US008091984B2

(12) **United States Patent**
Silverbrook

(10) **Patent No.: US 8,091,984 B2**
(45) **Date of Patent: *Jan. 10, 2012**

(54) **INKJET PRINTHEAD EMPLOYING ACTIVE AND STATIC INK EJECTION STRUCTURES**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 222 days.

This patent is subject to a terminal disclaimer.

(21) Appl. No.: **12/505,525**

(22) Filed: **Jul. 19, 2009**

(65) **Prior Publication Data**

US 2009/0278894 A1 Nov. 12, 2009

Related U.S. Application Data

(63) Continuation of application No. 10/728,784, filed on Dec. 8, 2003, now Pat. No. 7,575,298, which is a continuation-in-part of application No. 10/307,330, filed on Dec. 2, 2002, now Pat. No. 6,666,544.

(51) **Int. Cl.**
B41J 2/25 (2006.01)

(52) **U.S. Cl.** **347/47**

(58) **Field of Classification Search** 347/40–43, 347/47, 62, 64–65

See application file for complete search history.

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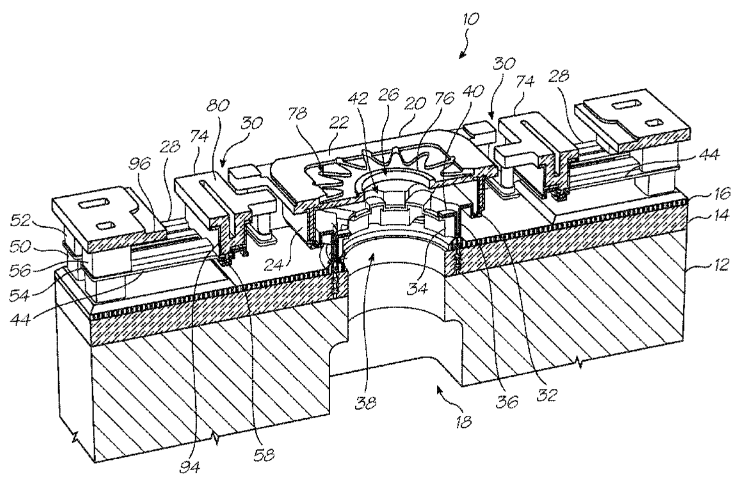
Primary Examiner — Lamson Nguyen

(57) **ABSTRACT**

An inkjet printhead includes a wafer having a droplet ejection side and a liquid supply side opposite the droplet ejection side; a plurality of active ink ejection structures formed on the droplet ejection side of the wafer, each active ink ejection structure partially defining a nozzle chamber, and defining an ink ejection port; a plurality of individual fluid passages formed in the wafer, each fluid passage providing fluid to corresponding nozzle chambers; a plurality of static ink ejection structures formed on the droplet ejection side of the wafer and inside of corresponding active ink ejection structures, each static ink ejection structure defining a nozzle chamber with a corresponding active ink ejection structure; and droplet ejection actuators respectively corresponding to each active ink ejection structure. The droplet ejection actuators are formed on the droplet ejection side of the wafer and attached to respective active ink ejection structures. The droplet ejection actuators are operable to displace an active ink ejection structures towards a corresponding static ink ejection structure to effect ejection of fluid in the nozzle chamber through the ink ejection port.

8 Claims, 15 Drawing Sheets



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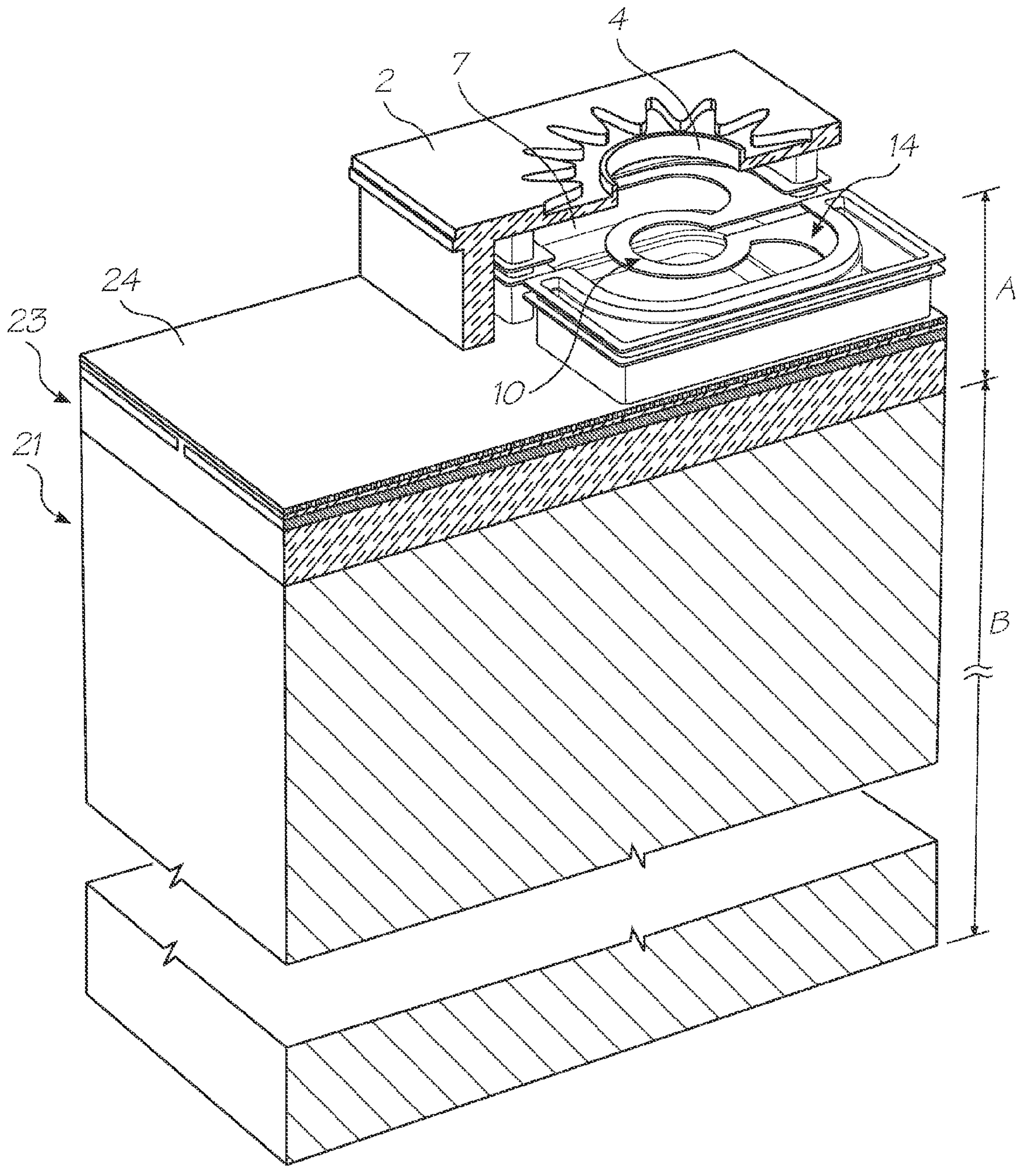

FIG. 1

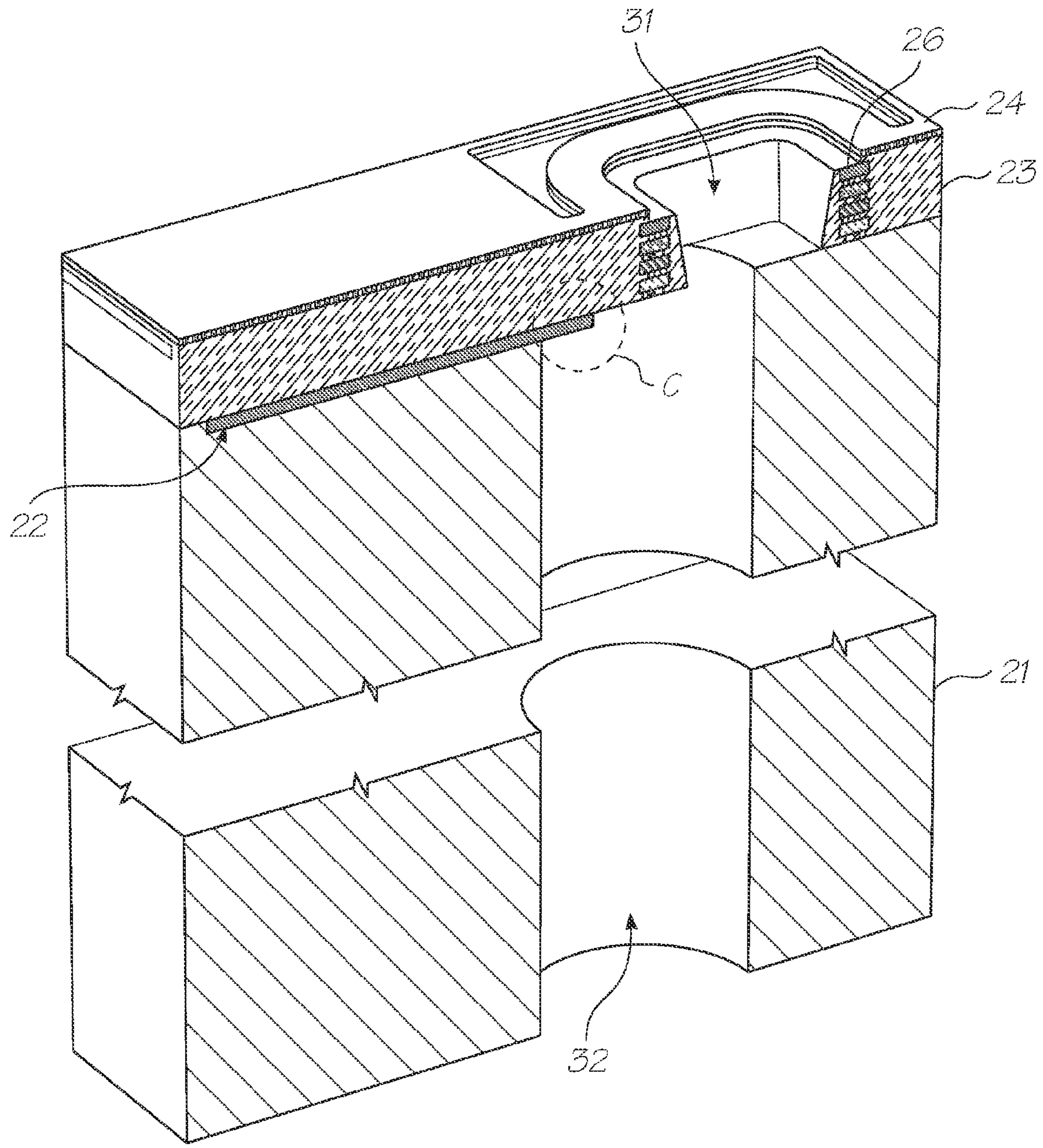

FIG. 2

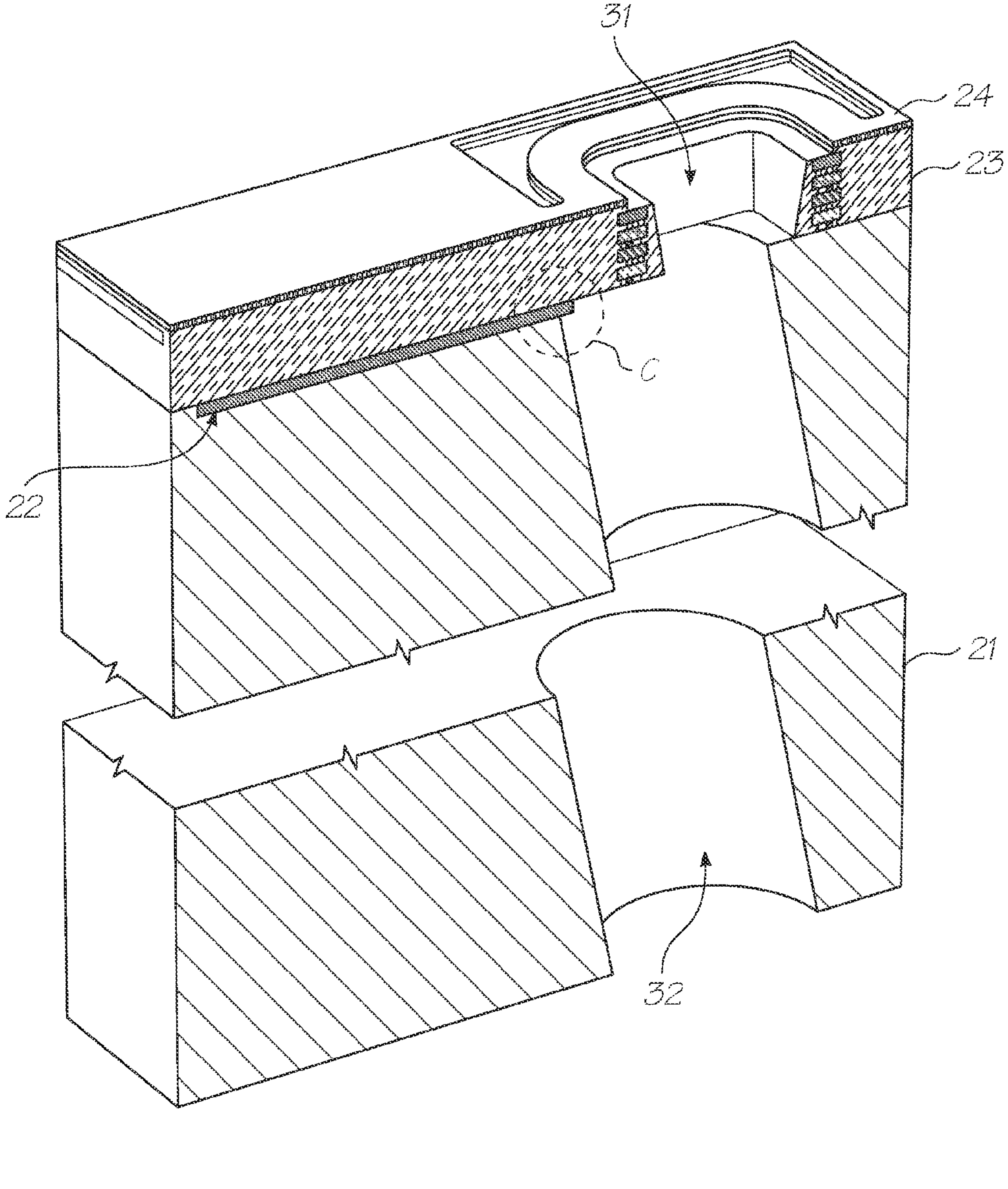

FIG. 3

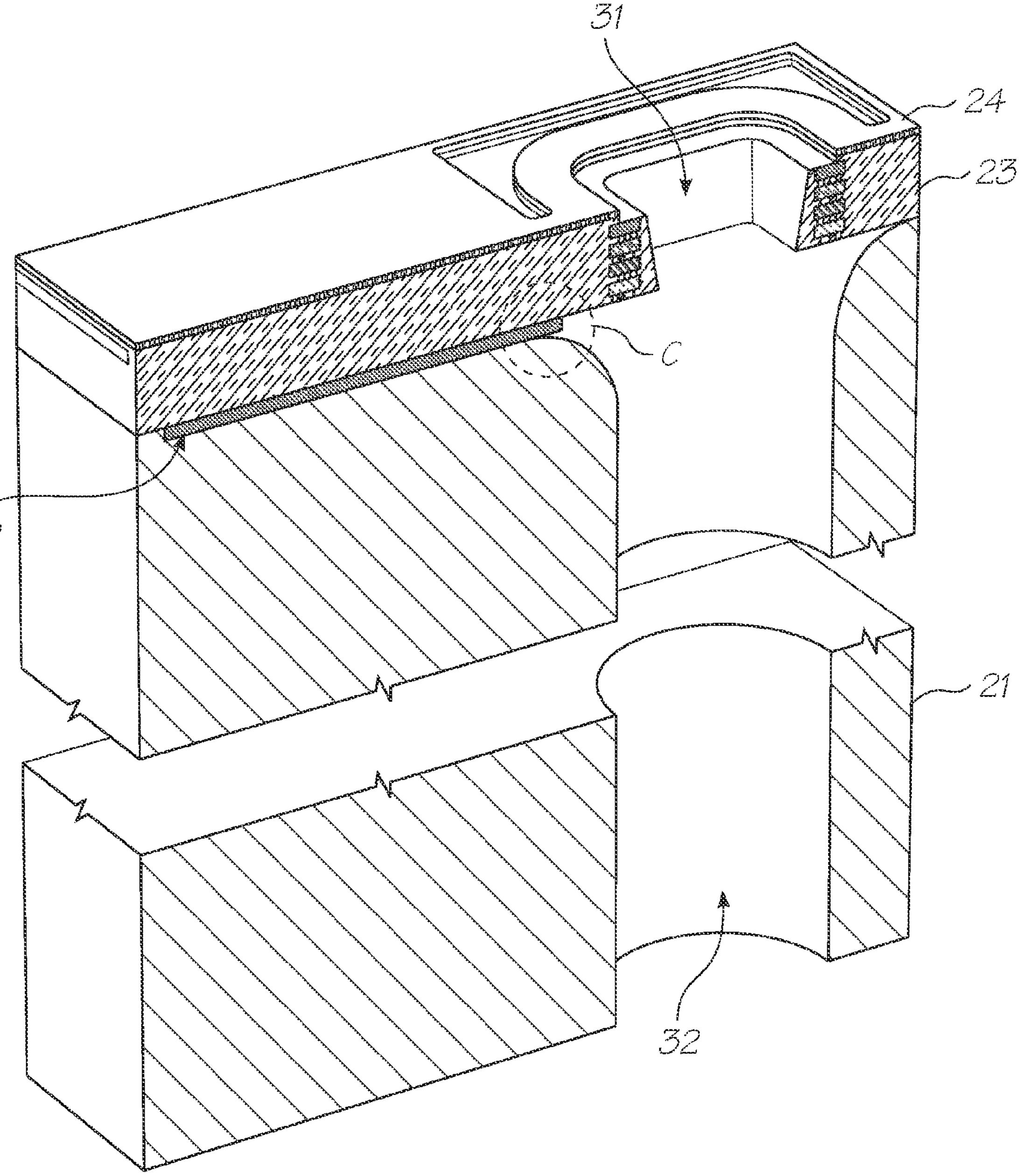

FIG. 4

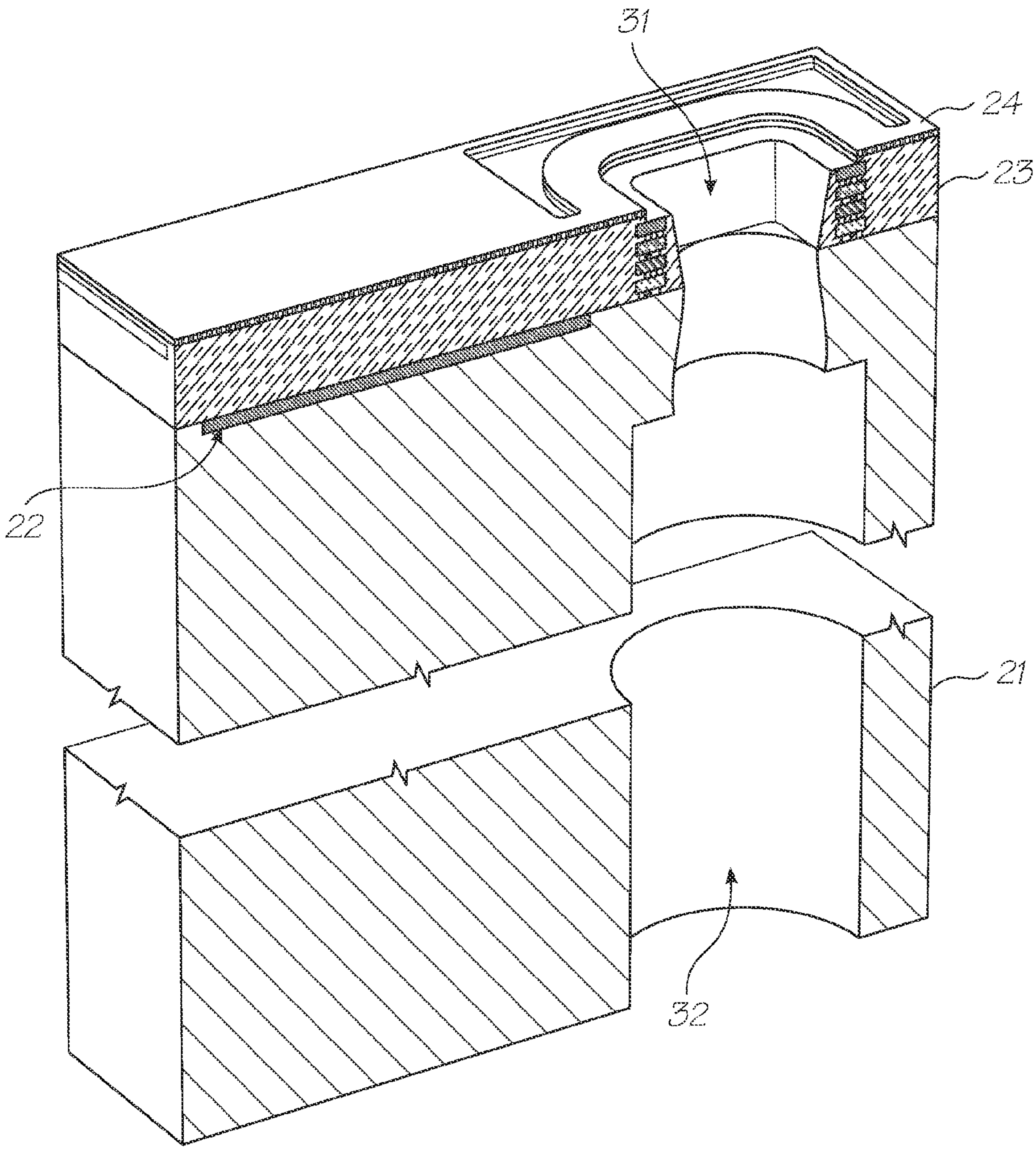

FIG. 5

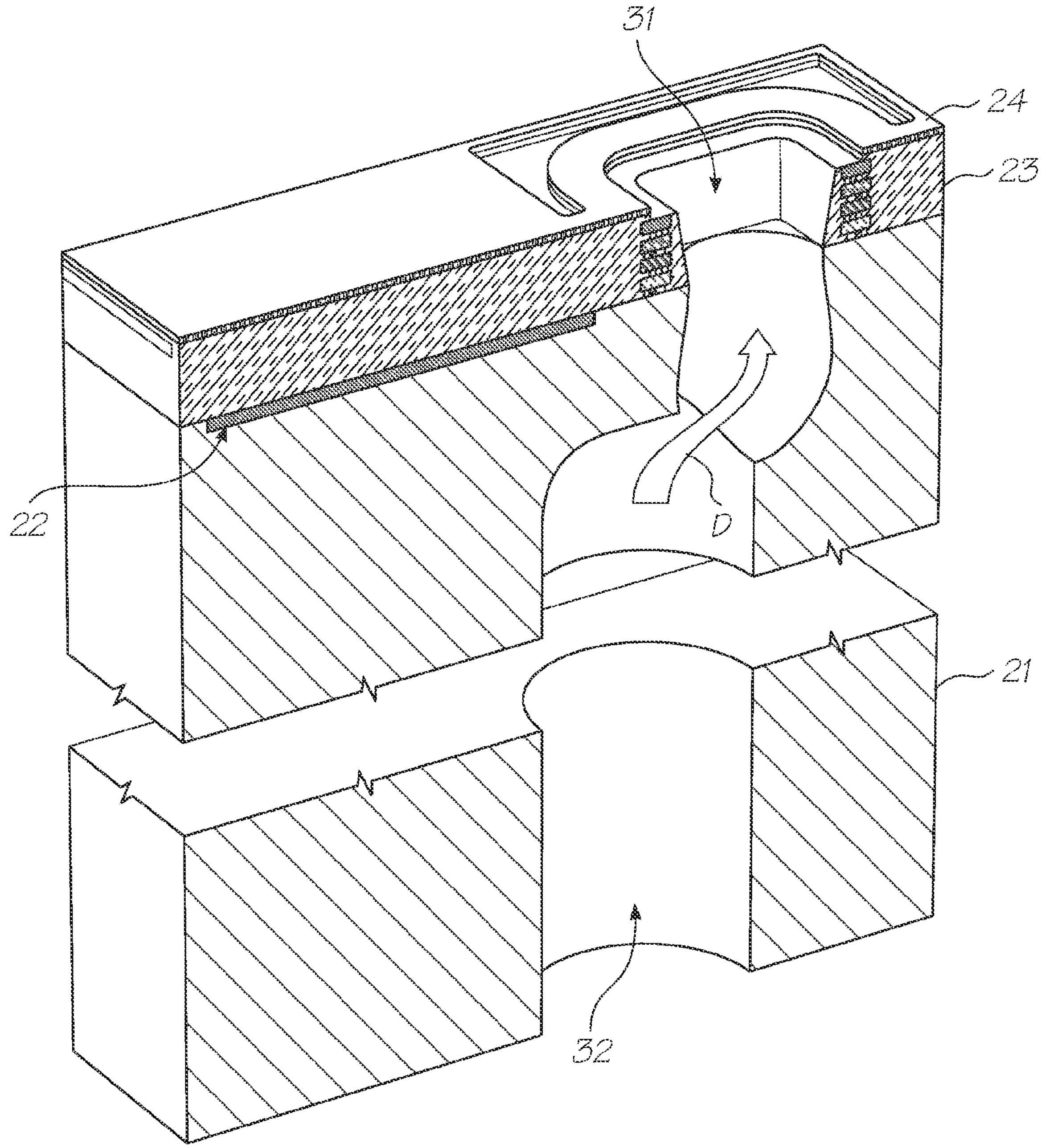

FIG. 6

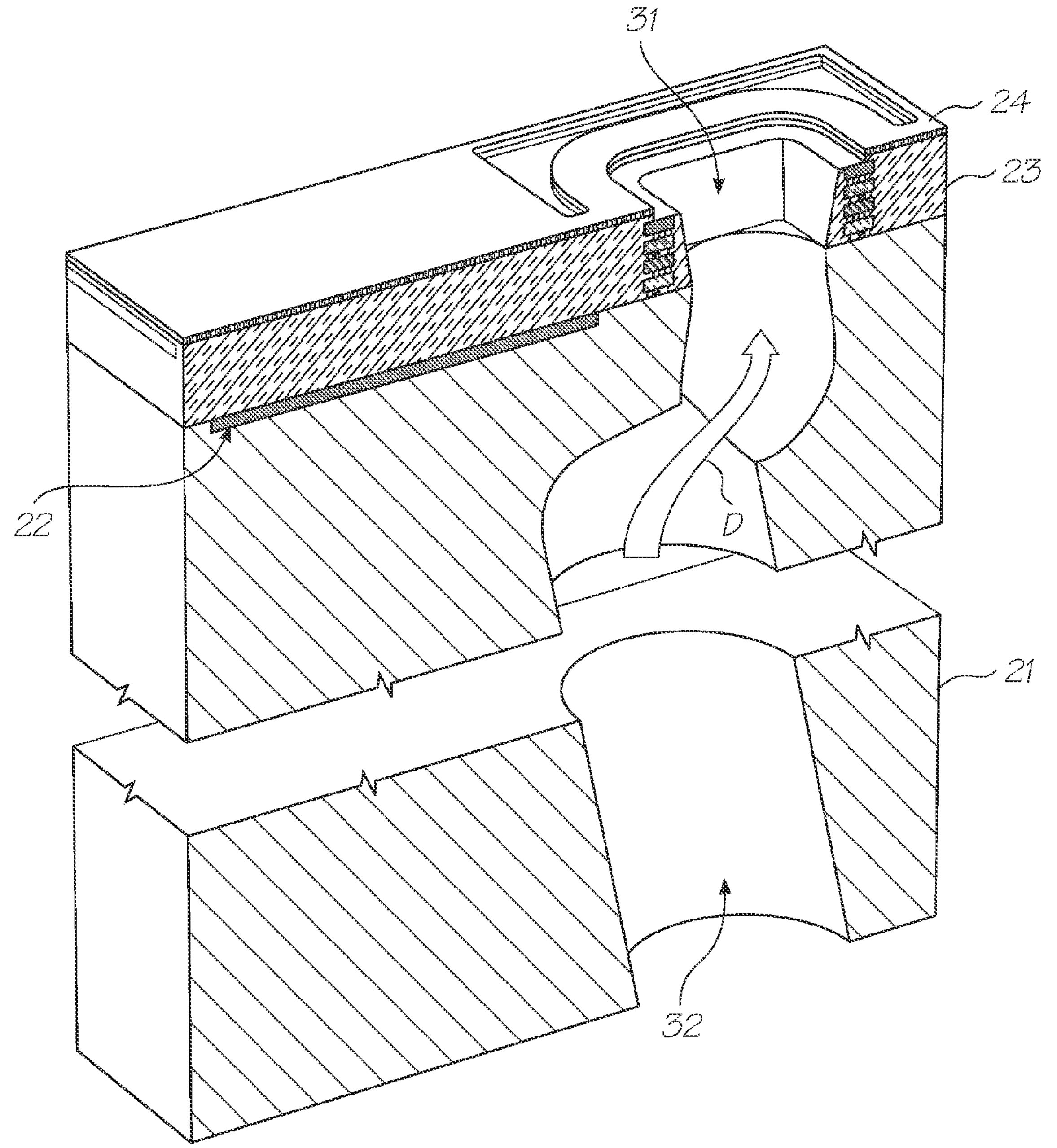

FIG. 7

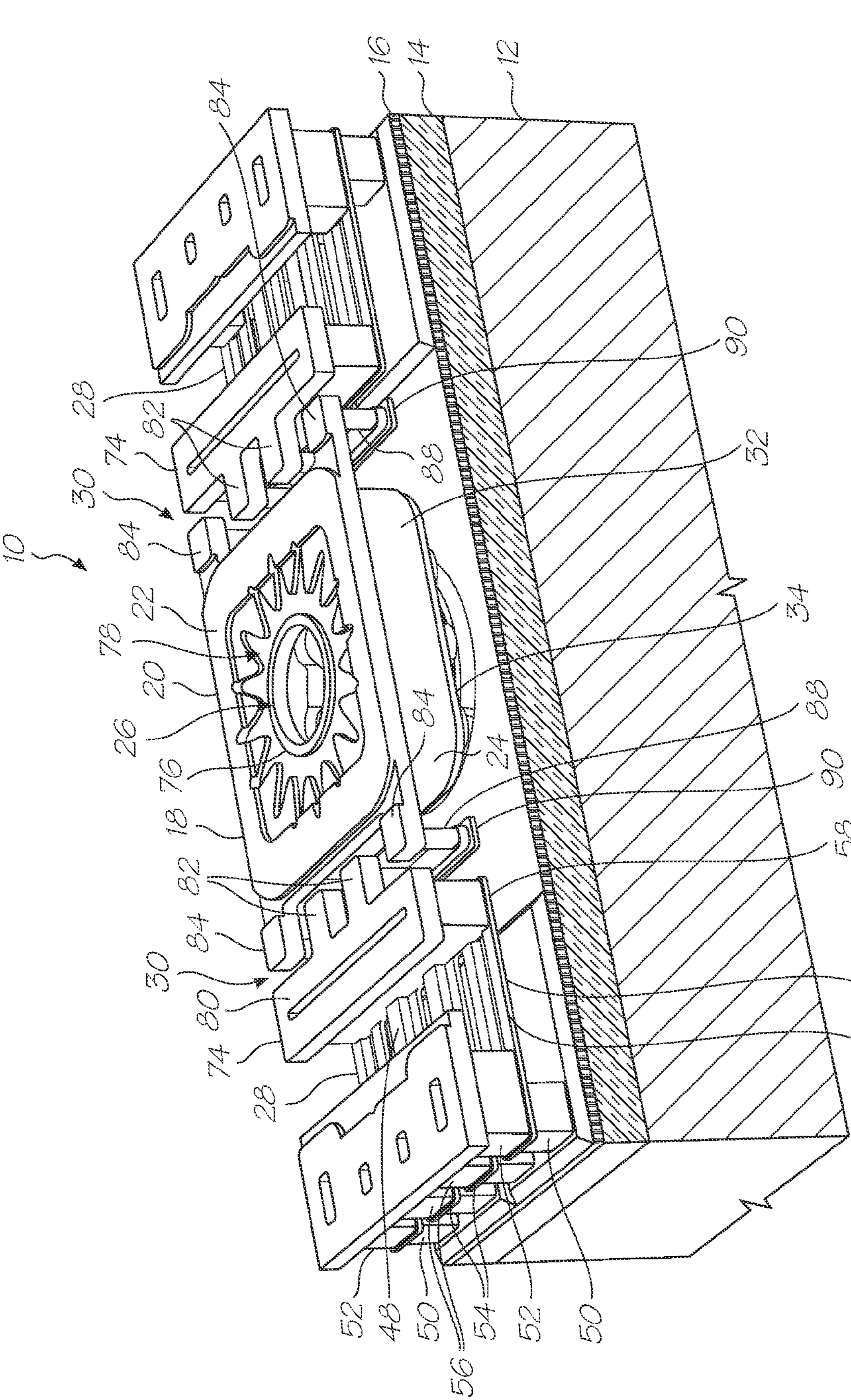
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FIG. 8

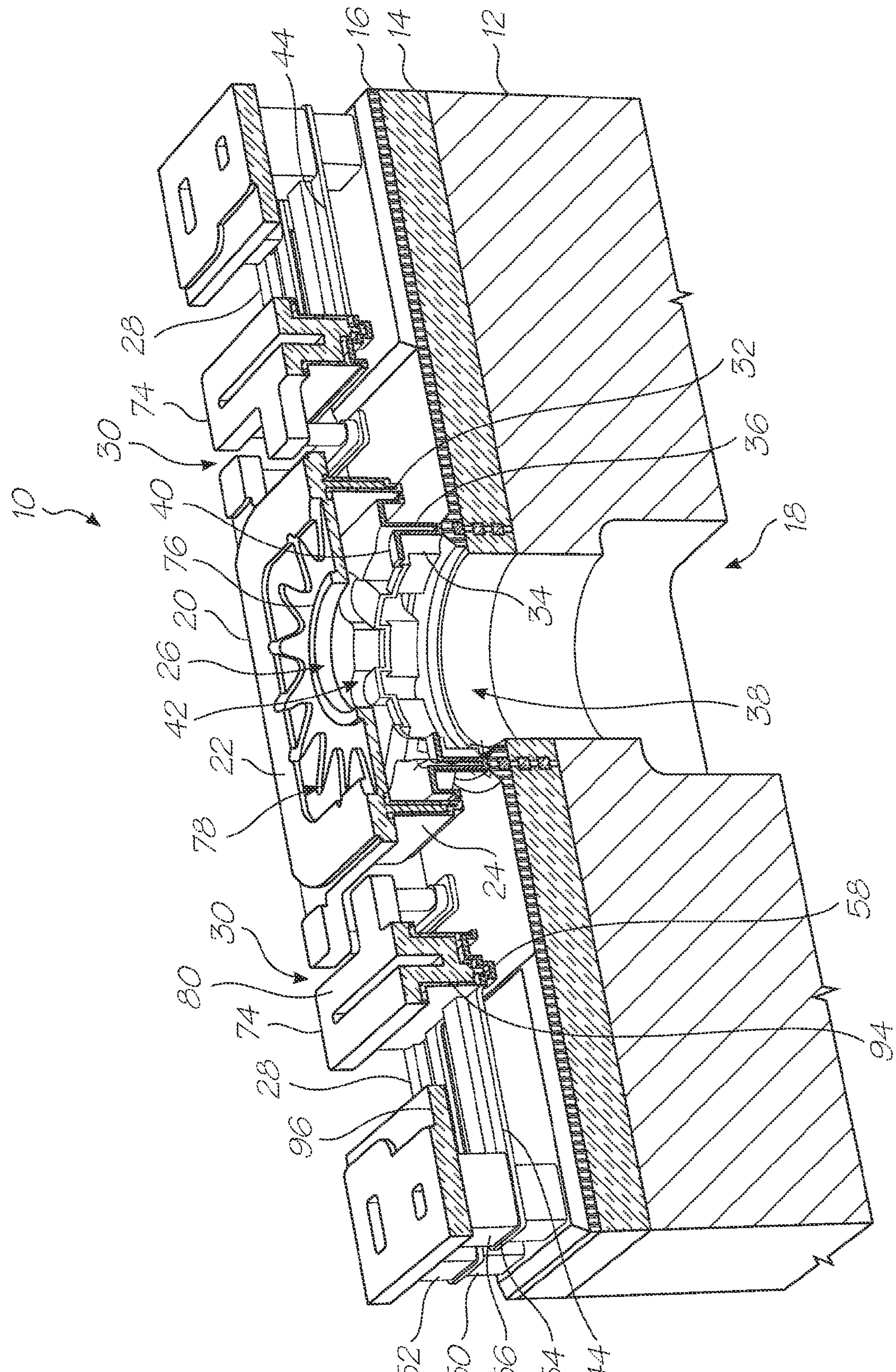
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FIG. 9

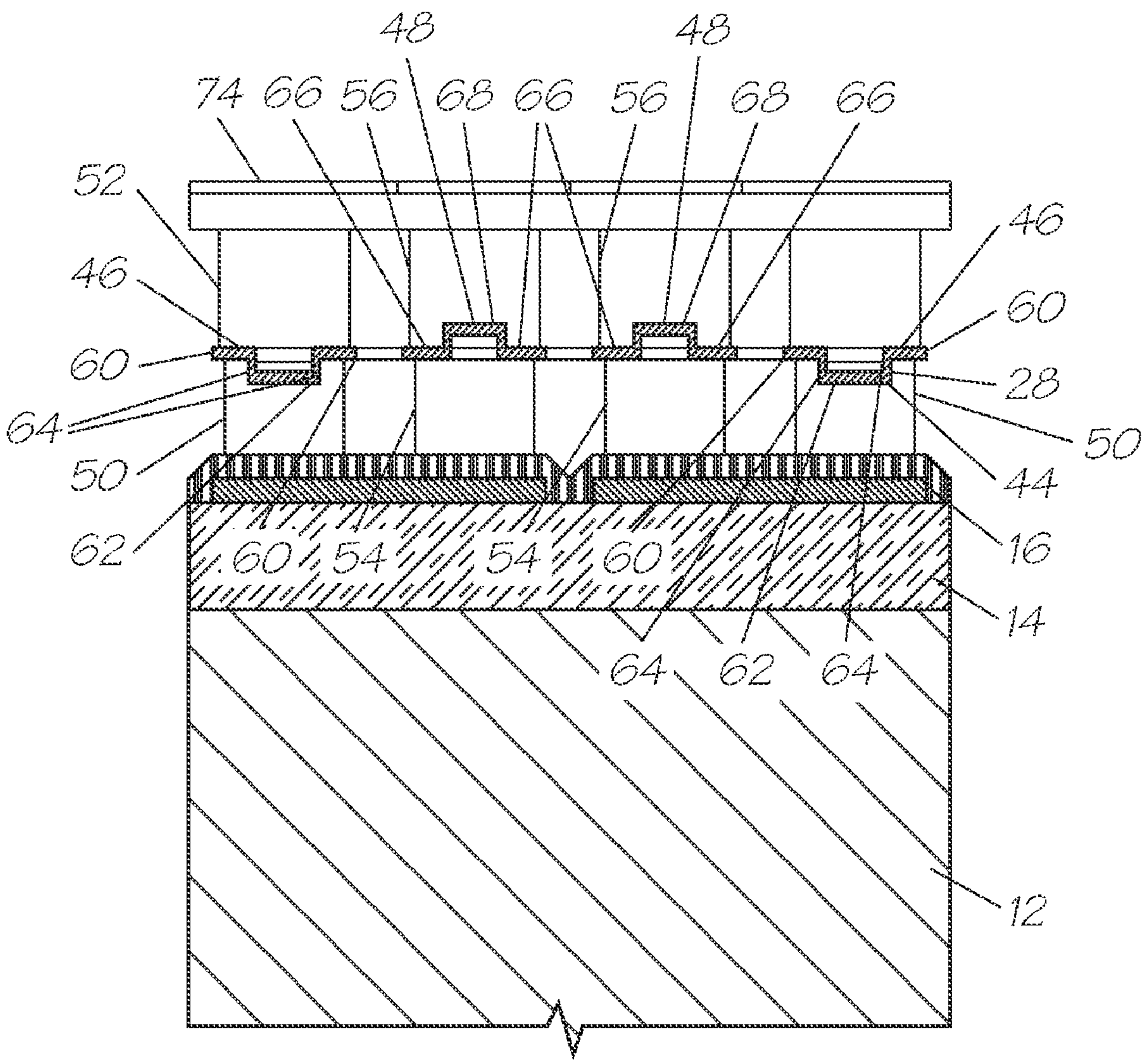
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FIG. 10

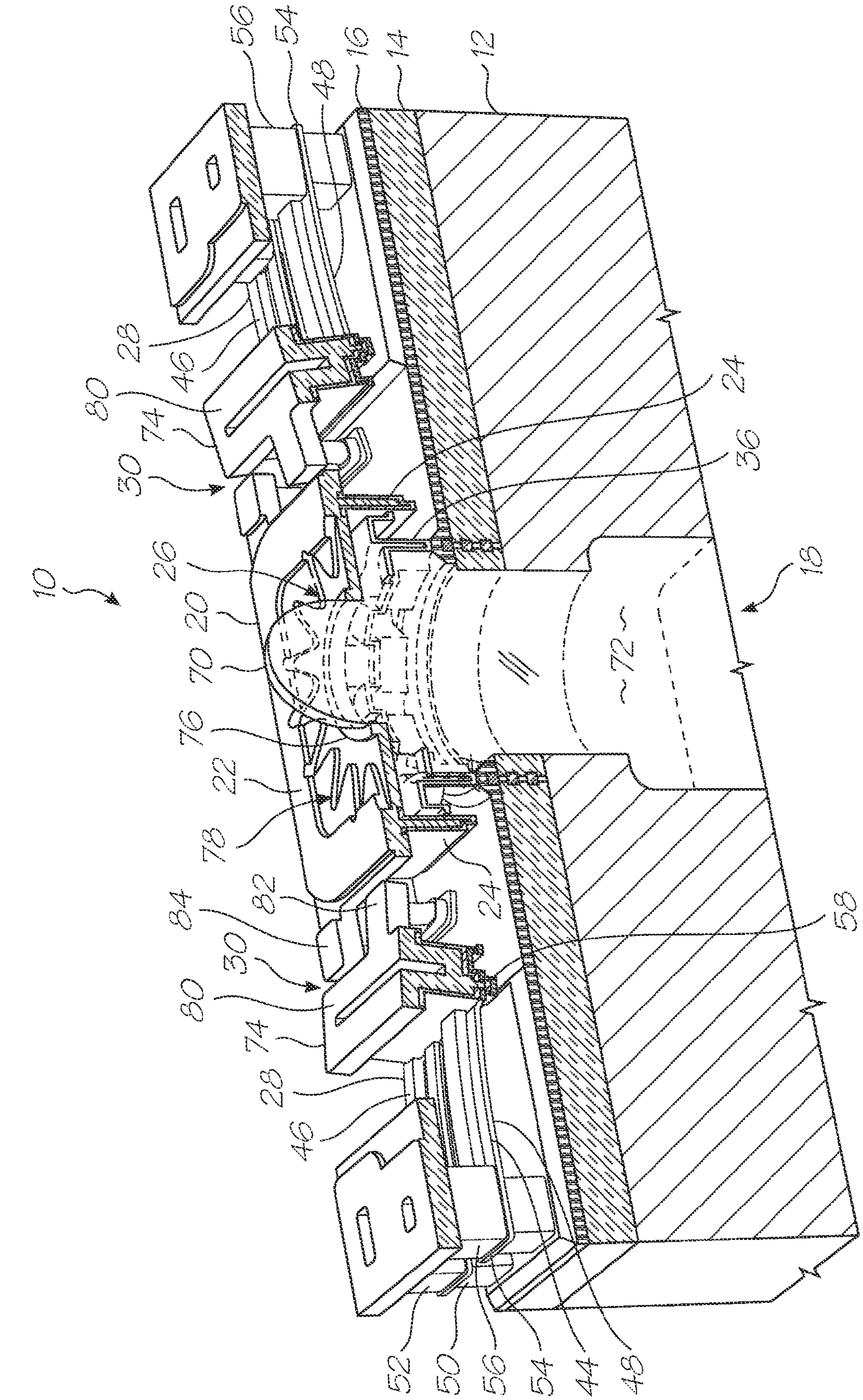
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FIG. 11

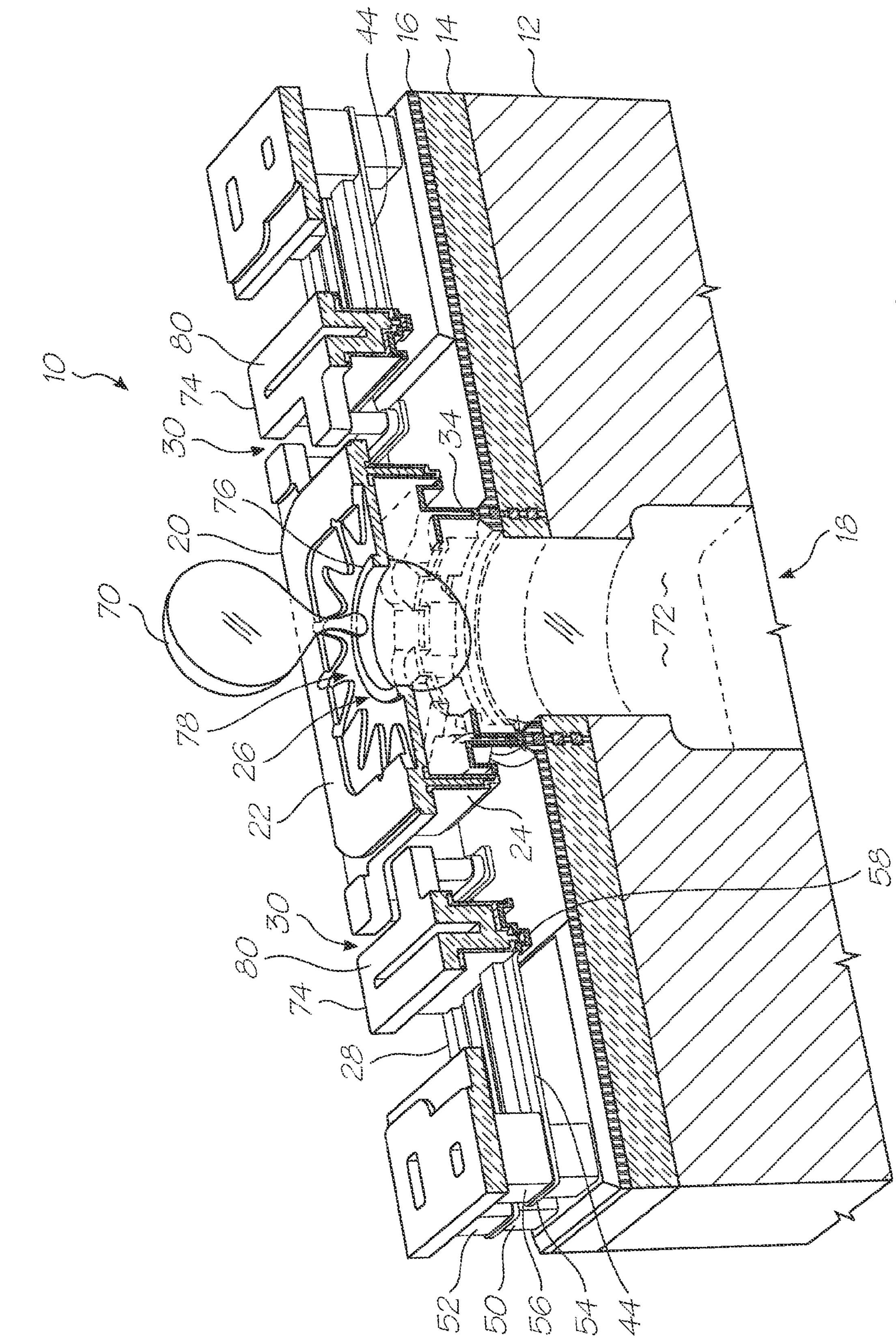
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FIG. 12

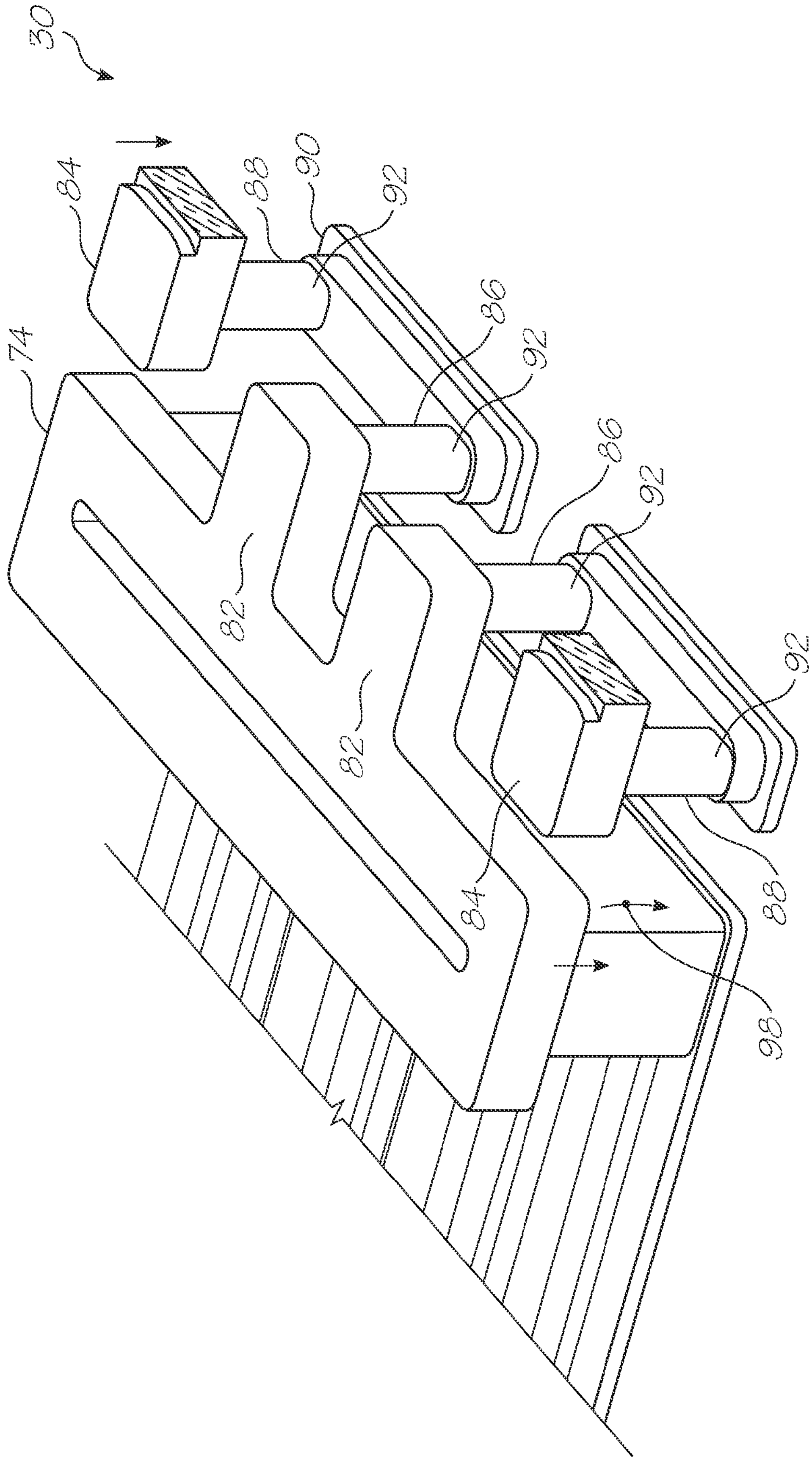

FIG. 13

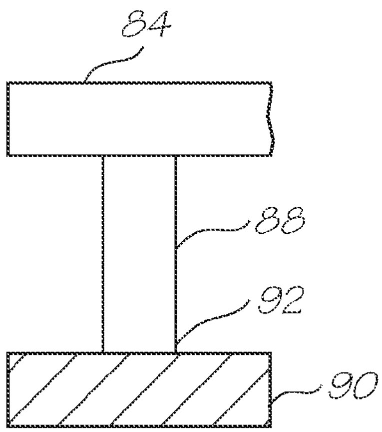

FIG. 14

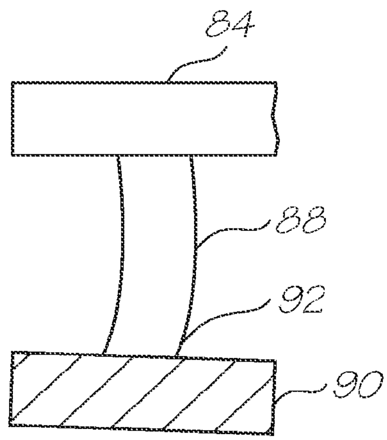

FIG. 15

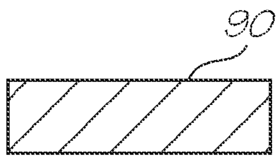

FIG. 16

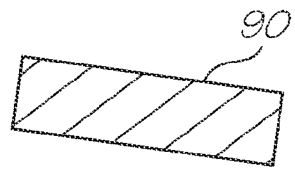

FIG. 17

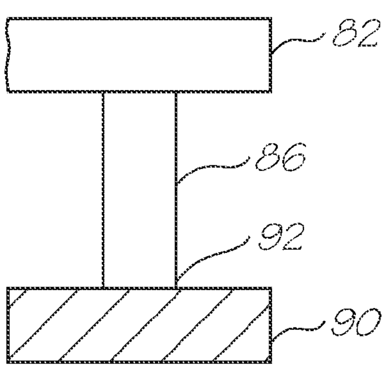

FIG. 18

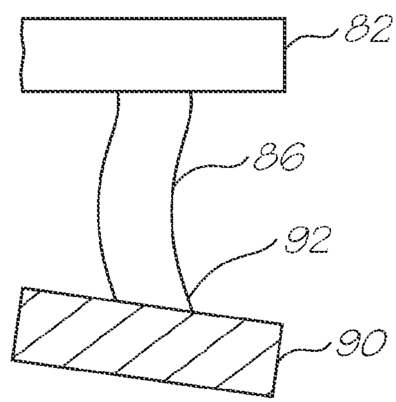

FIG. 19

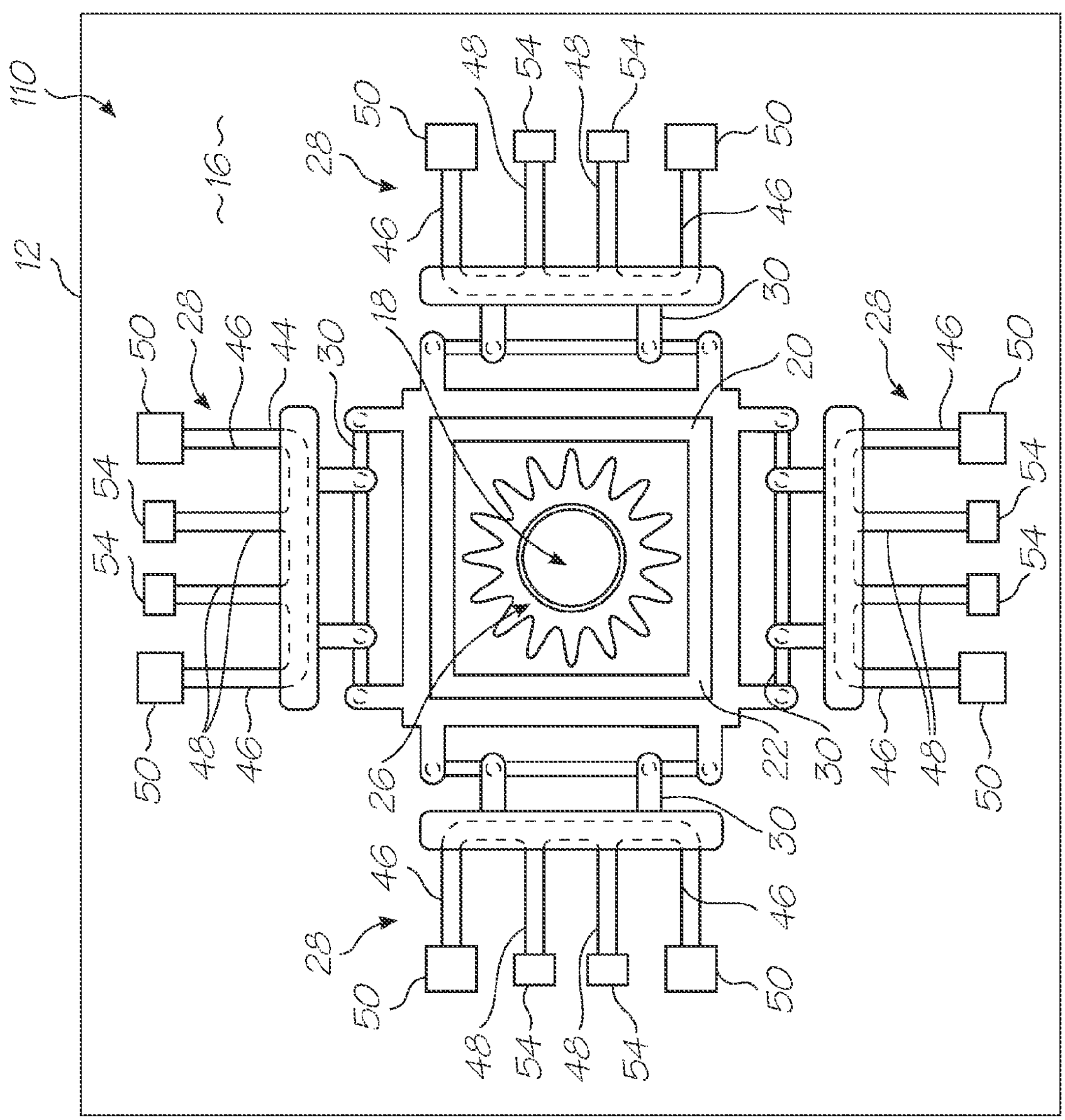

FIG. 20

INKJET PRINTHEAD EMPLOYING ACTIVE AND STATIC INK EJECTION STRUCTURES

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation of U.S. Ser. No. 10/728,784 filed Dec. 8, 2003, which is a Continuation In Part Application of U.S. Ser. No. 10/307,330 filed on Dec. 2, 2002, now issued U.S. Pat. No. 6,666,544, all of which are herein incorporated by reference.

FIELD OF THE INVENTION

This invention relates to the fabrication of fluid ejection chips. More particularly, this invention relates to fabrication techniques of fluid ejection chips that minimize the spacing between adjacent nozzles.

REFERENCED PATENT APPLICATIONS

The following applications are incorporated by reference:

6,362,868	6,227,652	6,213,588	6,213,589	6,231,163	6,247,795
6,394,581	6,244,691	6,257,704	6,416,168	6,220,694	6,257,705
6,247,794	6,234,610	6,247,793	6,264,306	6,241,342	6,247,792
6,264,307	6,254,220	6,234,611	6,302,528	6,283,582	6,239,821
6,338,547	6,247,796	6,557,977	6,390,603	6,362,843	6,293,653
6,312,107	6,227,653	6,234,609	6,238,040	6,188,415	6,227,654
6,209,989	6,247,791	6,336,710	6,217,153	6,416,167	6,243,113
6,283,581	6,247,790	6,260,953	6,267,469	6,273,544	6,309,048
6,420,196	6,443,558	6,439,689	6,378,989	6,848,181	6,634,735
6,623,101	6,406,129	6,505,916	6,457,809	6,550,895	6,457,812
6,428,133	6,755,509				

BACKGROUND OF THE INVENTION

As set out in the above referenced applications/patents, the Applicant has spent a substantial amount of time and effort in developing printheads that incorporate micro electro-mechanical system (MEMS)—based components to achieve the ejection of ink necessary for printing.

As a result of the Applicant's research and development, the Applicant has been able to develop printheads having one or more printhead chips that together incorporate up to 84 000 nozzle arrangements. The Applicant has also developed suitable processor technology that is capable of controlling operation of such printheads. In particular, the processor technology and the printheads are capable of cooperating to generate resolutions of 1600 dpi and higher in some cases. Examples of suitable processor technology are provided in the above referenced patent applications/patents.

The Applicant has overcome substantial difficulties in achieving the necessary ink flow and ink drop separation within the ink jet printheads.

It is generally beneficial to increase the nozzle densities on a printhead to enhance the print resolution. MEMS fabrication of the nozzles on silicon wafer allows very high nozzle density. However, the wafer is typically about 200 microns thick with the nozzle guards, ink chambers, ejection actuators and so on occupying a layer about 20 microns thick on one side. Ink supply passages must be formed through the wafer to the nozzles.

It is not practical to form the ink supply passages from the nozzle side of the wafer through to the supply side. The fabrication of other nozzle structures would require the entire supply passage to be filled with resist while the other structures were lithographically form on top. The resist subsequently needs to be stripped out of the passage. To strip a 200-micron deep passage of resist would be difficult and time consuming.

Forming the ink supply passages from the supply side of the wafer through to the nozzle side presents its own difficulties. Firstly, the precise alignment of the masking on the supply side with the ink chambers of each nozzle on the other side is difficult. At present, the best equipment available for aligning the mask have ±2 microns accuracy. Secondly, a deep etch will often deviate from a straight path because the ions in the etchant are influenced by any charged particles in the wafer. Thirdly, the plasma etchant will often track sideways along an interface between silicon wafer and dielectric material.

Misalignment of the supply passage can lead to the plasma etch contacting and damaging other components of the nozzle, for example, the drive circuitry for the ejection actuator. Furthermore, the above causes of misalignment can compound into large inaccuracies which imposes limits on the size of the nozzle structure and the spacing between nozzles. This, of course, reduces the density of nozzles and lowers the resolution.

It is an object of the present invention to provide a useful alternative to known printheads and the techniques for fabricating them. In particular the invention aims to provide a method of making printhead chips that accommodate the standard manufacturing tolerances involved while minimizing the spacing between adjacent nozzles.

SUMMARY OF THE INVENTION

According to one aspect of the present disclosure, an inkjet printhead includes a wafer having a droplet ejection side and a liquid supply side opposite the droplet ejection side; a plurality of active ink ejection structures formed on the droplet ejection side of the wafer, each active ink ejection structure partially defining a nozzle chamber, and defining an ink ejection port; a plurality of individual fluid passages formed in the wafer, each fluid passage providing fluid to corresponding nozzle chambers; a plurality of static ink ejection structures formed on the droplet ejection side of the wafer and inside of corresponding active ink ejection structures, each static ink ejection structure defining a nozzle chamber with a corresponding active ink ejection structure; and droplet ejection actuators respectively corresponding to each active ink ejection structure. The droplet ejection actuators are formed on the droplet ejection side of the wafer and attached to respective active ink ejection structures. The droplet ejection actuators are operable to displace an active ink ejection structures towards a corresponding static ink ejection structure to effect ejection of fluid in the nozzle chamber through the ink ejection port.

BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings,

FIG. **1** is a schematic perspective view, partially cut away, of a unit cell of a printhead according to the invention;

FIG. **2** shows a schematic, sectioned perspective of a unit cell of the type shown in FIG. **1**, at an intermediate stage of its fabrication;

FIG. **3** shows a schematic, sectioned perspective of a unit cell of the type shown in FIG. **1**, at an intermediate stage of its fabrication;

FIG. **4** shows a schematic, sectioned perspective of a unit cell of the type shown in FIG. **1**, at an intermediate stage of its fabrication;

FIG. **5** shows a schematic, sectioned perspective of the unit cell shown in FIG. **1**, at an intermediate stage of its fabrication in accordance with the present invention;

FIG. **6** shows a schematic, sectioned perspective of the unit cell shown in FIG. **1**, at an intermediate stage of its fabrication in accordance with the present invention;

FIG. **7** shows a schematic, sectioned perspective of the unit cell shown in FIG. **1**, at an intermediate stage of its fabrication in accordance with the present invention;

FIG. **8** shows a three-dimensional view of a nozzle arrangement of a thermal bend actuator embodiment of a printhead chip in accordance with the invention, for an inkjet printhead;

FIG. **9** shows a three-dimensional sectioned view of the nozzle arrangement of FIG. **8**;

FIG. **10** shows a transverse cross sectional view of a thermal bend actuator of the nozzle arrangement of FIG. **8**;

FIG. **11** shows a three-dimensional sectioned view of the nozzle arrangement of FIG. **8**, in an initial stage of ink drop ejection;

FIG. **12** shows a three-dimensional sectioned view of the nozzle arrangement of FIG. **8**, in a terminal stage of ink drop ejection;

FIG. **13** shows a schematic view of one coupling structure of the nozzle arrangement of FIG. **8**;

FIG. **14** shows a schematic view of a part of the coupling structure attached to an active ink ejection structure of the nozzle arrangement, when the nozzle arrangement is in a quiescent condition;

FIG. **15** shows the part of FIG. **14** when the nozzle arrangement is in an operative condition;

FIG. **16** shows an intermediate section of a connecting plate of the coupling structure, when the nozzle arrangement is in a quiescent condition;

FIG. **17** shows the intermediate section of FIG. **16**, when the nozzle arrangement is in an operative condition;

FIG. **18** shows a schematic view of a part of the coupling structure attached to a connecting member of the nozzle arrangement when the nozzle arrangement is in a quiescent condition;

FIG. **19** shows the part of FIG. **18** when the nozzle arrangement is in an operative condition; and

FIG. **20** shows a plan view of a nozzle arrangement of a second embodiment of a printhead chip, in accordance with the invention, for an ink jet printhead.

DETAILED DESCRIPTION OF THE INVENTION

The present invention is applicable to printheads formed on and through silicon wafers by lithographic etching and deposition techniques, regardless of whether bubble forming heater elements or thermal bend actuators are used.

Bubble Forming Heater Element Actuated Printheads

FIG. **1** shows a nozzle of this type. The nozzles, ejection actuators, associated drive circuitry and ink supply passages are formed on and through a wafer using lithographically masked etching techniques described in great detail in U.S. Ser. No. 10/302,274. In the interests of brevity, the disclosure of the '274 application is incorporated herein in its entirety. For convenience, the reference numerals on FIGS. **1** to **7** accord with the reference numbering used in '274. Corresponding features of the embodiments shown in FIGS. **8** to **20** do not necessarily use the same reference numerals.

The unit cell **1** is shown with part of the walls **6** and nozzle plate **2** cut-away, which reveals the interior of the chamber **7**. The heater **14** is not shown cut away, so that both halves of the heater element **10** can be seen.

In operation, ink **11** passes through the ink inlet passage **31** (see FIGS. **2**-**7**) to fill the chamber **7**. Then a voltage is applied across the electrodes **15** to establish a flow of electric current through the heater element **10**. This heats the element **10**, to form a vapor bubble in the ink within the chamber **7** to eject a drop of ink.

It is generally beneficial to increase the nozzle densities on a printhead to enhance the print resolution. MEMS fabrication of the nozzles on silicon wafer allows very high nozzle density. However, the wafer is typically about 200 microns thick with the nozzle guards, ink chambers, ejection actuators and so on occupying a layer about 20 microns thick on one side. These dimensions are indicated generally by A and B on FIG. **1**.

FIGS. **2** to **7** show the unit cell with the ink chamber **7** and heater element **10** removed for clarity. Ink is supplied to the chambers by passages **32** extending to the opposite side of the wafer. It would be convenient to etch these passages **32** from the nozzle side of the wafer as this side will be subject to etching and deposition to form the nozzle structures. Unfortunately, it is not practical to form the ink supply passages from the nozzle side of the wafer. The entire supply passage **32** would have to be filled with resist while the nozzle structures were lithographically formed. Stripping the resist out of a 200-micron deep passage of resist would be prohibitively difficult and time consuming.

Forming the ink supply passages from the supply side of the wafer through to the nozzle side presents its own difficulties. These problems are schematically illustrated in FIGS. **2**, **3** and **4**.

Referring to FIG. **2**, the ink supply passage is etched through the wafer **21** to the CMOS metallisation layers of the interconnect **23**. The inlet **31** in the interconnect **23** provides a fluid connection between the supply passage **32** and the nozzle chamber (not shown) to be formed on the passivation layer **24**. Guard rings **26** prevent ink from diffusing from within the inlet **31** to the wiring in the interconnect **23** and the CMOS drive circuitry **22** between the wafer substrate **21** and the interconnect **23**. Unfortunately, the precise alignment of the masking on the supply side of the wafer with the ink chambers of each nozzle on the nozzle side is difficult. At present, the best equipment available for aligning the mask has ±2 microns accuracy. If the drive circuitry **22** is too close to the inlet **31**, a portion C of the circuitry **22** risks damage by the etchant due to misalignment of the passage **32**.

Another problem is schematically shown in FIG. **3**. A deep etch will often deviate from a straight path. Ions in the etchant are influenced by any charged particles in the wafer **21**. While the mask may be perfectly aligned on the supply side of the wafer **21**, the deep etch is slightly angled and can result in a significant misalignment at the interface of the wafer **21** and the interconnect **23**. Again, if the drive circuitry **22** is too close, a portion C may be destroyed by the oxygen plasma etchant.

FIG. **4** illustrates another potential problem. The plasma etchant will often track sideways along an interface between silicon wafer **21** and dielectric material of the interconnect **23**. Once again, this can lead to inadvertent etching of the drive circuitry **22**.

The above causes of misalignment can compound into large inaccuracies that imposes limits on the size of the nozzle structure and the spacing between nozzles. This, of course, reduces the density of nozzles and lowers the resolution.

Referring to **5**, **6** and **7**, the present invention addresses this by etching the inlet **31** through the interconnect **23** and into the wafer **21** so that the ink supply passage **32** can stop short of the interface between the dielectric **23** and the wafer **21**. As best shown in FIG. **5**, the plasma does not get the opportunity to track along the interface and damage the CMOS drive circuitry. As the inlet hole **31** is relatively shallow, the removal of the resist is not overly difficult. This permits a more compact overall design and higher nozzle packing density. Using this technique, the sizes of the ink conduits are also relative small. Typically, the width of the inlet hole **31** is between 8 microns and 24 microns, and the width of the supply passage **32** is between 10 microns and 28 microns.

Thermal Bend Actuated Printheads

In FIGS. **8** to **12**, reference numeral **10** generally indicates a nozzle arrangement of a printhead chip, for an ink jet printhead in accordance with a related aspect of the invention.

The nozzle arrangement **10** is one of a plurality of such nozzle arrangements formed on a silicon wafer substrate **12** to define the printhead chip of the invention. As set out in the background of this specification, a single printhead can contain up to 84 000 such nozzle arrangements. For the purposes of clarity and ease of description, only one nozzle arrangement is described. It is to be appreciated that a person of ordinary skill in the field can readily obtain the printhead chip by simply replicating the nozzle arrangement **10** on the wafer substrate **12**.

The printhead chip is the product of an integrated circuit fabrication technique. In particular, each nozzle arrangement **10** is the product of a MEMS—based fabrication technique. As is known, such a fabrication technique involves the deposition of functional layers and sacrificial layers of integrated circuit materials. The functional layers are etched to define various moving components and the sacrificial layers are etched away to release the components. As is known, such fabrication techniques generally involve the replication of a large number of similar components on a single wafer that is subsequently diced to separate the various components from each other. This reinforces the submission that a person of ordinary skill in the field can readily obtain the printhead chip of this invention by replicating the nozzle arrangement **10**.

An electrical drive circuitry layer **14** is positioned on the silicon wafer substrate **12**. The electrical drive circuitry layer **14** includes CMOS drive circuitry. The particular configuration of the CMOS drive circuitry is not important to this description and has therefore not been shown in any detail in the drawings. Suffice to say that it is connected to a suitable microprocessor and provides electrical current to the nozzle arrangement **10** upon receipt of an enabling signal from said suitable microprocessor. An example of a suitable microprocessor is described in the above referenced patents/patent applications. It follows that this level of detail will not be set out in this specification.

An ink passivation layer **16** is positioned on the drive circuitry layer **14**. The ink passivation layer **16** can be of any suitable material, such as silicon nitride.

The nozzle arrangement **10** includes an ink inlet channel **18** that is one of a plurality of such ink inlet channels defined in the substrate **12**.

The nozzle arrangement **10** includes an active ink ejection structure **20**. The active ink ejection structure **20** has a roof **22** and sidewalls **24** that depend from the roof **22**. An ink ejection port **26** is defined in the roof **22**.

The active ink ejection structure **20** is connected to, and between, a pair of thermal bend actuators **28** with coupling structures **30** that are described in further detail below. The roof **22** is generally rectangular in plan and, more particularly, can be square in plan. This is simply to facilitate connection of the actuators **28** to the roof **22** and is not critical. For example, in the event that three actuators are provided, the roof **22** could be generally triangular in plan. There may thus be other shapes that are suitable.

The active ink ejection structure **20** is connected between the thermal bend actuators **28** so that a free edge **32** of the sidewalls **24** is spaced from the ink passivation layer **16**. It will be appreciated that the sidewalls **24** bound a region between the roof **22** and the substrate **12**.

The roof **22** is generally planar, but defines a nozzle rim **76** that bounds the ink ejection port **26**. The roof **22** also defines a recess **78** positioned about the nozzle rim **76** which serves to inhibit ink spread in case of ink wetting beyond the nozzle rim **76**.

The nozzle arrangement **10** includes a static ink ejection structure **34** that extends from the substrate **12** towards the roof **22** and into the region bounded by the sidewalls **24**. The static ink ejection structure **34** and the active ink ejection structure **20** together define a nozzle chamber **42** in fluid communication with an opening **38** of the ink inlet channel **18**. The static ink ejection structure **34** has a wall portion **36** that bounds an opening **38** of the ink inlet channel **18**. An ink displacement formation **40** is positioned on the wall portion **36** and defines an ink displacement area that is sufficiently large so as to facilitate ejection of ink from the ink ejection port **26** when the active ink displacement structure **20** is displaced towards the substrate **12**. The opening **38** is substantially aligned with the ink ejection port **26**.

The thermal bend actuators **28** are substantially identical. It follows that, provided a similar driving signal is supplied to each thermal bend actuator **28**, the thermal bend actuators **28** each produce substantially the same force on the active ink ejection structure **20**.

In FIG. **3** there is shown the thermal bend actuator **28** in further detail. The thermal bend actuator **28** includes an arm **44** that has a unitary structure. The arm **44** is of an electrically conductive material that has a coefficient of thermal expansion which is such that a suitable component of such material is capable of performing work, on a MEMS scale, upon expansion and contraction of the component when heated and subsequently cooled. The material can be one of many. However, it is desirable that the material has a Young's Modulus that is such that, when the component bends through differential heating, energy stored in the component is released when the component cools to assist return of the component to a starting condition. The Applicant has found that a suitable material is Titanium Aluminum Nitride (TiAlN). However, other conductive materials may also be suitable, depending on their respective coefficients of thermal expansion and Young's Modulus.

The arm **44** has a pair of outer passive portions **46** and a pair of inner active portions **48**. The outer passive portions **46** have passive anchors **50** that are each made fast with the ink passivation layer **16** by a retaining structure **52** of successive layers of titanium and silicon dioxide or equivalent material.

The inner active portions **48** have active anchors **54** that are each made fast with the drive circuitry layer **14** and are electrically connected to the drive circuitry layer **14**. This is also achieved with a retaining structure **56** of successive layers of titanium and silicon dioxide or equivalent material.

The arm **44** has a working end that is defined by a bridge portion **58** that interconnects the portions **46**, **48**. It follows that, with the active anchors **54** connected to suitable electrical contacts in the drive circuitry layer **14**, the inner active portions **48** define an electrical circuit. Further, the portions **46**, **48** have a suitable electrical resistance so that the inner active portions **48** are heated when a current from the CMOS drive circuitry passes through the inner active portions **48**. It will be appreciated that substantially no current will pass through the outer passive portions **46** resulting in the passive portions heating to a significantly lesser extent than the inner active portions **48**. Thus, the inner active portions **48** expand to a greater extent than the outer passive portions **46**.

As can be seen in FIG. **3**, each outer passive portion **46** has a pair of outer horizontally extending sections **60** and a central horizontally extending section **62**. The central section **62** is connected to the outer sections **60** with a pair of vertically extending sections **64** so that the central section **62** is positioned intermediate the substrate **12** and the outer sections **60**.

Each inner active portion **48** has a transverse profile that is effectively an inverse of the outer passive portions **46**. Thus, outer sections **66** of the inner active portions **48** are generally coplanar with the outer sections **60** of the passive portions **46** and are positioned intermediate central sections **68** of the inner active portions **48** and the substrate **12**. It follows that the inner active portions **48** define a volume that is positioned further from the substrate **12** than the outer passive portions **46**. It will therefore be appreciated that the greater expansion of the inner active portions **48** results in the arm **44** bending towards the substrate **12**. This movement of the arms **44** is transferred to the active ink ejection structure **20** to displace the active ink ejection structure **20** towards the substrate **12**.

This bending of the arms **44** and subsequent displacement of the active ink ejection structure **20** towards the substrate **12** is indicated in FIG. **4**. The current supplied by the CMOS drive circuitry is such that an extent and speed of movement of the active ink displacement structure **20** causes the formation of an ink drop **70** outside of the ink ejection port **26**. When the current in the inner active portions **48** is discontinued, the inner active portions **48** cool, causing the arm **44** to return to a position shown in FIG. **1**. As discussed above, the material of the arm **44** is such that a release of energy built up in the passive portions **46** assists the return of the arm **44** to its starting condition. In particular, the arm **44** is configured so that the arm **44** returns to its starting position with sufficient speed to cause separation of the ink drop **70** from ink **72** within the nozzle chamber **42**.

On the macroscopic scale, it would be counter-intuitive to use heat expansion and contraction of material to achieve movement of a functional component. However, the Applicant has found that, on a microscopic scale, the movement resulting from heat expansion is fast enough to permit a functional component to perform work. This is particularly so when suitable materials, such as TiAlN are selected for the functional component.

One coupling structure **30** is mounted on each bridge portion **58**. As set out above, the coupling structures **30** are positioned between respective thermal actuators **28** and the roof **22**. It will be appreciated that the bridge portion **58** of each thermal actuator **28** traces an arcuate path when the arm **44** is bent and straightened in the manner described above. Thus, the bridge portions **58** of the oppositely oriented actuators **28** tend to move away from each other when actuated, while the active ink ejection structure **20** maintains a rectilinear path. It follows that the coupling structures **30** should accommodate movement in two axes, in order to function effectively.

Details of one of the coupling structures **30** are shown in FIG. **13**. It will be appreciated that the other coupling structure **30** is simply an inverse of that shown in FIG. **13**. It follows that it is convenient to describe just one of the coupling structures **30**.

The coupling structure **30** includes a connecting member **74** that is positioned on the bridge portion **58** of the thermal actuator **28**. The connecting member **74** has a generally planar surface **80** that is substantially coplanar with the roof **22** when the nozzle arrangement **10** is in a quiescent condition.

A pair of spaced proximal tongues **82** is positioned on the connecting member **74** to extend towards the roof **22**. Likewise, a pair of spaced distal tongues **84** is positioned on the roof **22** to extend towards the connecting member **74** so that the tongues **82**, **84** overlap in a common plane parallel to the substrate **12**. The tongues **82** are interposed between the tongues **84**.

A rod **86** extends from each of the tongues **82** towards the substrate **12**. Likewise, a rod **88** extends from each of the tongues **84** towards the substrate **12**. The rods **86**, **88** are substantially identical. The connecting structure **30** includes a connecting plate **90**. The plate **90** is interposed between the tongues **82**, **84** and the substrate **12**. The plate **90** interconnects ends **92** of the rods **86**, **88**. Thus, the tongues **82**, **84** are connected to each other with the rods **86**, **88** and the connecting plate **90**.

During fabrication of the nozzle arrangement **10**, layers of material that are deposited and subsequently etched include layers of TiAlN, titanium and silicon dioxide. Thus, the thermal actuators **28**, the connecting plates **90** and the static ink ejection structure **34** are of TiAlN. Further, both the retaining structures **52**, **56**, and the connecting members **74** are composite, having a layer **94** of titanium and a layer **96** of silicon dioxide positioned on the layer **74**. The layer **74** is shaped to nest with the bridge portion **58** of the thermal actuator **28**. The rods **86**, **88** and the sidewalls **24** are of titanium. The tongues **82**, **84** and the roof **22** are of silicon dioxide.

When the CMOS drive circuitry sets up a suitable current in the thermal bend actuator **28**, the connecting member **74** is driven in an arcuate path as indicated with an arrow **98** in FIG. **13**. This results in a thrust being exerted on the connecting plate **90** by the rods **86**. One actuator **28** is positioned on each of a pair of opposed sides **100** of the roof **22** as described above. It follows that the downward thrust is transmitted to the roof **22** such that the roof **22** and the distal tongues **84** move on a rectilinear path towards the substrate **12**. The thrust is transmitted to the roof **22** with the rods **88** and the tongues **84**.

The rods **86**, **88** and the connecting plate **90** are dimensioned so that the rods **86**, **88** and the connecting plate **90** can distort to accommodate relative displacement of the roof **22** and the connecting member **74** when the roof **22** is displaced towards the substrate **12** during the ejection of ink from the ink ejection port **26**. The titanium of the rods **86**, **88** has a Young's Modulus that is sufficient to allow the rods **86**, **88** to return to a straightened condition when the roof **22** is displaced away from the ink ejection port **26**. The TiAlN of the connecting plate **90** also has a Young's Modulus that is sufficient to allow the connecting plate **90** to return to a starting condition when the roof **22** is displaced away from the ink ejection port **26**. The manner in which the rods **86**, **88** and the connecting plate **90** are distorted is indicated in FIGS. **14** to **19**.

For the sake of convenience, the substrate **19** is assumed to be horizontal so that ink drop ejection is in a vertical direction.

As can be seen in FIGS. **18** and **19**, when the thermal bend actuator **28** receives a current from the CMOS drive circuitry, the connecting member **74** is driven towards the substrate **12** as set out above. This serves to displace the connecting plate **90** towards the substrate **12**. In turn, the connecting plate **90** draws the roof **22** towards the substrate **12** with the rods **88**. As described above, the displacement of the roof **22** is rectilinear and therefore vertical. It follows that displacement of the distal tongues **84** is constrained on a vertical path. However, displacement of the proximal tongues **82** is arcuate and has both vertical and horizontal components, the horizontal components being generally away from the roof **22**. The distortion of the rods **86**, **88** and the connecting plate **90** therefore accommodates the horizontal component of movement of the proximal tongues **82**.

In particular, the rods **86** bend and the connecting plate **90** rotates partially as shown in FIG. **19**. In this operative condition, the proximal tongues **82** are angled with respect to the substrate. This serves to accommodate the position of the proximal tongues **82**. As set out above, the distal tongues **84** remain in a rectilinear path as indicated by an arrow **102** in FIG. **15**. Thus, the rods **88** that bend as shown in FIG. **15** as a result of a torque transmitted by the plate **90** resist the partial rotation of the connecting plate **90**. It will be appreciated that an intermediate part **104** between each rod **86** and its adjacent rod **88** is also subjected to a partial rotation, although not to the same extent as the part shown in FIG. **19**. The part shown in FIG. **15** is subjected to the least amount of rotation due to the fact that resistance to such rotation is greatest at the rods **88**. It follows that the connecting plate **90** is partially twisted along its length to accommodate the different extents of rotation. This partial twisting allows the plate **90** to act as a torsional spring thereby facilitating separation of the ink drop **70** when the roof **22** is displaced away from the substrate **19**.

At this point, it is to be understood that the tongues **82**, **84**, the rods **86**, **88** and the connecting plate **90** are all fast with each other so that relative movement of these components is not achieved by any relative sliding movement between these components.

It follows that bending of the rods **86**, **88** sets up three bend nodes in each of the rods **86**, **88**, since pivotal movement of the rods **86**, **88** relative to the tongues **82**, **84** is inhibited. This enhances an operative resilience of the rods **86**, **88** and therefore also facilitates separation of the ink drop **70** when the roof **22** is displaced away from the substrate **12**.

In FIG. **20**, reference numeral **110** generally indicates a nozzle arrangement of a second embodiment of a printhead chip, in accordance with the invention, for an ink jet printhead. With reference to FIGS. **8** to **19**, like reference numerals refer to like parts, unless otherwise specified.

The nozzle arrangement **110** includes four symmetrically arranged thermal bend actuators **28**. Each thermal bend actuator **28** is connected to a respective side **112** of the roof **22**. The thermal bend actuators **28** are substantially identical to ensure that the roof **22** is displaced in a rectilinear manner.

The static ink ejection structure **34** has an inner wall **116** and an outer wall **118** that together define the wall portion **36**. An inwardly directed ledge **114** is positioned on the inner wall **116** and extends into the nozzle chamber **42**.

A sealing formation **120** is positioned on the outer wall **118** to extend outwardly from the wall portion **38**. It follows that the sealing formation **120** and the ledge **114** define the ink displacement formation **40**.

The sealing formation **120** includes a re-entrant portion **122** that opens towards the substrate **12**. A lip **124** is positioned on the re-entrant portion **122** to extend horizontally from the re-entrant portion **122**. The sealing formation **120** and the sidewalls **24** are configured so that, when the nozzle arrangement **10** is in a quiescent condition, the lip **124** and a free edge **126** of the sidewalls **24** are in horizontal alignment with each other. A distance between the lip **124** and the free edge **126** is such that a meniscus is defined between the sealing formation **120** and the free edge **126** when the nozzle chamber **42** is filled with the ink **72**. When the nozzle arrangement **10** is in an operative condition, the free edge **126** is interposed between the lip **124** and the substrate **12** and the meniscus stretches to accommodate this movement. It follows that when the chamber **42** is filled with the ink **72**, a fluidic seal is defined between the sealing formation **120** and the free edge **126** of the sidewalls **24**.

The Applicant believes that this related aspect of the invention provides a means whereby substantially rectilinear movement of an ink-ejecting component can be achieved. The Applicant has found that this form of movement enhances efficiency of operation of the nozzle arrangement **10**. Further, the rectilinear movement of the active ink ejection structure **20** results in clean drop formation and separation, a characteristic that is the primary goal of ink jet printhead manufacturers.

I claim:

1. An inkjet printhead comprising:

a wafer having a droplet ejection side and a liquid supply side opposite the droplet ejection side;

a plurality of active ink ejection structures formed on the droplet ejection side of the wafer, each active ink ejection structure partially defining a nozzle chamber, and defining an ink ejection port;

a plurality of individual fluid passages formed in the wafer, each fluid passage providing fluid to corresponding nozzle chambers;

a plurality of static ink ejection structures formed on the droplet ejection side of the wafer and inside of corresponding active ink ejection structures, each static ink ejection structure defining a nozzle chamber with a corresponding active ink ejection structure; and,

droplet ejection actuators respectively corresponding to each active ink ejection structure, the droplet ejection actuators being formed on the droplet ejection side of the wafer and attached to respective active ink ejection structures, wherein,

the droplet ejection actuators are operable to displace an active ink ejection structures towards a corresponding static ink ejection structure to effect ejection of fluid in the nozzle chamber through the ink ejection port.

2. The inkjet printhead according to claim **1**, wherein the active ink ejection structure includes a roof and sidewalls depending from the roof.

3. The inkjet printhead according to claim **2**, wherein the roof is supported by corresponding droplet ejection actuators.

4. The inkjet printhead according to claim **3**, wherein the roof is supported by a pair of drop ejection actuators at opposite sides thereof.

5. The inkjet printhead according to claim **2**, wherein the static ink ejection structure extends from the wafer towards the roof, within a region bounded by the sidewalls.

6. The inkjet printhead according to claim **1**, wherein each of the plurality of individual fluid passages extends through the wafer from the drop ejection side to the liquid supply side.

7. The inkjet printhead according to claim **6**, wherein each of the plurality of individual fluid passage terminates at an opening located at the drop ejection side.

8. The inkjet printhead according to claim **7**, wherein each static ink ejection structure includes a wall portion bounding the opening.

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