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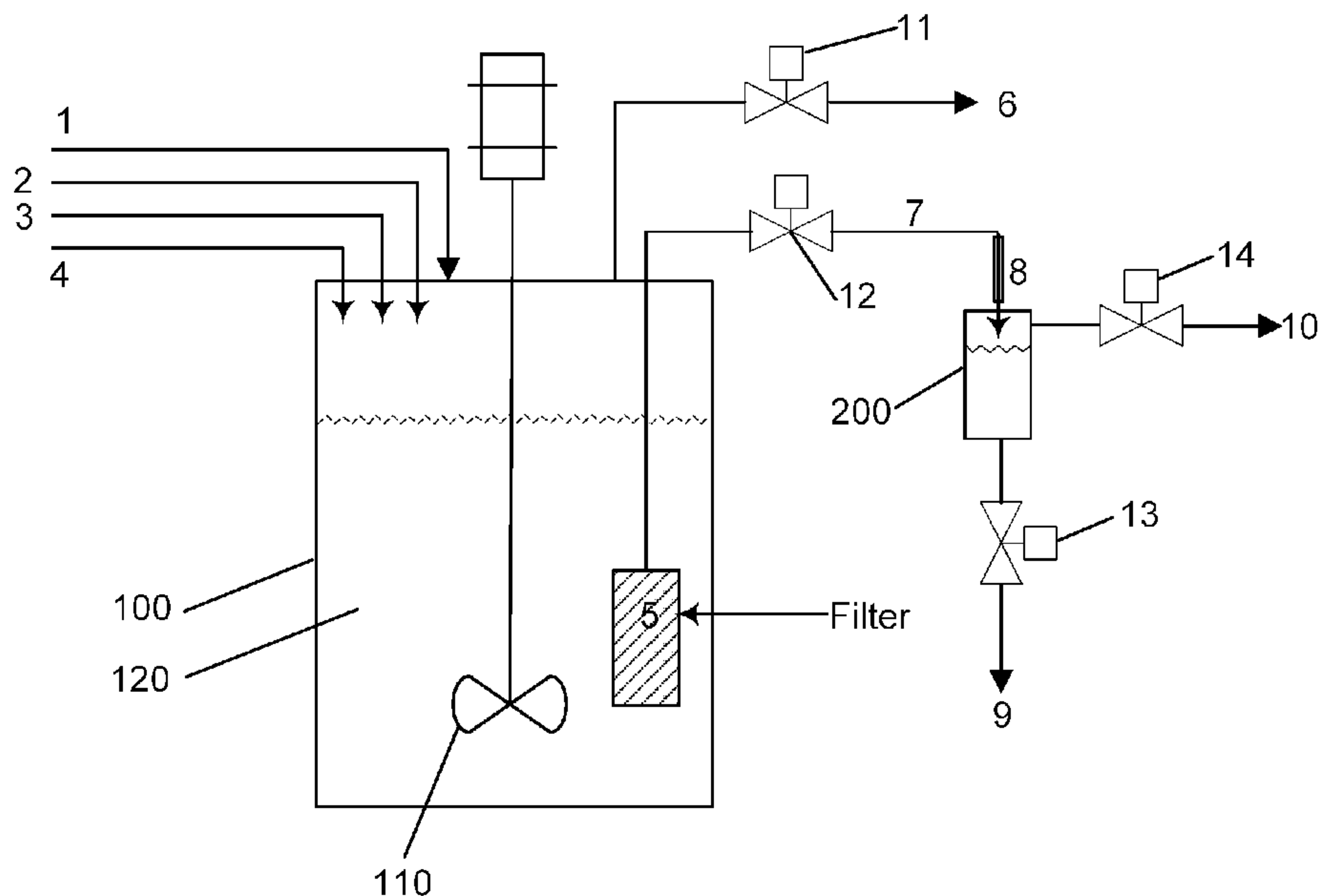
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(54) Titre : PROCEDE DE PRODUCTION DE GLYCOLS
(54) Title: PROCESS FOR THE PRODUCTION OF GLYCOLS

FIGURE 1



(57) **Abrégé/Abstract:**

A process for the production of glycols is provided, the process comprising contacting a saccharide-containing feedstock with hydrogen in the presence of a catalyst composition and a solvent, wherein the solvent comprises water and at least 25% by weight, based on the total weight of the solvent, of one or more alcohols selected from a C₁ to C₆ alcohol, a C₁ to C₆ polyalcohol, and a combination thereof.

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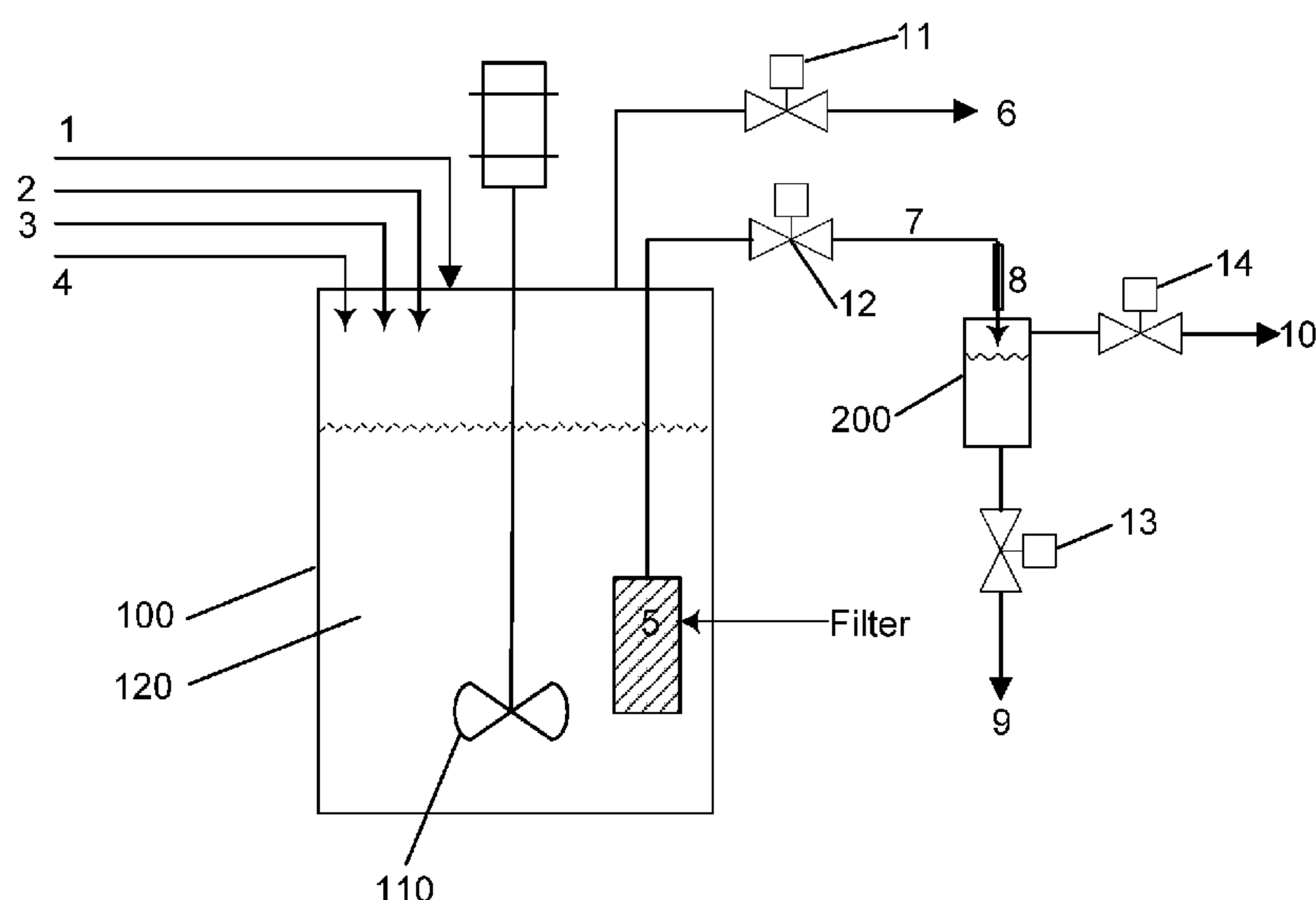
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(54) Title: PROCESS FOR THE PRODUCTION OF GLYCOLS

FIGURE 1

(57) Abstract: A process for the pro-
duction of glycols is provided, the pro-
cess comprising contacting a sacchar-
ide-containing feedstock with hydrogen
in the presence of a catalyst composi-
tion and a solvent, wherein the solvent
comprises water and at least 25% by
weight, based on the total weight of the
solvent, of one or more alcohols selec-
ted from a C₁ to C₆ alcohol, a C₁ to C₆
polyalcohol, and a combination thereof.

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PROCESS FOR THE PRODUCTION OF GLYCOLS

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims priority to U.S. Provisional Application Serial No. 62/243,704 filed October 20, 2015, the entire disclosure of which is hereby incorporated by reference.

Background

Ethylene glycol and propylene glycol are valuable materials with a multitude of commercial applications, e.g. as heat transfer media, antifreeze, and precursors to polymers, such as PET. Ethylene and propylene glycols are typically made on an industrial scale by hydrolysis of the corresponding alkylene oxides, which are the oxidation products of ethylene and propylene, produced from fossil fuels.

In recent years, increased efforts have focused on producing chemicals, including glycols, from renewable feedstocks, such as sugar-based materials. The conversion of sugars to glycols can be seen as an efficient use of the starting materials with the oxygen atoms remaining intact in the desired product.

Current methods for the conversion of saccharides to sugars revolve around a hydrogenation/hydrogenolysis process as described in Angew. Chem. Int. Ed. 2008, 47, 8510-8513.

WO 2015/028398 describes a continuous process for the conversion of a saccharide-containing feedstock into glycols. In this process the saccharide-containing feedstock is contacted in a reactor with a catalyst composition comprising at least two active catalytic components comprising, as a first active catalyst component, one or more materials selected from transition metals from groups 8, 9 or 10 or compounds

thereof, with catalytic hydrogenation capabilities;
and, as a second active catalyst component, one or more
materials selected from tungsten, molybdenum and
compounds and complexes thereof.

5 An important aim in this area is the provision of
a process that is high yielding in desirable products,
such as mono-ethylene glycol (MEG) and mono-propylene
glycol (MPG), and that can be sustained with such
yields over time.

10 However, the present inventors have found that,
when using catalysts known in the art, such as those
taught in WO 2015/028398, for the hydrogenation/
hydrogenolysis of saccharide-containing feedstock,
significant catalyst deactivation was found to occur
15 over time.

It would, therefore, be advantageous to provide a
process for the production of glycols from saccharide-
containing feedstocks in which catalyst deactivation is
reduced or avoided.

20 Summary

Accordingly, in one aspect, a process for the
production of glycols is provided, the process
comprising:

25 contacting a saccharide-containing feedstock with
hydrogen in the presence of a solvent and a catalyst
composition,

 wherein the solvent comprises water and at least
25% by weight, based on the total weight of the
solvent, of one or more alcohols selected from a C₁ to
30 C₆ alcohol, a C₁ to C₆ polyalcohol, and a combination
thereof, and

 wherein the catalyst composition comprises at
least two active catalytic components, the active
catalyst components comprising, as a first active

catalyst component, one or more materials selected from transition metals from groups 8, 9 or 10 or compounds thereof, with catalytic hydrogenation capabilities; and, as a second active catalyst component, one or more materials selected from tungsten, molybdenum, lanthanum, tin or compounds or complexes thereof.

Brief Description of the Drawings

Figure 1 is a schematic representation of the experimental apparatus used in Examples 1 and 2.

Detailed Description

The present disclosure relates to hydrogenation/hydrogenolysis processes for the production of ethylene and propylene glycols in which a saccharide-containing feedstock is contacted with hydrogen in the presence of a solvent and a catalyst composition, wherein the solvent comprises water and at least 25% by weight, based on the total weight of the solvent, of one or more alcohols selected from a C₁ to C₆ alcohol, a C₁ to C₆ polyalcohol, and a combination thereof. These processes allow the hydrogenation/ hydrogenolysis reactions to be carried out while minimising any deactivation of the catalyst composition used therefor.

The present inventors have surprisingly found that the amounts of ethylene and propylene glycols yielded by known hydrogenation/hydrogenolysis processes are reduced over time, due to deactivation of the catalytic compositions. It is postulated, without wishing to be bound by any theory, that such deactivation is, at least in part, caused by the deposition of water-insoluble carbonaceous materials on one or more of the active catalytic components of the catalyst composition. Such carbonaceous materials are generally believed to be formed as a result of the decomposition of at least a portion of the saccharide-containing

feedstock and/or the formation of reaction by-products. By utilising a solvent comprising water and at least 25% by weight, based on the total weight of the solvent, of one or more alcohols selected from a C₁ to C₆ alcohol, a C₁ to C₆ polyalcohol, and a combination thereof as a reaction medium, such carbonaceous materials are more readily dissolved therein and thus, more readily hydrogenated, thereby minimising or preventing the fouling of one or more of the active catalytic components of the catalyst composition.

Suitable saccharide-containing feedstocks comprise at least one saccharide selected from the group consisting of monosaccharides, disaccharides, oligosaccharides, polysaccharides and a combination thereof. Examples of suitable polysaccharides include cellulose, hemicelluloses, starch, glycogen, chitin and any combination thereof. Examples of monosaccharides include glucose, fructose, etc. If the feedstock comprises oligosaccharides or polysaccharides, it is preferable that it is subjected to pre-treatment before being fed to a reactor in a form that can be converted in the processes of the present disclosure. Suitable pre-treatment methods are known in the art and include, but are not limited to, one or more of sizing, drying, blending, grinding, washing, de-watering, solids removal, steeping, milling, hot water treatment, steam treatment, hydrolysis (e.g. acid-catalysed hydrolysis, enzymatic hydrolysis), pyrolysis, thermal treatment, chemical treatment, biological treatment, purification, etc.

Suitable saccharide-containing feedstocks may be derived from grains such as corn, wheat, millet, oats, rye, sorghum, barley or buckwheat, from rice, from pulses such as soybean, pea, chickpea or lentil, from

bananas and/or from root vegetables such as potato, yam, sweet potato, cassava and sugar beet, or any combinations thereof. A preferred source of a saccharide-containing feedstock is corn.

5 Preferably, a saccharide-containing feedstock supplied to a reactor after any optional pre-treatment comprises one or more saccharides selected from glucose, sucrose, and starch. Suitably, a saccharide-containing feedstock is generally supplied to a reactor
10 as a solution, a suspension or slurry in the solvent, or in one or more components of the solvent.

Solvents suitable for use herein comprise water and at least 25% by weight, based on the total weight of the solvent, of one or more alcohols selected from a
15 C₁ to C₆ alcohol, a C₁ to C₆ polyalcohol, and a combination thereof. Preferred C₁ to C₆ alcohols include methanol, ethanol, 1-propanol and iso-propanol. Polyalcohols of use include glycols, particularly products of the hydrogenation/ hydrogenolysis reaction,
20 glycerol, erythritol, threitol, sorbitol, 1,2-hexanediol and mixtures thereof. Preferably, a solvent comprises from 25% to 75% by weight, based on the total weight of the solvent, of the one or more alcohols and from 25% to 75% by weight, based on the total weight of
25 the solvent, of water.

The solvent, or one or more of the components of the solvent (e.g. water and the one or more alcohols), may be added to the reactor in one or more separate feed streams. Similarly, the solvent, or one or more
30 components thereof, may be added to the saccharide-containing feedstock before it enters the reactor.

The saccharide-containing feedstock is contacted with hydrogen in the presence of a catalyst composition comprising at least two active catalytic components,

said active catalyst components comprising, as a first active catalyst component, one or more materials selected from transition metals from groups 8, 9 or 10 or compounds thereof, with catalytic hydrogenation capabilities; and, as a second active catalyst component, one or more materials selected from tungsten, molybdenum, lanthanum, tin and compounds and complexes thereof.

The saccharide-containing feedstock may be contacted with hydrogen in the presence of a catalyst composition in one or more reactors in parallel or in series.

The catalyst composition and the components contained therein may be heterogeneous or homogeneous with respect to the solvent or solvents present in the reactor. The catalyst composition may also contain both heterogeneous and homogeneous components.

Depending on the physical state of the catalyst composition and any components contained therein, they may be preloaded into the reactor or, if they are in liquid form or present as a solution or slurry in a solvent, they may be fed into the reactor as required in a continuous or discontinuous manner.

The catalyst composition comprises at least two active catalytic components comprising, as a first active catalyst component, one or more materials selected from transition metals from groups 8, 9 or 10 or compounds thereof, with catalytic hydrogenation capabilities; and, as a second active catalyst component, one or more materials selected from tungsten, molybdenum, lanthanum, tin or compounds or complexes thereof.

Preferably, the first active catalyst component consists of one or more of the group selected from

iron, cobalt, nickel, ruthenium, rhodium, palladium, iridium and platinum. This component may be present in the elemental form or as a compound. It is also suitable that this component is present in chemical combination with one or more other ingredients in the catalyst system. It is required that the first active catalyst component has catalytic hydrogenation capabilities and it is capable of catalysing the hydrogenation of material present in the reactor.

Preferably, the second active catalyst component comprises of one or more compound, complex or elemental material comprising tungsten, molybdenum, lanthanum or tin. More preferably, the second active catalyst component comprises one or more material selected from the list consisting of tungstic acid, molybdic acid, ammonium tungstate, ammonium metatungstate, ammonium paratungstate, tungstate compounds comprising at least one Group I or II element, metatungstate compounds comprising at least one Group I or II element, paratungstate compounds comprising at least one Group I or II element, heteropoly compounds of tungsten, heteropoly compounds of molybdenum, tungsten oxides, molybdenum oxides and combinations thereof. The metal component is suitably in a form other than a carbide, nitride, or phosphide. Preferably, the second active catalyst component comprises one or more compound, complex or elemental material selected from those containing tungsten or molybdenum.

Preferably, at least one of the active catalyst components is supported on a solid support. In this embodiment, any other active catalyst component may be present in either heterogeneous or homogeneous form. Said any other active catalyst component may also be supported on a solid support. In one embodiment of the

invention, the first active catalyst component is supported on one solid support and the second active catalyst component is supported on a second solid support which may comprise the same or different material. In another embodiment, both active catalyst components are supported on one solid support.

The solid supports may be in the form of a powder or in the form of regular or irregular shapes such as spheres, extrudates, pills, pellets, tablets, monolithic structures. Alternatively, the solid supports may be present as surface coatings, for example on the surfaces of tubes or heat exchangers. Suitable solid support materials are those known to the skilled person and include, but are not limited to aluminas, silicas, zirconium oxide, magnesium oxide, zinc oxide, titanium oxide, carbon, activated carbon, zeolites, clays, silica alumina and mixtures thereof.

Suitably, the weight ratio of the first active catalyst component to the second active catalyst component is in the range of from 0.02:1 to 3000:1, preferably in the range of from 0.1:1 to 100:1, on the basis of the weight of metal present in each component.

The weight ratio of the first active catalyst component (based on the amount of metal in said component) to sugar is suitably in the range of from 1:100 to 1:1000. The weight ratio of the second active catalyst component (based on the amount of metal in said component) to sugar is suitably in the range of from 1:10 to 1:100.

If more than one reactor is used in series, a catalyst composition may optionally be present in the second and any subsequent reactors. If a catalyst composition is present in the second and any subsequent reactor, the catalyst composition used in each of the

reactors may be the same or different. Additionally, the weight ratio of the active catalyst components may be varied between the first and second reactors (and any subsequent reactors) and it may be advantageous to alter the composition of the catalyst systems between the reactors to suit the different feed streams provided to each reactor. Suitably, reaction conditions, particularly temperature and pressure, can be varied between the reactors if more than one reactor is used. This can lead to a more tailored process to suit the different constituents of the feeds provided to each reactor.

The reaction temperature at which the saccharide-containing feedstock is contacted with hydrogen in the presence of the catalyst composition described herein is suitably at least 130°C, preferably at least 150°C, more preferably at least 170°C, most preferably at least 190°C. The temperature in the reactor is suitably at most 300 °C, preferably at most 280°C, more preferably at most 270°C, even more preferably at most 250°C. Preferably, the reactor is heated to a temperature within these limits before addition of the saccharide-containing feedstock and is maintained at such a temperature as the reaction proceeds.

The pressure in the reactor or reactors in which the saccharide-containing feedstock is contacted with hydrogen in the presence of the catalyst composition described herein is suitably at least 1 MPa, preferably at least 2 MPa, more preferably at least 3 MPa. The pressure in the reactor is suitably at most 15 MPa, preferably at most 12 MPa, more preferably at most 10 MPa, most preferably at most 8 MPa. Preferably, the reactor is pressurised to a pressure within these limits by addition of hydrogen before addition of any

saccharide-containing feedstock and is maintained at such a pressure as the reaction proceeds through on-going addition of hydrogen.

5 The processes of the present disclosure takes place in the presence of hydrogen. Preferably, the processes take place in the absence of air or oxygen. In order to achieve this, it is preferable that the atmosphere in the reactor be evacuated and replaced an inert gas, such as nitrogen, and then with hydrogen
10 repeatedly, after loading of any initial reactor contents, before the reaction starts.

Suitable reactors include stirred tank reactors, slurry reactors, ebulated bed reactors, jet flow reactors, mechanically agitated reactors, bubble
15 columns, such as slurry bubble columns and external recycle loop reactors. The use of these reactors allows dilution of the saccharide-containing feedstock and intermediates to an extent that provides high degrees of selectivity to the desired glycol product
20 (mainly ethylene and propylene glycols), such as by effective back-mixing.

The residence time in the reactor is suitably at least 1 minute, preferably at least 2 minutes, more preferably at least 5 minutes. Suitably the residence
25 time in the reactor is no more than 5 hours, preferably no more than 2 hours, more preferably no more than 1 hour.

Having generally described the invention, a further understanding may be obtained by reference to the
30 following examples, which are provided for purposes of illustration and are not intended to be limiting unless otherwise specified.

Examples

Experimental Apparatus:

The apparatus used to perform the experiments shown in examples 1 and 2 is schematically represented in Figure 1. A one-liter Hastelloy-C autoclave (100) was
5 equipped with automatic controls for the control of reactor temperature, back-pressure, liquid level, and stirrer speed. Feed line (1) was equipped with a gas flow meter and was used to provide a continuous flow of hydrogen gas into the reactor. Each of the liquid feed
10 lines (2) and (3) was equipped with a pump and a mass flow meter. Liquid feed line (4) was equipped with a pump capable of pumping slurry feeds, such as a suspension of starch in water. These feed lines were used to continuously feed the carbohydrate feed in the
15 form of a solution or slurry, the sodium meta-tungstate (NaMT) retro-Aldol catalyst, a solvent, and optionally a pH control agent. The excess gas pressure present in the reactor (100) was vented via line (6) by the use of back-pressure control valve (11). Filter element (5)
20 was used to retain the heterogeneous hydrogenation catalyst inside reactor (100) while allowing the flow of the liquid product, which was controlled by valve (12), via line (7). Line (8) was a coaxial in-line product cooler with the ability to cool down the
25 product mixture to or below room temperature. The gas-saturated product effluent passing through line (8) was set up to flow into gas-liquid separator (200). Valve (14) was used to control the pressure in the gas-liquid separator (200). Valve (13) was used to control the
30 level in gas-liquid separator (200). Samples of the product stream were taken via line (9) for analysis. Experimental results are reported in the following examples.

Materials

Raney-nickel (WR Grace Raney-nickel 2800), sodium metatungstate (NaMT), sodium bicarbonate (NaHCO₃), ethylene glycol (EG), 1,2-propylene glycol (PG), 1,2-butanediol (12BDO), and glycerol were purchased from Sigma-Aldrich chemical company. A sample of Kingsford-Knorr corn starch was purchased from a grocery store in Amsterdam.

Analytical Methods

1. pH measurements were made using Thermo Scientific's Orion Star A211 bench top pH meter and the meter was calibrated with standard buffer solutions in the 4-10 pH range.

2. HPLC analysis of the liquid samples was performed using the following method and conditions:

Liquid Chromatography System - Shimadzu
Controller - SCL-10Avp
Pump - LC-20AD
Degasser - DGU-20A 5r
Autosampler - SIL-10AF
Column Oven - CTO-20AC
UV detector - SPD-20AV
RI detector - RID-10A

HPLC instrument conditions:

Column: Bio-Rad Aminex HPX-87H (300 mm x 7.8 mm)
Flow Rate: 0.6 ml/minute
Column Oven: 30C
Injection Volume: 10 µl
UV Detector: @320 NM
RI Detector: mode - A; range - 100
Run Time: 66 minute
Mobile Phase: 5 mM Sulfuric Acid in water

Standard solutions containing glucose, sorbitol,

ethylene glycol (EG), 1,2-propylene glycol (PG), 1,2-butanediol (12BDO), glycerol, erythritol, threitol, xylitol, etc. were prepared using water as the solvent at various concentrations. These solutions were
5 analyzed to create the HPLC calibration curves. Samples were analyzed, with or without further dilution, and the calibration factors were applied to calculate the concentrations of the various products present in the experimental samples.

10 Example 1 (inventive): Production of glycols from starch using Raney-Ni and sodium meta-tungstate (NaMT) catalysts in water-methanol solvent mixture

In this example, 27.95 grams of a sample of WR
15 Grace Raney-nickel 2800 was added to the autoclave (Reactor 100) as slurry in 500 ml of water. The autoclave level control was set up to maintain 500 ml of liquid holdup volume in the reactor. A continuous flow of hydrogen was provided and the reactor pressure was controlled in the range of 1000 psig. The catalyst
20 was washed with deionized water at a rate of 5 ml per minute until the pH of the reactor effluent reached near neutrality. The catalyst was then activated by ramping up the temperature to 100°C and holding at
25 temperature overnight.

Preparation of water-washed starch sample: A batch washing procedure was employed in which 750 grams of
30 Kingsford-Knorr corn starch was mixed with 7.5 kg of deionized water in a 2-gallon plastic container. The resulting slurry was shaken for a minimum of two hours and then filtered under vacuum using a Buchner funnel and filter paper. The filter cake was allowed to air dry overnight, transferred onto a plastic tray placed inside a fume hood, and then crushed to a powder. The

powder was allowed to further dry under the normal laboratory humidity conditions and then transferred to a sealed container for storage. The dry weight of the starch was determined by drying a small sample in a vacuum oven at a temperature of 50–60°C until no further weight loss occurred in successive weight measurements.

A slurry of the water-washed Kingsford-Knorr corn starch was prepared in a solvent mixture containing methanol and water in 50:50 weight ratio with a starch concentration of 10.28 wt% on dry weight basis. The slurry was added to a feed vessel that was equipped with a mixer in order to maintain the suspension with a uniform concentration. The slurry was pumped into Reactor 100 with the use of a specially designed positive displacement pump that is suitable for slurry feeding. A solution of 2.00 wt% sodium meta-tungstate, the retro-Aldol catalyst, in water was prepared and loaded into another feed vessel. This solution was pumped into reactor 100 with the use of a HPLC pump.

The following experimental conditions for the reactor were used: combined slurry plus liquid feed rate in the range of 320–355 grams per hour, reaction temperature of 230°C, pressure of 1500 psig, hydrogen flow rate of 25 standard liters per hour, and stirrer RPM of 1500. The experimental conditions are additionally given in Table 1. Samples of the product stream taken via line (9) were analyzed by pH probe and HPLC to determine pH and the concentrations of the various products. The experimental results are given in Table 2.

At the end of the run the solids present in Reactor 100 were recovered as slurry in water, and the slurry was separated into a Raney-nickel fraction and a

fraction consisting of the oxides of tungsten. The Raney-Ni fraction was filtered, washed with water, and dried in air to obtain 33.71 grams of a passivated sample of the spent Raney-Ni catalyst.

5 Table 1

	Autoclave Conditions			Feed Rate [G/min]		Conc. in Rxn Mixture, %wt		
Run Time (h)	Temp (°C)	Pressure (PSIG)	RPM	Starch Conc	NaMT	Starch	NaMT	pH
5.1	230	1500	1500	4.43	0.91	8.53	0.3408	3.2
7.1	230	1500	1500	4.43	0.91	8.53	0.3408	3.2
22.6	230	1500	1500	4.43	0.91	8.53	0.3408	3.4
24.6	230	1500	1500	4.43	0.91	8.53	0.3408	3.4
31.0	230	1500	1500	4.43	1.45	7.75	0.4932	3.2
46.9	230	1500	1500	4.43	1.45	7.75	0.4932	3.3
49.4	230	1500	1500	4.43	1.45	7.75	0.4932	3.4
55.0	230	1500	1500	4.45	1.39	7.84	0.4760	3.5
67.4	230	1500	1500	4.42	1.39	7.82	0.4785	3.6
84.7	230	1500	1500	4.42	1.45	7.74	0.4940	4.0
89.2	230	1500	1500	4.42	1.45	7.74	0.4940	4.1
113.2	230	1500	1500	4.42	1.45	7.74	0.4940	4.0
116.2	230	1500	1500	4.47	1.45	7.77	0.4899	3.9
131.7	230	1500	1500	4.47	1.45	7.77	0.4899	3.9

Yields are defined as weight of product recovered divided by weight of glucose times 100%. Based on weight of starch, the yields are defined as weight of product recovered divided by weight of starch times 90%. The average of MEG yields is 34.9 %w/w and the average of the total glycols (MEG, MPG, and 1,2-BDO combined) is 39.6%w/w. For the majority of the run time these yields are nearly constant without significant decline in yield during time.

Table 2 - product yields, Example 1

*Wt% Yields - Calculated on the Basis of Glucose Content of Starch										
Run time (h)	Glucose	Sorbitol	C4 Sugars	Glycerol	Isosorb	EG	PG	HA	1,2BDO	Total
5.1	0.0	13.8	11.9	5.1	1.9	35.9	5.3	0.4	1.1	75.5
7.1	0.0	7.5	9.3	3.6	1.6	47.1	4.1	0.3	1.2	74.8
22.6	0.0	9.1	9.4	2.7	1.7	42.1	2.9	0.2	1.0	69.3
24.6	0.0	9.2	9.4	2.6	1.6	40.9	2.7	0.2	1.0	67.6
31.0	0.0	10.0	10.5	2.7	1.7	41.9	2.8	0.1	0.9	70.7
46.9	0.0	10.2	9.9	2.4	1.9	38.7	2.6	0.0	0.9	66.6
49.4	0.0	10.9	10.7	2.3	2.3	43.8	2.6	0.2	1.5	74.4
55.0	0.0	9.9	10.7	2.0	1.6	50.8	2.8	0.2	2.0	80.0
67.4	0.0	6.9	7.7	1.7	1.7	42.4	2.3	0.1	1.9	64.7
84.7	0.0	5.4	6.5	1.8	1.9	44.6	3.5	0.6	3.2	67.5
89.2	0.0	4.2	5.2	1.5	1.6	40.4	3.3	0.6	3.2	60.0
113.2	0.0	2.9	3.4	1.3	1.9	11.3	3.4	6.7	1.7	32.6
116.2	0.0	0.0	3.4	1.5	2.0	7.0	3.1	7.6	2.2	26.8
131.7	0.0	0.0	2.9	0.0	1.8	2.1	1.6	6.3	1.0	15.8

*C4 sugars include erythritol and threitol; isosorb = isosorbide, HA = hydroxyacetone; 1,2-BDO = 1,2-butanediol

Example 2 (Comparative): Production of glycols from starch using Raney-Ni and sodium meta-tungstate (NaMT) catalysts in water solvent

5 In this example, 29.63 grams of a sample of WR Grace Raney-nickel 2800 was added to the autoclave (Reactor 100) as slurry in 500 ml of water. The autoclave level control was set up to maintain 500 ml of liquid holdup volume in the reactor. A continuous flow of hydrogen was provided and the reactor pressure was controlled in the
10 range of 1000 psig. The catalyst was washed with deionized water at a rate of 5 ml per minute until the pH of the reactor effluent reached near neutrality. The catalyst was then activated by ramping up the temperature to 100°C and holding at temperature overnight.

15 A slurry of the water-washed Kingsford-Knorr corn starch was prepared in deionized water with a starch concentration of 10.94 wt% on dry weight basis. The slurry was added to a feed vessel that was equipped with a mixer in order to maintain the suspension with a
20 uniform concentration. The slurry was pumped into Reactor 100 with the use of a specially designed positive displacement pump that is suitable for slurry feeding. A solution of 2.00 wt% sodium meta-tungstate, the retro-Aldol catalyst, in water was prepared and loaded into
25 another feed vessel. This solution was pumped into Reactor 100 with the use of a HPLC pump.

The following experimental conditions for Reactor 100 were used: combined slurry plus liquid feed rate of 397 grams per hour for the first 52 hours and 154 grams per
30 hour for the last 27 hours, reaction temperature of 230°C, pressure of 1500 psig, hydrogen flow rate of 25 standard liters per hour, and stirrer RPM of 1250 or 1700. The experimental conditions are additionally given

in Table 3. Samples of the product stream taken via line (9) were analyzed by pH probe and HPLC to determine pH and the concentrations of the various products. The experimental results are given in Table 4.

At the end of the run the solids present in Reactor 100 were recovered as slurry in water, and the slurry was separated into a Raney-nickel fraction and a fraction consisting of the oxides of tungsten. The Raney-Ni fraction was filtered, washed with water, and dried in air to obtain 33.0 grams of a passivated sample of the spent Raney-Ni catalyst.

Table 3

	Autoclave Conditions			Feed Rate [G/min]		Conc in Rxn Mixture, %wt		
Run Time (h)	Temp (°C)	Pressure (PSIG)	RPM	Starch Conc	NaMt	Starch	NaMT	pH
4.5	230	1500	1250	5.67	0.95	9.37	0.2870	3.1
5.5	230	1500	1250	5.67	0.95	9.37	0.2870	3.1
20.8	230	1500	1250	5.67	0.95	9.37	0.2870	3.1
23.0	230	1500	1250	5.67	0.95	9.37	0.2870	3.1
26.7	230	1500	1250	5.67	0.95	9.37	0.2870	3.1
29.0	230	1500	1250	5.67	0.95	9.37	0.2870	3.2
44.7	230	1500	1250	5.67	0.95	9.37	0.2870	3.2
46.9	230	1500	1250	5.67	0.95	9.37	0.2870	3.3
49.5	230	1500	1250	5.67	0.95	9.37	0.2870	3.6
52.5	230	1500	1250	5.67	0.95	9.37	0.2870	3.3
54.8	230	1500	1700	2.07	0.49	9.32	0.3828	3.3
56.2	230	1500	1700	2.07	0.49	9.32	0.3828	3.3
71.1	230	1500	1700	2.07	0.49	9.32	0.3828	3.2
75.4	230	1500	1700	2.07	0.49	9.32	0.3828	3.1
79.4	230	1500	1700	2.07	0.49	9.32	0.3828	3.1

The average of MEG yields is 29.3% and the average of total glycols (MEG, MPG, and 1,2-BDo combined) is 34.6%. Severe catalyst deactivation is apparent, as glycol yields are low and yields of the corresponding hydroxyl-ketone intermediates are higher.

Table 4 - product yields, Example 2 (Comparative)

*Wt% Yields - Calculated on the Basis of Glucose Content of Starch										
Run time (h)	Glucose	Sorbitol	C4 Sugars	Glycerol	Isosorb	EG	PG	HA	1,2BDO	Total
4.5	0.4	25.2	13.4	4.2	0.0	27.8	4.0	0.3	1.2	76.5
5.5	0.3	23.1	13.5	3.8	0.0	31.6	4.1	0.3	1.3	77.9
20.8	0.3	16.6	13.3	1.7	0.0	45.8	2.5	0.3	1.5	82.2
23.0	0.4	14.6	13.3	1.6	0.0	48.0	2.3	0.5	1.7	82.4
26.7	0.4	12.7	12.9	1.7	0.0	50.5	2.2	0.4	1.9	82.8
29.0	0.4	11.2	12.6	1.6	0.0	52.2	2.3	0.5	2.3	83.0
44.7	0.4	3.7	7.2	1.4	0.0	45.6	3.7	1.7	4.3	67.9
46.9	0.3	2.1	4.8	1.0	0.0	34.1	3.1	1.2	3.7	50.3
49.5	0.3	1.3	3.2	0.7	0.0	23.2	2.2	1.1	2.7	34.7
52.5	0.4	1.2	3.5	0.8	0.0	21.2	2.7	3.2	2.8	35.7
54.8	0.4	1.5	3.9	1.1	0.0	26.2	4.9	2.6	5.0	45.6
56.2	0.3	1.3	3.6	1.2	0.0	26.3	5.0	3.0	5.4	46.0
71.1	0.2	0.3	1.2	0.0	0.0	4.6	1.4	4.2	1.7	13.5
75.4	0.2	0.0	0.9	0.0	0.0	1.6	0.8	4.1	0.9	8.5
79.4	0.2	0.0	0.8	0.0	0.0	1.1	0.6	4.1	0.8	7.6

*C4 sugars include erythritol and threitol; isosorb = isosorbide, HA = hydroxyacetone; 1,2-BDO = 1,2-butanediol

Example 3: Analysis of spent catalyst

A sample of the spent Raney-Ni catalyst recovered from Example-1 was extracted with methanol solvent in a Soxhlet extractor and the methanol solution was
5 evaporated to obtain a carbonaceous residue. The amount of the residue accounted for 0.4% wt of the recovered catalyst, indicating a relatively clean catalyst with respect to fouling by the decomposition products of starch.

10

Example 4 (Comparative): Analysis of spent catalyst

A sample of the spent Raney-Ni catalyst recovered from Example-2 was extracted with methanol solvent in a Soxhlet extractor and the methanol solution was
15 evaporated to obtain a carbonaceous residue. The amount of the residue accounted for 16.2% wt of the recovered catalyst, indicating a catalyst that was heavily fouled by the decomposition products of starch.

20

The Examples clearly demonstrate that the use of an alcoholic solvent in the reaction medium has the benefits of 1) higher average glycols product yields, 2) longer run time before the catalyst deactivates due to fouling by the heavy ends produced in the reaction, and 3) lack
25 of fouling by carbonaceous materials thus making it easier to regenerate the catalyst.

C L A I M S

1. A process for the production of glycols comprising:
contacting a saccharide-containing feedstock with
hydrogen in the presence of a catalyst composition and a
5 solvent,

wherein the solvent comprises water and at least 25%
by weight, based on the total weight of the solvent, of
one or more alcohols selected from a C₁ to C₆ alcohol, a
C₁ to C₆ polyalcohol, and a combination thereof, and

10 wherein the catalyst composition comprises at least
two active catalytic components, the active catalyst
components comprising, as a first active catalyst
component, one or more materials selected from transition
metals from groups 8, 9 or 10 or compounds thereof, with
15 catalytic hydrogenation capabilities; and, as a second
active catalyst component, one or more materials selected
from tungsten, molybdenum, lanthanum, tin or compounds or
complexes thereof.

2. A process as claimed in Claim 1, wherein the solvent
20 comprises from 25% to 75% by weight, based on the total
weight of the solvent, of the one or more alcohols.

3. A process as claimed in Claim 1 or Claim 2, wherein
the saccharide-containing feedstock comprises one or more
saccharides selected from glucose, sucrose, and starch.

25 4. A process as claimed in any one of Claims 1 to 3,
wherein the solvent comprises one or more C₁ to C₆
alcohols selected from methanol, ethanol, 1-propanol and
iso-propanol.

5. A process as claimed in any one of Claims 1 to 4,
30 wherein the solvent comprises one or more C₁ to C₆
polyalcohols selected from glycerol, erythritol,
threitol, and sorbitol.

6. A process as claimed in any one or Claims 1 to 5, wherein the glycols comprise monoethylene and monopropylene glycols.

FIGURE 1

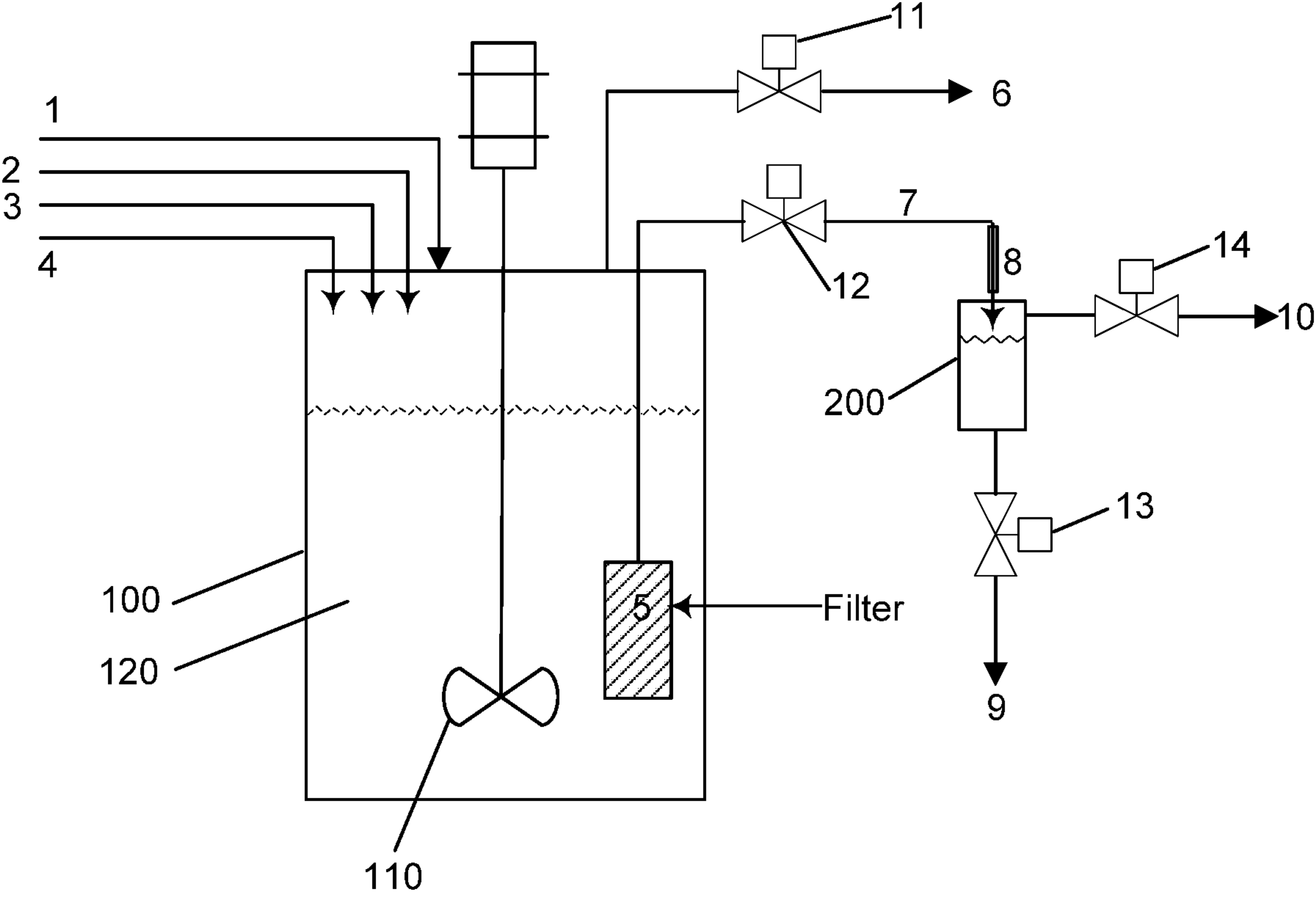


FIGURE 1

