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Moshier

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(54) **SINGLE PASSENGER AIRCRAFT**

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Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

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(51) **Int. Cl.**⁷ **B64C 29/00**

(52) **U.S. Cl.** **244/4 A; 244/4 R**

(58) **Field of Search** **244/4 R, 17.14, 244/7 R, 7 A, 17.11, 73 A, 4 A; 74/502, 503**

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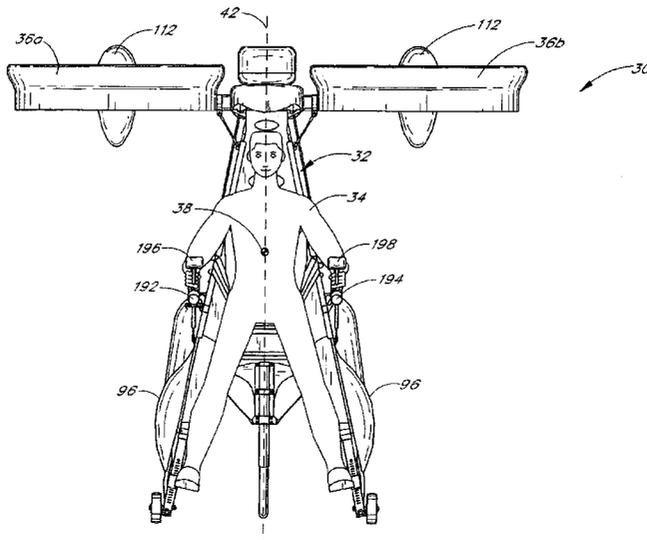
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(57) **ABSTRACT**

Disclosed is a single passenger aircraft configured to vertically take-off and land. An airframe is configured to support the passenger in an upright position during take-off and landing and during flight. The aircraft includes a pair of propulsion devices that are mounted on an airframe above the level of the pilot. A set of hand operated control devices are mechanically linked to the propulsion devices for varying the orientation of the propulsion devices during flight.

19 Claims, 21 Drawing Sheets



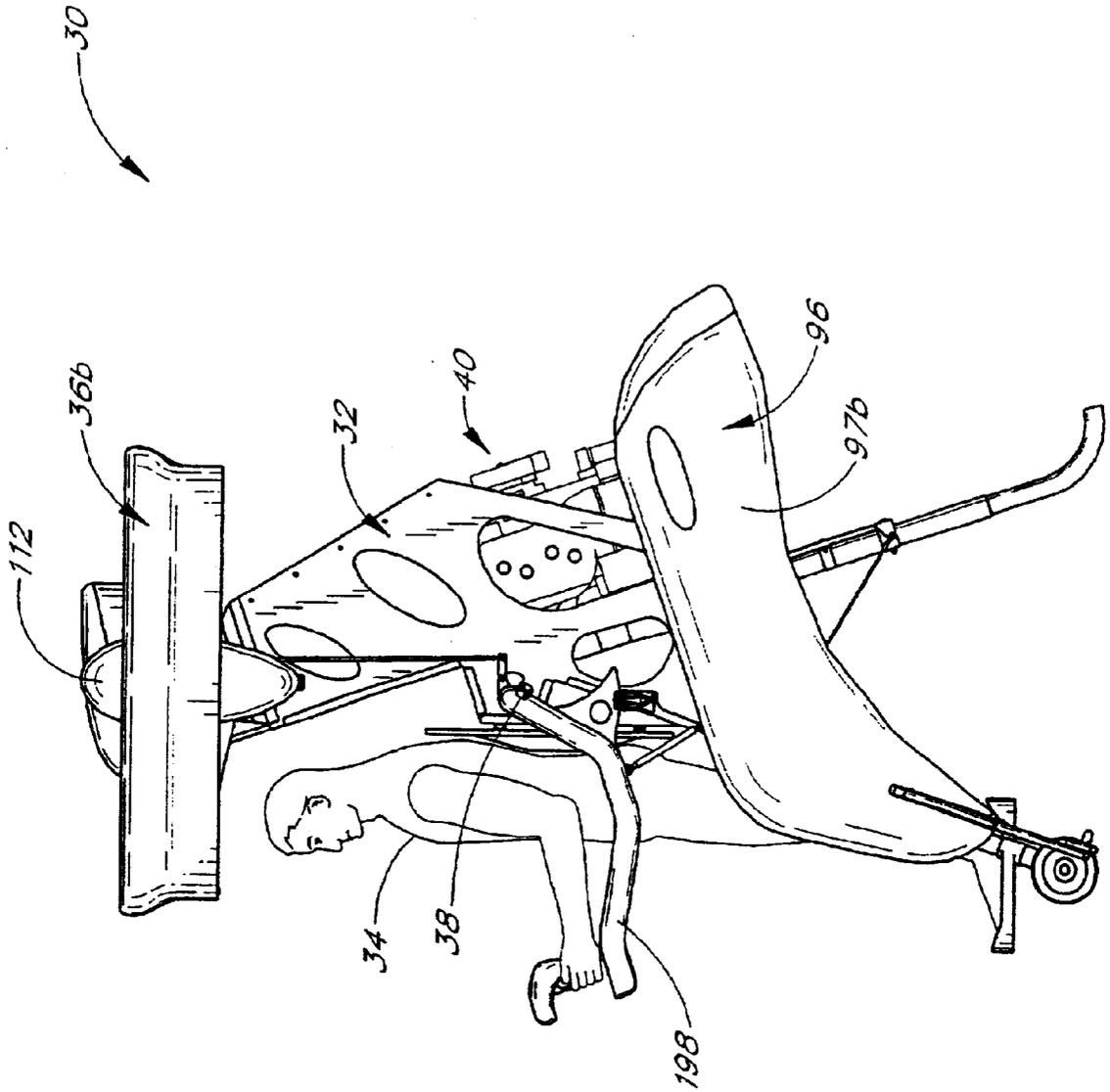


FIG. 2

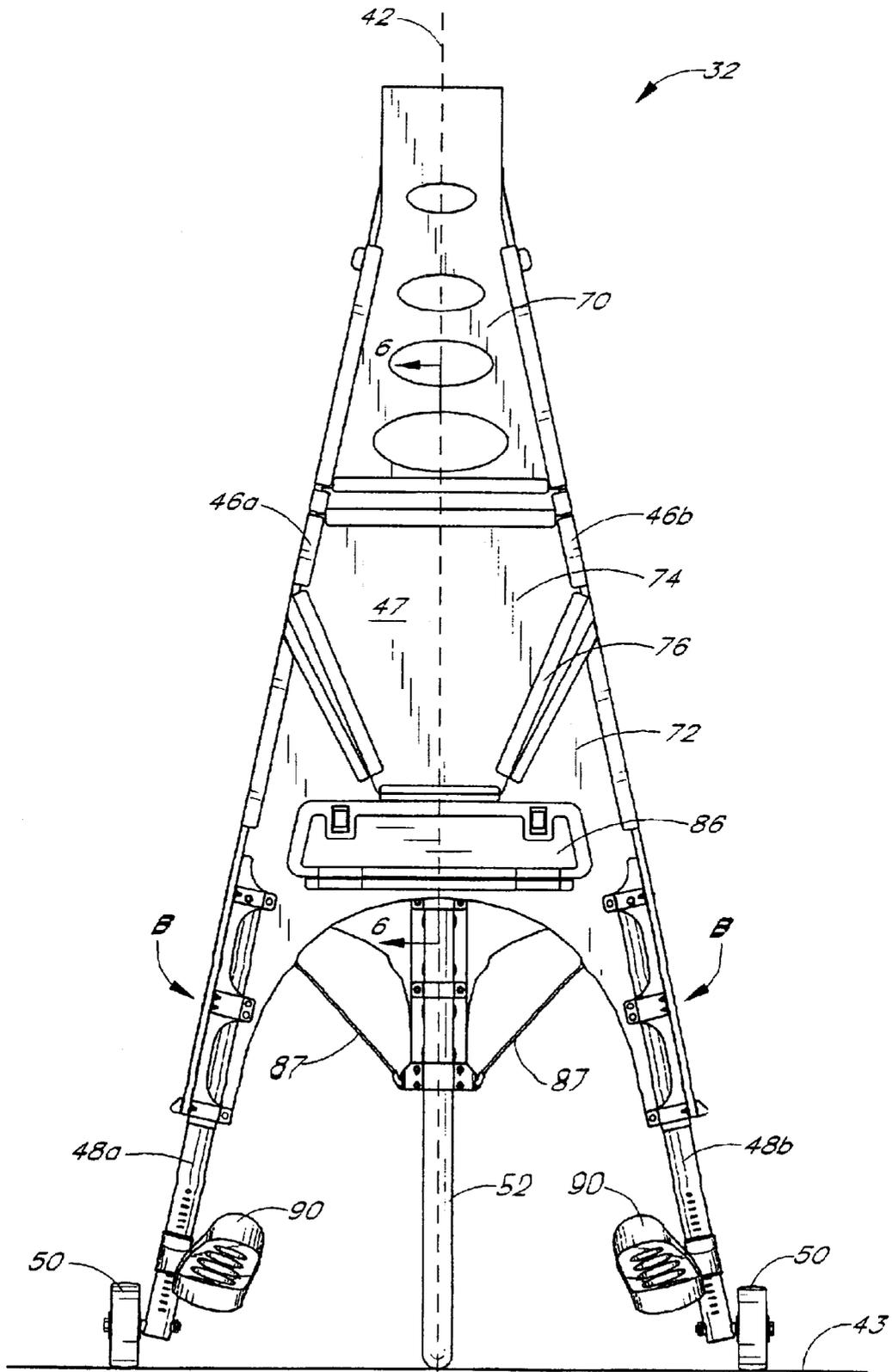


FIG. 3

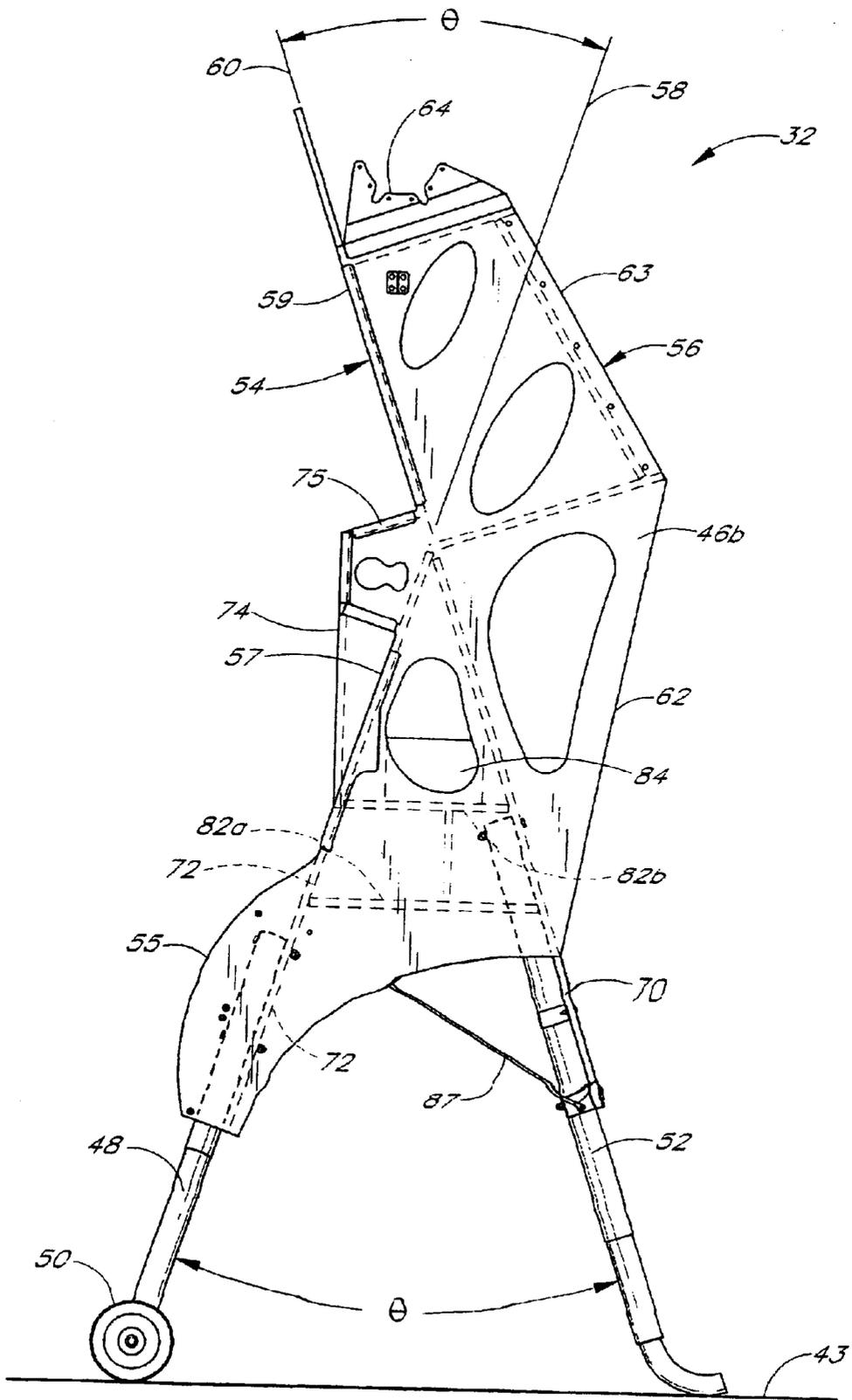


FIG. 4

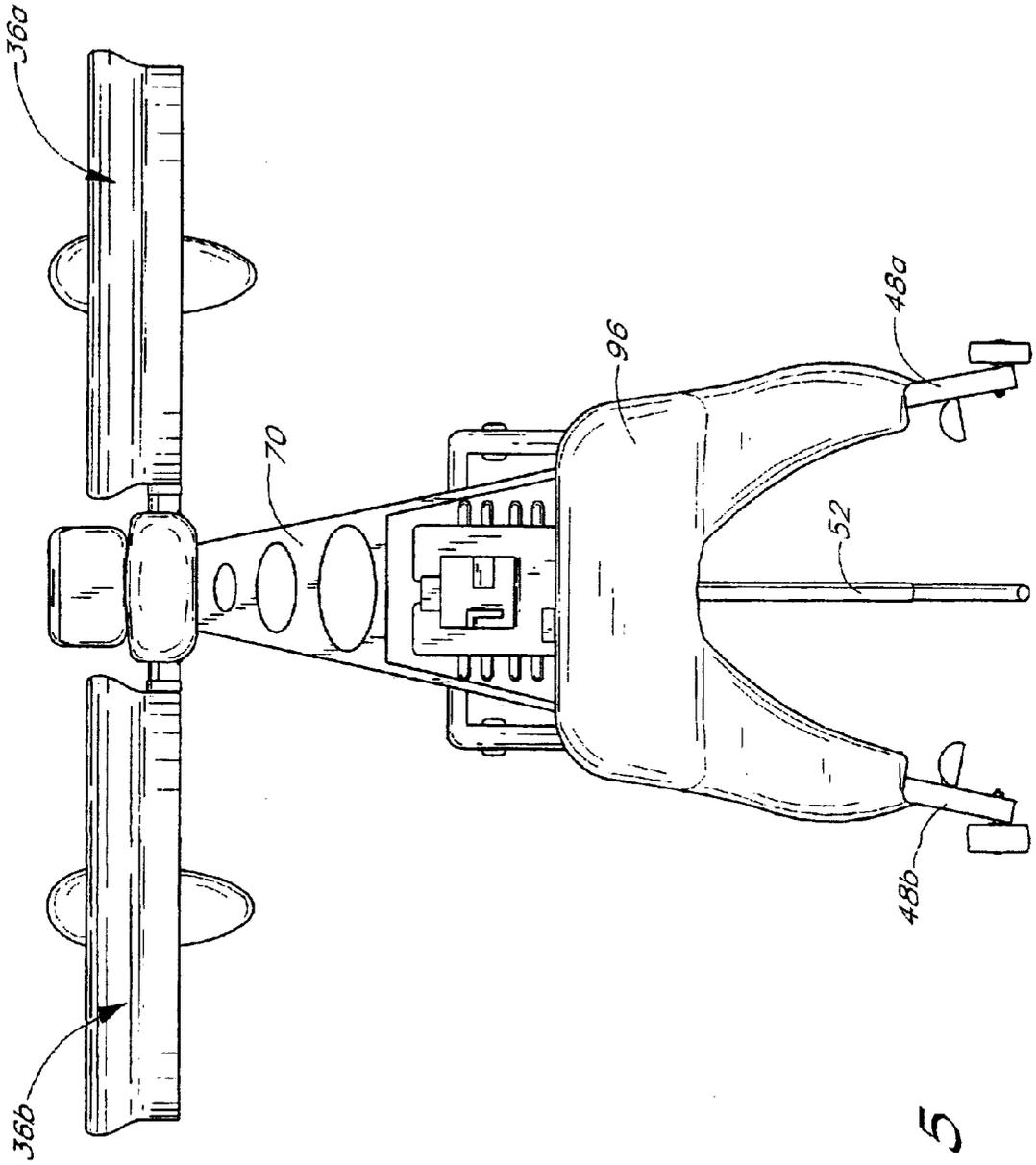


FIG. 5

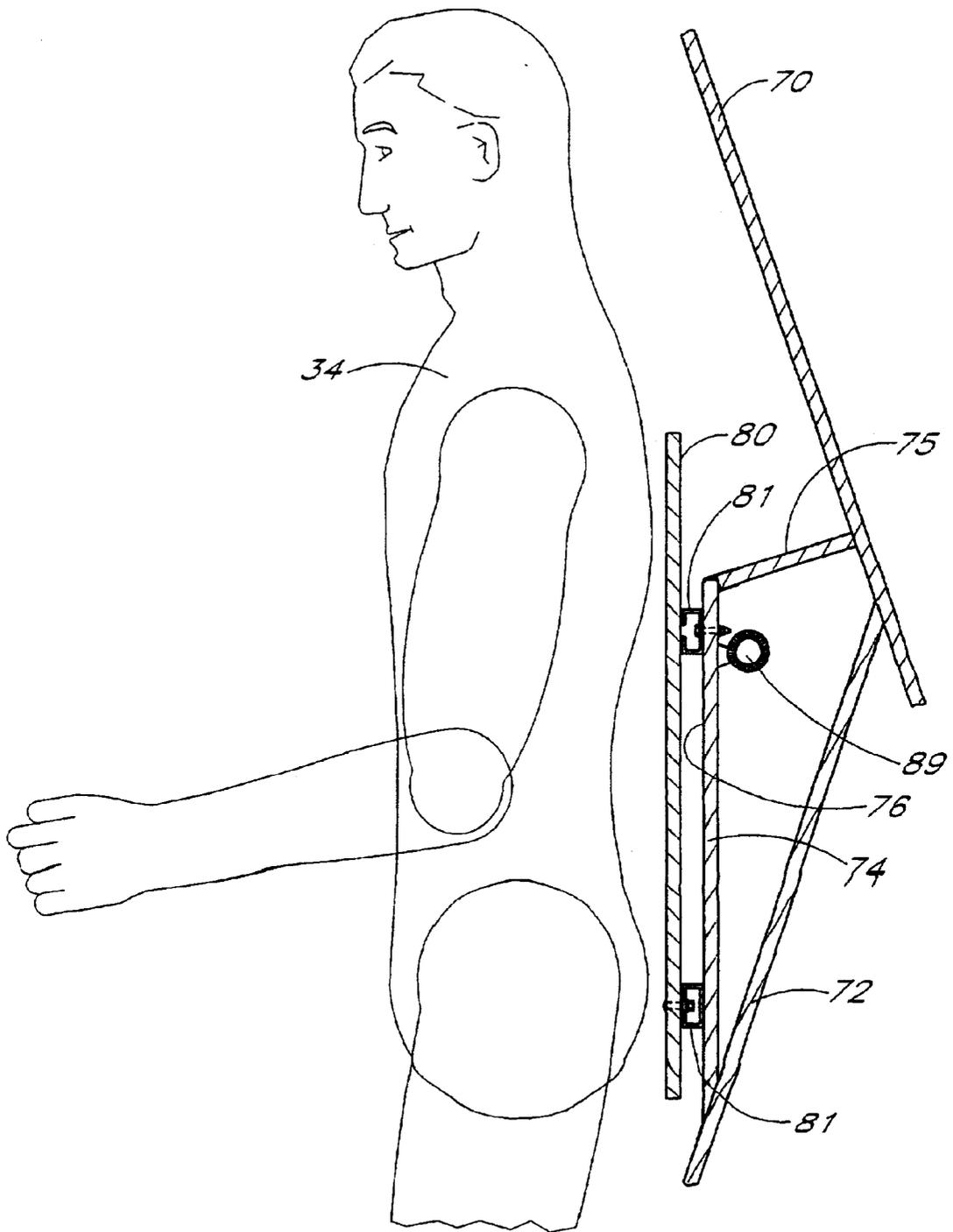


FIG. 6

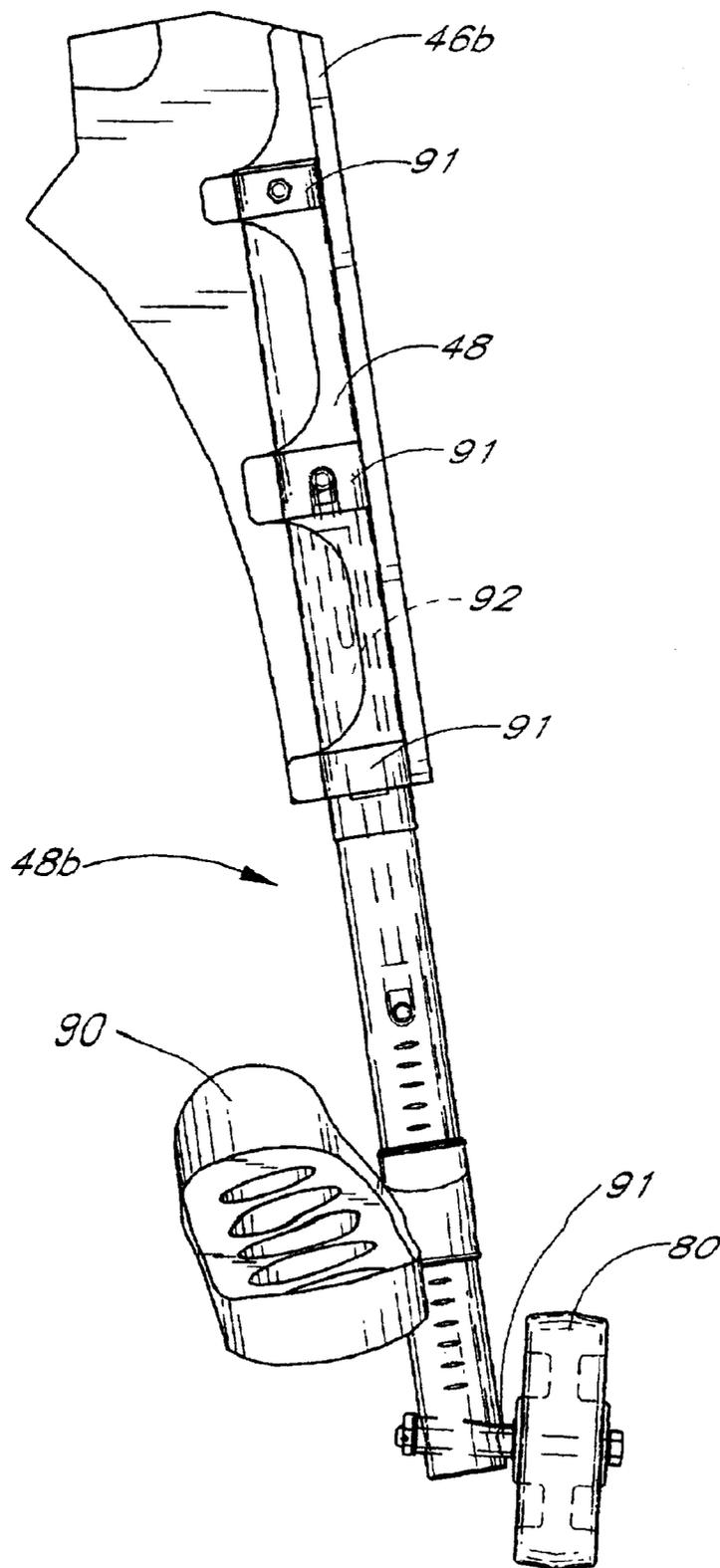


FIG. 7

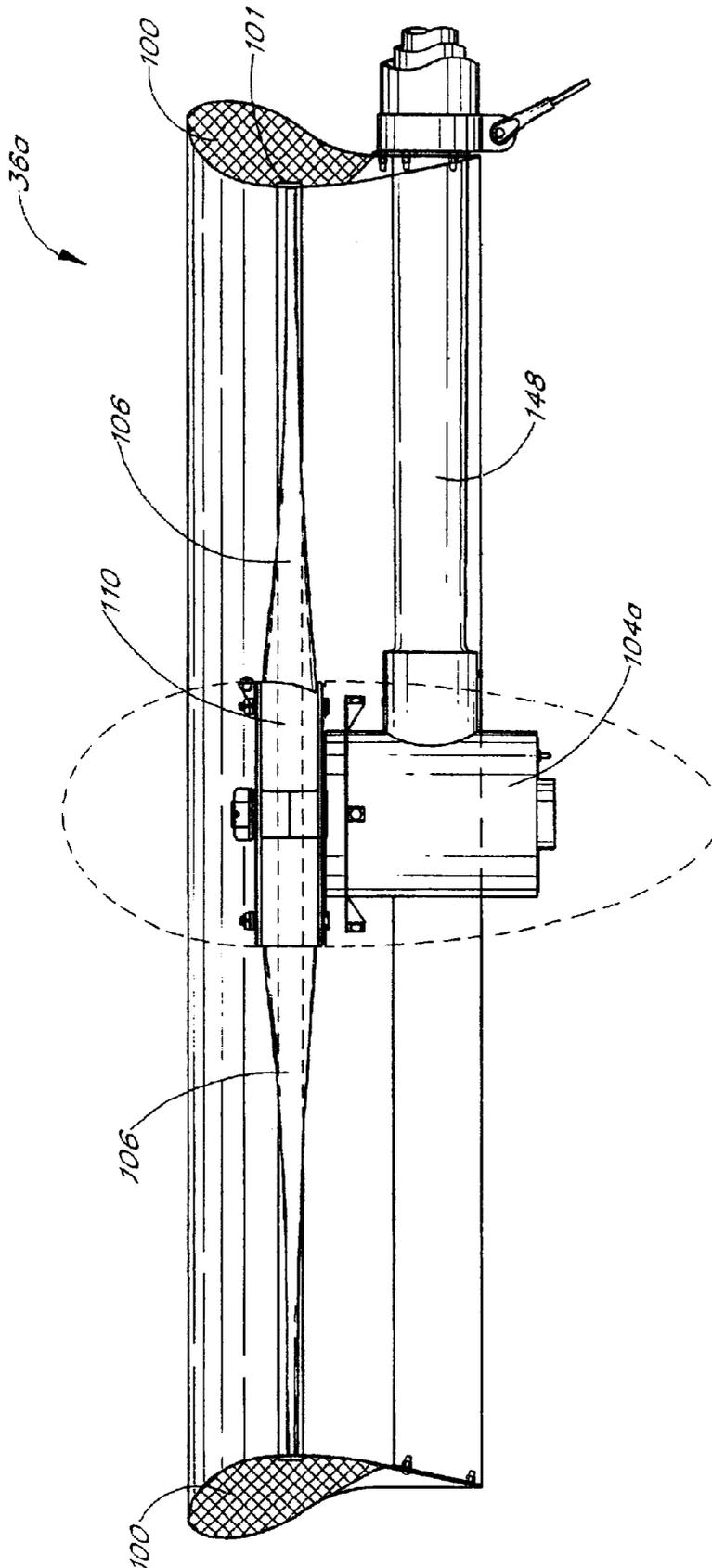


FIG. 10

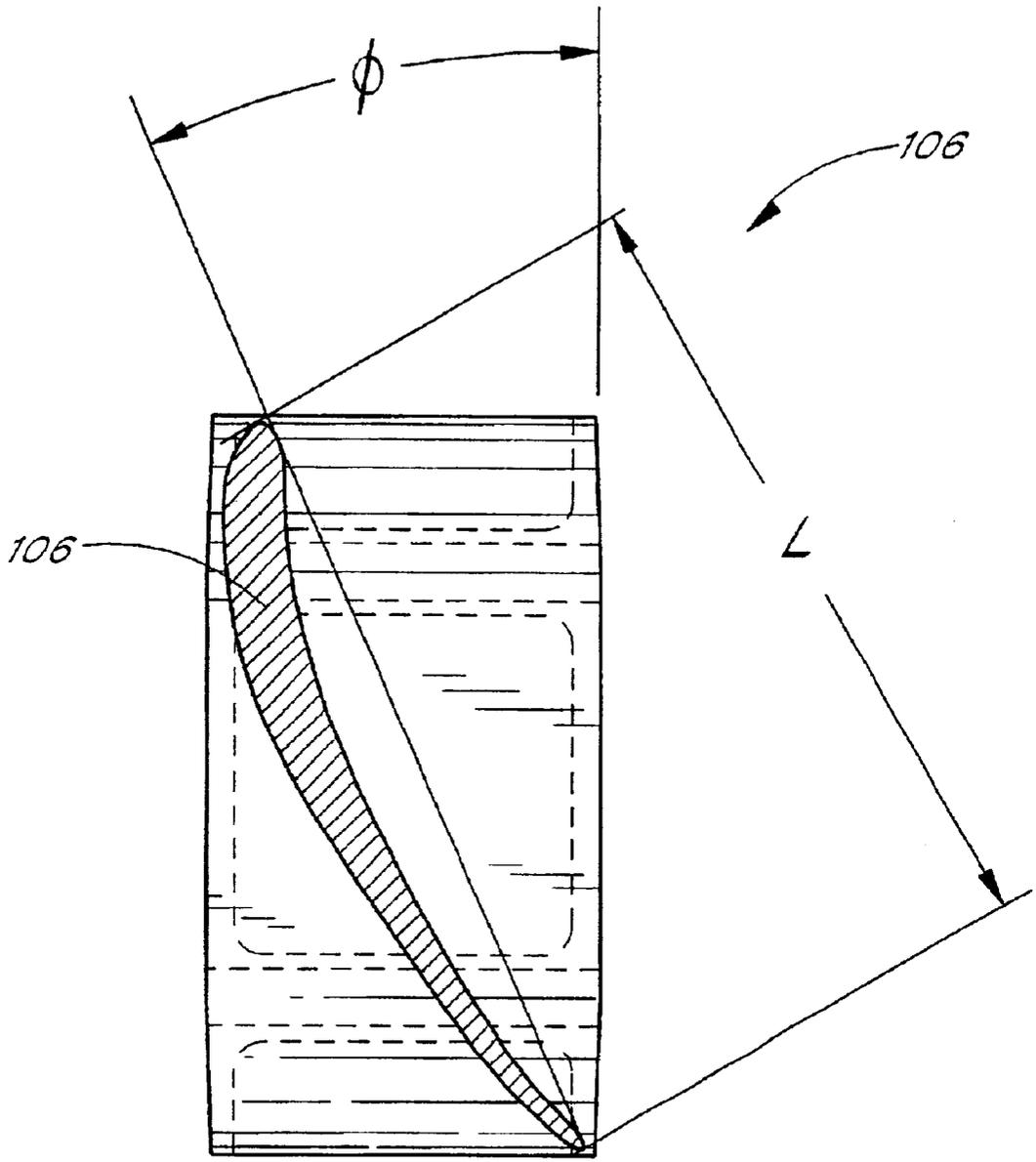


FIG. 11

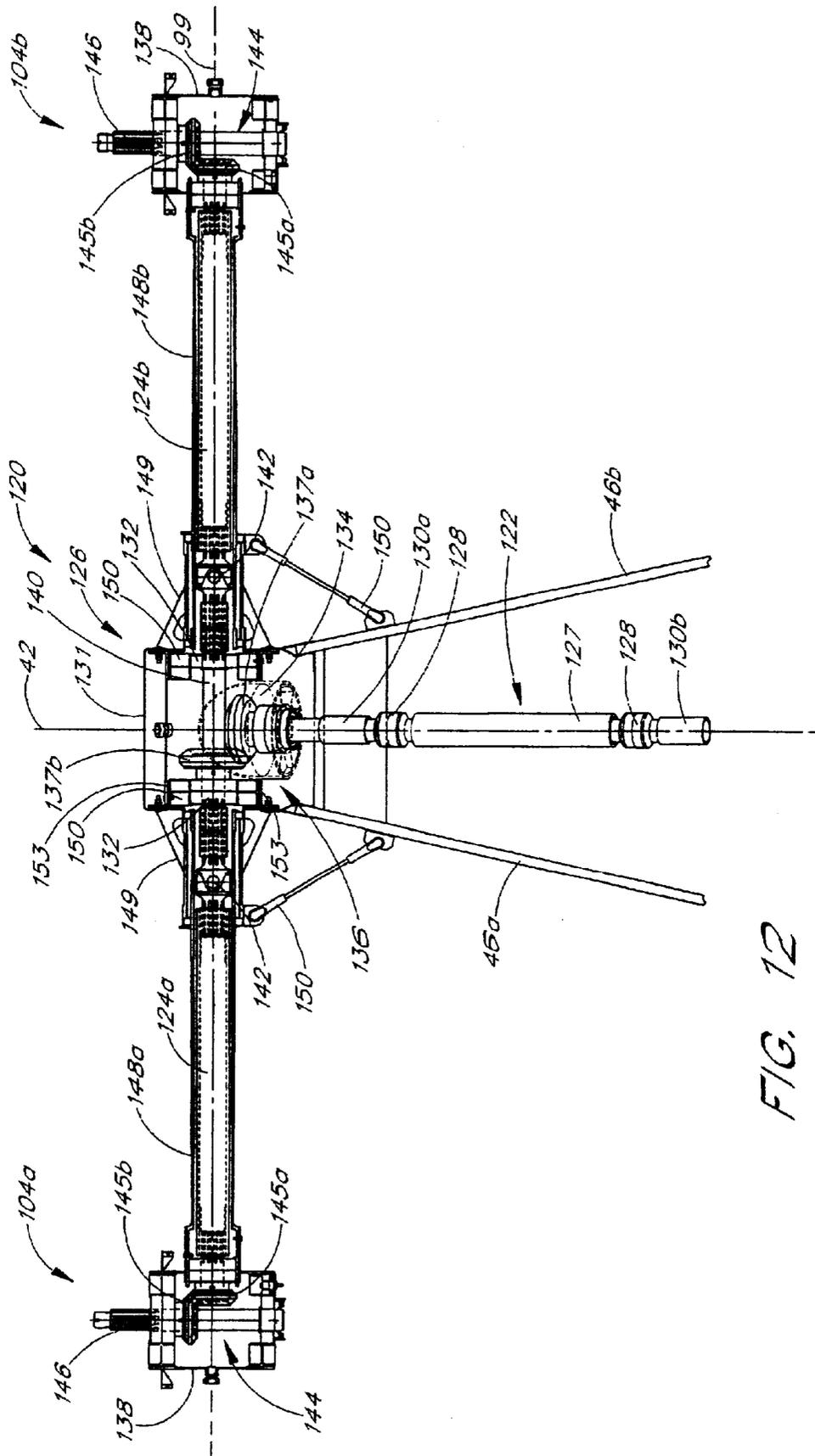
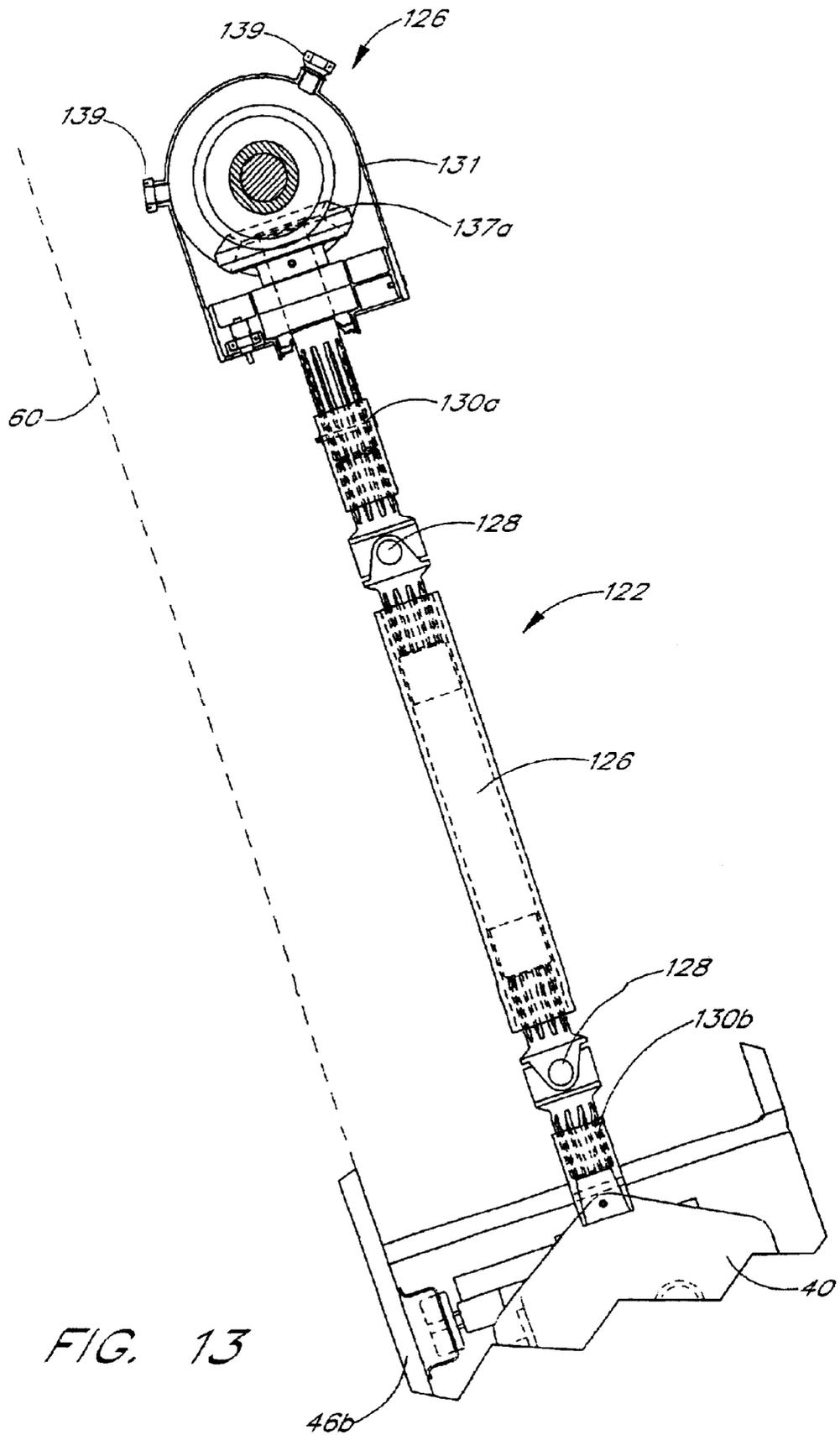


FIG. 12



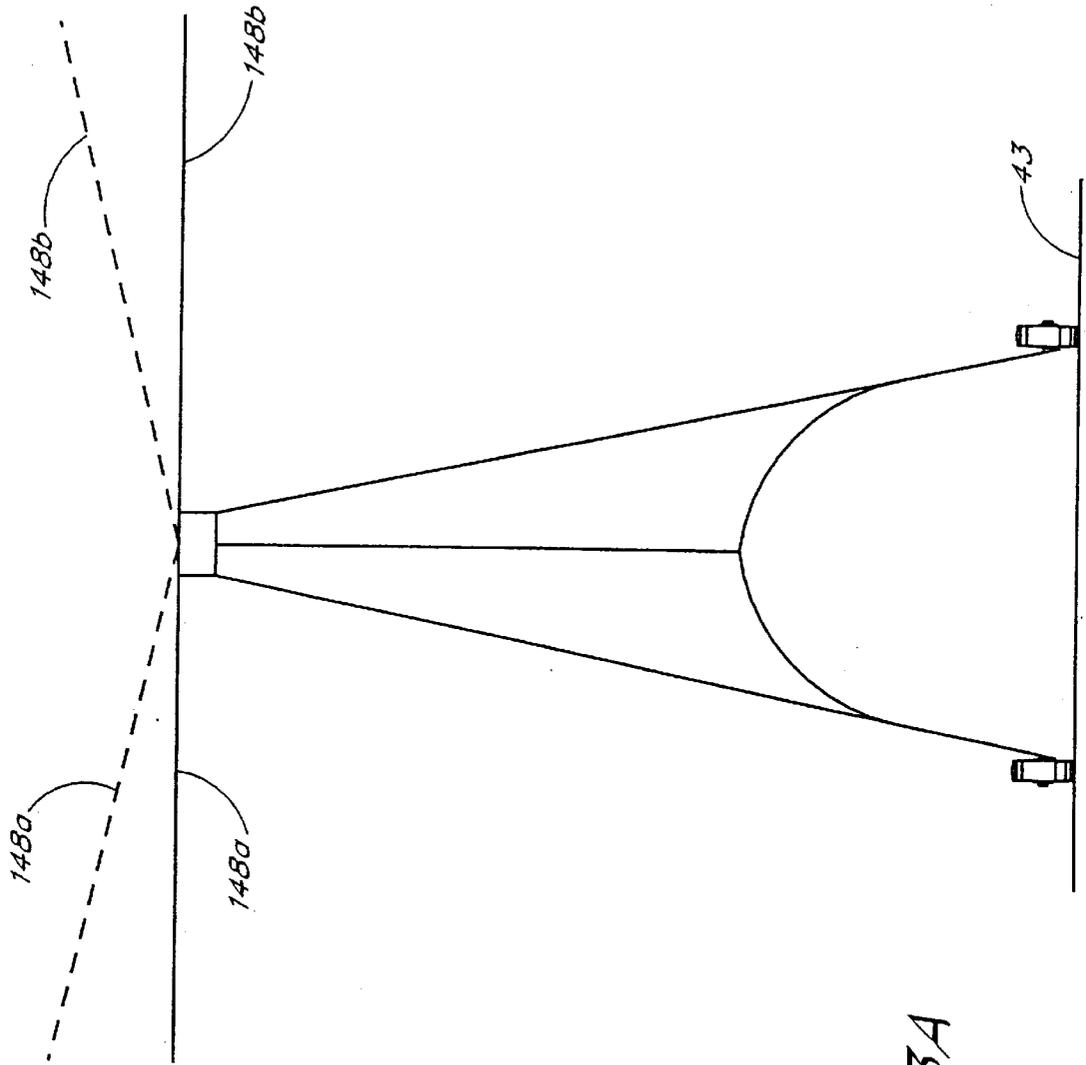


FIG. 13A

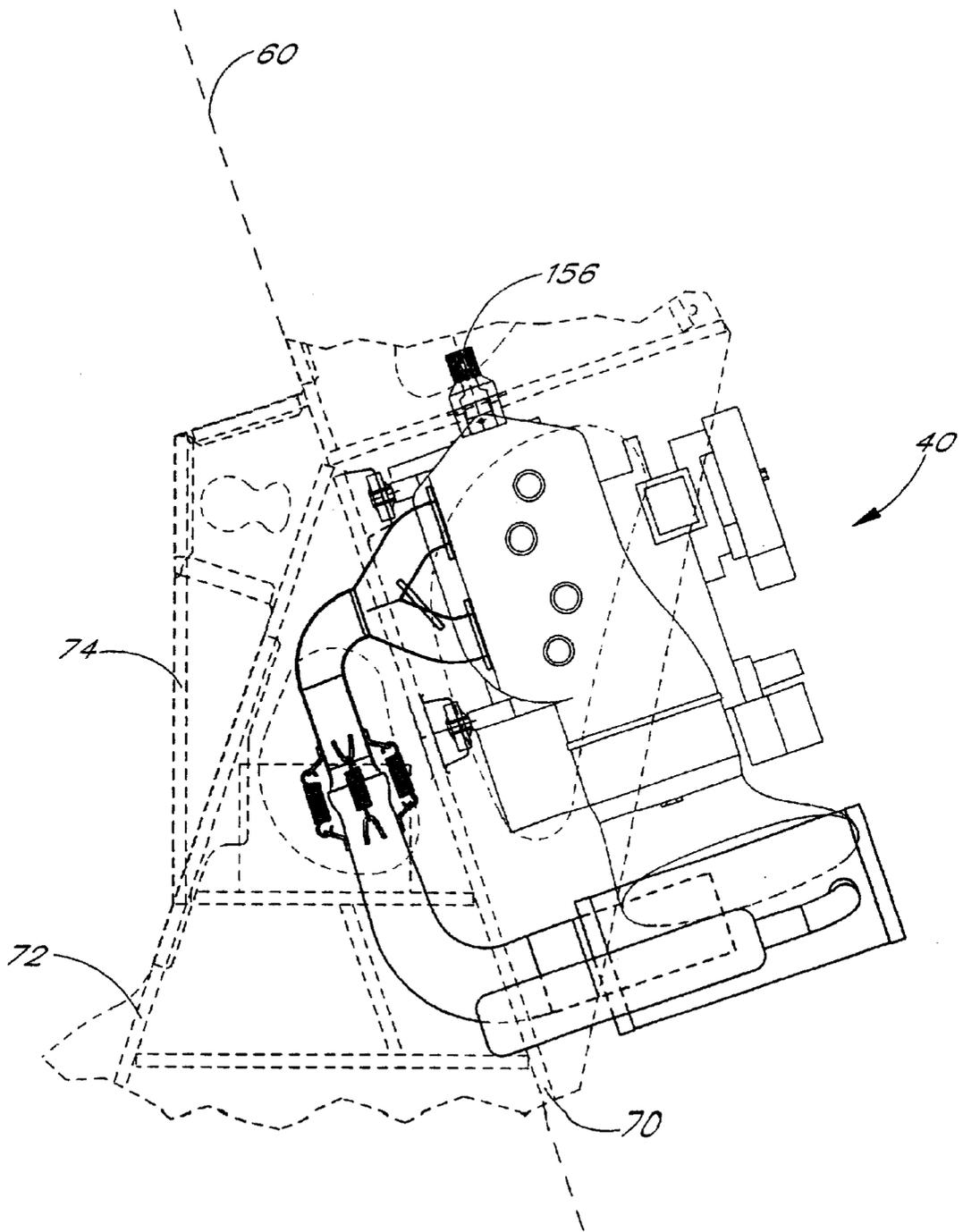


FIG. 14

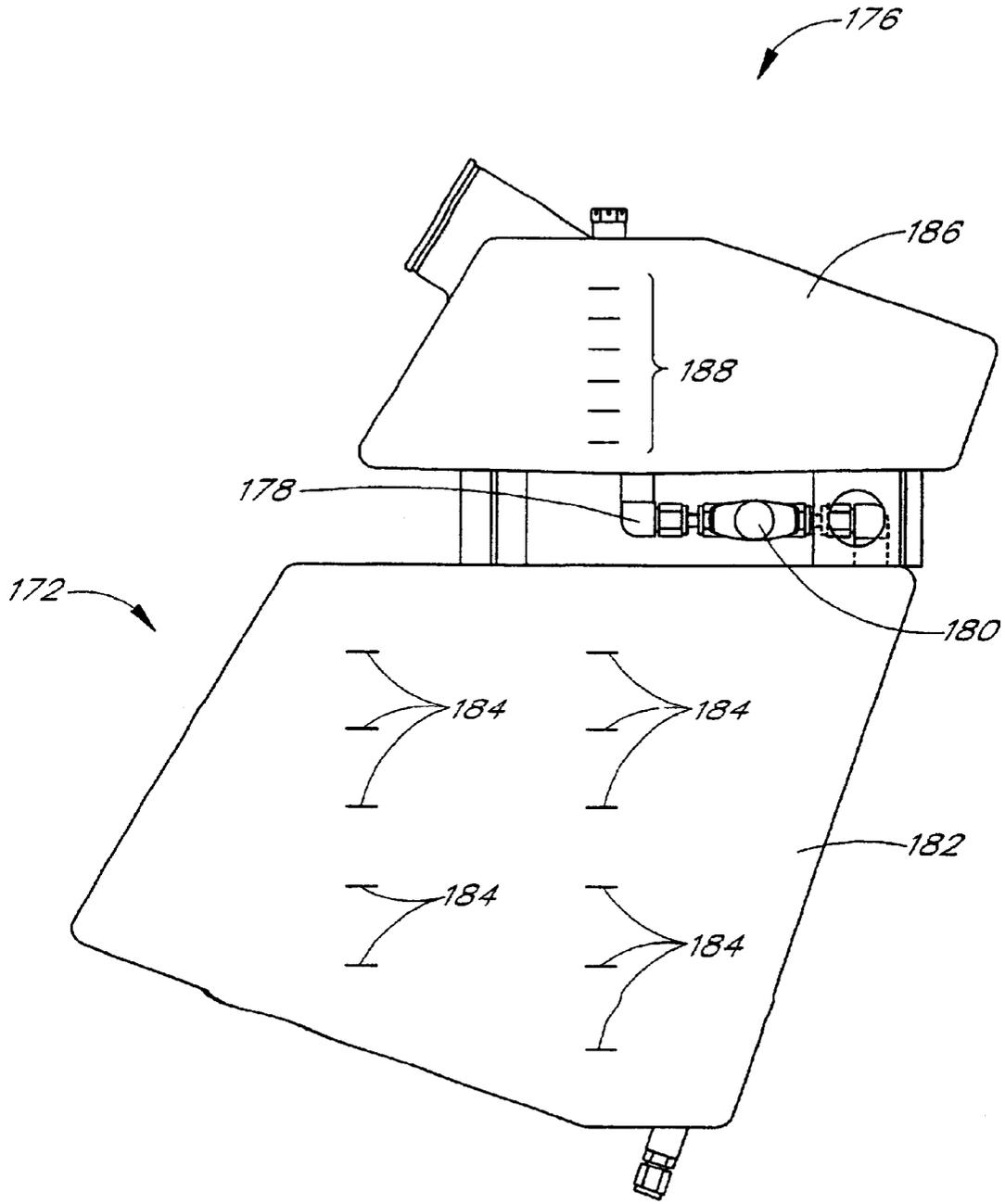


FIG. 15

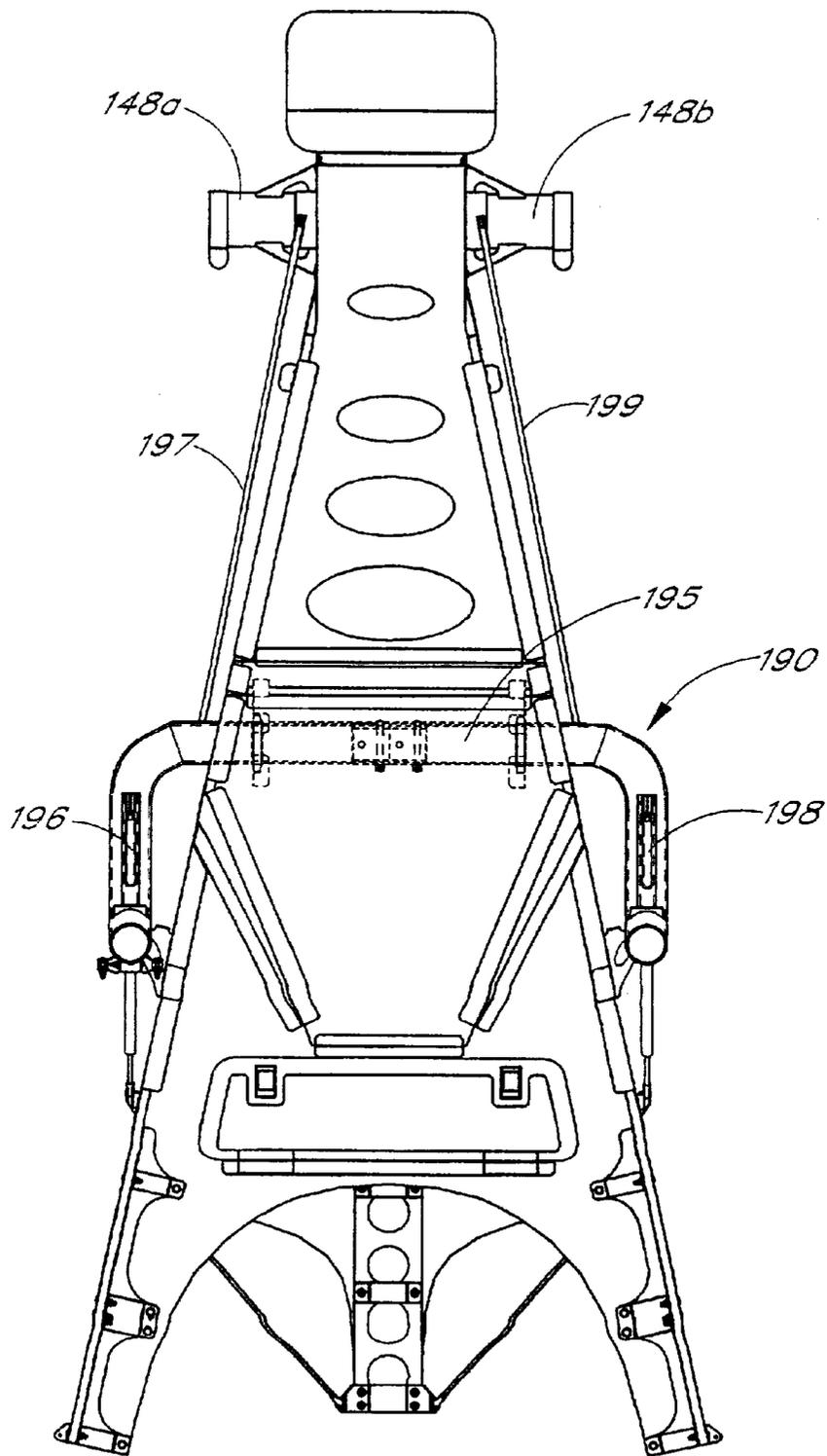


FIG. 16

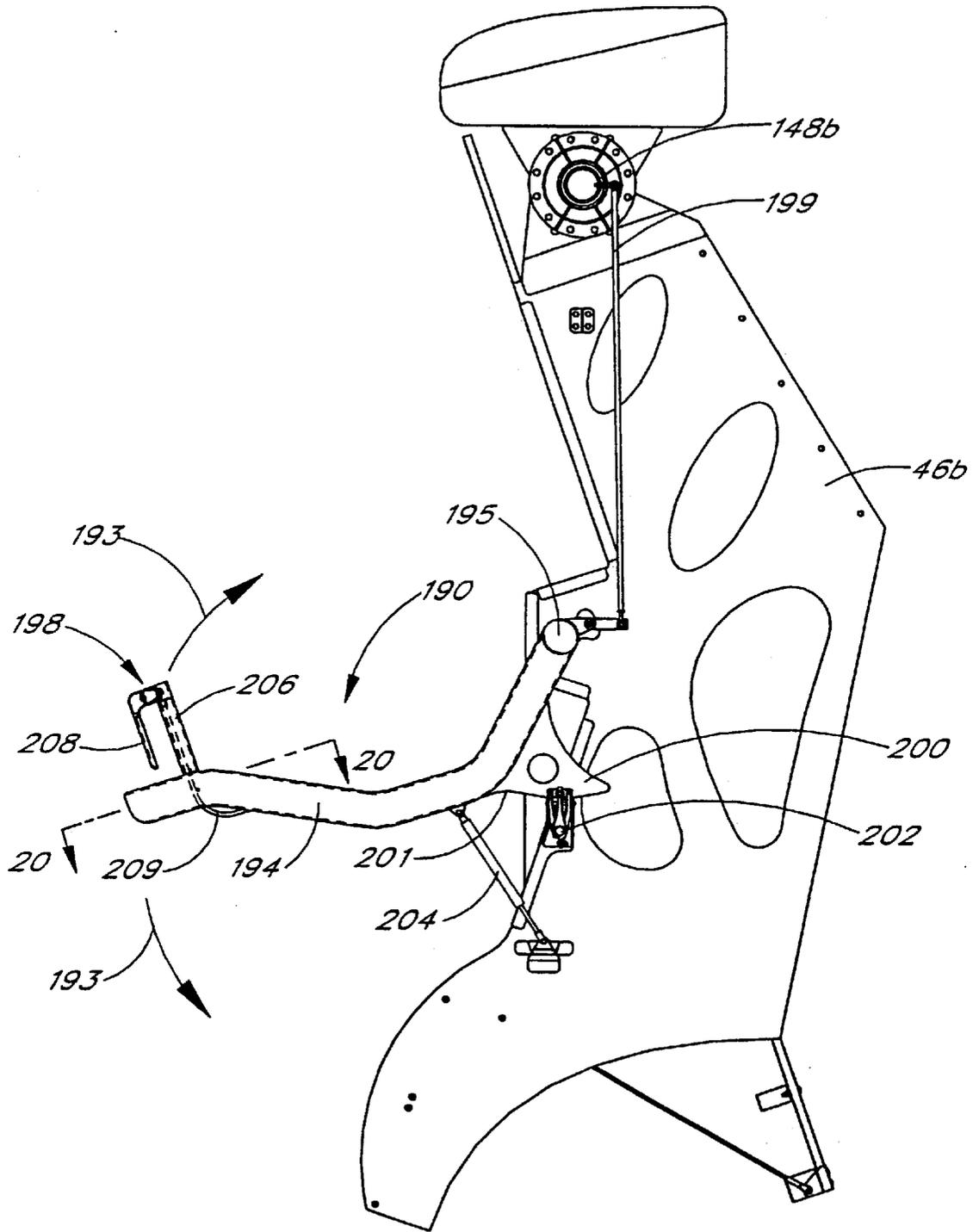


FIG. 17

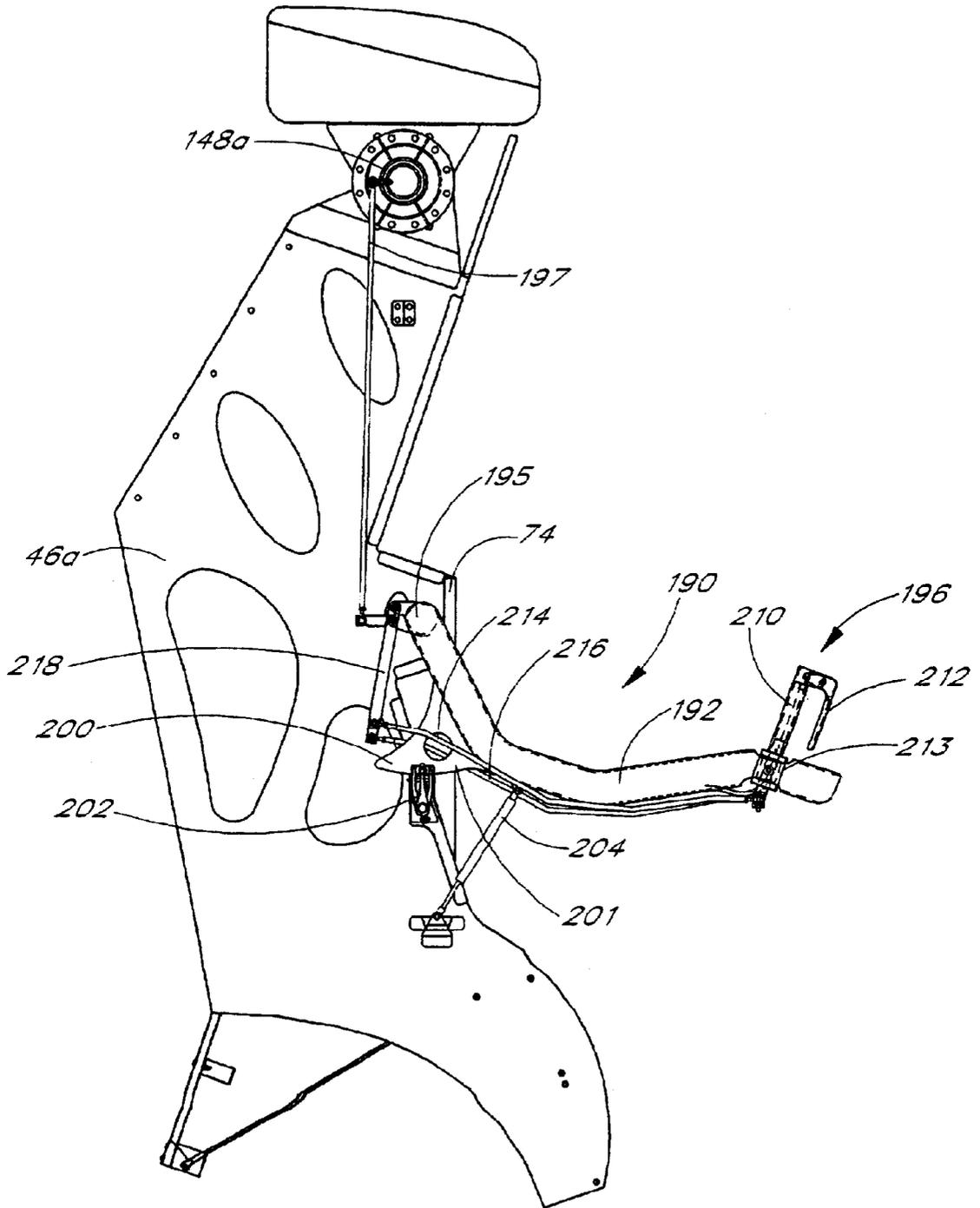


FIG. 18

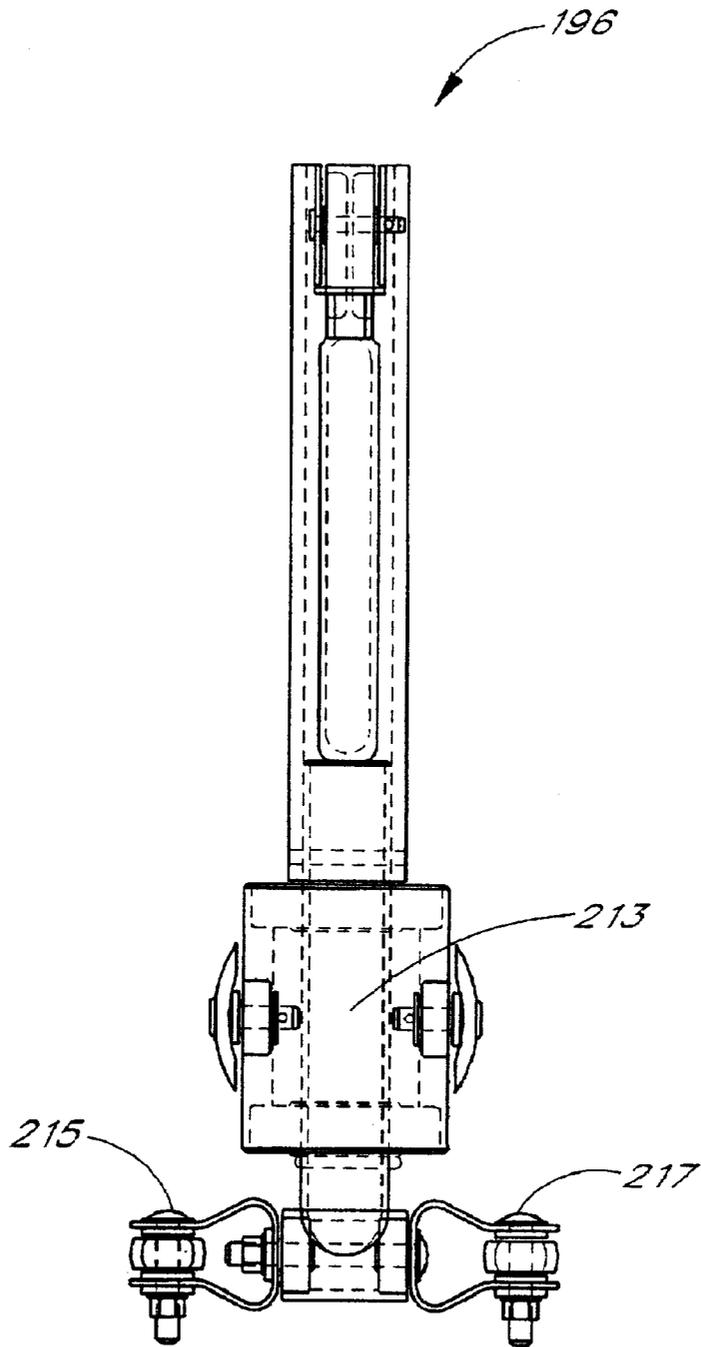


FIG. 19

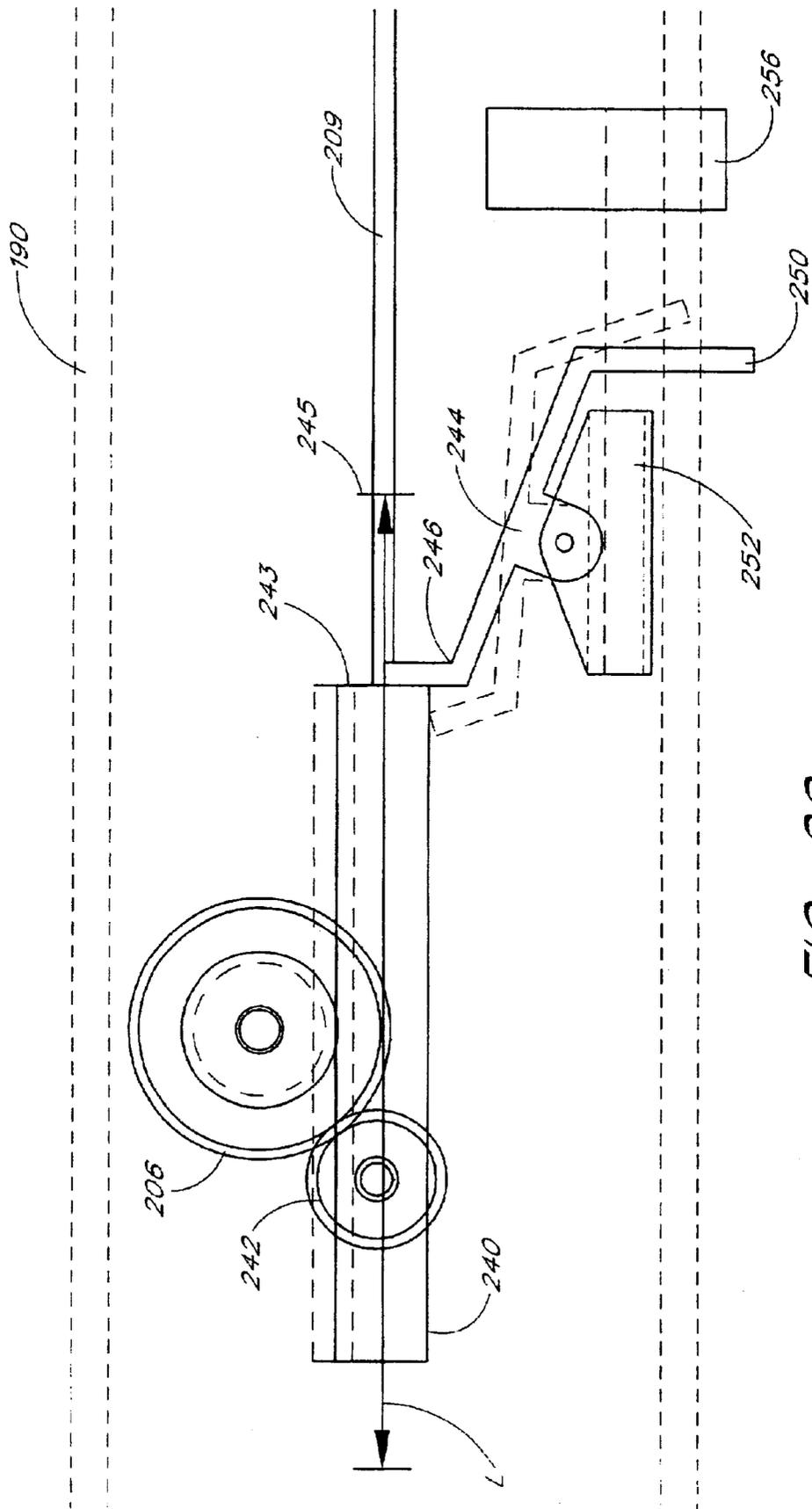


FIG. 20

SINGLE PASSENGER AIRCRAFT**BACKGROUND OF THE INVENTION**

1. Field of the Invention

The present invention relates to the field of aircraft. More particularly, the present invention relates to a vertical take-off and landing aircraft that transports a passenger in an upright position during flight.

2. Description of the Related Art

There have been numerous efforts to design a reliable personal or single passenger aircraft that transports a passenger easily and safely from one location to another. Unfortunately, past single-passenger aircraft designs are impractical for everyday type use by the average person. Past designs also suffer from other drawbacks, such as the use of hazardous fuel, the consumption of a great amount of storage space, or they suffer from unstable and unsafe flight characteristics.

For example, one type of design comprises a conventional type of aircraft having a propulsion device, such as a fan unit, and a plurality of flight surfaces, such as wings, extending outwardly therefrom. Such aircraft are large and bulky and are generally not suitable for quick transportation from one location to another. These types of aircraft generally require long landing and take off strips that consume large amounts of land space. Additionally, such aircraft are generally difficult to control during flight, requiring the pilot to become well-versed in the flight mechanics of the aircraft. This makes these aircraft unsuitable for the quick traversing of great distances and, therefore, impractical for day-to-day travel.

Another type of design consists of a "flightpack" comprised of a small structure that fits on or around the torso of the pilot. The flight pack designs typically include propulsion devices, such as propellers, jets, or rockets, that are supported by the pilot's torso. While these flightpacks are small and require little take-off and landing space, they are unfortunately generally unstable and dangerous during flight and therefore unsafe for the general population. The high likelihood of the passenger losing control of such aircraft is a strong drawback. One additional drawback of current flightpacks is that the passenger is typically required to support the heavy airframe on his or her back, which is highly uncomfortable. Alternatively, the passenger may be required to orient himself in awkward positions during flight which makes the use of such aircraft uncomfortable and impractical.

Another drawback of current personal aircraft designs is that they are generally powered using complex, aircraft-type engine structures which require expensive and highly volatile aircraft fuel for operation. These engines are also loud which makes use of these aircraft in populated areas very inefficient.

There is therefore a need for a single passenger aircraft that is more practical in use than past designs.

SUMMARY OF THE INVENTION

The aforementioned needs are satisfied by the present invention which relates to an aircraft which is configured to accommodate a single passenger. The aircraft is comprised of an airframe that supports the passenger in an upright position. The airframe advantageously maintains the pilot in the same upright orientation during both take-off and landing and during flight. This increases the comfort level of the

pilot during operation of the aircraft and provides an advantageously unobstructed field of vision. The single passenger aircraft is stable during flight and relatively compact in size to reduce the amount of required storage space when the aircraft is not in use. Additionally, because the aircraft is a vertical take-off and landing craft, it does not require large amounts of take-off and landing space.

In a preferred embodiment, a pair of propulsion devices, such as high-powered fan units, are attached to the airframe above the level of the pilot for providing lift and propulsion to the aircraft. The propulsion devices are desirably configured to be tilted to vary the direction of thrust to thereby control the aircraft during flight. Preferably, a single engine is mounted on the airframe for driving the propulsion devices via a powertrain system comprised of a drive shaft that extends along the body line of the pilot. The engine is desirably disposed on the airframe behind and slightly below the level of the pilot for facilitating a centered and relatively low center of gravity position.

The aircraft also includes a control and stability system preferably comprised of a set of hand-operated control devices that allow the pilot to vary the orientation and power of the propulsion devices. In one embodiment, the control device comprises a main control bar that may be raised or lowered to collectively tilt the propulsion devices. A pair of small hand controls are mounted on the main control bar for providing additional control over the propulsion devices. One of the hand controls is preferably used for both collectively and differentially tilting the fan units to thereby vary the direction of thrust and control the direction of flight. The other hand grip desirably controls the engine throttle. Desirably, the pilot may shift his or her weight port or starboard to induce moments on the aircraft and thereby provide additional control over the aircraft.

The aircraft takes-off and lands vertically to eliminate the need for landing strips. Additionally, the airframe has a relatively small footprint so that ground storage space is minimized. The aforementioned features combine to make the aircraft practical for everyday use.

In one aspect of the invention, there is disclosed a single passenger, vertical take-off and landing aircraft, comprising an airframe configured to support a pilot in an upright position, the airframe being symmetric about a medial plane; a pair of propulsion devices mounted on an upper end of the airframe above the pilot, the propulsion devices each being rotatable about a common axis of rotation; an engine mounted on the airframe adjacent the pilot, the engine being drivably coupled to each of the propulsion devices; and a movable control arm on the airframe, the control arm being mechanically coupled to the propulsion devices so that the propulsion devices rotate about the common axis in response to movement of the control arm.

The aircraft is a convenient and safe means of transporting a single passenger between locations. The single passenger aircraft is stable during flight and extremely compact in size so that the aircraft footprint and the necessary amount of ground storage space is minimal. The natural, upright position of the pilot during flight and small level of take-off and landing space make the aircraft ideal for day-to-day use.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other features of the invention will now be described with reference to the drawings of a preferred embodiment, which are intended to illustrate and not to limit the invention, and in which:

FIG. 1 is a front elevational view of the aircraft of the present invention;

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FIG. 2 is a port side elevational view of the aircraft of the present invention;

FIG. 3 is a front elevational view of the airframe of the aircraft;

FIG. 4 is a port side elevational view of the airframe;

FIG. 5 is a rear elevational view of the airframe;

FIG. 6 is a cross-sectional view of the airframe along line 6—6 of FIG. 3 with the pilot superimposed thereon;

FIG. 7 is a front elevational view of a front leg of the aircraft;

FIG. 8 is a top plan view of the aircraft;

FIG. 9 is a top plan view of a single fan assembly of the aircraft;

FIG. 10 is a cross-sectional view of the fan assembly of FIG. 9;

FIG. 11 is a cross-sectional view of a fan blade of the fan assembly;

FIG. 12 is a front elevational view of a powertrain system of the aircraft;

FIG. 13 is a side elevational view of the powertrain system of FIG. 12;

FIG. 13A is a schematic front view of the aircraft showing the aircraft dihedral effect that occurs during flight;

FIG. 14 is a side elevational view of the engine used to power the aircraft;

FIG. 15 is a side elevational view of an oil tank and fuel tank used with the aircraft;

FIG. 16 is a front elevational view of the aircraft showing various components of the control and stability system;

FIG. 17 is a port side elevational view of the aircraft;

FIG. 18 is a starboard side elevational view of the aircraft;

FIG. 19 is a front elevational view of a control stick used with the aircraft; and

FIG. 20 is a cross-sectional view of a control arm of the aircraft along line 20—20 of FIG. 17.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

FIGS. 1 and 2 are front and side elevational views, respectively, of an aircraft 30 that is configured to accommodate a single pilot 34. The aircraft 30 takes-off and lands vertically and transitions to forward flight with the pilot 34 supported in a standing, or upright, orientation. Advantageously, the pilot 34 remains in a natural upright position continuously during flight. The weight of the pilot 34 is supported by a compact airframe 32 that stands in an upright position when the aircraft is not in use. Desirably, the pilot 34 controls the aircraft 30 using a combination of ergonomic control mechanisms and weight-shifting of the pilot's torso on the airframe. As described more fully below, the aircraft 30 is powered by an internal combustion engine that is fueled by standard gasoline for ease of use and high reliability.

The aircraft 30 generally comprises a plurality of interlinked systems that are each described in detail below. The aircraft systems include an airframe 32 comprised of a plurality of panels and interconnecting bracketry. A propulsion system is supported by the airframe for providing lift and propulsion. The propulsion system is preferably comprised of a pair of propulsion devices, such as fan assemblies 36a, 36b (referred to collectively as "fan assemblies 36") that are symmetrically disposed on an upper portion of the frame 32 above the pilot 34. A control and stability system com-

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prised of a plurality of hand-operated control mechanisms and linkages is mechanically coupled to the fans 36 for varying the orientation thereof during flight. As best shown in FIG. 2, a powerplant system comprised of an engine 40 is disposed on the frame 32 rearward of the pilot 34 and generally below the torso level of the pilot 34. The aircraft 30 further comprises a powertrain system including a set of drive axles for drivingly coupling the engine 40 to the fan assemblies 36.

The various systems of the aircraft 30 combine to provide the aircraft with a reliable and safe flight profile. The upwardly-extending airframe consumes a relatively small amount of ground area so that the aircraft 30 may be easily stored when not in use. The small size of the aircraft combined with the vertical take-off and landing characteristics make the aircraft ideal for practical or everyday use. Each of the aircraft systems is described in detail in the following sections.

Airframe

FIGS. 3 and 4 are front and port side elevational views, respectively, of the airframe 32 of the aircraft 30 at rest on a flat ground plane 43. FIG. 5 is a rear elevational view of the airframe 32. The airframe 32 generally comprises a plurality of structural panels that are coupled together so as to provide the airframe 32 with a generally "A" shaped profile when viewed from the front. The "A" shape of the airframe 32 provides the aircraft 30 with a compact, solid ground base that reduces the likelihood of the aircraft toppling when parked or during transport. The "A" shape also provides the aircraft 30 with a weight distribution that advantageously positions the aircraft center of gravity 38 at a location that increases the stability of the aircraft 30 during flight, as described more fully below.

The shape of the airframe 32 may be described with respect to a medial plane 42 that extends vertically relative to the ground plane 43 and normal to a plane defined by FIG. 3. The medial plane 42 defines the centerline of the airframe 32 and is generally aligned with the medial plane of the torso of the pilot 34 when positioned on the aircraft 30, as best seen in FIG. 1. The aircraft 30 has a center of gravity ("CG") 38 that is located along the medial plane 42. When the pilot is positioned on the airframe 32, the center of gravity 38 is also located along the medial plane of the pilot's torso when viewed from the front (FIG. 1) and slightly rearward of the pilot's torso when viewed from the side (FIG. 2).

As best shown in FIG. 3, the airframe 32 is preferably configured to be symmetric about the medial plane 42. That is, the portion of the airframe 32 on the starboard outboard side of the medial plane 42 is a mirror image of the portion of the airframe on the port outboard side of the medial plane 42. As used herein, the term "outboard" refers to a direction moving perpendicularly away from the medial plane 42. The term "inboard" refers to a direction opposite the outboard direction.

As best shown in FIGS. 3 and 4, the airframe 32 includes a pair of opposed, planar side panels 46a, b (collectively referred to as "side panels 46") that define the outboard peripheral edges of the aircraft 30. The side panels 46 define opposed planes having a space therebetween that gradually reduces in width moving upwardly from the ground plane 43 to thereby provide the aircraft 30 with the generally triangular "A" shape. In the illustrated embodiment, a plurality of irregularly-shaped apertures extend through each of the side panels 46 to allow access therethrough. It will be appreciated, however, that the side panels 46 could also have uninterrupted surfaces. The side panels 46 define a pilot space 47 therebetween along the front portion of the aircraft 30. The pilot space 47 is sized to receive the torso of the pilot 34.

As best shown in FIG. 4, each of the illustrated side panels 46 defines a contoured leading edge 54 and an opposed trailing edge 56. The leading edge 54 includes a forwardly curved lower section 55 that is disposed adjacent the leg of the pilot 34 when the pilot is boarded on the aircraft 30. The leading edge 54 also includes a straight medial section 57 that defines a first axis 58 oriented at an angle relative to the vertical. A straight upper section 59 of the leading edge 54 is oriented at a diagonal relative to the straight medial section 57. The straight upper section 59 defines a second axis 60 that intersects the first axis 58. The first and second axes 58, 60 generally define the position of the aircraft legs and also outline the "A"-shaped profile of the airframe 32 when viewed from the side.

With reference to FIG. 4, the trailing edge 56 of each side panel 56 includes a straight lower section 62 that is opposed to the medial section 57 of the leading edge 54. The trailing edge 56 also includes a straight, forwardly-extending upper section 63 that is opposed to the upper section 59 of the leading edge 54. As mentioned, the side panels 46 are preferably shaped to maintain the "A" shape of the aircraft and to optimally position the center of gravity thereof. As can be seen in FIG. 4, the side panels 46 are desirably shaped to extend farther in the rearward direction than in the forward direction with respect to the intersection point between the first and second axes 58 and 60. The rearward weight distribution of the side panels counterbalances the weight of the pilot 34 when the pilot 34 boards the aircraft 30. The resulting position of the center of gravity 38 is generally near the midway point of the side profile of the aircraft, as can be seen in FIG. 2.

As best shown in FIG. 4, the upper edges of the side panels 46 are rounded so as to define a generally semi-circular seat 64 that is sized to receive and support thereon a transverse or secondary drive axle of the powertrain system.

With reference to FIGS. 4 and 5, the airframe 32 further includes a rear or trailing panel 70 that is fixedly mounted between the side panels 46. As best shown in FIG. 5, the trailing panel 70 has triangular-shape so as to fit snug between the side panels 46 and structurally maintain the "A" shape of the airframe 32. The trailing panel 70 is preferably oriented at an angle to the vertical and aligned with the second axis 60. In the illustrated embodiment, the trailing panel 70 includes a plurality of apertures extending therethrough to allow access and visibility therethrough. However, the trailing panel 70 could also define an uninterrupted surface.

As shown in FIGS. 3 and 4, the airframe 32 further comprises a flat front panel 72 that is mounted between the side panels 46 and forwardly-opposed to the rear panel 70. The front panel 72 is generally triangular-shaped so as to fit snug between the side panels 56 and to structurally support the relative positions of the side panels 56. As best shown in FIG. 4, the front panel 72 lies in a plane that is disposed at an angle relative to a plane defined by the rear panel 70. The front panel 82 is also aligned with the first axis 58.

As shown in FIG. 4, the front panel 72 and the opposed rear panel 70 define a triangular hollow volume or space therebetween. A pair of transverse support panels 82a,b are preferably mounted in the space between the front panel 72 and the rear panel 70. The support panels 82a, 82b are disposed in a horizontal orientation relative to the ground plane 43 and provide structural stability to the airframe 32. The support panels 82 are preferably used as support surfaces for storage of various devices within the airframe 32. For example, in a preferred embodiment, a battery for the

engine 40 may be positioned atop the support panel 82a. An opening may be provided in either the front or rear panels 72, 70 for providing access to the storage space. In the embodiment shown in FIG. 3, an elongated door 86 is pivotably mounted on the front panel 72 so as to provide access to the space between the support panels 82a, 82b.

With reference to FIGS. 3 and 4, a back support panel 74 is disposed forward of the front panel 72 and generally rearward of the location where the torso of the pilot is positioned during flight. In the illustrated embodiment, the back support panel 74 is disposed in a vertical orientation relative to the ground plane 43. A transverse support panel 75 is interposed between the top edge of the back support panel 74 and the rear panel 70 for providing structural support therebetween.

FIG. 6 is a cross-sectional view of the aircraft 30 along line 6—6 of FIG. 3 with an outline of the pilot 34 superimposed thereover. The back support panel 72 defines a flat front surface 76. A back support member, such as a cushion 80, is preferably mounted on the front surface 76 of the back support panel 72. The cushion 80 is preferably disposed rearward of the pilot's torso and is configured to provide support thereto during operation of the aircraft 30. For ease of illustration, the cushion 80 is shown having a flat, planar shape. However, those skilled in the art will appreciate that the cushion 80 may take on any of a wide variety of shapes and sizes that are configured to provide various degrees of support and comfort to the pilot 34.

As shown in FIG. 6, the cushion 80 is preferably coupled to at least one bracket 81. Each of the brackets 81 is elongated and extends in the inboard-outboard direction on the support panel 72. Preferably, the cushion 80 is configured to slidably move along the length of the brackets 81. The pilot 34 may slidably reposition his or her torso relative to the airframe 32 by exerting directional pressure on the cushion 80 and sliding the cushion along the brackets 81. The pilot 34 may control the aircraft 30 by shifting his or her weight using the movable cushion 80, as described in more detail below.

As shown in FIGS. 3 and 4, a pair of struts 87 preferably extend between the bottom end of the rear panel 70 and the side panels 56. The struts 87 provide additional structural support and stability to the airframe 32.

With reference to FIGS. 3 and 4, the airframe 30 preferably includes a leg support system comprised of a pair of front legs 48a,b (collectively "front legs 48") and a rear leg 52 that are disposed on the bottom of the airframe 32 in a tripod configuration. The front legs 48a,b extend downwardly from each of the leading edges 54 of the side panels 46a,b, respectively. As best shown in FIG. 3, the outboard edge of each of the front legs 48a,b is disposed substantially flush with or adjacent a plane defined by the respective side panel 46a,b so as to maintain the "A"-shaped profile of the aircraft 30. The front legs 48 define an angle β therebetween, which is preferably approximately 20–30 degrees. Additionally, as best shown in FIG. 4, each of the front legs 48a,b is positioned substantially adjacent with the first axis 58 defined by the leading edges 54 of the side panels 46a,b. A wheel 50 is preferably rotatably mounted on a bottom end of each of the front legs 48.

A single rear leg 52 extends downwardly from the rear panel 70 of the airframe 32. The rear leg 52 is preferably mounted on the inner surface of the rear panel 70 via a set of brackets. In the articulated embodiment, the rear leg 52 has a straight, elongated upper portion and a rearwardly-curved or rounded bottom portion that abuts the ground plane 43 when the aircraft 30 is at rest. The rounded bottom

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portion of the rear leg 52 anchors the position of the aircraft 30 when at rest. However, the rear leg 52 could also be equipped with a wheel in the same manner as the front legs 48. As best shown in FIG. 3, the rear leg 52 is aligned with the medial plane 42 so that the weight distribution of the airframe 32 is symmetric about the rear leg 52. With reference to FIG. 4, the rear leg 52 is also axially aligned with the second axis 60 so that the front and rear legs 48, 52 define an angle θ therebetween. In one embodiment, the angle θ is approximately 30–40 degrees.

FIG. 7 is cross-sectional front view of the port front leg 48b of the aircraft 30. The starboard front leg 48a is a mirror image of the port front leg 48b. The front leg 48 is preferably attached to an inboard surface of the side panel 46 using a plurality of clamps or mounts 91. The wheel 80 is preferably mounted on a rotatable shaft 91 that extends through a bottom end of the front leg 48. Each of the front legs 48 comprises a pair of generally hollow tubular members that are telescopically coupled to one another. Accordingly, one of the tubular members may be moved relative to the other tubular member to provide shock absorbing capabilities thereto when the legs 48 impact a surface. Toward this end, a gas spring 92 (shown in phantom lines) is preferably mounted within each of the front legs 48 to absorb loads thereon during takeoff and landing of the aircraft 30. The rear leg 52 is preferably also fitted with a gas spring in a similar manner.

With reference to FIG. 7, a foot rest 90 is mounted near a bottom end of each of the front legs 48. The foot rest 90 comprises a plate that defines a substantially flat, elongated surface that is sized and shaped to support the foot of the pilot 34 during flight. Preferably, the foot rest 90 is adjustably mounted on the front legs 48b to allow the vertical location of the foot rests 90 to be optimized for pilots of various heights. The starboard leg 48b is preferably also equipped with a foot rest 90.

In a preferred embodiment, a leg fairing 96 (FIG. 1) is attached to the side panels 46 of the airframe 32. The leg fairing 96 is preferably contoured so as to wrap around the airframe and to provide a smoothing shape to the aircraft 30 for reducing drag thereon. In the illustrated embodiment, the leg fairing 96 comprises an elongated structure having a pair of rounded leg sections 97 that are positioned adjacent the side panels 46. Each leg section 97 has a curved leading edge that slopes downwardly toward the lower end of the front legs 48 and a trailing edge that slopes upwardly toward the trailing edge of the side panels 46. As best shown in FIG. 1, the leg sections 97 of the fairings 96 flair outwardly away from the medial plane 42 of the aircraft 30. The fairing 96 may take on other shapes to vary the drag profile of the aircraft 30. Fairings may also be mounted on other locations of the airframe 30.

As mentioned, the airframe 32 is advantageously configured to support the pilot 34 in an upright or standing position. The pilot 34 boards the aircraft 34 by placing his or her feet upon the footrests 90 and positioning his or her torso in the passenger space 47. The rear torso of the pilot 34 is preferably positioned adjacent the cushion 80 on the back support panel 74. Advantageously, the tripod configuration of the front and rear legs 48, 52 provide a stable support structure for the aircraft 30 to reduce the risk of the aircraft 30 toppling during transport, take-off or landing. As mentioned, the weight of the pilot 34 counterbalances the weight distribution of the airframe 32 so that the center of gravity 38 is located at or near the midpoint of the front to rear dimension of the aircraft 30.

The airframe 32 is preferably configured to accommodate a pilot in the 95 percentile range of heights. The adjustable

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footrests 90 allow the pilot 34 to be positioned on the airframe 32 with his or her torso at the same position relative to the cushion 80 regardless of the height of the pilot 34. Because the control mechanisms of the aircraft 30 are also positioned relative to the cushion, the pilot's torso is always in the same location relative to the control mechanisms regardless of the height of the pilot.

The aircraft 30 is preferably sized to support an average sized human. In one embodiment, the aircraft is approximately 94 inches tall. There is a distance of approximately 102 inches between the starboard and port peripheral edges of the fan ducts 100. The aircraft 30 is approximately 19 inches deep from front to rear.

The airframe 32 is preferably manufactured of a lightweight material that is suitably strong to support the air loads that the aircraft experiences during flight. In one embodiment, the planar structural members of the airframe 30, such as the side panels 46, are comprised of a honeycomb material. The interconnecting bracketry that connect the structural members to one another is preferably manufactured of titanium, aluminum, or combinations thereof. Additional structural components may be made of aircraft grade aluminum tubing and various machined and welded aluminum parts. The fairings may be made of carbon, Kevlar, or low density foam cores or combinations thereof.

Propulsion System

FIG. 8 is a top plan view of the aircraft 30 showing the aircraft propulsion system which in a preferred embodiment comprises a pair of rotary fan assemblies 36a,b (collectively referred to as "fan assemblies 36") that are rotatably mounted on the top end of the aircraft 30. The fan assemblies 36 are desirably mounted on opposite outboard sides of the medial plane 42 such that the fan assemblies 36 are positioned symmetrically thereabout. In a default position, the fan assemblies 36 are positioned to spin within a common, horizontal plane. However, the fan assemblies may be collectively or differentially tilted about a common axis 99 to vary the direction of thrust and thereby control the aircraft during flight. The axis 99 is positioned directly above the center of gravity 38 so that the fan assemblies do not generate a moment thereabout when the fan assemblies are in the default position.

FIGS. 9 and 10 are top plan and cross-sectional views, respectively, of the starboard fan assembly 36a, which is a mirror of the port fan assembly 36b. The following description of the starboard fan assembly 36a is therefore also applicable to the port fan assembly 36b. The fan assembly 36a comprises an annular fan duct 100 and a fan 102 rotatably mounted therein. A pair of radially-extending struts 103 and tubular housing 148a (FIG. 12) couple the fan duct 100 to an outboard gear box 104a (FIG. 10) that is disposed below the centerpoint of the fan duct 100. As best shown in FIG. 10, the fan duct 100 has a cross-sectional shape corresponding to the shape of an airfoil. This reduces drag on the fan assembly 100 during flight and also reduces the amount of noise generated by the fans 102. The shape of the fan ducts 100 also increases the efficiency of the fans 102. The airfoil shape creates a low pressure region at the upper tips of the fan ducts 100 which causes the fans 102 to produce more thrust during operation.

The fans 102 preferably each spin in an opposite rotational directions during operation of the aircraft 30. Because the fans 102 are disposed symmetrically with respect to the medial plane, the opposite spin directions of the fans 100 advantageously result in a zero net torque by the fans 102 on the aircraft 30 and no net gyroscopic effect by the fans 102.

Each fan 102 preferably comprises a set of fan blades 106 that extend radially outward from a central fan hub 110. The

fan hub **110** is mounted atop the outboard gear box **104a** and is coupled to the powertrain system through the outboard gear box **104a**, as described in detail below. In the illustrated embodiment, the fan **102** includes seven fan blades **106** that extend radially outward from the fan hub **110** and each fan blade **106** is spaced from an adjacent fan blade by an equal angular distance of approximately 51° .

The fans **102** are configured to spin within the fan hubs **110** to thereby generate a propulsion force in a direction parallel to the spinning axis of the fans **102**. Toward this end, each of the fan blades **106** has a cross-sectional shape that is selected to generate an airflow when the fans **102** spin. FIG. **11** is a cross-sectional view of a fan blade **106** at the location where the blade **106** is mounted to the fan hub **110**. Each fan blade **106** has a chord length L and a pitch angle ϕ . In a preferred embodiment, the chord length L is approximately 3.5 inches and the pitch angle ϕ is approximately 24° at the location where the fan blade **106** is mounted to the fan hub **110**. The fan blade **106** then gradually transitions to a chord length L of approximately 2 inches and a pitch angle ϕ of approximately 7° moving radially outward from the fan hub **110**. The fan **102** preferably has a radius of approximately 19 inches from the center of the fan hub **110** to the tip of the fan blade **106**.

The fan blades **106** preferably have a fixed pitch. This increases the reliability of the fans **102** by reducing the number of moving parts thereon with respect to variable-pitch fans. The pitch of the fan blades **106** is preferably nominally optimized for an operational range between cruise and hover.

The fan duct **100** defines an inner diameter that is larger than the diameter of the fan **102**. Preferably, there is approximately a 0.030 inch radial clearance between the inner surface of the fan duct **100** and the outer radial tip of the fan blades **106**. As shown in FIG. **10**, an annular strip **101** of material is located on or within the inner radial surface of the duct **100** along the periphery of the fan blades **106**. The strip **101** is desirably positioned where the outer radial tip of the fan blades spins nearest the fan duct **100**. That is, the strip **101** is located in the same plane in which the tips of the fan blades **106** rotate.

The clearance distance between the fan blades **106** and the inner surface of the fan ducts is preferably as small as possible to increase the efficiency of the fan **102**. However, a smaller clearance introduces a greater risk that the fan blades **106** will collide with the duct **100** if the duct **100** is deformed. Advantageously, the strip **101** preferably comprises a relatively soft material, such as balsa wood, that will deform if contacted by the tips of the fan blades **106**. The strip **101** will therefore not impede rotation of the fan blades **106** if the blades **106** collide with the duct **100**. The strip **101** desirably has a radial thickness of approximately 0.25 inch so that it comprises merely a small portion of the duct **100**.

The fan blades **106** are preferably manufactured of a material configured to withstand air loads generated during propulsion of the aircraft **30**. In a preferred embodiment, the fan blades **106** are made of a robust chopped-fiber reinforced nylon which is not affected by UV radiation. Such a material is capable of absorbing traumatic events that may occur during flight, such as impact with birds and other objects, without failing catastrophically. The fan ducts **100** may be manufactured of a composite material, such as carbon-Kevlar disposed over a foam core.

As best shown in FIGS. **1** and **2**, a preferred embodiment of the aircraft **30** includes a rounded centerbody **112** that extends over and under the fan hub **110** of the fan assembly **36**. The centerbody **112** is circular when viewed from the top

and are substantially ovoid when viewed from the side. The centerbodies **112** increase the aerodynamic efficiency of the aircraft **30**.

The fans **102** preferably normally operate at a rotational rate in the range of approximately 4,400 RPM to 5,500 RPM. These rotational speeds maintain the outer tips of the fan blades **106** below the sonic range. Such a range of operation produces sufficient propulsion while also producing relatively low noise levels. The fans **102** preferably generate a collective lift of at least approximately 900 pounds at maximum rotational speeds.

Powertrain System and Powerplant Systems

FIGS. **12** and **13** are front and side elevational views, respectively, of the aircraft powertrain system which comprises a set of drive shafts that drivingly couple the engine **40** to the fan assemblies **36**. The powertrain system preferably includes a main drive shaft **122** that is directly coupled at a bottom end to the engine **40** (FIG. **13**). A pair of starboard and port secondary drive shafts **124a,b** (collectively "secondary drive shafts **124**") are disposed transverse to the main drive shaft **122** and drivingly coupled thereto via a central gear box **126**. The secondary drive shafts **124** drivingly couple the main drive shaft **122** to the starboard and port fan assemblies **36a,b** via a pair of starboard and port outboard gear boxes **104a,b**, respectively. The secondary drive shafts **124** are co-axially aligned with the tilting axis **99** of the fan assemblies **36**.

With reference to FIGS. **12** and **13**, the main drive shaft **122** is connected at a first end to the engine **40** (FIG. **13**) and at a second end to the central gear box **126** that is disposed at the upper end of the airframe **30**. In the illustrated embodiment, the main drive shaft **122** is comprised of several components including an elongated torque tube **127** having universal joints **128** mounted on opposite ends thereof. The universal joints **128** couple the torque tube **127** to a pair of shafts **130a,b** (collectively referred to as "shafts **130**") on either end of the torque tube **127**. The shaft **130a** is drivingly attached to a gear assembly within the central gear box **126**, as described more fully below. The shaft **130b** on the bottom end of the torque tube **127** is drivingly attached to an output shaft of the engine **40**. A standard SAE spline assembly is preferably used to couple the shafts **130** and the torque tube **127** to the universal joint **128**. In a preferred embodiment, the universal joints **128** operate at a zero offset angle. However, the universal joints **128** may also operate at small angles produced by air loads during flight.

As best shown in the front view of FIG. **12**, the main drive shaft **122** defines an axis that is preferably disposed within the medial plane **42** of the aircraft **30**. As mentioned above, the aircraft center of gravity **38** is also disposed within the medial plane **42**. With reference now to the side view of FIG. **13**, the main drive shaft **122** is further oriented such that an axis defined by the main drive shaft **122** is disposed at an angle relative to the vertical. In a preferred embodiment, the main drive shaft **122** is disposed in a parallel relationship with the second axis **60** defined by the leading edges **54** of the airframe side panels **46**. The main drive shaft **122** is therefore also positioned in a generally parallel relationship with the rear leg **52** (FIG. **4**).

As mentioned, the airframe **32** has a rearward weight distribution that counterbalances the weight of the pilot **34** when the pilot **34** boards the aircraft **30** so that the center of gravity is positioned generally midway of the front to rear dimension of the aircraft **30**. The aforementioned orientation of the main drive shaft **122** is selected to evenly distribute the weight of the powertrain system between the front and rear of the aircraft **30**. The front-to-rear angled orientation of

the main drive shaft **122** allows the engine **40** to be mounted toward the rear of the aircraft **30**, which counterbalances the weight of the forwardly-positioned pilot **34**. The fans **102** are positioned directly over the center of gravity.

With reference again to FIGS. **12** and **13**, the central gear box **126** comprises a central housing **131** having a pair of opposed apertures **132** on outboard sides thereof. A central aperture **134** extends through a bottom side of the central housing **131** for receipt of the main drive shaft **122**. The central housing **131** encloses a gear assembly **136** comprised of a pair of spiral bevel gears **137a,b** that are mounted in a meshed relationship with one another and are preferably configured to rotate along axes that are disposed in a perpendicular relationship. The upper end of the main drive shaft **122** is coupled to the bevel gear **137a** for driving the bevel gear assembly **136**. The dual bevel gear configuration preferably provides a 1:1 power transfer ratio between the gears **137a,b**, which provides for an efficient and reliable operation. It will be appreciated, however, that the number and types of gear configurations may be varied within the central gear box **126**.

With reference to FIG. **13**, at least one inspection or breather plug **139** is preferably removably mounted on the central housing **131** of the central gear box **126**. The breather plug **139** may be removed to provide maintenance personnel with inspection access to the internal gear assembly **136**, such as through the use of a borescope. Furthermore, the central gear box **126** is preferably equipped with oil chip and temperature sensors (not shown), as will be known to those skilled in the art. Such sensors provide early warning of pending or developing temperature or friction problems. The gear box **126** may also be equipped with vibration detectors to provide early warning of undesired vibration, such as vibration above a threshold value.

With reference again to FIG. **12**, the secondary drive shafts **124** are transversely disposed with respect to the main drive shaft **122**. That is, the secondary drive shafts **124** extend in an outboard direction away from the medial plane **42** and toward the outboard gear boxes **104a,b**. Preferably, the secondary drive shafts **124a,b** are each coupled at inboard ends to a co-axial central shaft **140** via pair of universal joints **142**. The central shaft **140** extends through the central gear box **126** through the outboard apertures **132**. The central shaft **140** is coupled to the bevel gear **137b** so that the bevel gear **137b** rotatably drives both the central shaft **140** and the attached secondary drive shafts **124**. As mentioned above with respect to the main drive shaft **122**, the universal joints preferably operate at a zero offset angle, although they may be configured to reliably operate at angles of relatively small values.

With reference to FIG. **12**, the starboard and port outboard gear boxes **104a,b** are disposed on starboard and port outboard ends of the secondary drive shafts **124a,b**, respectively, and below the fan assemblies **36**. The outboard gear boxes **104** each comprise a box-like outer housing **138** having an inboard aperture dimensioned to receive the secondary drive shafts **124** therethrough. A bevel gear assembly **144** comprised of a pair of coupled bevel gears **145a,b** is disposed within each of the outboard gear boxes **104**. The gear assembly **144** is preferably configured similarly to the central gear assembly **136** in that the rotational axes of the gears **145a,b** are disposed normal to one another. The bevel gears **145a** are drivingly coupled to the secondary drive shafts **124** through a spline assembly. Each of the bevel gears **145b** also is drivingly coupled to an upwardly extending fan shaft **146** that drives each of the fan assemblies **36**. The gear assemblies preferably transfer rotational power

from the secondary drive shafts **124** to the fan shafts **146** according to a 1:1 power transfer ratio.

With reference to FIG. **13**, the secondary drive shafts **124** are preferably enclosed by a pair of starboard and port elongate, tubular housings **148a,b** (collectively referred to as "tubular housings **148**"). The outboard ends of the tubular housings **148** are rigidly connected to the outer gear housings **138**. The tubular housings **148** are preferably journaled within the central gear box **126** via a pair of annular bearing assemblies **150**. The bearing assemblies **150** allow the tubular housings to be rotated about the axis **99** when a torque is applied. The outer gear housings **138** and the attached fan assemblies **36** also rotate or tilt about the axis **99** when the tubular housings are rotated. The fan assemblies **36** may thus be reoriented by rotating the tubular housings **148** to thereby tilt the fan assemblies **36** about the transverse axis **99** and provide directional control of the aircraft during flight.

The tubular housings **148** and the gear box housings **131, 138** collectively comprise a housing assembly for the secondary drive shafts **124** of the aircraft powertrain system. The housing assembly is preferably entirely supported by the airframe **32** via the seats **64** on the side panels **46** and a pair of struts **151** that connect the side panels **46** to a pair of rigid flanges **149**. Advantageously, the housing assembly **128** and the airframe **32** effectively support all airloads and lifting loads on the aircraft **30** so that the main and secondary drives shafts **122, 124** do not experience any airloads or lifting loads during flight. The housing assembly is desirably manufactured of a high-strength material configured to withstand the airloads and lifting loads generated during flight, such as titanium, aluminum, or combinations thereof.

The main and secondary drive shafts **122, 124** are preferably manufactured of a material that is configured to withstand the operational loads. Applicant has observed that woven carbon-Kevlar is a suitable material for the drive shafts. In a preferred embodiment, the ratio of Kevlar to carbon is optimized to provide the drive shafts with load absorbing capabilities such that the shafts absorb engine pulses and such pulses are not transferred to the gear boxes. This reduces wear on the gear mechanisms to improve the reliability of the aircraft. The use of a composite material allows for the use of components of reduced weight and mass, such as small-diameter drive shafts, with low moments of inertia. The components of the drive train system are less resistant to changes in rotation to provide for quick throttle response.

With reference to FIG. **12**, the outer and central gear boxes **104, 126** preferably each utilize a unique gear assembly system that facilitates adjustment of the backlash between the gears. The gear assembly systems will be described with respect to the gear **137b** of the central gear box **126**, although it is preferably utilized in each of the gear boxes **104, 126**. The bearing assembly **150** preferably comprise a pair of bearings that are journaled within a disk or end plate **153** that is threaded into the gear box housing **130**. The bearing assembly **150** is in turn coupled to the central shaft **140** to relative sliding movement therebetween along the axis of the central shaft **140**. The gear **137b** is also fixedly mounted to the central shaft **140**, such as through a press-fit. The end plate **153**, bearing assembly **150**, central shaft **140**, and gear **137b** are thus coupled to one another in a manner that allows the components to rotate relative to one another but prohibits the components from sliding relative to one another in a direction parallel to the axis of the shaft **140**. Translation of the gear **137b** in a direction parallel to the axis of the central shaft **140** is therefore directly coupled to

translation of the end plate **153**. As the end plate **153** moves into or out of the housing **130**, the gear **137b** also moves with the end plate **153** in a direction parallel to the axis of the central shaft **140**.

The movement of the gear **137b** may be calibrated with respect to the threaded rotation of the endplate **153** so that the position of the gear **137b** relative to the gear **137a** may be adjusted a predetermined distance by turning the endplate **153**. An operator may adjust the relative positions of the gears **137**, and the resulting gear backlash, by simply rotating the endplate **153**. Preferably, each gear in the gear assemblies of the aircraft utilize the configuration described above. In a preferred embodiment, each radian (or fractional portion thereof) of rotation of the endplate moves the gear by approximately 0.002 inch.

FIG. **13a** is a schematic front view of the aircraft **30**. When the aircraft **30** is not in operation, the tubular housings **148** are preferably oriented relative to the airframe **32** such that the tubular housings **148a** and **148b** are aligned along a common axis and exhibit no dihedral. The tubular housings **148** are preferably slightly flexible so they bend when the fan assemblies produce lift as shown in phantom lines. The tubular housings **148a** and **148b** thus provide dihedral with respect to one another when the aircraft **30** is in flight, which improves the lateral stability of the aircraft.

With reference now to FIG. **14**, there is shown an enlarged side plan view of the powerplant system of the aircraft **30**. In a preferred embodiment, the powerplant system comprises an internal combustion engine **40** having an output drive shaft **156** that is coupled to the main drive shaft **122** of the powertrain system using an SAE spline connection to provide power thereto. As best shown in FIGS. **2** and **14**, the engine **40** is preferably mounted on the airframe **32** just rearward of the rear panel **70** and between the side panels **46**. The engine **40** is preferably positioned slightly below the torso level of the pilot. Desirably, the engine **40** is positioned in a generally offset vertical orientation such that the output drive shaft **156** is aligned in a parallel relationship with the second axis **60**.

Preferably, the engine **40** is directly coupled to the main drive shaft **122** without the use of a clutch therebetween. The fans **102** thus begin to spin as soon as the engine is activated. When the engine **40** is not operating, the level of play in rotation of the fans **102** is proportional to the level of backlash in the gear assemblies **136**, **144**. The pilot **34** may easily monitor the drivetrain system by attempting to spin the fans **102** when the engine is off. If the play in the fans **102** is excessive then there may be excessive wear in the drivetrain.

In a preferred embodiment, the engine **40** comprises a four cylinder, two cycle engine that is nominally rated at approximately 120–130 horsepower. Two spark plugs and one or more electronically-operated fuel injectors are preferably coupled to each cylinder of the engine **40**. The engine **40** also preferably includes dual CDI ignitions and dual electronics spark-advance timing, and dual electronic fuel pumps that feed each of the fuel injectors. Each of the electronic fuel pumps are preferably coupled to one of a pair of fuel manifolds and the fuel tank. A pair of primary and secondary exhaust manifolds are also coupled to the engine **40**. In one embodiment, the engine weighs approximately 124 pounds and produces approximately 1 horsepower per pound. The aforementioned engine **40** preferably uses a mixture of standard automobile gasoline fuel and synthetic oil or mineral oil. Applicant has determined that a 100:1 ratio mixture of gasoline to synthetic oil is a suitable mixture for the engine **40**. A 50:1 ratio mixture of gasoline to mineral oil is also a suitable mixture for the engine **40**.

FIG. **15** shows a side elevational view of a preferred fuel supply system that is used with the aircraft **30**. The system comprises at least one fuel tank **172** and one oil tank **176**. Preferably, the fuel tank **172** and the oil tank **176** are mounted to the airframe **32** above the engine **40** and behind the pilot's head. The oil tank **176** is preferably coupled to the fuel tank **172** via an oil line comprised of a flow tube **178** that provides a passageway for oil to flow from the oil tank **176** into the fuel tank **172** via a gravity feed. A valve **180** is preferably mounted along the flow tube **178** to allow an operator to control the flow of oil into the fuel tank **172**. Additionally, a filter, such as a permeable membrane, is preferably mounted along the flow tube to intercept any undesired particulates in the oil.

In a preferred embodiment, the fuel tank **172** comprises a transparent container **182** having a plurality of graduated markings **184** thereon. The markings **184** are positioned on the container **182** to indicate the current volume of fuel remaining within the container **182**. Desirably, a second set of markings **184** are configured to indicate the volume of fuel required to completely fill the container **182**. For example, if the container **182** holds one gallon of fuel, the fuel level within the container **182** will be located at a marking **184** which indicates "1 gallon." For a 10 gallon tank, the fuel level is also located at "9 gallons" for the second set of markings, indicating that 9 gallons of fuel are required to completely fill the container **182**. The position of the markings **184** on the container **182** may be determined through routine experimentation. The markings **184** are preferably divided into even increments of volumetric fuel levels, although the increments may vary widely. Additionally, the particular units of fuel volume could also vary.

The oil tank **176** preferably comprises a transparent container **186** having graduated markings **188** thereon. The markings **188** are preferably arranged to indicate the current volume of oil within the containers **186** in the manner described above with respect to the fuel tank **172**.

The mixing of the gas and oil is preferably performed during refueling, which is advantageously facilitated by using the transparent fuel and oil tanks **172**, **176** and the graduated markings **184**, **188** thereon. An operator may easily determine the volume of fuel necessary to fill the fuel tank **172** by reading the second set of graduated markings **184**. The operator then opens the valve in the flow tube **178** to allow oil to flow into the fuel tank **172**. The particular volume of oil to be transferred is dependent upon the remaining volume of fuel in the fuel tank **172**. Advantageously, the volume of oil released from the oil tank **176** may be monitored using the graduated markings **188**. After the desired amount of oil is added, the fuel tank **172** is then filled with fuel.

In operation, the engine **40** is activated so that it transfers power to the main drive shaft **122** of the powertrain system via the engine output shaft **156**. As mentioned, the main drive shaft **122** is coupled at one end to the bevel gear **137a** of the central gear assembly. The central gear assembly **136** transfers power from the main drive shaft **122** to the secondary drive shafts **124**, which are drivingly coupled to the gears **145a** of the outboard gear assemblies **144**. The fan shafts **146** are then driven by the outboard gear assemblies **144** so that the fans **102** begin to spin. The rotational speed of the fans **102** is controlled by varying the throttle level of the engine **40**. Upon spinning of the fans **102**, the fan assemblies **36** generate a thrust force that provides lift to the aircraft. As described below, the direction of fan thrust may be varied to control the aircraft during flight.

Control and Stability System

FIG. 16 is a front elevational view of the aircraft 30 showing various components of the control and stability system. FIGS. 17 and 18 are port and starboard side elevational views, respectively, of the aircraft 30. Preferably, the control and stability system provides the pilot 34 with three-axis translational control and two-axis attitude control over the aircraft 30 during flight. The three-axes translational control pertains to the forward/backward directions, the starboard and port lateral directions, and the upward/downward directions. The two-axes attitude control pertains to roll and yaw.

Forward and backward translational control of the aircraft 30 is preferably accomplished by collectively tilting the fan assemblies 36 in a forward or backward direction. Lateral translation of the aircraft 30 is preferably achieved by inducing a rolling moment to the airframe 32 through weight-shifting of the pilot. Vertical translation is preferably achieved by varying the engine throttle. Roll control is preferably achieved by shifting the pilot's weight on the airframe. Lastly, aircraft yaw is preferably achieved by differentially tilting the fan assemblies 36. The pilot 34 may easily accomplish these functions by shifting his or her weight and manipulating the main control member 190 and/or the hand control mechanisms 196, 198, as described more fully below.

With reference to FIG. 16, the control and stability system preferably comprises a u-shaped tubular main control member 190 and a plurality of control linkages attached thereto that mechanically couple the main control member 190 to the fan assemblies 36. Preferably, the pilot 34 may vary the orientation of the fan assemblies 36 by lifting and/or lowering the main control member 190, as described more fully below. A set of starboard and port-side control mechanisms 196 and 198, respectively, are mounted near opposite ends of the main control member 190 for providing additional control over the orientation of the fan assemblies 36 and over the level of engine throttle, as described more fully below.

With reference to FIGS. 16-18, the main control member 190 comprises an elongated, contoured tube having two bends that form opposed starboard and port arms 192 and 194, respectively, and a straight, elongated connecting section 195 therebetween. The main control member 190 is rotatably coupled to the airframe 32 at a location rearward of the back support panel 74 such that connecting section 195 extends along the outboard direction. As best shown in FIGS. 17 and 18, the starboard and port arms 192, 194 extend forwardly relative to the airframe 32 along opposite sides of the pilot mounting space. The main control member 190 is preferably journaled to be rotatable about an axis extending through the connecting section 195. The main control member 190 may thus be rotated about the connecting section 195 by lowering or lifting the arms 192, 194, as exhibited by the arrows 193 in FIG. 17.

As shown in FIGS. 16-18 a pair of starboard and port elongated push rods or control linkages 197 and 199 are mechanically connected at a lower end to each of the starboard and port arms 192, 194, respectively. The control linkages 197 and 199 are also connected at an upper end to the inboard ends of the starboard and port tubular housings 148a,b, respectively. The control linkages 197, 199 thereby provide a mechanical link between the main control member 190 and the tubular housings 148 that enclose the secondary drive shafts 124. The pilot may provide a torque to the tubular housings 148 by lifting or lowering the starboard and port arms 192, 194, as described in more detail below.

As best shown in FIGS. 17 and 18, a fin or triangular plate 200 extends rearwardly from the starboard and port arms 192, 194. Alternatively, a single plate 200 could extend rearwardly from any location on the main control member 190, such as from the center thereof. Each of the plates 200 has a curved bottom edge 201 that slidably mates with a caliper 202 mounted on each of the side panels 46. The bottom edge 201 of each plate 200 slides within the calipers 202 as the main control member 190 is lifted or lowered. The main control member 190 is lifted or lowered by exerting sufficient force thereon to overcome the friction force between the plate 200 and the calipers 202. In one embodiment, the calipers 202 retain sufficient friction on the plates 200 to maintain the position of the main control member 190 when it is released by the pilot 34.

In another embodiment, the calipers 202 are mechanically coupled to the hand control mechanism 196, 198. In a default state, the calipers 202 maintain a constant friction engagement with the plates 200 to inhibit or prevent movement of the main control member 190. The pilot may manipulate the starboard and/or port side control mechanisms 196 and 198 to release the calipers 202 from engagement with the plates 200 so that the main control member 190 may be moved. This is preferably accomplished by the pilot squeezing a grip on at least one of the control mechanisms 196 or 198, as described more fully below. Alternatively, a single, rather than multiple, plate-caliper may be coupled to one or both of the control mechanisms 196, 198.

Preferably, the calipers 202 or plate 200 include a detent interface therebetween that limits the rotational range of motion of the main control member 190. For example, the caliper and plate interface may prevent the main control member 190 from being pushed downward beyond a predetermined rotational position or pulled upward beyond a predetermined rotational position. This desirably prevents the pilot 34 from inadvertently tilting the fan assemblies 36 to an undesired or unsafe orientation, which may cause the aircraft to accelerate too rapidly or to achieve too great of an airspeed.

With reference to FIGS. 17 and 18, a pair of rate dampeners, such as gas springs 204, are coupled to the main control member 190 for limiting the rate at which the control member 190 may be rotatably moved. In the illustrated embodiment, one end of each gas spring 204 is attached to a bottom edge of each of the starboard and port arms 192, 194. The other end of each gas spring 204 is attached to the respective side panel 46. The gas springs 204 are stretched or compressed as the main control member 190 is lifted or lowered, respectively. Preferably, the gas springs are configured to resist stretching or compressing beyond a predetermined threshold rate to thereby inhibit the pilot from moving the main control member 190 and the fan assemblies 36 too quickly during flight, which may cause the aircraft to accelerate or maneuver at an unsafe rate. Advantageously, the resistance level of the gas springs 204 may be varied to set the resistance to movement of the main control member 190. The behavior of the aircraft 30 may thus be customized for different training situations, such as by making the aircraft 30 more docile or more aggressive depending on the skill level of the pilot.

With reference to FIGS. 16 and 17, the port-side control mechanism 198 comprises a stick 206 and a grip 208 that is pivotably mounted to the upper end of the stick 206. The stick 206 extends upwardly from a forward end of the port arm 194, preferably at a location where the pilot 34 may reach by extending his or her arm. The stick 206 is prefer-

ably coupled to the throttle of the engine **40** in a well known manner, such as, for example, via a throttle cable **209**. The pilot **34** preferably rotates the stick **206** to translate the cable and thereby vary the throttle of the engine **40**. In one embodiment, two complete revolutions of the stick **206** varies the throttle approximately $\pm 4,000$ rpm. The rotational rate of the fan blades **106** increases proportionally as the engine throttle is increased. The pilot may thereby use the portside control mechanism **198** to control the amount of thrust generated by the fan assemblies **36**.

FIG. **20** is a top-down cross-sectional view of a section of the port arm **194** along line **20—20** of FIG. **17**. The aircraft **30** preferably includes a throttle interlock system that is configured to prevent the pilot from accidentally reducing the throttle of the engine below a safe flight level. The throttle interlock system includes a rack and pinion system comprised of a rack **240** and pinion **242** that are coupled to the stick **206**. The pinion **242** is configured to rotate in response to rotation of the stick **206**. As the pinion **242** rotates, it translates the rack **240** over a linear translational path L. The rack **240** is connected at a distal end **243** to the throttle cable **209** so that linear movement of the rack **240** is directly translated into linear movement of the throttle cable **240** along the path L. The throttle level of the engine **40** is a function of the position of the rack **240**. Preferably, the engine throttle is at a minimum level, or “ground throttle,” when the distal end **243** of the rack **240** is fully translated to a location **245** along the path L.

With reference to FIG. **20**, an actuator, such as a levered detent member **244**, is movably coupled to the port arm **194**. The detent member **244** has a first abutment end **246** that may be moved into and out of an engagement relationship with the distal end **243** of the rack **240**, as described below. A second end **250** of the detent member **244** protrudes outwardly from the port arm **194**. The detent member **244** is pivotably mounted to a flight idle adjustment member **252** that may be linearly translated in a direction parallel to the path L through rotation of a knob **256**.

With reference to FIG. **20**, the detent member **244** is movable between an engaged position and a disengaged position. In the engaged position, the abutment end **246** intersects the translational path L of the rack **240** so that the abutment end **246** acts as a detent to inhibit movement of the rack **240** toward the position **245**. Thus, when in the engaged position, the detent member **244** engages with the rack **240** and prevents the engine throttle from being reduced below a certain level. In a non-engaged position (shown in phantom), the abutment end **246** is positioned outside of the translational path L. The knob **256** may be rotated to vary the location at which the abutment end **246** intersects the translational path L of the rack **240**.

At startup of the engine **40**, the detent member is in the disengaged position and the distal end **243** of the rack **240** is at the position **245**, corresponding to ground throttle. As the pilot **34** increases the throttle, the distal end **243** of the rack **240** passes beyond the abutment end **246** of the detent member **244** so that the detent member **244** snaps into the engaged position. The detent member **244** thereby prevents the throttle from being reduced below a predetermined level, referred to herein as the “safe throttle level.”

The safe throttle level preferably corresponds to the minimum throttle at which the fans **102** will provide some percentage (preferably 70%–90%) of lift required to keep the aircraft at hover, which is based on the power characteristics of the aircraft and the pilot’s weight. In one embodiment, the safe throttle level is the particular minimum throttle level sufficient to keep the aircraft **30** at hover

for the particular weight of the pilot. In a preferred embodiment, the knob **256** is provided with markings that correspond to the weight of the pilot. Prior to flight, the pilot **34** sets the knob **256** to his or her weight so that the safe throttle level is set at a calibrated, predetermined RPM value that is configured to provide sufficient lift for the particular weight of the pilot. This system greatly reduces the likelihood of the pilot **34** inadvertently reducing the throttle below a safe level during flight. The pilot **34** may disengage the detent member **244** and override the minimum safe throttle level by inwardly pressing the second end **250** of the detent member **244** to move the detent member to the disengaged position. Advantageously, this requires the pilot to use two hands, one to press the detent member **244** and the other to rotate the distal end **243** of the rack **240** beyond the detent end **246** of the detent member **244**.

The aforementioned throttle system increases the safety of the aircraft **30**. Once the pilot has increased the throttle beyond a certain level and achieved flight, he or she is required to affirmatively actuate the detent member **244** prior to reducing the throttle below the safe throttle level. This eliminates the likelihood of the pilot **34** accidentally reducing the throttle to an unsafe level and inadvertently initiating an unsafe descent of the aircraft.

With reference to FIGS. **16** and **18**, the starboard-side control mechanism **196** comprises a stick **210** and a grip **212** pivotably mounted thereto. FIG. **19** is an enlarged front elevational view of the starboard-side control mechanism **196**. The starboard-side control mechanism **196** preferably includes a gimbaled base member **213** that is rotatably and pivotably mounted within the starboard arm **192**. The gimbaled base member **213** allows the starboard-side control mechanism **196** to be rotated about an axis extending through the stick **210** and to also be rearwardly and forwardly tilted about base member **213**.

With reference to FIG. **19**, a pair of opposed brackets **215**, **217** are disposed on a bottom end of the starboard-side control mechanism **196** below the gimbaled base member **213**. As best shown in FIG. **18**, a pair of first and second elongated bell cranks **214**, **216** are mechanically coupled at respective forward ends to the brackets **215**, **217**. The elongated bell cranks **214**, **216** extend along the bottom edge of the starboard arm **192** toward the rear of the starboard arm **192**. A rearward end of the first bell crank **214** is mechanically connected to a starboard linkage arm **218** that extends upwardly and is mechanically attached to the bottom end of the starboard control linkage **197**. As mentioned above, the upper end of the starboard control linkage **197** is connected to the starboard tubular housing **148a**. The bell crank **214**, linkage arm **218**, and starboard control linkage **197** thus provide a mechanical link between the starboard-side control mechanism **196** and the starboard tubular housing **148a**.

Similarly, the second bell crank **216** provides a mechanical link between the starboard-side control mechanism **196** and the port tubular housing **148b**. The second bell crank **216** extends rearwardly along the starboard arm **192** from the bracket **215**. The bell crank **216** is connected at a rearward end to an elongated tube (not shown) that preferably extends parallel to the connecting section **195** to the port control linkage **199** (FIG. **17**).

The grip **212** is preferably coupled to the calipers **202** such that the pilot may pivot the grip **212** toward the stick **210** to release the calipers **202** from engagement with the plates **200**. This allows the pilot **34** to move the main control member **190** to a desired position. The pilot **34** then releases the grip **212** to return the calipers **202** to engagement with the plates **200** and maintain the current position of the main

control member **190**. It will be appreciated that the calipers **202** may also be coupled to the grip **208** on the port side control mechanism **198**.

Preferably, "gross" movement of the fan assemblies **36** is accomplished by lifting and/or lowering the main control member **190** by applying a force to the starboard and port arms **192**, **194**. "Gross" movement of the fan assemblies refers to tilting the fan assemblies **36** up to approximately $\pm 20^\circ$. When the pilot lifts or lowers the main control member **190**, the attached control linkages **197**, **199** provide a torque to the rotatable tubular housings **148** to thereby collectively tilt the attached fan assemblies **138**. The pilot **34** may thus vary the direction of fan thrust during flight and control the forward and backward translation of the aircraft **30**. As mentioned, the gas springs **204** advantageously reduce the likelihood of the pilot moving the main control member **190** too quickly by limiting the rate of movement thereof.

The starboard-side control mechanism **196** preferably provides "fine" control over the orientation of the fan assemblies **36**. That is, the starboard-side control mechanism **196** allows the pilot **34** to vary the tilt of the fan assemblies **36** in increments of up to $\pm 5^\circ$ relative to the current gross setting. Preferably, the pilot **34** tilts the starboard-side control mechanism **196** forwardly or backwardly to collectively tilt the fan assemblies **36**. Specifically, when the starboard-side control mechanism **196** is tilted forward or backward, the attached bell cranks **214**, **216** are also translated forward or backward via their attachments to the brackets **215** and **217**. The translation of the bell cranks **214** is transferred to the attached control linkages **197**, **199** via the starboard linkage arm **218** and a similar linkage arm on the port-side of the aircraft **30**. The control linkages **197**, **199** move upward or downward and apply a torque to the tubular housings **148** so that the tubular housings **148** rotate and collectively tilt the attached fan assemblies **138**.

The pilot **34** preferably rotates or twists the starboard-side control mechanism **196** about the stick **210** to provide a differential motion to the bell cranks **214**, **216**. As the starboard-side control mechanism **196** rotates, the brackets **215**, **217** move the first bell crank **214** in a forward direction and the second bell crank **216** in a rearward direction (or vice-versa depending on the rotational direction which the stick **210** is rotated). The bell cranks **214**, **216** thus move in opposite directions when the starboard-side control mechanism **198** is twisted. The bell cranks thereby provide a differential motion to the starboard and port control linkages **197**, **199** so that the attached starboard and port tubular housings **148a,b** rotate in opposite directions. Accordingly, the attached fan assemblies **36** are also differentially tilted when the portside control mechanism **198** is twisted. Differential tilting of the starboard and port fan assemblies **36** creates a moment about the aircraft center of gravity which results in yaw of the aircraft **30**. By varying the level of tilt differential of the fan assemblies **36**, the pilot may vary the amount of yaw rate provided to the aircraft **30**.

As mentioned, the main control member **190** preferably provides a gross range of approximately 20° of rotational motion of tilt to the fan assemblies **36**. Preferably, every one degree of rotation of the main control member **190** provides approximately ± 2 degrees of tilt to each of the fan assemblies **36**. The main control member **190** provides a leveraged moment arm to the fan assemblies **36** so that the fan assemblies may **26** overcome airloads when tilting during flight. The starboard-side control member **196** preferably provides a mechanically advantaged movement to the fan assemblies **36**. Preferably, approximately 6–8 degrees of pivot of the control member **190** results in approximately ± 1

degree of tilt to the fan assemblies **36** relative to the current gross setting. Approximately 4 degrees of rotation of the control member **190** preferably provides approximately ± 1 degree of differential tilt to the fan assemblies **36**. The starboard-side control member **196**, even with its short moment arm, provides a high mechanical advantage over the tilt of the fan assemblies **36** to overcome airloads thereon during flight.

Starboard and port translational control is preferably achieved by the pilot shifting his or her weight in the starboard or port directions, respectively, to thereby induce a moment to the airframe. As mentioned, the center of gravity **38** of the aircraft **30** is aligned with both the median plane of the aircraft and with the median plane of the pilot's torso. The pilot **34** shifts his or her torso toward the starboard or port side of the aircraft **30** to induce a rolling moment about the aircraft center of gravity **38**. The pilot **34** repositions the torso by exerting a force on the back cushion **80** so that the cushion **80** slides along the rails **81** (FIG. 6). An adjustable harness is used to positively secure the pilot **34** to the cushion **80** and the airframe **32** during such weight adjustments.

The "A" shape of the aircraft **30** facilitates the pilot's control of the aircraft with respect to weight shifting. The pilot's body weight is distributed across the width of the airframe **32** as a result of the spread-out orientation of the pilot's legs, which are aligned with the front legs **48**. The shifting of the pilot's torso toward the port or starboard sides of the airframe **32** manifests the weight shifting across the width of the airframe **32** via the pilot's legs. Additionally, the pilot's spread legs create a small front-view profile that produces less drag than if the pilot's legs were juxtaposed with one another.

Shifts in the pilot's position may be combined with various fan assembly orientations to maneuver the aircraft **30** during flight. Advantageously, the location of the center of gravity **38** at the midway point of the forward/rearward dimension of the aircraft **30** and at the torso level of the pilot increases the pilot's kinesthetic control over the aircraft **30**. Because the center of gravity of the aircraft **30** is positioned near the pilot's torso, shifts in the pilot's torso in the starboard and port direction correspond relatively directly to shifts in the moments about the aircraft center of gravity.

The pilot **34** has convenient access to the various control mechanisms of the control system. The starboard and port arms **192**, **194** of the main control member **190** are desirably dimensioned such that the pilot may rest his or her arms thereon during flight. Advantageously, the starboard and port-side control mechanisms **196** **198** are positioned where the pilot's hands are located to provide easy access to the "fine" adjustment of the fan assemblies **36** and engine throttle. The ergonomic design of the control system advantageously allows the pilot **34** to control the aircraft without having to change his or her line of sight to search for the control mechanisms.

In operation, the pilot **34** first boards the aircraft by positioning his or her feet on respective foot rests **90** on the front legs **48**. The pilot **34** faces forward so that the back of the torso is adjacent the cushion **80**. The cushion **80** or the back support panel **74** is equipped with a harness for securing the pilot **34** in place. After boarding, the pilot **34** is in a standing or upright orientation with the airframe **32** supporting the entire weight of the pilot. Advantageously, the pilot **34** has an unobstructed forward field of vision. The "A" shape of the airframe **32** provides a gradual decrease in size of thereof moving in the upward direction, so that the pilot also has a relatively unobstructed rear field of vision. None of the aircraft weight is supported by the pilot.

The pilot 34 then activates the engine 40 in a well known manner to provide power to the fan assemblies 36. Preferably, the fans 102 are facing such that they are initially spinning in a plane parallel to the ground plane so that the resulting thrust force is directly vertical or in a “leveled” position. Preferably, the main control member 190 includes a detent that allows the pilot to position the fans 102 at the leveled position and verify the same. The pilot 34 increases the level of throttle of the engine 40 using the port-side control mechanism 198 until the fan assemblies 36 generate sufficient force to vertically lift the aircraft 30. After the aircraft 30 has reached a desired altitude, the pilot 34 may transfer to forward flight by collectively tilting the fan assemblies 36 using the main control member 190 and/or the starboard-side control mechanism 196. The aircraft 34 maintains the pilot 34 in a general upright orientation continuously during flight. The entire aircraft 30, including the pilot 34, may tilt into the direction of flight during cruise.

The aircraft 30 is a convenient and reliable means of transportation. The gasoline-powered engine 40 is easily fueled and maintained to reduce maintenance costs of the aircraft 30 and increase reliability. The control mechanisms provide the pilot 34 with intuitive control over the aircraft 30 during flight. Advantageously, the pilot 34 may also shift his or her torso during flight to perform fully coordinated turns during cruise of the aircraft. The position of the center of gravity 38 near the midpoint of the both the front-to-rear and outboard dimensions of the aircraft increases the stability of the aircraft 30 during flight.

Although the foregoing description of the preferred embodiment of the invention has shown, described, and pointed out certain novel features of the invention, it will be understood that various omissions, substitutions, and changes in the form of the detail of the apparatus as illustrated as well as the uses thereof, may be made by those skilled in the art without departing from the spirit of the present invention. Consequently, the scope of the present invention should not be limited by the foregoing discussion, which is intended to illustrate rather than limit the scope of the invention.

What is claimed is:

1. A single passenger, vertical take-off and landing aircraft, comprising:

an airframe configured to support a pilot in a standing position toward a front portion of the airframe, the airframe having essentially an A-shaped configuration and being symmetric about a medial plane and comprising three legs arranged in a tripod configuration for supporting the airframe upright, with a pilot alignment line defined as extending from about the feet of the standing pilot and passing through his head, the pilot alignment line lying in the medial plane;

a pair of fans mounted on an upper end of the airframe above the pilot, the fans each being tiltable about a common axis, wherein the fans are positioned symmetrically with respect to the medial plane and wherein each of the fans are rotatably mounted within a fan duct comprised of a first material, the fan duct including an annular strip of material surrounding the corresponding fan, wherein the annular strip of material comprises a material softer than the first material;

an engine mounted on the airframe to the rear of the pilot, the engine drivingly coupled to each of the pair of fans and the engine being mounted at a height about even with the torso of the standing pilot so that the center of gravity of the aircraft lies in the medial plane at about the height of the torso of the standing pilot;

a movable control on the airframe, the control coupled to the pair of fans so that the fans tilt about the axis in response to movement of the control; and

a powertrain system drivingly coupling the engine to each of the fans, the powertrain system comprising a first drive axle extending upwardly behind the pilot within the medial plane and a second drive axle extending above the pilot transverse to the medial plane, the engine and the first drive axle being longitudinally aligned and defining an engine alignment line in the medial plane from the engine along the first drive axle, the engine alignment line being angled slightly toward the front portion of the airframe and forming an acute angle with said pilot alignment line.

2. The aircraft as in claim 1 wherein the fans rotate in opposite directions.

3. The aircraft as in claim 1 wherein each of the fans comprises fixed pitch rotor blades.

4. A single passenger, vertical take-off and landing aircraft, comprising:

an airframe configured to support a pilot in a standing position toward a front portion of the airframe, the airframe having essentially an A-shaped configuration and being symmetric about a medial plane and comprising three legs arranged in a tripod configuration for supporting the airframe upright, with a pilot alignment line defined as extending from about the feet of the standing pilot and passing through his head, the pilot alignment line lying in the medial plane;

a pair of fans mounted on an upper end of the airframe above the pilot, the fans each being tiltable about a common axis, wherein the fans are positioned symmetrically with respect to the medial plane;

an engine mounted on the airframe to the rear of the pilot, the engine drivingly coupled to each of the pair of fans and the engine being mounted at a height about even with the torso of the standing pilot so that the center of gravity of the aircraft lies in the medial plane at about the height of the torso of the standing pilot;

a movable control on the airframe, the control coupled to the pair of fans so that the fans tilt about the axis in response to movement of the control;

a powertrain system drivingly coupling the engine to each of the fans, the powertrain system comprising a first drive axle extending upwardly behind the pilot within the medial plane and a second drive axle extending above the pilot transverse to the medial plane, the engine and the first drive axle being longitudinally aligned and defining an engine alignment line in the medial plane from the engine along the first drive axle, the engine alignment line being angled slightly toward the front portion of the airframe and forming an acute angle with said pilot alignment line; and

a back support member disposed on the airframe, the back support member positioned to support the torso of the pilot, wherein the back support member is movably mounted so as to be translatable along a direction transverse to the medial plane.

5. A single passenger, vertical take-off and landing aircraft, comprising:

an airframe configured to support a pilot in a standing position toward a front portion of the airframe, the airframe being symmetric about a medial plane;

a pair of propulsion devices mounted on an upper end of the airframe above the pilot, the propulsion devices each being tiltable about a common axis;

- an engine mounted on the airframe to the rear of the pilot, the engine being mounted at a height about even with the torso of the standing pilot so that the center of gravity of the aircraft lies in the medial plane at about the height of the torso of the standing pilot, the engine drivingly coupled to each of the propulsion devices; 5
- a movable control on the airframe adjacent the pilot, the control being coupled to the propulsion devices so that the propulsion devices tilt about the axis in response to movement of the control; 10
- a powertrain system drivingly coupling the engine to each of the propulsion devices the powertrain system comprising a first drive axle extending upwardly behind the pilot within the medial plane and a second drive axle extending above the pilot transverse to the medial plane; 15
- a central gear box mechanically coupling the first drive axle to the second drive axle;
- a pair of outboard gear boxes each including a gear system mechanically coupling the second drive axle to one of the fans, wherein each gear box comprises an outer housing including an end plate rotatably mounted to the gear box, a first gear, and a second gear in meshed engagement with the first gear, wherein the first gear is fixedly coupled to the end plate so that rotational movement of the end plate translates the first gear with respect to the second gear; 20
- a fuel tank coupled to the engine, the fuel tank comprising a transparent container having markings positioned to indicate the volumetric level of fuel in the fuel tank and the volumetric level of fuel required to fill the fuel tank; and 25
- an oil tank fluidly coupled to the fuel tank, the oil tank comprising a transparent container having markings positioned to indicate the volumetric level of oil in the oil tank. 30
- 6. A single passenger, vertical take-off and landing aircraft, comprising:
 - an airframe configured to support a pilot in a standing position toward a front portion of the airframe, the airframe being symmetric about a medial plane; 40
 - a pair of propulsion devices mounted on an upper end of the airframe above the pilot, the propulsion devices each being tiltable about a common axis; 45
 - an engine mounted on the airframe to the rear of the pilot, the engine being mounted at a height about even with the torso of the standing pilot so that the center of gravity of the aircraft lies in the medial plane at about the height of the torso of the standing pilot, the engine drivingly coupled to each of the propulsion devices; 50
 - a movable control on the airframe adjacent the pilot, the control being coupled to the propulsion devices so that the propulsion devices tilt about the axis in response to movement of the control; 55
 - a powertrain system drivingly coupling the engine to each of the propulsion devices the powertrain system comprising a first drive axle extending upwardly behind the pilot within the medial plane and a second drive axle extending above the pilot transverse to the medial plane; 60
 - a central gear box mechanically coupling the first drive axle to the second drive axle;
 - a pair of outboard gear boxes each including a gear system mechanically coupling the second drive axle to one of the fans, wherein each gear box comprises an outer

- housing including an end plate rotatably mounted to the gear box, a first gear, and a second gear in meshed engagement with the first gear, wherein the first gear is fixedly coupled to the end plate so that rotational movement of the end plate translates the first gear with respect to the second gear and wherein the end plate is threaded into the outer housing;
- a fuel tank coupled to the engine, the fuel tank comprising a transparent container having markings positioned to indicate the volumetric level of fuel in the fuel tank and the volumetric level of fuel required to fill the fuel tank; and
- an oil tank fluidly coupled to the fuel tank, the oil tank comprising a transparent container having markings positioned to indicate the volumetric level of oil in the oil tank.
- 7. A single passenger, vertical take-off and landing aircraft, comprising:
 - an airframe configured to support a pilot in a standing position toward a front portion of the airframe, the airframe being symmetric about a medial plane and comprising three legs arranged in a tripod configuration for supporting the airframe upright, with a pilot alignment line defined as extending from about the feet of the standing pilot and passing through his head, the pilot alignment line lying in the medial plane;
 - a pair of fans mounted on an upper end of the airframe above the pilot, the fans each being tiltable about a common axis, wherein the fans are positioned symmetrically with respect to the medial plane and each of the fans are rotatably mounted within a fan duct comprised of a first material, the fan duct including an annular strip of material surrounding the corresponding fan, wherein the annular strip of material comprises a material softer than the first material;
 - an engine mounted on the airframe to the rear of the pilot, the engine drivingly coupled to each of the pair of fans and the engine being mounted at a height about even with the torso of the standing pilot so that the center of gravity of the aircraft lies in the medial plane at about the height of the torso of the standing pilot;
 - a movable control on the airframe, the control coupled to the pair of fans so that the fans tilt about the axis in response to movement of the control; and
 - a powertrain system drivingly coupling the engine to each of the fans, the powertrain system comprising a first drive axle extending upwardly behind the pilot within the medial plane and a second drive axle extending above the pilot transverse to the medial plane, the engine and the first drive axle being longitudinally aligned and defining an engine alignment line in the medial plane from the engine along the first drive axle, the engine alignment line being angled slightly toward the front portion of the airframe and forming an acute angle with said pilot alignment line.
- 8. The aircraft of claim 7, additionally comprising a back support member on the airframe, the back support member positioned to support the torso of the pilot, wherein the back support member is movably mounted so as to be translatable along a direction transverse to the medial plane.
- 9. The aircraft of claim 7 further comprising a pilot adjustment system for adjusting the position of the pilot to maintain the center of gravity of the aircraft at about the torso of the pilot regardless of the height of the pilot.
- 10. The aircraft of claim 7 wherein each of the pair of fans comprises fixed pitch rotor blades.

- 11. The aircraft of claim 7 wherein the pair of fans may be tilted about the axis in the same direction in response to movement of the control.
- 12. The aircraft of claim 7 wherein the pair of fans may be tilted about the axis in opposite directions in response to movement of the control.
- 13. A vertical take-off and landing aircraft, comprising:
 - an airframe configured to support a pilot in a standing position toward the front of the airframe, the airframe being symmetric about a medial plane and comprising at least three legs for supporting the airframe in an upright position;
 - a pair of fans mounted on an upper end of the airframe above the pilot, the fans each being tiltable about a common axis and being positioned symmetrically about the medial plane;
 - an engine mounted on the airframe to the rear of the pilot and generally at about the height of the torso of the pilot, the engine being drivingly coupled to each of the pair of fans;
 - a powertrain system mounted on the airframe for drivingly coupling tie engine to each of the fans and positioned above the engine and generally at about the height of the shoulders and head of the pilot whereby the resulting center of gravity of the aircraft is at about the height of the torso of the pilot and below the center of drag of the aircraft to achieve maneuverability and stability during flight; and
 - a pilot support system for adjusting the position of the pilot to maintain the center of gravity of the aircraft at about the height of the torso of the pilot regardless of the height of the pilot.
- 14. The aircraft of claim 13 wherein the pilot support system comprises a movable footrest upon the airframe of the aircraft, the footrest being capable of being positioned at a variety of vertical heights along the airframe.
- 15. The aircraft of claim 14 wherein the pilot support system further comprises a second movable footrest upon the airframe of the aircraft.
- 16. The aircraft of claim 14 wherein each of the pair of fans comprises fixed pitch rotor blades.
- 17. The aircraft of claim 14 wherein the pair of fans rotate in opposite directions.
- 18. A single passenger, vertical take-off and landing aircraft, comprising:
 - an airframe configured to support a pilot in a standing position toward a front portion of the airframe, the airframe being symmetric about a medial plane;
 - a pair of propulsion devices mounted on an upper end of the airframe above the pilot, the propulsion devices each being tiltable about a common axis;
 - an engine mounted on the airframe to the rear of the pilot, the engine being mounted at a height about even with the torso of the standing pilot so that the center of

- gravity of the aircraft lies in the medial plane at about the height of the torso of the standing pilot, the engine drivingly coupled to each of the propulsion;
- a moveable control on the airframe adjacent the pilot, the control being coupled to the propulsion devices so that the propulsion devices tilt about the axis in response to movement of the control;
- a powertrain system drivingly coupling the engine to each of the propulsion devices, the powertrain system comprising a first drive axle extending upwardly behind the pilot within the medial plane and a second drive axle extending above the pilot transverse to the medial plane;
- a fuel tank coupled to the engine, the fuel tank comprising a transparent container having markings positioned to indicate the volumetric level of fuel in the fuel tank and the volumetric level of fuel required to fill the fuel tank;
- an oil tank fluidly coupled to the fuel tank, the oil tank comprising a transparent container having markings positioned to indicate the volumetric level of oil in the oil tank;
- a central gear box mechanically coupling the first drive axle to the second drive axle; and
- a pair of outboard gear boxes each including a gear system mechanically coupling the second drive axle to one of the fans, wherein each gear box comprises an outer housing including an end plate rotatably mounted to the gear box, a first gear, and a second gear in meshed engagement with the first gear, wherein the first gear is fixedly coupled to the end plate so that rotational movement of the end plate translates the first gear with respect to the second gear.
- 19. A VTOL aircraft, comprising:
 - an airframe configured to support one passenger in a standing position, the airframe being symmetric about a medial plane and supported on the ground in an upright position;
 - a pair of fans mounted on an upper end of the airframe above the passenger and positioned symmetrically about the medial plane;
 - a power system mounted on the airframe and generally at about the height of the torso of the standing passenger, the power system coupled to each of the pair of fans;
 - the airframe being configured such that its mass is primarily distributed generally at about the height of the standing passenger such that, considering the power system and the pair of fans, the center of gravity of the aircraft is at about the height of the torso of the standing passenger; and
 - a passenger adjustment system for maintaining the center of gravity at approximately the same location independent of the height of the passengers.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 6,488,232 B2
DATED : December 3, 2002
INVENTOR(S) : Michael Moshier

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Column 22.

Line 37, please change "with the torso of the standing pilot so tat the center of" to -- with the torso of the standing pilot so that the center of --.

Column 25.

Line 23, please change "ingly coupling tie engine to each of the fans and" to -- ingly coupling the engine to each of the fans and --.

Line 30, please change "a pilot support system for adjusting the position of the" to -- a pilot support system for adjusting a vertical position of the --

Column 26.

Line 3, please add the word "devices" at the end of the line so that it reads -- drivingly coupled to each of the propulsion devices --

Line 44, please add the word "being" between the words "system" and "coupled" so that the line reads -- the power system being coupled to each of the pair of fans; --

Line 54, after "dent of the height of the passengers", please add -- wherein the passenger adjustment system comprises a movable footrest upon the airframe of the aircraft, the footrest being capable of being positioned at a variety of vertical heights along the airframe. --

Signed and Sealed this

Eighteenth Day of March, 2003



JAMES E. ROGAN
Director of the United States Patent and Trademark Office