a perspective view of a smooth trowel (prior art).

FIG. 2 is a perspective view of a rough trowel (prior art).

FIG. 3 is an elevation view of a concrete wall partially covered with mortar (prior art).

FIG. 4 is a flow chart showing one preferred method of applying a concrete-based mortar to the exterior of a building or other structure.

FIG. 5A is a side view of an exterior wall showing the application of a concrete-based mortar.

FIG. 5B is a side view of the exterior wall of FIG. 5A showing the process of scraping the exterior wall with a rough trowel.

FIG. 5C is a side view of the exterior wall of FIG. 5B showing the exterior wall after completely

scraping the exterior wall with the rough trowel.

FIG. 6A is a schematic, close-up side view of a portion of the exterior wall of FIG. 5A.

FIG. 6B is a schematic, close-up side view of a portion of the exterior wall of FIG. 5B.

FIG. 6C is a schematic, close-up side view of a portion of the exterior wall of FIG. 5C.

FIG. 7 is a hose and spray nozzle for pumping the mortar material to a desired location.

FIG. 8 shows the mortar exiting the spray nozzle of the hose.

FIG. 9 shows the mortar mixture applied to the wall surface at different stages of application.

FIGS. 10a-10b show a transversal view of mortar applied on a wall surface.

FIG. 11 shows a transversal view of mortar applied on a ceiling surface.

FIGS. 12a-12b show a panoramic view of the mortar application to a ceiling.

FIG. 13 shows a panoramic view of a high-rise building where the mortar is pumped.

FIG. 14 is a table showing different types of cement.

FIG. 15 is a table showing several combinations of components and additives according to a preferred embodiment of the invention.

FIG. 16 is an exemplary illustration of one combination described in the table shown in FIG. 15.

DETAILED DESCRIPTION

With reference to **FIG. 4**, one preferred method of implementing the invention will be described. The process begins at step 410 by mixing an accelerant with water. As used herein, an accelerant is any compound, mixture, substance, liquid, powder or process that reduces the drying time of a concrete-based material. Here the accelerant, BETTACEL, available from BETTOR MBT, S.A., is mixed with

water. The properties of this particular product are set forth above.

Next, at step 412, the accelerant and water mixture is added to a concrete-based mortar. As used herein, concrete-based mortar is any compound having sand, aggregates and cement as components of the mortar. Here, one of the concrete-based mortars, PROPAM REVOC or REVAT RASPADO, available from PROPAMSA, S.A., is used. The properties of these particular products are set forth above.

As one alternative, the accelerant and any other additives are included with the concrete-based mortar. In a single step, this mortar is then mixed with water. This method is particularly well suited for applications where the mortar is pre-mixed.

Next, at step 414, the resulting mixture is applied to the exterior or interior of a building or other structure. As those skilled in the art will appreciate, the surface should be clean and free of any oils, dust, dirt, debris, etc., to aid the formation of a strong bond between the mixture and the building or other structure. The mixture is applied with a smooth trowel 100 (shown in **FIG. 1**) in a layer that is approximately 1 cm thick. When applied to rough surfaces the thickness may vary somewhat. Preferably, however, the mixture is applied to a relatively smooth surface such as a flat block wall.

As an alternative method of application, the resulting mixture can be sprayed upon the building. In this preferred method, the concrete mortar is mixed so that it can pass through a hose and a spray nozzle. The mixture is made using various additives, which are described below. The mortar is then sprayed or protected upon the surface of a building in relatively continuous beads. After this application, the beads are smoothed with a flat trowel.

After application, at step 416, the mixture is allowed to set so that a skin begins to form on the exterior

of the mixture. As the mixture is setting, the mason(s) may continue to apply the mixture on other parts of the building. As the mason finishes such other parts, the first application will have set and is ready to be scraped with the rough trowel 200 (shown in **FIG. 2**). Likewise, as the mason finishes scraping the first application, the subsequent application will have begun to set. Such areas may then be scraped with the rough trowel 200 as well.

At step 416, the applied mixture is tested to determine whether it has sufficiently set so that it is ready to be scraped with the rough trowel 200. The rough trowel 416 is briskly scraped against a small section of the mixture, in an inconspicuous area. If the mixture sticks to the spikes 212 of the rough trowel 416, then it is not dry yet and cannot be scraped. When the rough trowel 200 can pass across the applied mixture in a way that removes the exterior skin but does not stick to the spikes 212, then the applied mixture is dry and the area is completely scraped. This process effectively removes the excess cement mixture and creates a relatively smooth and even surface on the wall of a building since the rough trowel guides you to prevent uneven scraping of the wall.

Where the concrete-based mortar is sprayed upon the building, the mixture is left to set for a time sufficient so that it will not stick to the rough trowel when the surface is scraped. The rough trowel is used both to level and smooth the surface.

The following table sets forth the expected dry time for the listed mixtures of the concrete-based mortar, PROPAM REVOC, the accelerant, BETTACEL, and water, in conditions of shade, high-humidity, and approximately 70 80 degrees Fahrenheit:

PROPAM REVOC (Kilograms)	WATER (grams)	Accelerant (grams)	Dry Time (hours:minutes)
2.5	400	0	3:50
2.5	400	50	3:30
2.5	400	62.5	2:45
2.5	400	75	2:15
2.5	400	87.5	1:30
2.5	400	100	0:55

This other table sets forth the expected dry time for the listed mixtures of the concrete-based mortar, PROPAM REVOC, the accelerant, BETTACEL, and water, in conditions of sunlight, high-humidity, and approximately 70 80 degrees Fahrenheit:

PROPAM REVOC (Kilograms)	WATER (liters)	Accelerant (cm ³)	Dry Time (hours:minutes)
25	5	0	3:00
25	5	100	2:30
25	5	200	2:10
25	5	300	1:45
25	5	400	1:50
25	5	500	1:32

Generally, a reduction in dry time helps to improve the efficiency of the labor-intensive application process. In particular, the shortened dry time helps to minimize the down time of a mason between the application and scraping steps. Without the shortened dry time, a mason might have to wait as the applied material sets. As the mixture is applied, it dries relatively quickly and the mason can then scrape the applied material. The resulting surface provides an attractive, even finish.

The preferred mixture consists of 2.5 kg of the above cement-based mortar, 400 grams of water, and 75 grams of the above accelerant. This mixture sets in approximately 2 hours to 2 hours and 15 minutes. Although further reductions in the dry time are possible, they can begin to cause other application problems. For example, a further reduction in dry time can cause the applied material to set completely before the mason has an opportunity to scrape the surface. This can make the scraping process much more difficult, if not impossible, in obtaining an attractive, even surface. It can also begin to crack because the faster it dries the higher the temperature of the concrete mixture. This high temperature causes it to crack, thus rendering it useless.

Similar results can be obtained with other concrete-based mortars. For example, the concrete-based mortar REVAT RASPADO, the above accelerant, and water can also be mixed to obtain a similar dry time. Specifically, a mixture of 3 kg of this concrete-based mortar, 75 grams of the accelerant, and 600 grams of water provide the preferred characteristics.

Again, the reduced drying time of these concrete-based mortars make the application and scraping of the concrete-based mortar much faster. This reduces labor time and associated costs. Also, the resulting material is very easy to scrape. The mixture also makes it possible for the job of applying and scraping to be finished the same day it was started. This reduces any wasted materials as may occur with a longer dry time.

As set forth above, in an alternative preferred embodiment of the invention, the concrete-based mortar is sprayed on the surface of a building. The mixture for this concrete-based mortar will depend upon the desired properties of the finished surface. For a fine-finished surface, the preferred mixture is as follows:

Material Used	(kg/ton of mortar)	(g/ton of mortar)
White Cement PB-42.5	150	
Sand	663	
Dust or Filler	187	
Rheomix 924		150
Rheomix 740		1,300
Rheomix 725		500
Water	180	

Although the above table sets for the preferred composition, the specific amount may vary somewhat. For example, the White cement PB-42.5 may vary from 75 225 Kg/ton of mortar. The sand may vary from 331.5 994.5 Kg/ton of mortar and the dust or filler may vary from 93.5 280 Kg/ton of mortar.

For a medium-finished surface, the preferred mixture is as follows:

Material Used	(kg/ton of mortar)	(g/ton of mortar)
White Cement PB-42.5	150	
Sand	621	
Dust or Filler	229	
Rheomix 924		150
Rheomix 740		1,300
Rheomix 725		500
Water	180	

Although the above table sets for the preferred composition, the specific amount may vary somewhat. For example, the White cement PB-42.5 may vary from 75 225 Kg/ton of mortar. The sand may vary from 310 931 Kg/ton of mortar and the dust or filler may vary from 93.5 280 Kg/ton of mortar.

For a coarse-finished surface, the preferred mixture is as follows:

Material Used	(kg/ton of mortar)	(g/ton of mortar)
White Cement PB-42.5	150	
Sand	637	
Dust or Filler	170	
Rheomix 924	43	150
Rheomix 740		1,300
Rheomix 725		500
Water	180	

Although the above table sets for the preferred composition, the specific amount may vary somewhat. For example, the White cement PB-42.5 may vary from 75 225 Kg/ton of mortar. The sand may vary from 318 955 Kg/ton of mortar; the dust or filler may vary from 85 255 Kg/ton of mortar; and the aggregate may vary from 21 64.5 Kg/ton of mortar.

In the above tables, Reomix 924 is an aerating-plasticizing additive. Its main function is to aerate and its secondary function is water reduction and to increase adherence. Reomix 740 is a hydrofuge agent. It acts as a hydrofuge impermeable to rain and improves adherence by cellulose. Finally, Reomix 725 is

an aerating-plasticizing additive. It acts as a water retainer and improves adherence by cellulose. These compounds, namely Reomix 924, Reomix 740 and Reomix 725, are commercially available from BETTOR, MBT, whose contact information was supplied above. Alternatively, other hydrofuge additives and aerating-plasticizing additives may be used. These are commercially available from a variety of sources.

Various additives are used to obtain the desired properties for projecting, drying and scraping. These include water retainers, plastifiers, hydrofuges, accelerants, retardants and resins.

Water retainers include cellulose ethers, bentonites and sepiolites. The cellulose ethers are used in projection mortars mainly in the form of methylcellulose (MC), methylhydroethylcellulose (MHEC) and methylhydroxypropylcellulose (MHPC) or mixed cellulose ethers. Small amounts already delay the quick penetration of the water in the absorbent base facilitating a homogeneous forge and hardening. Premature drying is prevented on the plasters and mortars, thereby guaranteeing the prolonged working time necessary for a rational construction. The power of water retention in types MC, MHEC and MHPC is determined by the grade of viscosity, size of the grain, time of dissolution, and temperature. The dissolution time depends on the size and the metric distribution of the grain and of the chemical modification. Bentonites are used as load and they have retention power. Sepiolites are also used as retainers and at the same time as a thixotropic product for the mortar.

The plastifiers are based on lignosulphates, melamines, naphthalenes and carboxylates.

The Hydrofuges are based on materials that use as a base sodium oleates, cadmium stearates, zinc, siliconates or others.

The accelerants include calcic formiate.

The retardants include salts derived from citric acid.

The resins include vinyl acetate in rediffusable powders.

Turning to **FIGS. 5A, 5B and 5C**, the process of finishing a wall with spray-on one-coat mortar is further described. As shown in **FIG. 5A**, after spraying the one-coat mortar 500 on a wall 502 and smoothing with a flat trowel, the surface is still somewhat uneven. The rough trowel 504 is touched against the surface to determine whether it has hardened sufficient to prevent sticking. When this is the case, the rough trowel is scraped in a circular motion about the surface.

As shown in **FIG. 5B**, this flattens the surface. Here, the lower portion of the one-coat mortar 500 has been scraped and the surface is relatively flat. The upper portion of the one-coat mortar has not been scraped and it is still uneven. As shown in **FIG. 5C**, the entire surface of the one-coat mortar is scraped so that it is flat and even. This provides a finished appearance.

Turning to **FIGS. 6A, 6B and 6C**, this process is further described on a macroscopic level. **FIG. 6A** shows the one-coat mortar 500 after being sprayed and smoothed on a wall but before being scraped. It includes sand particles of the size and in the percentages used to make the one-coat mortar. Preferably, the one-coat mortar includes a fraction of relatively large particles, approximately 1 mm in diameter. These are shown as the largest dots in **FIG. 6A**.

FIG. 6B shows the plane 600 along which the surface is leveled. The rough trowel 504 scrapes the surface so that it becomes even along this plane 600. A number of the large particles will lie in this plane 600.

FIG. 6C shows the finished surface, which is flat and even. The large particles along the plane 600

have been removed. This leaves small traces, or divots, where the large particles had been. These divots give the surface a pleasant appearance.

Preferred mixtures of sand are used to create these surfaces. For a fine-finished surface, the composition of one preferred mixture is specified by the following table:

TABLE

Diameter (mm)	<u>Fine #1</u>	Weight percent
1.0		5.4
0.5		21.1
0.25		16.0
0.125		15.1
0.063		14.2
<0.063		28.2

The tolerance with respect to the diameter of particle extends up to the next larger sized particle. Thus, particles as large as 0.99 mm in diameter are considered to be approximately 0.5 mm. Likewise, particles as small as large as 0.49 mm in diameter are considered to be approximately 0.25 mm. The size of the largest particle, 1.0 mm, extends up to approximately 1.5 mm. For each of the diameter sizes, the weight percentages preferably are within $\pm 1\%$ of the total weight or $\pm 10\%$ of the stated value, whichever is greater. These tolerances also apply to each of the following tables.

For a medium-finished surface, the composition of two preferred mixtures are specified by the

following tables:

TABLE

<u>Medium #1</u>	
Diameter (mm)	Weight percent
1.0	15.1
0.5	11.7
0.25	10.8
0.125	25.2
0.063	13.6
<0.063	23.6

TABLE

<u>Medium #2</u>	
Diameter (mm)	Weight percent
1.0	15.1
0.5	11.7
0.25	10.8
0.125	25.2
0.063	13.6
<0.063	23.6

For a coarse-finished surface, the composition of one preferred mixture is specified by the following table:

TABLE

<u>Coarse #1</u>		
Diameter		Weight
(mm)		percent
2.0		0.1
1.6		5.7
1.0		17.5
0.5		17.3
0.25		9.8
0.125		8.7
0.063		3.4
<0.063		36

Finally, for an extra-coarse-finished surface, the composition of two preferred mixtures are specified by the following tables:

TABLE

<u>Extra Coarse #1</u>		
Diameter		Weight
(mm)		percent
4.0		0.2
2.0		13.2
1.6		4.4
1.0		12.2
0.5		13.6
0.25		9.8
0.125		8.7
0.063		3.4
<0.063		34.5

TABLE

Diameter (mm)	<u>Extra Coarse #2</u>	Weight percent
4.0		0.1
2.0		10.1
1.6		4.6
1.0		5.7
0.5		23.2
0.25		9.8
0.125		8.7
0.063		3.4
<0.063		34.5

The above mixtures of sand can be summarized by the following table, which sets forth the preferred ranges for all diameters and textures (i.e., fine, medium, coarse, etc.):

TABLE

Diameter (mm)	<u>All Textures</u>	Weight percent
------------------	---------------------	-------------------

4.0	0-5
2.0	0-15
1.0	5-20
0.5	10-35
0.25	10-20
0.125	5-30
0.063	2-15
<0.063	20-40

The above mixtures produce optimal results when using the methods shown and described with reference to **FIGS. 5A, 5B, 5C, 6A, 6B and 6C**. The compositions provide a smooth and even surface and, at the same time, produce a pleasant appearance by the selective removal of the larger particles.

The remaining divots provide a unique surface character.

As previously explained, a composition can be sprayed on a surface (interior or exterior) of a structure. In a preferred embodiment of the invention, this can be efficiently achieved by means of a composition with particular properties that allows not only easily pumping the composition through a hose and spraying it on a surface but also allows adhesion to said surface substantially immediately after being sprayed.

The composition is prepared by selectively mixing cement, sand and the following additives: water retainers, aerating agents, thickening agents and plastifiers. Water retainers are used in the composition to control setting times and to maintain the composition wet over an extended period of time. This property is essential in the construction industry which generally requires extended working schedules. It is important to point out that the degree of retaining capacity given to the composition by the additive is determined by several factors including but not limited to: the amount and strength of the water retainer, the size of sand particles and the temperature at the time of mixing. Water retainers also add a lubricating characteristic and a slimy appearance to the composition. Aerating agents produce air incorporation into the composition by means of relatively small bubbles of air that facilitates rotation

and interaction among all the particles within the composition. A bubbling appearance is given to the composition by the addition of aerating agents. Thickening agents are generally used to achieve a better cohesion of components within the composition in order to provide better surface adherence and to substantially eliminate detachment of the composition from the surface. Plastifiers are used to reduce the amount of water needed to knead the composition while maintaining fluency and the appropriate consistency without affecting the composition frictional resistance. Furthermore, there are instances where less or more water will be needed to achieve a desired application and the additives will play an important role by selectively interacting with cement at a chemical level.

All the additives within the composition become chemically active when mixed with water to provide the composition with the necessary properties to allow pumping, application and adhesion of said composition. The interaction among all the additives allows the composition to be properly pumped. The above-mentioned additives do not react with other additives so that additional properties can be obtained by adding new additives. Thus, any coating mortar can be pumped by mixing the coating mortar with these additives and the appropriate mixtures of sand. Furthermore, the coating mortar will change its appearance while in a wet state and the addition of water will cause that the composition becomes viscous and less dense. The composition will have a bubbling, slimy look like whip cream.

FIGS. 15 and 16 will be used to explained the invention. **FIG. 15** shows several combinations of components and/or additives according to the invention, wherein all the amounts are expressed in percentage by weight of the composition. The table illustrates eight different combinations of components and/or additives along with particular amounts for each combination. However, it is important to point out that these combinations are selected to achieve specific results and that other combinations are encompassed by this invention to achieve different results. The rows define the different combinations of components and/or additives according to the invention. The columns define different proportions of sand in relation to the composition. The last column of the table (Mix) defines

for each combination the percentage by weight of each component and/or additive needed to provide a ready to use unit. For the purpose of this disclosure, a ready to use unit is defined as any containing means such as but not limited to bags that encloses all the components and/or additives so that only water needs to be added and mixed with the composition. The rest of the columns define the situation where additional portions of sand are combined with a combination mix having adjusted amounts of components and/or additives in order to obtain a plurality of ready to use units for each combination .

Explanation of **FIG. 16** will provide a better understanding of the above-mentioned concept. **FIG. 16** is an illustrative example of the combination V as detailed in the table shown in **FIG. 15**. In this example, a ready to use unit (Mix) would have cement in about 13.69% by weight of the composition; sand in about 86.20% by weight of the composition; retainer in about 0.10% by weight of the composition; and thickener in about 0.01% by weight of the composition. According to the invention, in order to obtain two ready to use units (Mix), a unit containing 100% of sand is mixed with a composition unit having the following adjusted amounts: cement in about 25.66% by weight of the composition; sand in about 74.14% by weight of the composition; retainer in about 0.19% by weight of the composition; and thickener in about 0.02% by weight of the composition. The sand unit and the adjusted composition unit are selectively combined by mixing means to obtain a homogeneous mixture. Then, the resulting homogeneous mixture is equally divided into two separate units having each substantially the same proportional amounts and percentages by weight of a single ready to use unit. This technique reduces the preparation and retail costs when compared to simply preparing two ready to use units individually.

FIG. 15 shows in the eight column (1+6-8) the situation where six units containing 100% sand is combined with an adjusted combination unit comprising: cement in about 99.19% by weight of the composition; retainer in about 0.7% by weight of the composition; thickener in about 0.105% by weight of the composition; and no sand at all to obtain seven ready to use units. The lack of sand in the adjusted combination unit responds mainly to the fact that at this proportional level, there would not be enough proportional presence of cement compared to the proportional presence of sand, thus, reducing

the chemical reactions between cement and the additives in the composition. In other words, the percentage by weight of cement in the composition can increase by reducing the amount of sand achieving greater resistance by maximizing the chemical reactions between cement and the additives. It is important to point out that experimental results demonstrated that further combining seven sand units (1+7) and eight sand units (1+8) with the same adjusted combination unit of (1+6) would still provide a composition having an average compressive strength above the minimum standard requirements of from about 545 psi to 761 psi. Moreover, the percentage by weight of at least one of the components present in the composition might need to be adjusted based on the type of use and/or the task at hand. For example, the percentage by weight of cement could be varied to achieve specific pressure and/or resistance.

For several reasons, the absorption capacity of sand varies and as a consequence the water retention capacity varies as well. In the case where less water is absorbed, less water retainer is needed in the composition and viceversa. Thus, all the values detailed in **FIG. 15** have a tolerance of about $\pm 30\%$.

Optimal pumping of said composition through a hose is achieved by selectively combining and mixing said additives. Water retainers are used to retain water particles within the coating mortar in order to delay hardening of said mortar. As a consequence, said composition can be pumped through the hose to longer distances without premature hardening inside said hose and avoids warming due to chemical reactions associated with cement. Typical distances achieved by the composition according to the invention are about 300 horizontal feet and from about 75 to about 200 vertical feet. In addition, water retainers provide lubrication between the mortar and the interior of the hose during the pumping process and allow ease of rotation among particles. Moreover, plastifiers give the coating mortar more fluidity and a reduced tendency to segregate while allowing rotation among particles with a reduced amount of water for an optimal moisture property. In other words, an increased wetness is achieved with a reduced amount of water. The use of plastifiers according to the invention allows maintaining

the physical consistency of the composition while traveling inside the hose for the entire pumping process without the need of an excess of added water to increase fluidity. It also reduces frictional interaction not only between the composition and the hose but also between sand and cement particles. Typically, the addition of excessive water to increase mobility of the composition would result in a decreased composition consistency and/or resistency. Thus, at least one additive is used to avoid reducing the composition's resistance due to the use of excessive water. According to the invention, aerating agents are used to add air into the composition by means of relatively small bubbles of air with a diameter typically between 0.01 mm and 1 mm with a substantially uniform distribution throughout the composition. This allows optimal rotation.

FIG. 7 shows a hose and spray nozzle for pumping the mortar material to a desired location. Optimal mortar flow along the hose is obtained due to interaction between the different particles that compose the mortar.

FIG.8 shows the mortar exiting the spray nozzle of the hose. The trained worker applies the material on a continuous sideways horizontal movement until a portion of a wall surface is covered with the mortar mixture.

FIG. 9 shows the mortar mixture attached to the wall surface at different stages of application. The wall surface is divided in several smaller areas and the mortar is applied on a continuous horizontal movement as previously discussed. A trained worker removes the surface skin of an already set mortar mixture. After application of the mortar to the wall surface and after the material had set according to the desired finish; a trained worker evens the mortar material by working the surface skin with a trowel. The desired finished surface is revealed after the surface skin is removed on its entirety.

FIGS.10a-10b show a transversal view of mortar applied on a wall surface. The spray nozzle is held preferably at a distance **d1** of about 0'-6" from the chosen wall surface. The mortar mixture is applied

to form a parallel material accumulation with a vertical width **d2** of preferably about 0'-4" in relation to the wall, as shown in **FIG. 10a**. When the mortar leaving the hose is applied to the wall surface, the preferred perpendicular accumulation thickness **d3** is about 0'-6" in relation to the wall, as shown in **FIG. 10b**. It is important to point out that the material accumulation width and/or thickness is directly dependent on the amount of time the hose remains static at a particular location while the material is being pumped.

FIG. 11 shows a transversal view of mortar applied on a ceiling surface. The mortar mixture is applied to form a parallel material accumulation with a horizontal width **d5** of preferably about 0'-4" in relation to the wall. When the mortar leaving the hose is applied to the ceiling surface, the preferred perpendicular accumulation thickness **d4** is about 0'-4" in relation to the wall. It is important to point out that the material accumulation width and/or thickness is directly dependent on the amount of time the hose remains static at a particular location while the material is being pumped. Moreover, the present invention provides a composition with optimal gravity resistance in order to allow the mortar to settle on the ceiling without any detachments maintaining the integrity of the mortar during and after application.

FIGS. 12a-12b show a panoramic view of the mortar application to a ceiling. The trained worker applies the mortar to the ceiling surface by directing the spray nozzle upwards. The mortar vertical accumulation thickness is preferably about 1/4". However, it is also envisioned that said vertical accumulation thickness can reach about 3"-4" depending on the application. The mortar of the present invention can be applied to a plurality of ceiling structures such as but not limited to: multiple structural panels made of cement, poured concrete, high-rib laths, or the like. In addition, the mortar of the present invention can be directly applied to an integral concrete ceiling as shown in **FIG. 12b**.

FIG. 13 shows a panoramic view of a high-rise building to where the mortar is pumped. The hose for delivering the mortar product is connected to a pump that is located a lower height compared to the mortar final destination. The mortar mixture may be pumped to a vertical distance or height of about 112 vertical feet.

FIG. 14 shows a table describing several cement types. One important aspect of the invention relies in the fact that the inventive composition can be used with any type of cement. However, it is important to point out that the components, additives and/or amounts used in the composition might be at least in part dictated by the type of cement used. In other words, the quality of the cement used must be taken into consideration when selecting the type of additives along with their corresponding amounts.

Although the invention has been described with reference to preferred embodiments, those skilled in the art will appreciate that many modifications are possible without departing from the scope of the invention. More specifically, although the invention has been described with reference to specific concrete-based mortars, accelerants and application steps, other compounds and steps may also be used. For example, the concrete-based mortar may be mixed with a solid accelerant in powder form in a composition that achieves the above-described benefits. Likewise, the mentioned compounds and mixtures are available from a wide variety of sources and the claims are not in any way limited to the specific commercial mixtures mentioned and described above. Many other modifications are also possible. The following claims are intended to cover all such modifications and variations of the invention.

In the Claims

1. A composition comprising: cement and at least one additive.
2. The composition of claim 1, wherein said at least one additive comprises: water retainer, air, plastifier and a thickener agent.
3. The composition of claim 1, wherein said at least one additive comprises: water retainer, air, and a thickener agent.
4. The composition of claim 1, wherein said at least one additive comprises: air, plastifier and a thickener agent.
5. The composition of claim 1, wherein said at least one additive comprises: water retainer, air, and plastifier.
6. The composition of claim 1, wherein said at least one additive comprises: water retainer, and a thickener agent.
7. The composition of claim 1, wherein said at least one additive comprises: water retainer, and air.
8. The composition of claim 1, wherein said at least one additive comprises: water retainer, and plastifier.
9. The composition of claim 1, wherein said at least one additive comprises: air, and a thickener agent.
10. The composition of claim 2, comprising:
water retainer from about 0.101% to about 0.700% by weight of said composition;

air from about 0.010% to about 0.070% by weight of said composition;
plastifier from about 0.010% to about 0.070% by weight of said composition; and
thickener agent from about 0.015% to about 0.105% by weight of said composition.

11. The composition of claim 3, comprising:
water retainer agent from about 0.101% to about 0.700% by weight of said composition;
air from about 0.101% to about 0.700% by weight of said composition; and
thickener agent from about 0.015% to about 0.105% by weight of said composition.

12. The composition of claim 4, comprising:
air from about 0.010% to about 0.070% by weight of said composition;
plastifier from about 0.010% to about 0.070% by weight of said composition; and
thickener agent from about 0.015% to about 0.105% by weight of said composition.

13. The composition of claim 5, comprising:
water retainer from about 0.101% to about 0.701% by weight of said composition;

air from about 0.010% to about 0.070% by weight of said composition; and
plastifier from about 0.010% to about 0.070% by weight of said composition.

14. The composition of claim 6, comprising:

water retainer from about 0.101% to about 0.700% by weight of said composition; and
thickener from about 0.015% to about 0.105% by weight of said composition.

15. The composition of claim 7, comprising:

water retainer from about 0.101% to about 0.701% by weight of said composition; and
air from about 0.010% to about 0.070% by weight of said composition.

16. The composition of claim 8, comprising:

water retainer from about 0.101% to about 0.701% by weight of said composition; and
plastifier from about 0.010% to about 0.070% by weight of said composition.

17. The composition of claim 9, comprising:

air from about 0.010% to about 0.070% by weight of said composition; and

thickener agent from about 0.015% to about 0.105% by weight of said composition.

18. The composition of claim 1, comprising sand with the following composition:

Diameter (mm)	Weight %
4.0	0-5
2.0	0-15
1.0	5-20
0.5	10-35
0.25	10-20
0.125	5-30
0.063	2-15
<0.063	20-40

19. The composition of claim 1 comprising:
said cement from about 13.691% to about 99.894% by weight of said composition; and
sand from about 86.206% to about 0.0% by weight of said composition.
20. The composition of claim 1, wherein each of said cement, said at least one additive, and sand have a tolerance of from about $\pm 40\%$ to about $\pm 60\%$ by weight of said composition.

FIG. 1

(PRIOR ART)



FIG. 2

(PRIOR ART)

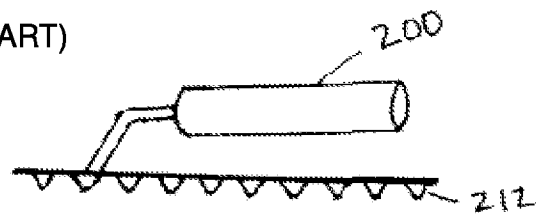


FIG. 3

(PRIOR ART)

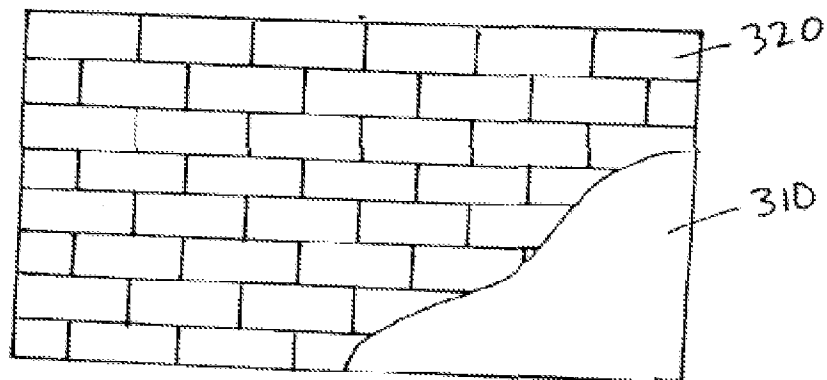


FIG. 4

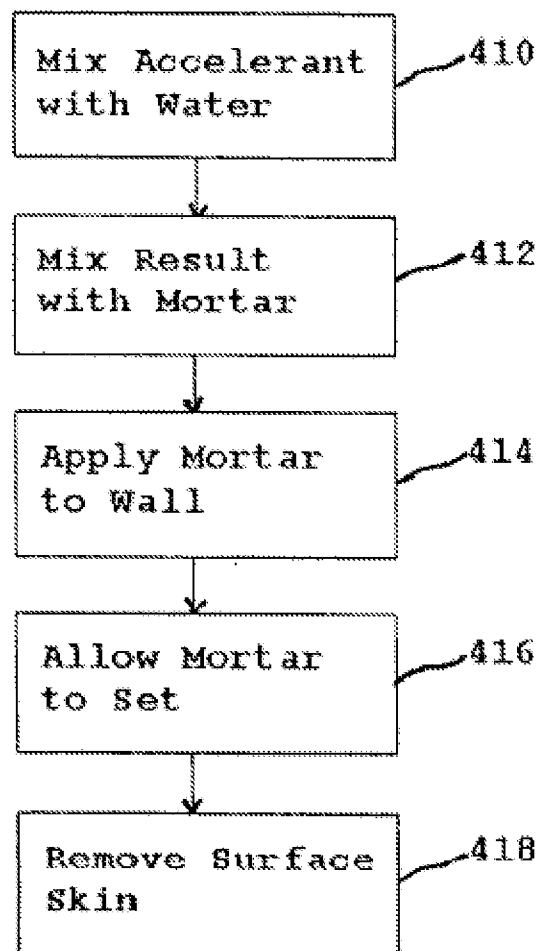


FIG. 5B

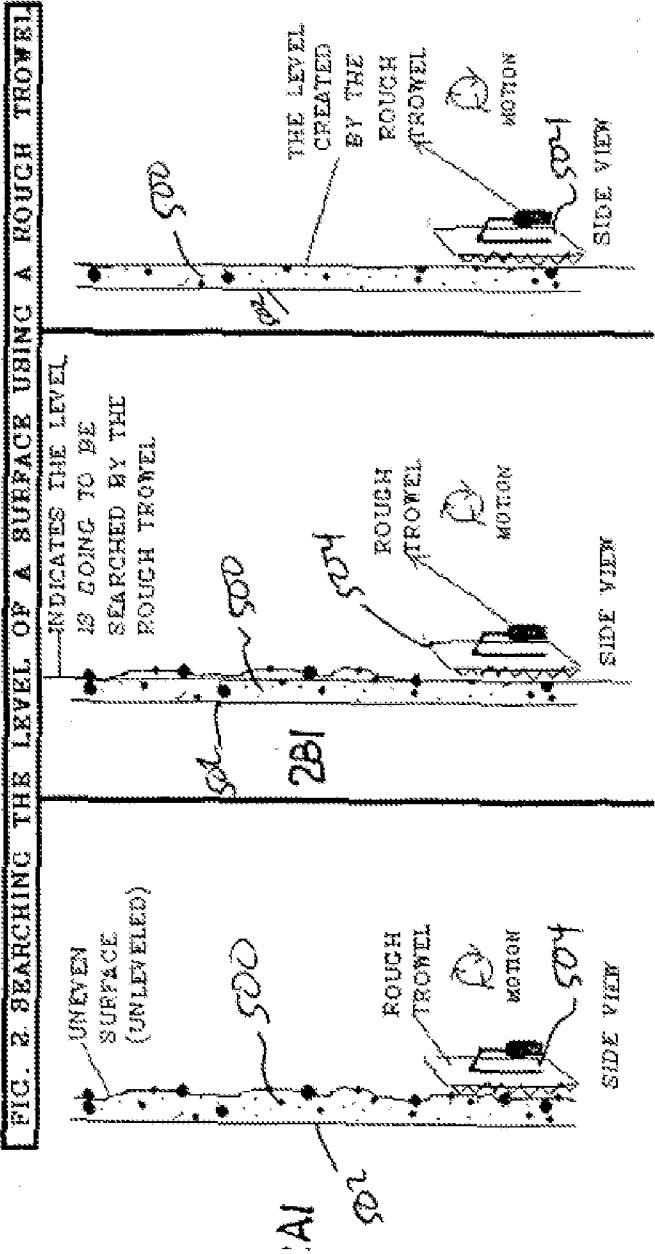


FIG. 5A

FIG. 5C

FIG. 6B

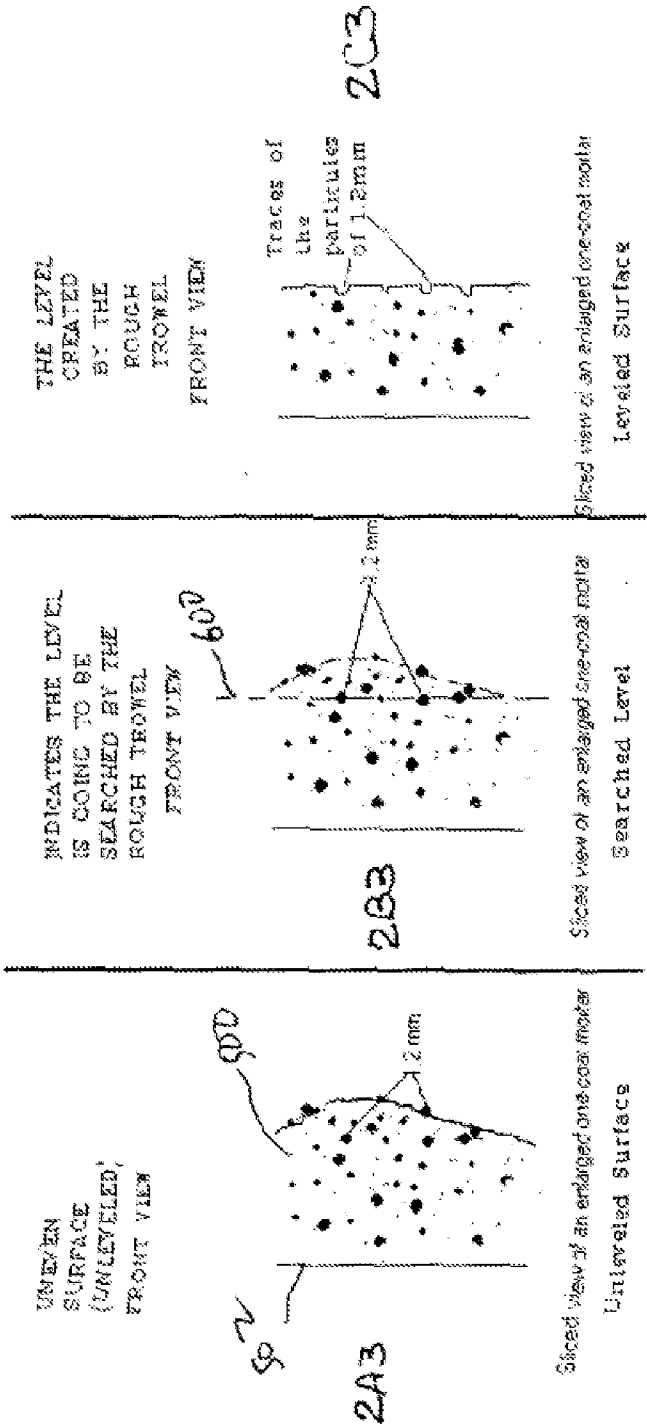


FIG. 6A

FIG. 6C

FIG. 7

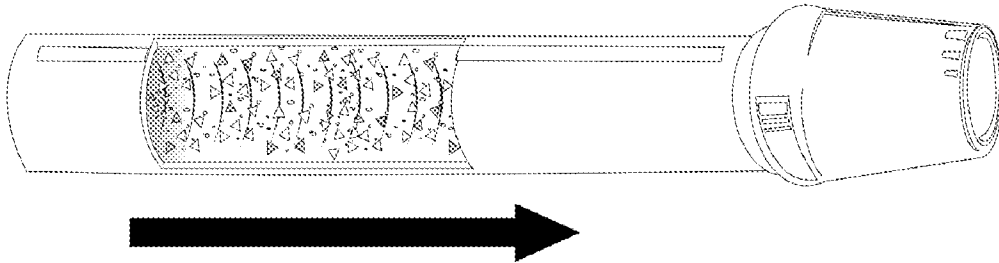


FIG. 8

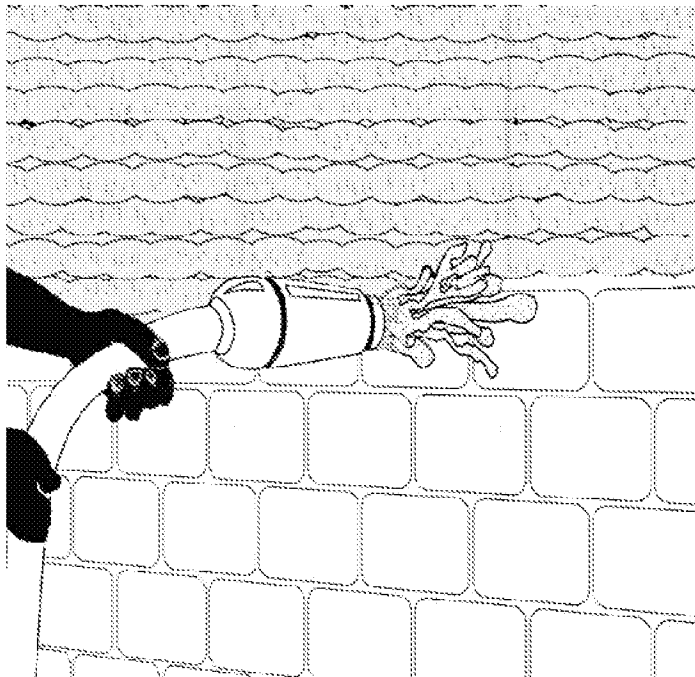


FIG. 9

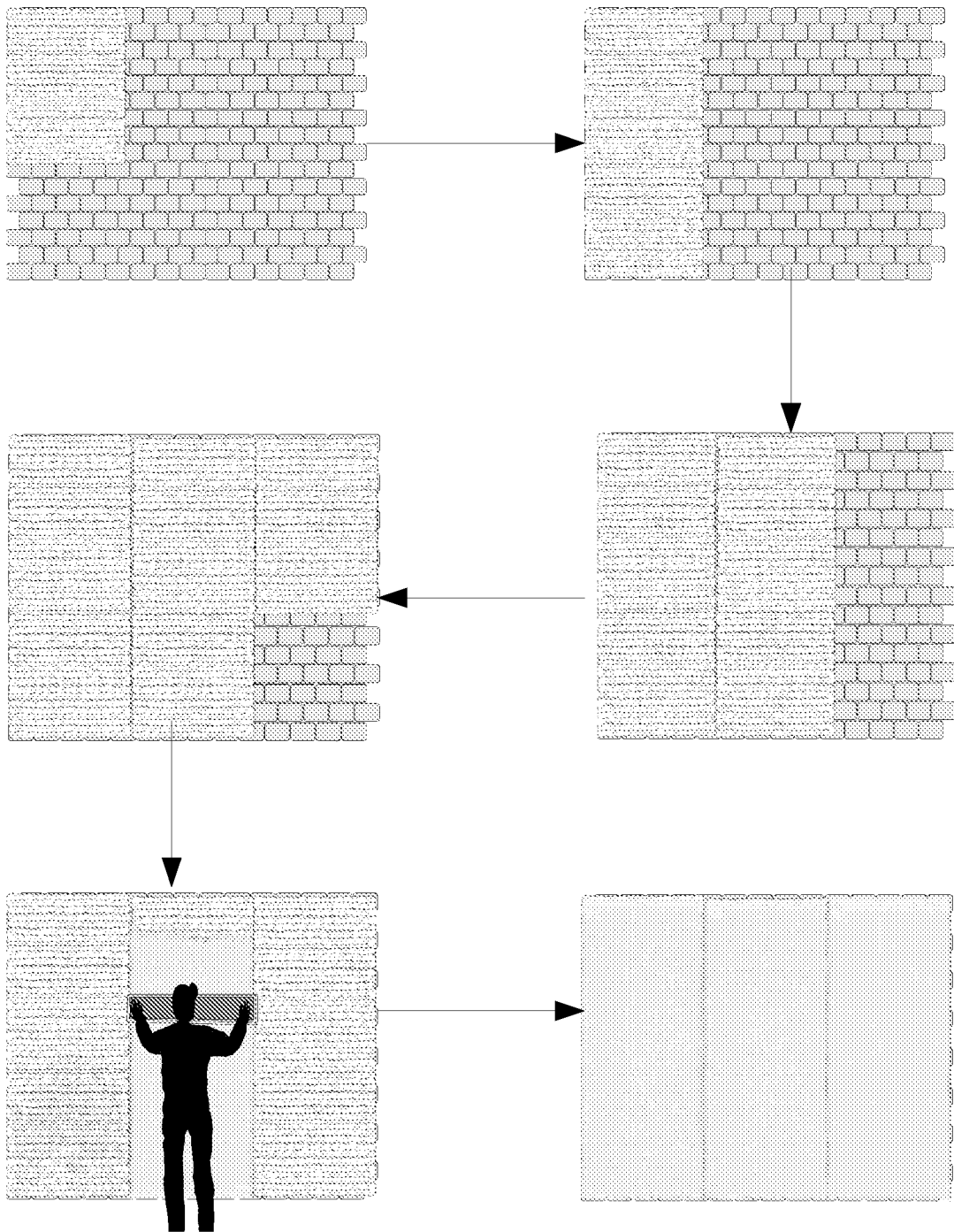


FIG. 10a

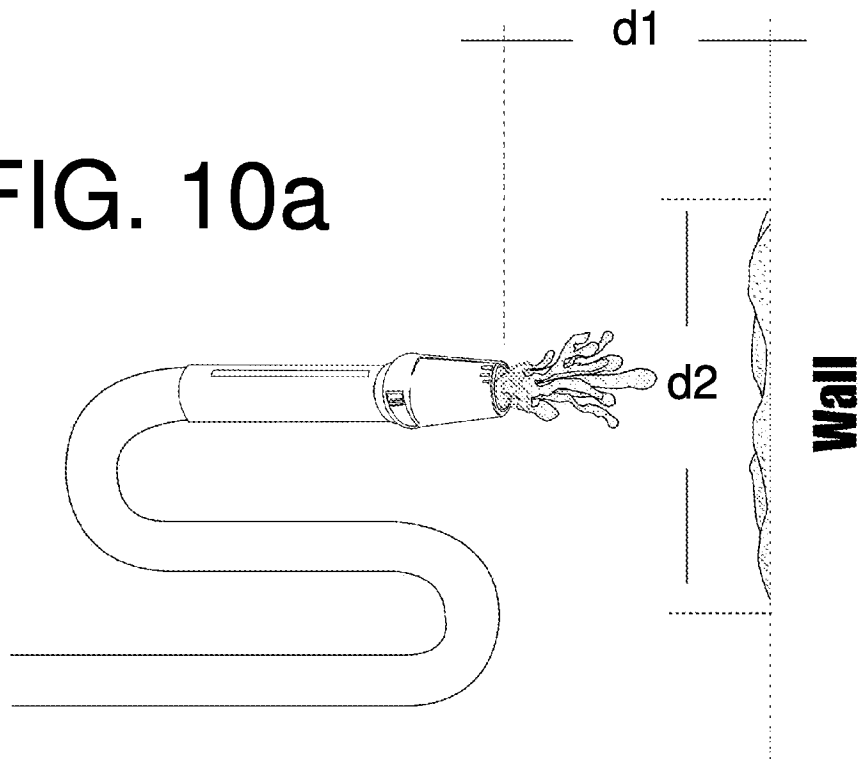


FIG. 10b

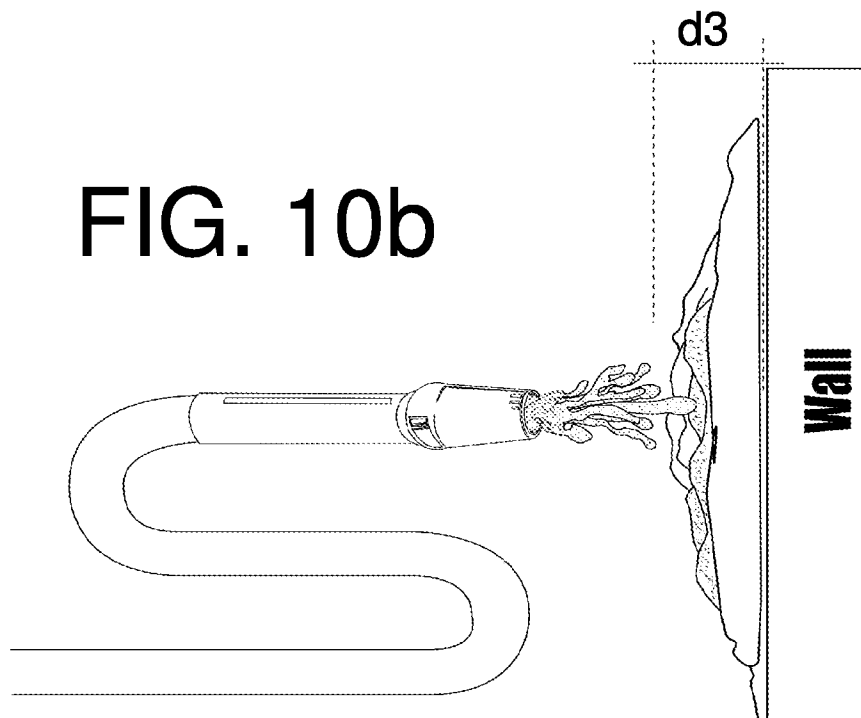


FIG. 11

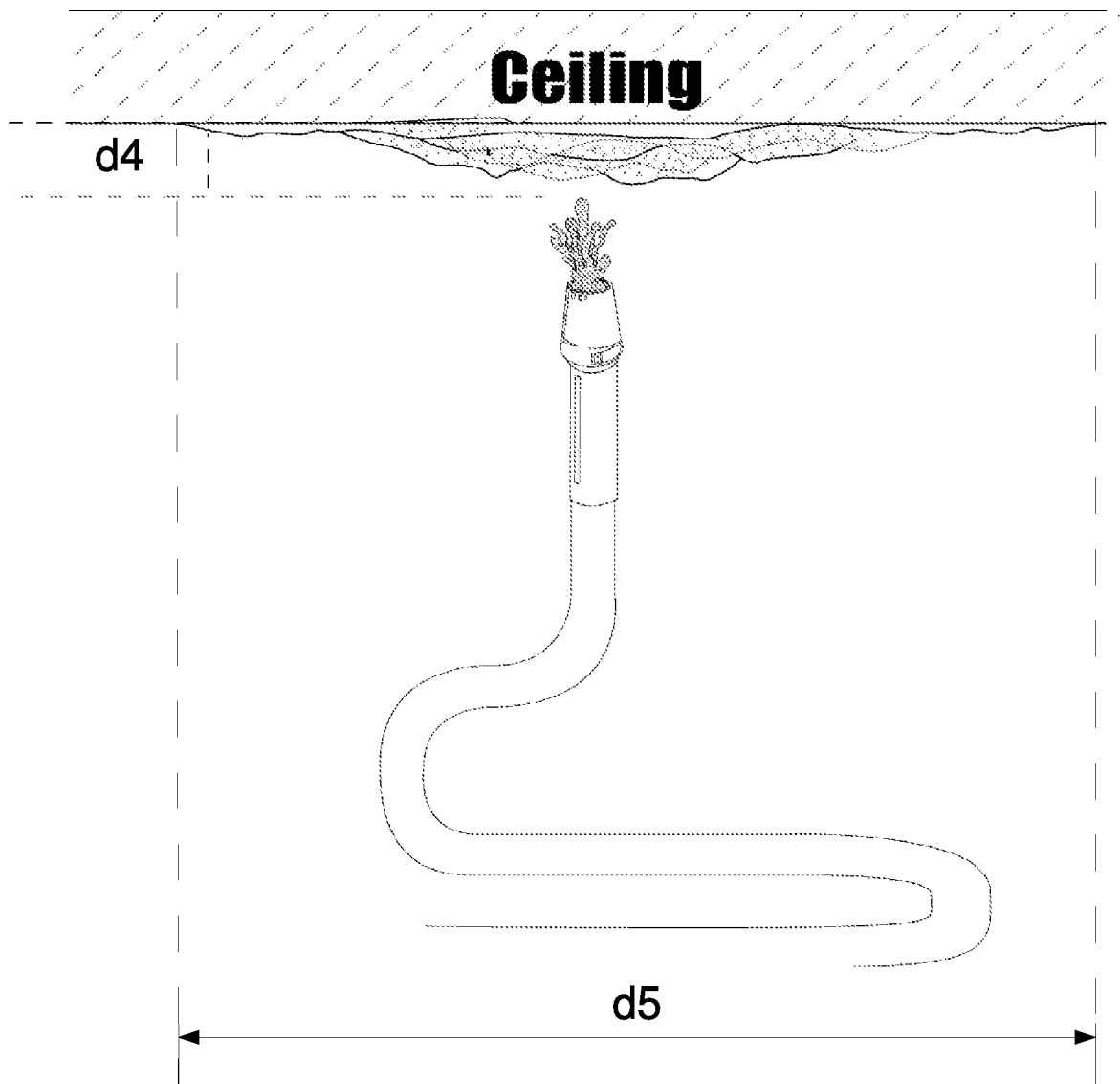


FIG. 12a

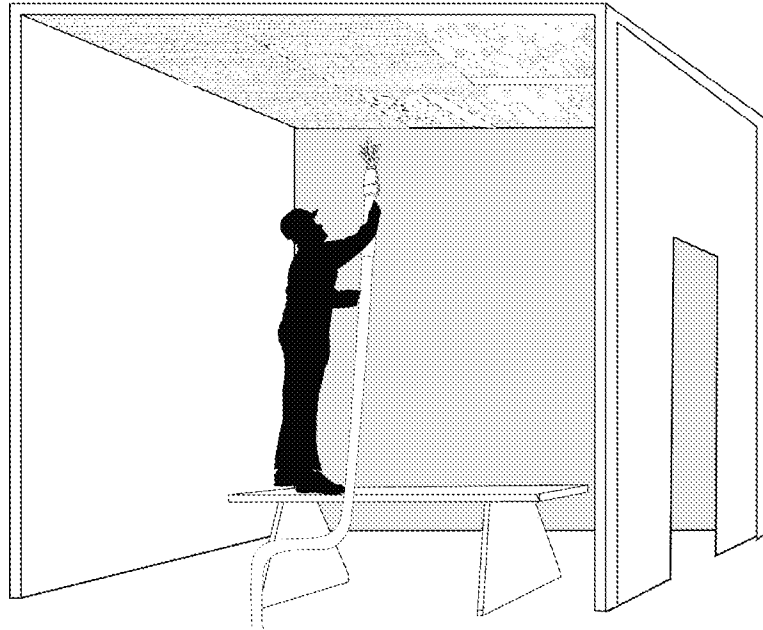


FIG. 12b

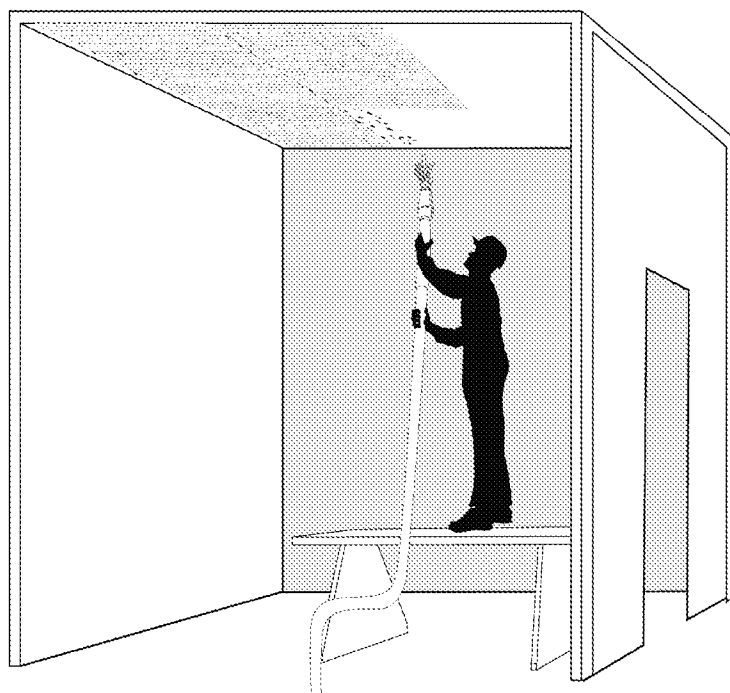


FIG. 13

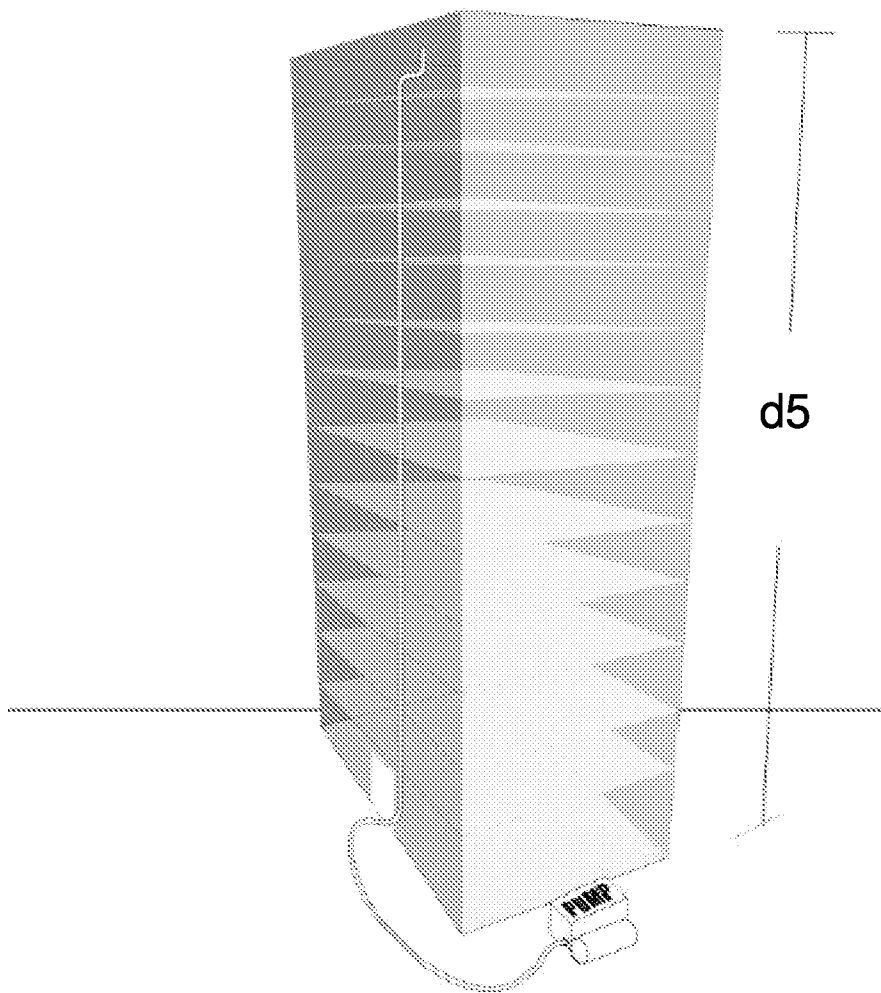


FIG. 14

Type	Name	Designation	Clinker	Blast furnace Slag	MicroSilice	Natural Pozzolans	Fly Ashes	Limestone	Minor Components
CEM I	Portland Cement	CEM I	95-100	---	---	---	---	---	0-5
CEM II	Portland Cement - Slag	CEM II / A-S	80-94	5-20	---	---	---	---	0-5
	Portland Cement	CEM II / B-S	65-79	21-35	---	---	---	---	0-5
	MicroSilice	CEM II / A-D	90-94	6-10	---	---	---	---	0-5
	Portland Cement - Pozzolans	CEM II / A-P	80-94	---	---	6-20	---	---	0-5
		CEM II / B-P	65-79	---	---	21-35	---	---	0-5
	Portland Cement - Fly Ashes	CEM II / A-V	80-94	---	---	---	6-20	---	0-5
		CEM II / B-V	65-79	---	---	---	21-35	---	0-5
	Portland Cement - Limestone	CEM II / A-L	80-94	---	---	---	---	6-20	0-5
CEM III	Portland Cement - Blast Furnace	CEM III / A-M	80-94	←	←	←	←	←	←
		CEM III / B-M	65-79	←	←	←	←	←	←
	Cement - Blast Furnace	CEM III / A	95-99	36-65	---	---	---	---	0-5
	Cement - Pozzolans	CEM III / B	20-34	66-80	---	---	---	---	0-5
CEM IV		CEM IV / A	65-89	---	←	←	←	←	←
		CEM IV / B	45-64	---	←	←	←	←	←
CEM V	Cement - Compound	CEM V / A	40-64	18-30	←	←	←	←	0-5

FIG. 15

	Components	1+1 (%)	1+2 (%)	1+3 (%)	1+4 (%)	1+5 (%)	1+6-8 (%)	Mix (%)
I	CEMENT	26.946089%	40.581101%	54.053978%	67.635152%	81.162154%	99.194096%	13.691679%
	SAND	72.854241%	59.118148%	45.545482%	31.863672%	18.236435%	0.000000%	86.206866%
	RETAINER	0.199601%	0.300601%	0.400400%	0.501001%	0.601201%	0.700665%	0.101420%
	AIR	0.019960%	0.030060%	0.040040%	0.050100%	0.060120%	0.070066%	0.010142%
	PLASTIFIER	0.019960%	0.030060%	0.040040%	0.050100%	0.060120%	0.070066%	0.010142%
	THICKENER	0.029940%	0.045090%	0.060060%	0.075150%	0.090180%	0.105100%	0.015213%
II	CEMENT	26.999981%	43.144744%	54.054000%	67.635186%	81.162203%	99.194165%	13.691680%
	SAND	72.999949%	56.567553%	45.545500%	31.863688%	18.236446%	0.000000%	86.206875%
	RETAINER	0.200000%	0.287632%	0.400400%	0.501001%	0.601202%	0.700665%	0.101420%
	AIR	0.020000%	0.028763%	0.040040%	0.050100%	0.060120%	0.070067%	0.010142%
	THICKENER	0.030000%	0.043145%	0.060060%	0.075150%	0.090180%	0.105100%	0.015213%
III	CEMENT	26.999981%	43.269187%	54.271280%	67.975711%	81.653053%	99.894018%	13.705579%
	SAND	72.999949%	56.730712%	45.728579%	32.024113%	18.346735%	0.000000%	86.294386%
	PLASTIFIER	0.020000%	0.028846%	0.040201%	0.050352%	0.060484%	0.070561%	0.010152%
	AIR	0.020000%	0.028846%	0.040201%	0.050352%	0.060484%	0.070561%	0.010152%
	THICKENER	0.030000%	0.043269%	0.060301%	0.075529%	0.090726%	0.105841%	0.015228%
IV	CEMENT	26.946097%	43.144750%	54.054011%	67.635203%	81.162227%	99.298458%	13.691681%
	SAND	72.854262%	56.567561%	45.545509%	31.863696%	18.236451%	0.000000%	86.206879%
	RETAINER	0.199601%	0.287632%	0.400400%	0.501002%	0.601202%	0.701402%	0.101420%
	AIR	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
	PLASTIFIER	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
V	CEMENT	25.665392%	43.144756%	54.054022%	67.635220%	81.162251%	99.194235%	13.691681%
	SAND	74.144466%	56.567569%	45.545518%	31.863704%	18.236457%	0.000000%	86.206883%
	RETAINER	0.190114%	0.287632%	0.400400%	0.501002%	0.601202%	0.700666%	0.101420%
	THICKENER	0.028517%	0.043145%	0.060060%	0.075150%	0.090180%	0.105100%	0.015213%
VI	CEMENT	26.946102%	43.144762%	54.054032%	67.635237%	81.162276%	99.298528%	13.691682%
	SAND	72.854277%	56.567577%	45.545527%	31.863711%	18.236462%	0.000000%	86.206888%
	RETAINER	0.199601%	0.287632%	0.400400%	0.501002%	0.601202%	0.701402%	0.101420%
	AIR	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
VII	CEMENT	26.946102%	43.144762%	54.054032%	67.635237%	81.162276%	99.298528%	13.691682%
	SAND	72.854277%	56.567577%	45.545527%	31.863711%	18.236462%	0.000000%	86.206888%
	RETAINER	0.199601%	0.287632%	0.400400%	0.501002%	0.601202%	0.701402%	0.101420%
	PLASTIFIER	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
VIII	CEMENT	26.999987%	43.269200%	54.271302%	67.975745%	81.653102%	99.894088%	13.705580%
	SAND	72.999964%	56.730728%	45.728597%	32.024129%	18.346746%	0.000000%	86.294394%
	AIR	0.020000%	0.028846%	0.040201%	0.050352%	0.060484%	0.070561%	0.010152%
	THICKENER	0.030000%	0.043269%	0.060301%	0.075529%	0.090726%	0.105841%	0.015228%

FIG. 16

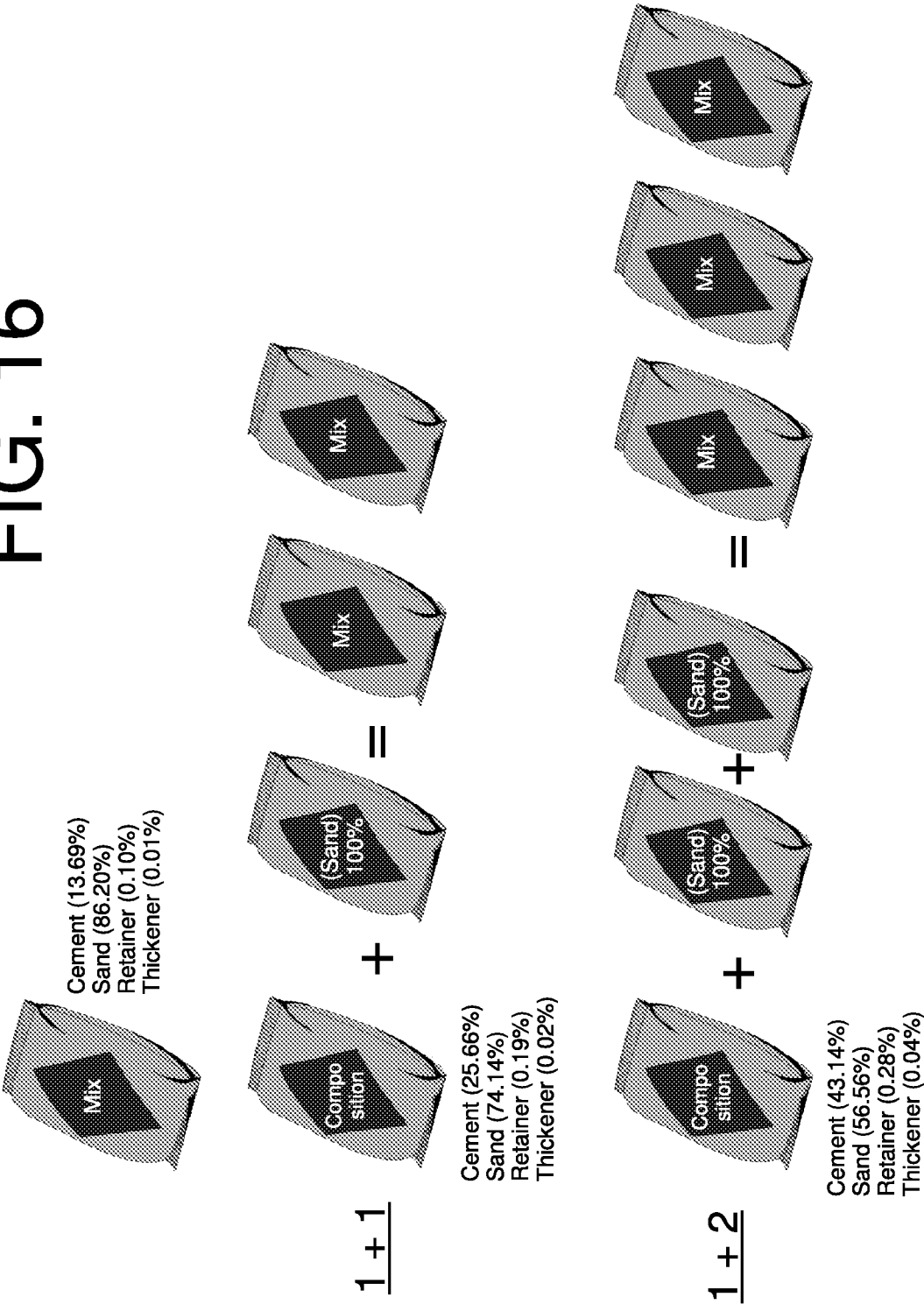


FIG. 1

(PRIOR ART)

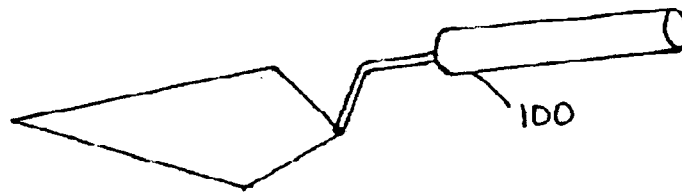


FIG. 2

(PRIOR ART)

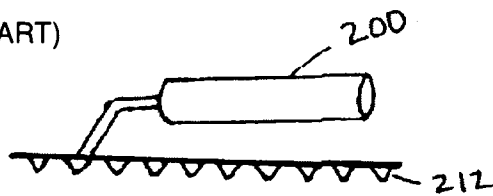


FIG. 3

(PRIOR ART)

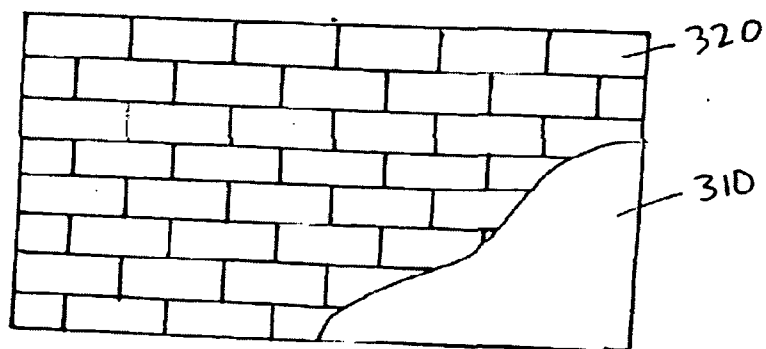


FIG. 4

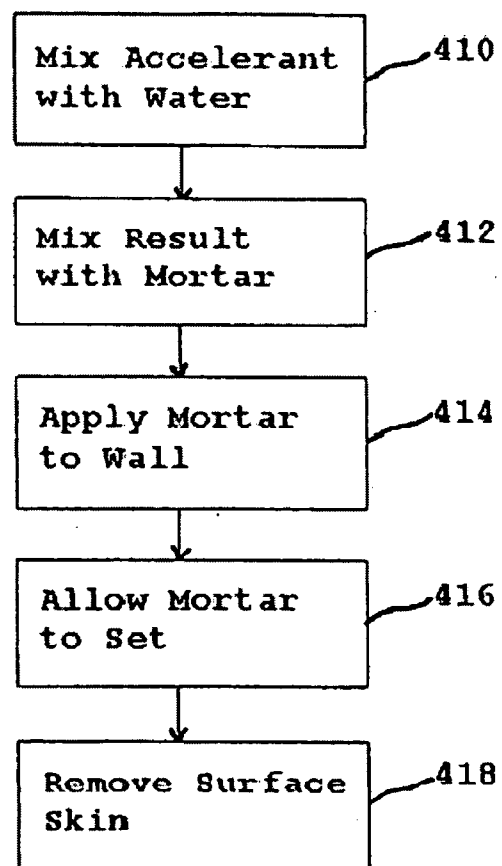


FIG. 5B

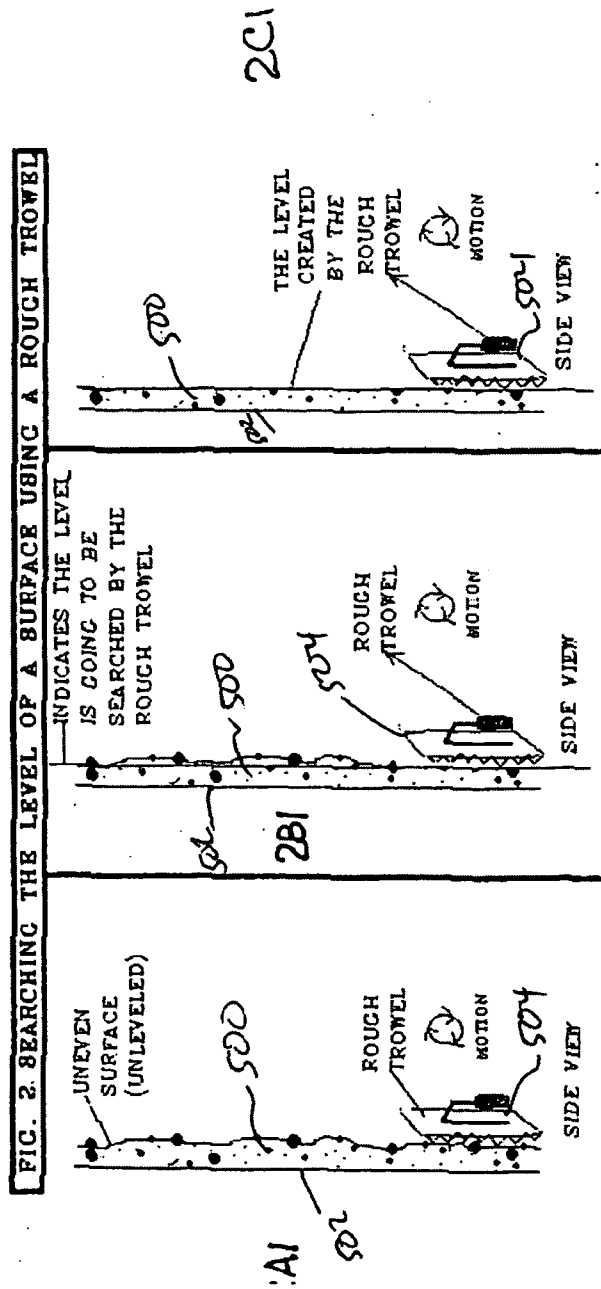


FIG. 5C

FIG. 5A

FIG. 6B

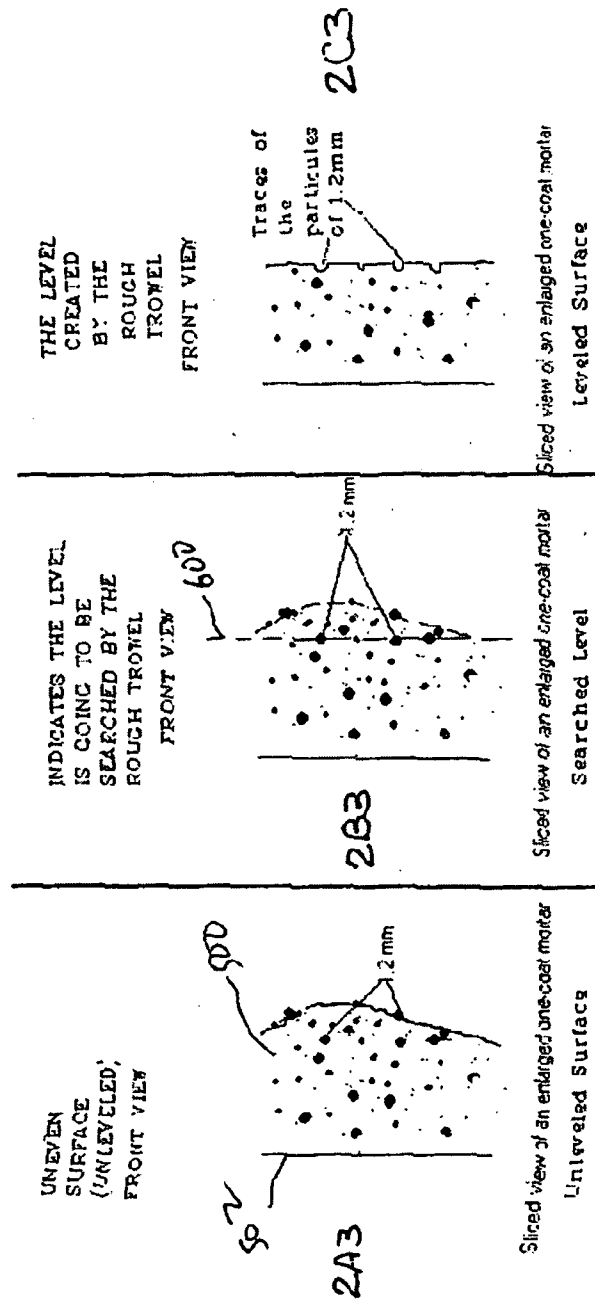


FIG. 6A

FIG. 6C

FIG. 7

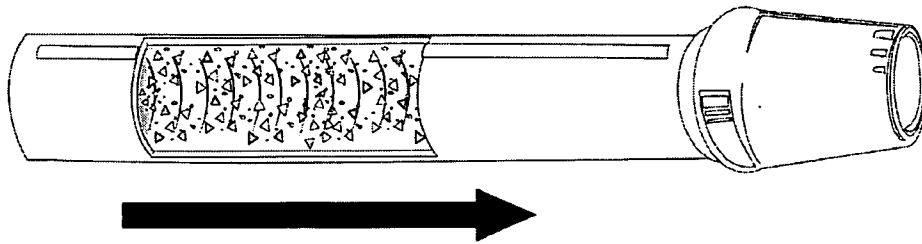


FIG. 8

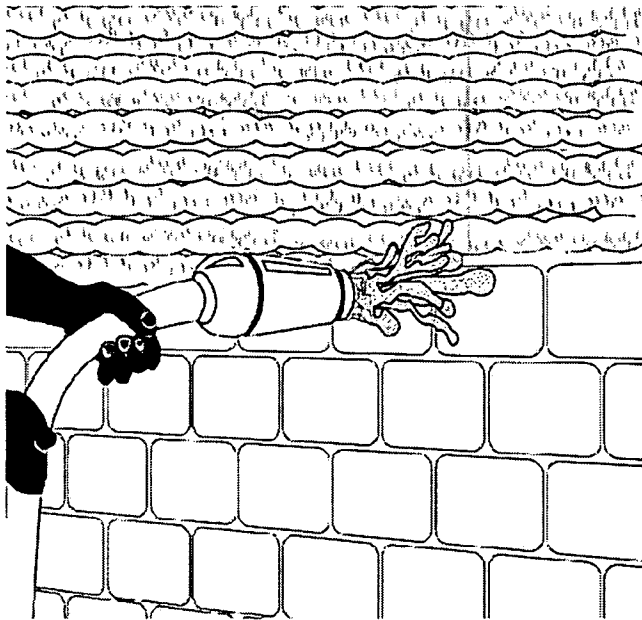


FIG. 9

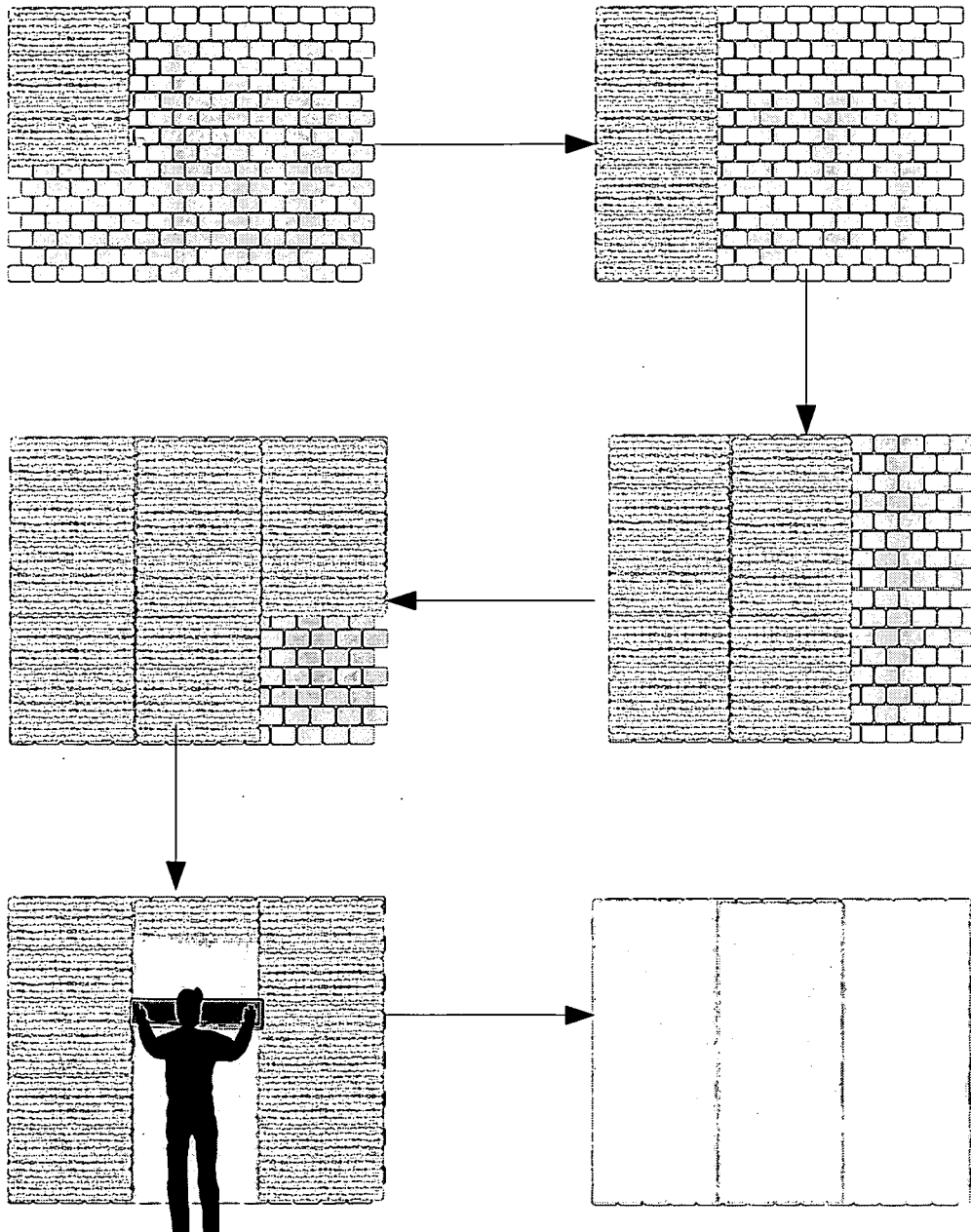


FIG. 10a

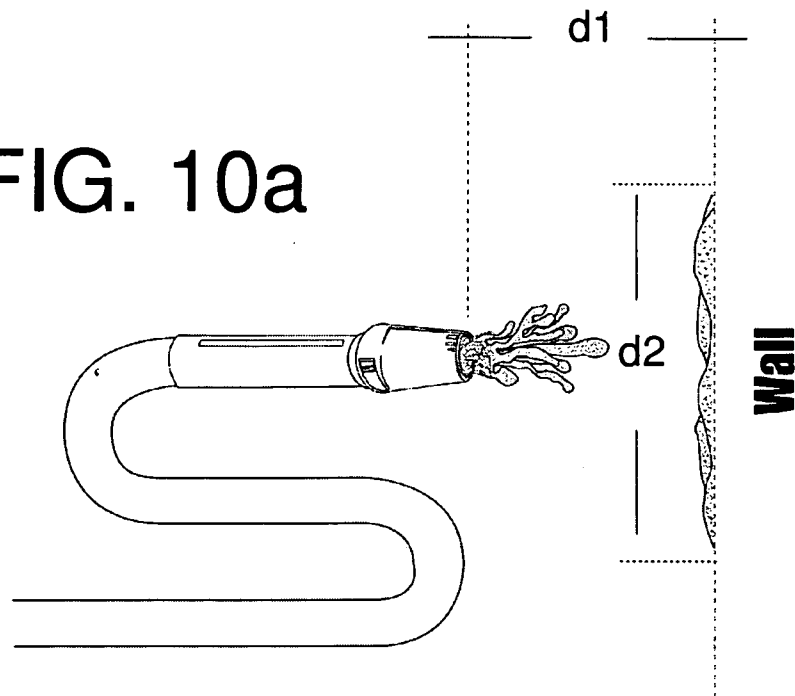


FIG. 10b

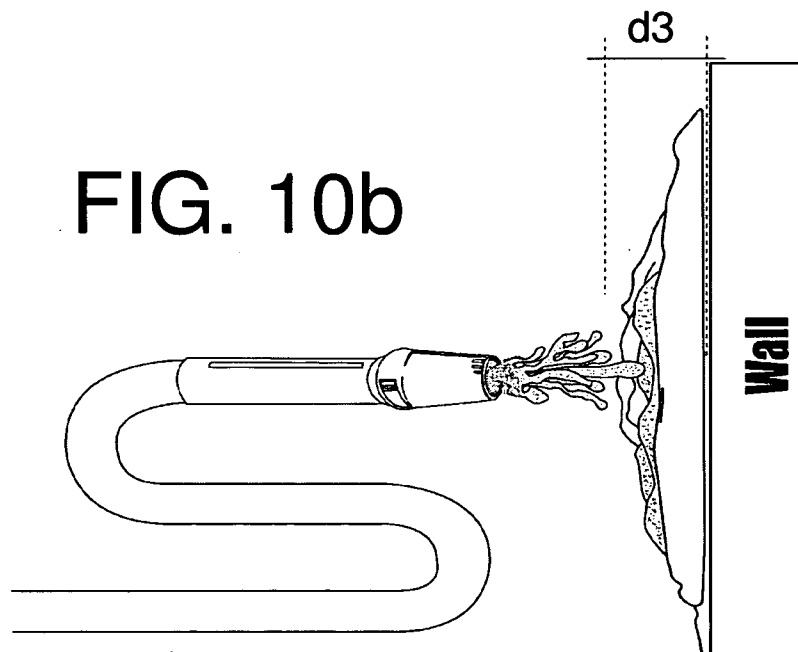


FIG. 11

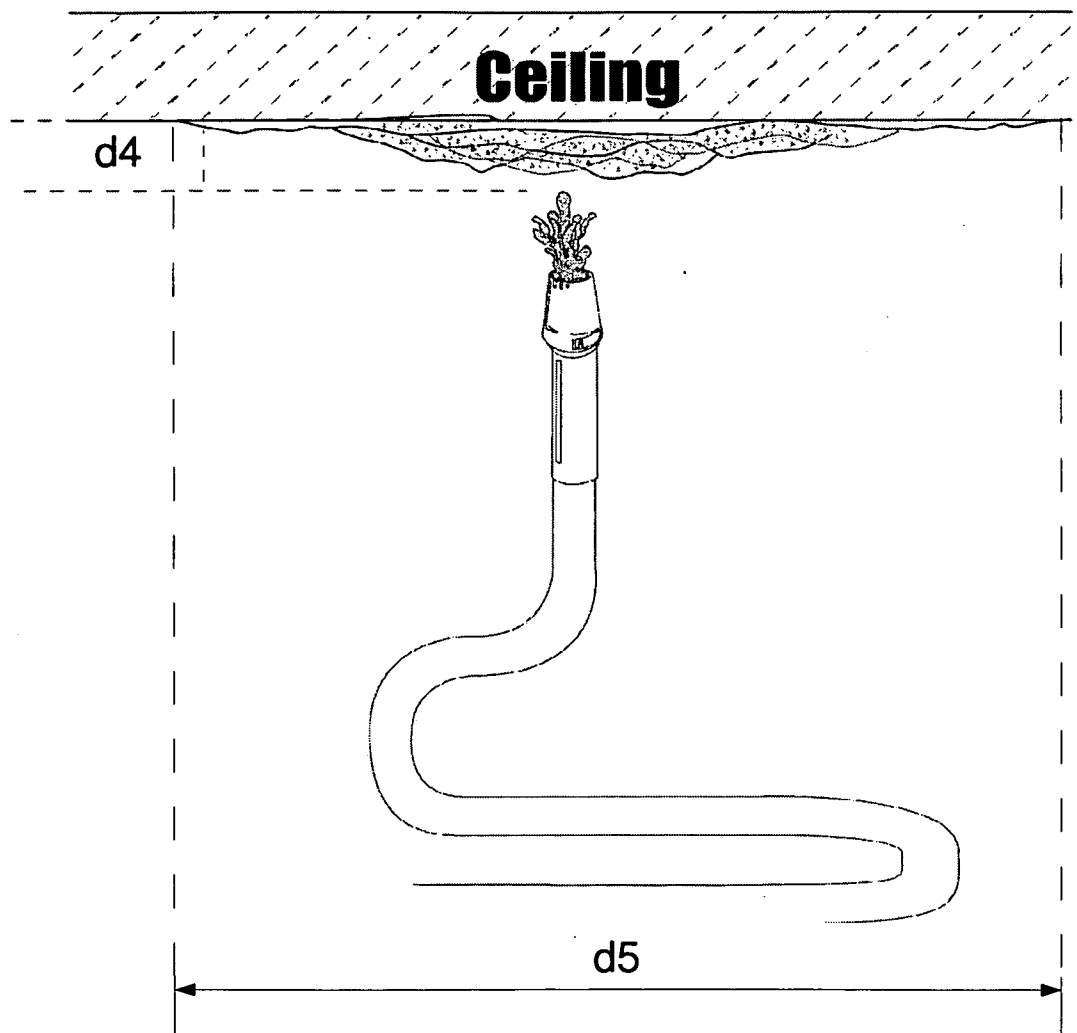


FIG. 12a

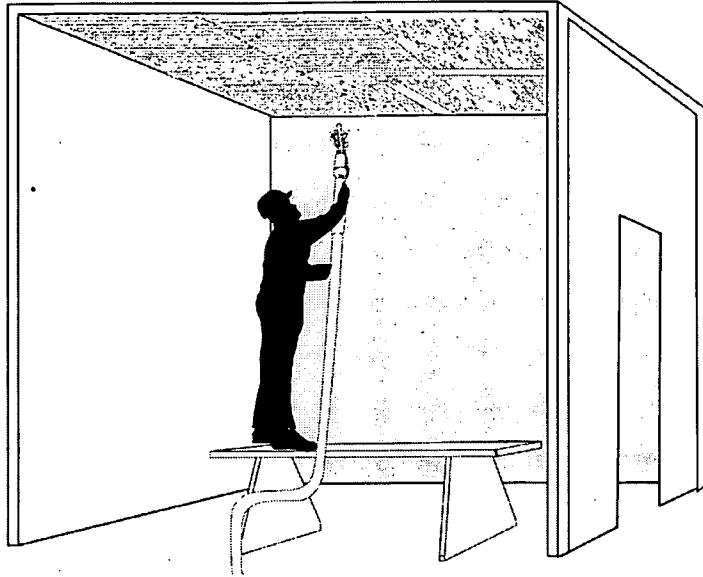


FIG. 12b

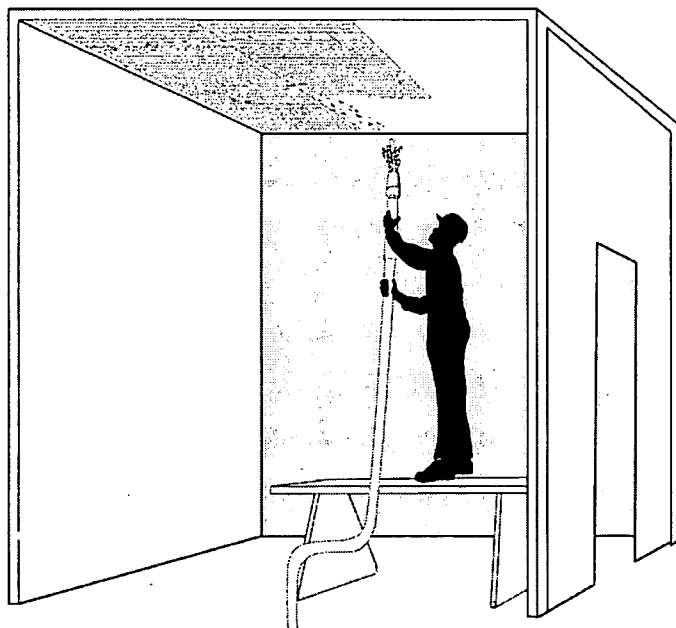


FIG. 13

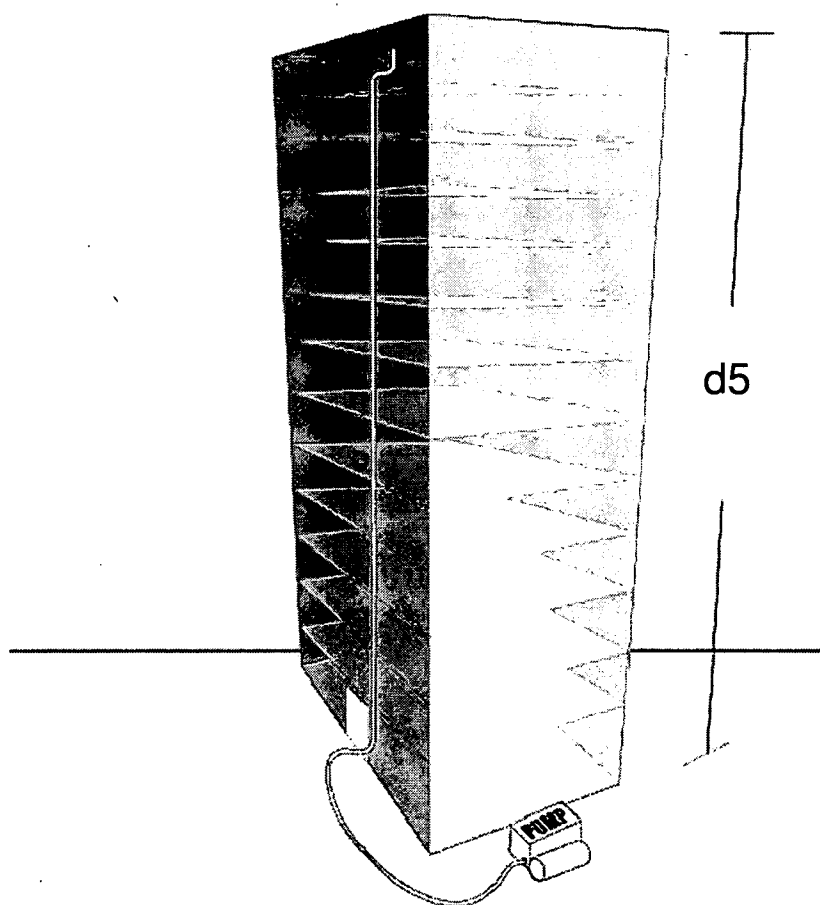


FIG. 14

Type	Name	Designation	Clinker	Blast Furnace Slag	MicroSilice	Natural Pozzolans	Fly Ashes	Limestone	Minor Components
CEM I	Portland Cement	CEM I	95-100	----	----	----	----	----	0-5
CEM II	Portland Cement - Slag	CEM II / A-S	80-84	5-20	----	----	----	----	0-5
	Portland Cement	CEM II / B-S	65-79	21-35	----	----	----	----	0-5
	MicroSilice	CEM II / A-D	90-94	----	6-10	----	----	----	0-5
	Portland Cement - Pozzolans	CEM II / A-P	80-84	----	----	6-20	----	----	0-5
	Portland Cement - Fly Ashes	CEM II / B-P	65-79	----	----	21-35	----	----	0-5
	Portland Cement - Fly Ashes	CEM II / A-V	80-84	----	----	----	6-20	----	0-5
	Portland Cement - Limestone	CEM II / B-V	65-79	----	----	----	21-35	----	0-5
	Portland Cement - Limestone	CEM II / A-L	80-84	----	----	----	----	6-20	0-5
	Portland Cement - Mode	CEM II / A-M	80-84	←	←	6-20	←	←	←
	Portland Cement - Mode	CEM II / B-M	65-79	←	←	21-35	←	←	←
CEM III	Cement - Blast Furnace	CEM III / A	35-61	36-65	----	----	----	----	0-5
CEM IV	Cement - Pozzolans	CEM III / B	20-34	66-80	----	----	----	----	0-5
	Cement - Pozzolans	CEM IV / A	65-69	----	←	11-35	←	←	0-5
	Cement - Compound	CEM IV / D	45-64	←	←	36-55	←	←	0-5
CEM V	Cement - Compound	CEM V / A	40-64	18-30	←	18-30	←	←	0-5

FIG. 15

	Components	1+1 (%)	1+2 (%)	1+3 (%)	1+4 (%)	1+5 (%)	1+6-8 (%)	Mix (%)
I	CEMENT	26.946089%	40.581101%	54.053978%	67.635152%	81.162154%	99.194096%	13.691679%
	SAND	72.854241%	59.118148%	45.545482%	31.863672%	18.236435%	0.000000%	86.206866%
	RETAINER	0.199601%	0.300601%	0.400400%	0.501001%	0.601201%	0.700665%	0.101420%
	AIR	0.019960%	0.030060%	0.040040%	0.050100%	0.060120%	0.070066%	0.010142%
	PLASTIFIER	0.019960%	0.030060%	0.040040%	0.050100%	0.060120%	0.070066%	0.010142%
	THICKENER	0.029940%	0.045090%	0.060060%	0.075150%	0.090180%	0.105100%	0.015213%
	THICKENER	0.029940%	0.045090%	0.060060%	0.075150%	0.090180%	0.105100%	0.015213%
II	CEMENT	26.999981%	43.144744%	54.054000%	67.635186%	81.162203%	99.194165%	13.691680%
	SAND	72.999949%	56.567553%	45.545500%	31.863688%	18.236446%	0.000000%	86.206875%
	RETAINER	0.200000%	0.287632%	0.400400%	0.501001%	0.601202%	0.700665%	0.101420%
	AIR	0.020000%	0.028763%	0.040040%	0.050100%	0.060120%	0.070067%	0.010142%
	THICKENER	0.030000%	0.043145%	0.060060%	0.075150%	0.090180%	0.105100%	0.015213%
III	CEMENT	26.999981%	43.269187%	54.271280%	67.975711%	81.653053%	99.894018%	13.705579%
	SAND	72.999949%	56.730712%	45.728579%	32.024113%	18.346735%	0.000000%	86.294386%
	PLASTIFIER	0.020000%	0.028846%	0.040201%	0.050352%	0.060484%	0.070561%	0.010152%
	AIR	0.020000%	0.028846%	0.040201%	0.050352%	0.060484%	0.070561%	0.010152%
	THICKENER	0.030000%	0.043269%	0.060301%	0.075529%	0.090726%	0.105841%	0.015228%
IV	CEMENT	26.946097%	43.144750%	54.054011%	67.635203%	81.162227%	99.298458%	13.691681%
	SAND	72.854262%	56.567561%	45.545509%	31.863696%	18.236451%	0.000000%	86.206879%
	RETAINER	0.199601%	0.287632%	0.400400%	0.501002%	0.601202%	0.701402%	0.101420%
	AIR	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
	PLASTIFIER	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
V	CEMENT	25.665392%	43.144756%	54.054022%	67.635220%	81.162251%	99.194235%	13.691681%
	SAND	74.144466%	56.567569%	45.545518%	31.863704%	18.236457%	0.000000%	86.206883%
	RETAINER	0.190114%	0.287632%	0.400400%	0.501002%	0.601202%	0.700666%	0.101420%
	THICKENER	0.028517%	0.043145%	0.060060%	0.075150%	0.090180%	0.105100%	0.015213%
VI	CEMENT	26.946102%	43.144762%	54.054032%	67.635237%	81.162276%	99.298528%	13.691682%
	SAND	72.854277%	56.567577%	45.545527%	31.863711%	18.236462%	0.000000%	86.206888%
	RETAINER	0.199601%	0.287632%	0.400400%	0.501002%	0.601202%	0.701402%	0.101420%
	AIR	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
VII	CEMENT	26.946102%	43.144762%	54.054032%	67.635237%	81.162276%	99.298528%	13.691682%
	SAND	72.854277%	56.567577%	45.545527%	31.863711%	18.236462%	0.000000%	86.206888%
	RETAINER	0.199601%	0.287632%	0.400400%	0.501002%	0.601202%	0.701402%	0.101420%
	PLASTIFIER	0.019960%	0.028763%	0.040040%	0.050100%	0.060120%	0.070140%	0.010142%
VIII	CEMENT	26.999987%	43.269200%	54.271302%	67.975745%	81.653102%	99.894088%	13.705580%
	SAND	72.999964%	56.730728%	45.728597%	32.024129%	18.346746%	0.000000%	86.294394%
	AIR	0.020000%	0.028846%	0.040201%	0.050352%	0.060484%	0.070561%	0.010152%
	THICKENER	0.030000%	0.043269%	0.060301%	0.075529%	0.090726%	0.105841%	0.015228%

FIG. 16

